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LINEAR SECOND-ORDER SYSTEM  
SOLUTION ACCURACIES WITH DIGITAL,  
ANALOG AND HYBRID COMPUTER METHODS

by

Guy A. Camifé

A thesis

submitted to the School of Graduate Studies  
in partial fulfilment of the requirements for  
the degree of Master of Science

Masters Program in Systems Science

University of Ottawa

JULY 1983

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## ABSTRACT

Four conceptual models for the solution of a linear second-order differential equation and their implementation on analog, hybrid and digital computers are described. A standard hybrid configuration is adopted whereby the integrations are performed on the analog computer. A discrete time equivalent of the hybrid computer model is solved on a digital computer. The difference between any two model solutions is characterized by a normalized root-mean-square error criterion. Three general digital programs were implemented to determine the accuracy of solution of the computerized models as a function of their parameters. Results are presented concerning the accuracy of the analog computer model, the hybrid computer model and its digital computer equivalent.

## ACKNOWLEDGEMENT

I wish to express my warmest thanks to my supervisor, Dr. J. R. Amyot of the Division of Mechanical Engineering, National Research Council of Canada, for his invaluable guidance. I am also very grateful to his fellow-workers in the Analysis Laboratory for the help they have given me.

I owe a special debt of gratitude to Mr. P. A. Hamill for access to the equipment and computer facilities of the Analysis Laboratory.

Thanks also to Dr. L. G. Birta for his co-operation in acting as administrative supervisor at the University of Ottawa.

I would like to make special acknowledgement to Ronald Jubainville for the helpful discussions along the development of this work.

Scholarships from the Natural Sciences and Engineering Research Council and from the University of Ottawa were greatly appreciated.

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## 1.0 INTRODUCTION

Until the late fifty's or early sixty's, the analog computer was the most used tool to solve scientific simulation problems. Then, analog and digital computers were linked together with a communication interface. This combination was called the "Hybrid Computer". The hybrid computer, like the analog computer alone, operates in synchronous time. The information is transferred discretely and at regular intervals between both computers in a high speed loop called "Hybrid Loop".

The hybrid computer offers certain advantages. On the analog computer, for instance, where the computing time is independent of problem complexity, the operations are performed in parallel and continuously. Using the analog computer to solve large sets of differential equations is usually faster and cheaper than using a digital computer alone. The operations of the digital computer are serial and discrete and the computing time is directly related to the complexity of computations. On the other hand, the digital computer is better suited to control the various hybrid simulation runs and to perform certain operations such as function generation, table look-up, logical decision-making and data storage.

Real time simulation of dynamic systems is advantageous and sometimes necessary in some cases, especially for hardware-in-the-loop and training simulation applications. With a hybrid computer, model parameters may be programmed for manual variation at any time during a simulation run and the effect of varying a parameter may be examined as the solution progresses. A real time simulation may be designed to interact with a real world system. Although digital models may be synchronous, their dynamic applications range can be inferior to hybrid models because of the superior speed of hybrid computation. However, the gap is being reduced by parallel digital processing.

In hybrid computation, the programmer must contend with certain sources of inaccuracy. In the hybrid loop, a set of analog variables is sampled, converted into digital form, processed by the digital computer, and converted back to analog signals for analog processing. Sources of error include precision limitations of typical analog computers and analog-digital converters. Another source of error is the time delay arising from digital computation and data conversion time in a hybrid loop. Hybrid computation is constrained by this time delay in that it prevents the analog computer from using all of its high speed capabilities and the digital computer from being fully utilized since digital

computation time increases with the amount of computation.

Furthermore, it seriously limits the allowable range of high frequency components in real time models. Digital to analog data reconstruction is another source of error in that the input signals to the analog computer are not the required ideal continuous signals. Instead they are signals reconstructed from discretely sampled data. Fortunately, there are methods of compensation for the effects of sampling and digital execution time upon solution accuracy and the related literature is reviewed briefly below.

Developments both in digital hardware and software have contributed to an increase in the popularity of simulation. High level simulation languages such as GPSS, CSMP, CSSL, ACSL and DARE have been developed to facilitate asynchronous digital computer modeling. Hardware devices such as array processors greatly speed up computations by providing parallel processing capabilities. Systems with built-in parallel processors, like Applied Dynamic International's AD-10, also increase speed but there are programming difficulties associated with scheduling of parallel computations. Ultimately, the speed of analog computation can only be approached digitally and its continuous nature can be obtained from discrete data only by digital to analog conversion. These digital improvements are useful to hybrid computation

also since increased digital speed leads to decreased hybrid loop time delay. Analog hardware developments such as programmable multivariable function generators and automatic patching are also improving the performance of hybrid computers, and their use is being simplified by high-level programming software such as the hybrid time-sharing system MACHYS being developed at the Technical University of Vienna.<sup>1</sup> It is difficult to predict the architecture of future computers precisely but the trend towards parallel computation is clear and analog computation is the supreme example of parallel processing. Hybrid computers, in their present state of evolution, are important and sometimes essential tools in computer simulation of dynamical systems, particularly for synchronous time applications.

Many authors have studied the effect of time delay in a hybrid loop. Various methods of compensation, usually based on approximations by series, have been proposed and analysed. A review of the most relevant literature on this subject follows.

Miura and Iwata<sup>2</sup> proposed three methods of compensation:

- a) analog compensation, where the derivative is multiplied by a constant and added to the output of the analog integrator,
- b) linear interpolation, where the output of the digital computer is modified using a first order numerical equation

and c) analog first order hold (FOH) where the step-function output of the digital computer, after a zero order hold (ZOH), is transformed into ramps via analog hardware before being integrated by the analog computer. In this thesis, the term "analog compensation" is used to identify method a) above.

Gilbert<sup>3</sup> suggested the input to the digital computer be modified using its derivatives. This method is effectively very similar to analog compensation. He also applied Z-transform theory and used it to determine the effects of sampling and time delay on accuracy. Other authors<sup>7,9,16,17,18</sup> have used Z-transform theory to predict dynamic errors analytically.

Papers by Matlock<sup>4</sup> and by Deiters and Nomura<sup>5</sup> extended the method of digital prediction. They derived higher order numerical equations to predict inputs to the integrators more precisely.

The analog compensation scheme was also suggested by Karplus<sup>6</sup> who presented an extensive analysis of several sources of error in hybrid computation, such as errors due to sampling.

Vichnevetsky<sup>7</sup> analyzed the analog compensation method as well as first and second order digital prediction. He derived equivalent difference equations for the hybrid loop with and

without these methods of compensation. These equations apply to a system of linear differential equations of any order and to the hybrid computer case where only the integrations are done on the analog computer, the rest of the operations being performed on the digital side. Vichnevetsky also applied Z-transforms to establish stability contours in system parameter space. This method of determining stability contours has been used by other authors,<sup>15,16,19</sup> however, it does not give accuracy information.

A paper by Curry<sup>8</sup> which is closely related to this thesis, gives experimental results with different methods of correction. He compares his results with theoretical results derived by Howe<sup>9</sup> using Z-transforms. The methods of compensation used in his experiments were: (1) first and second order digital compensation, (2) analog FOH, and (3) a method called "kickoff" where the knowledge of the solution over a period corresponding to the first three frame-times is used to start the solution. Curry concludes that the complexity of both producing an analog FOH circuit and programming for kickoff are not worth the relatively insignificant gain in accuracy. The aim of Curry's paper is to make available to the hybrid programmer the results of his experiments with a second order linear differential equation (SOLDE) and a specific method of compensation. He is one of

the first to provide experimental results in readily accessible chart form. From the charts, the programmer can obtain an error estimate for a SOLDE problem with a certain frequency and damping ratio knowing the hybrid sampling frequency.

A paper by Deiters, Kano and Inoue<sup>10</sup> is one of the few other papers providing experimental results. Their experiments include analog compensation and other methods. For analog compensation, they use the best compensation parameter value in the Taylor Series sense.

Most of the accuracy and stability studies were for linear systems since nonlinear systems cannot generally be solved analytically. The requirement that a sufficiently large number of samples per cycle of solution be maintained for stability and accuracy in hybrid implementations is akin to a similar requirement in purely digital methods.

The ultimate goal of the research reported here is to develop a software package for modeling continuous systems in real time on a hybrid computer such that the user will not be required to get involved with analog computer programming. This will be achieved initially by utilizing the analog computer as a set of general purpose integrators with compensation for time delay in a standard patching arrangement. This may be viewed as a hybrid computer

continuous simulation package where the analog subsystem will be called by an integration subroutine. Also, the compensation parameters may be optimized automatically to minimize solution errors for a given set of model parameters and time delay.

In order to produce this package, a compensation method is required. The analog compensation method of Miura and Iwata will be adopted for this package, initially, since it requires a simple hardware arrangement on the analog side and does not increase the digital computation time delay in the hybrid loop. Also, Vichnevetsky has shown that stability is better with this method than first order digital compensation.

Four different but equivalent mathematical models are defined in the sense that each one generates the solution of a second-order linear differential equation with constant coefficients or a close approximation thereof. They are also implemented on computers as computerized models and solutions are compared. One of the mathematical models is the sampled-data model implemented on a hybrid computer. Another is the discrete time equivalent to sampled-data (DTESD) model implemented on a digital computer. It is a theoretical representation of the hybrid computer model for which Vichnevetsky produced stability contours and Deiters,<sup>10</sup> accuracy curves. A third mathematical model is the continuous

time model programmed on an analog computer. It is interesting to investigate the region of accuracy of this model since it represents, in a sense, the hybrid computer model with no digital computing delay. It will be seen that it does not always produce the perfect solution. The discrete time analytical model is the fourth mathematical model. It generates analytical solutions of the SOLDE asynchronously on the digital computer. Its solutions are used as references for accuracy analyses of the three other models.

As it is the objective of this thesis to produce accuracy results for these computerized models, a normalized root mean square (RMS) error criterion is adopted here. It gives a unique value for the difference between two solutions and a feel for its significance can be developed by examining certain well-chosen cases.

The input parameters to be varied and their range of values for acceptable accuracies of solution are also established. In each of the computerized models, the two parameters of the SOLDE, damping ratio and natural frequency, are varied. In addition, the sampled-data model and its discrete time equivalent involve two more parameters, namely, time-delay and compensation factor.

A set of digital programs has been implemented to facilitate the analyses of accuracy. These programs solve the different computerized models after accepting their input data and they compute the RMS errors between solutions. The errors are then compiled into tables and displayed on graphs for pre-definable sets of values of input parameters. The programs are general in the sense that they can perform the error analysis for any additional computerized model with the same parameters or they can easily be modified to handle computerized models involving different parameters.

Useful data are produced and displayed by these programs concerning the accuracy of the first three computerized models relative to the fourth (i. e., the analytical solution) as well as to each other. These data are collected and arranged in such a way that it is relatively easy to estimate the errors for arbitrary values of the parameters within specified ranges.

A more detailed overview is given in Section 2.0. This is followed in Section 3.0 by an explanation of the hybrid loop time delay and the theory of compensation for it. Sections 4.0 and 5.0 respectively describe the mathematical models and their documented implementation. Performance criteria to determine the accuracy of one model compared to another are discussed in Section 6.0. The performance

analysis computer programs are described in Section 7.0 with reference to their detailed documentation in Appendices C to J. Section 8.0 discusses the accuracy of the computerized models with the aid of results documented in Appendix B. Overall conclusions are formulated in Section 9.0.

## 2.0 OVERVIEW

A computerized model solution occurs in model time whereas reality occurs in real time.<sup>11</sup> Here, real time is represented by variable  $t$  and model time by  $t' = Bt$  where  $B = f(t)$ . If  $f(t) = 1$  then the model is solved in real time ( $t = t'$ ). If, however,  $f(t)$  is not equal to 1 but is known (i. e., model time is slowed down or speeded up by a known function relative to real time), then the model is 'synchronous' whereas if  $f(t)$  is not known, the model is 'asynchronous'. Analog computer models and hybrid computer models are generally synchronous. Digital computer models are usually asynchronous but they may be synchronous. This work and its results are aimed at synchronous hybrid computer models.

A computerized model is defined to be a computer program which implements a mathematical model. An input-process-output diagram of four computerized models is shown in Figure 1. The four mathematical models in this figure can generate good approximations to the solution of a linear second-order

differential equation with step input for sets of parameter values defined by this investigation. The dashed arrows between the mathematical model and computer program blocks indicate that the mathematical models are implemented in the computer programs to produce 'computerized models'. Every computerized model is identified as a system. System A is a discrete-time analytical solution implemented on a digital computer, System B is a continuous-time model which is solved by an analog computer, System C is a sampled-data model implemented on a hybrid computer and System D is an asynchronous digital model equivalent to the hybrid implementation. Each system accepts a set of input data (model parameters) gathered in data sets DSA and DSB. Furthermore, each computerized model produces a set of response data which are stored in data sets DSRA to DSRD, respectively. Response data are discrete values of system solutions.

The purpose of developing these computerized models is to compare their solutions and analyse their performance. This is achieved by a set of three digital computer programs. Program RESPLT (Fig. 2) solves the user specified system (S) and plots the solution as a function of time. The model input parameters are also specified interactively as data sets DSAU and DSBU. A similar program, called RESPONS. (Fig. 3) also

solves a user specified system (S) but for various combinations of input parameter values included in data sets DSA and DSB. The solutions are stored as discrete data points into data set DSRA or DSRB depending on whether System A or System B is being solved. Subsets DSRC1 to DSRC5 or DSRD1 to DSRD5 are used for storage if System C or System D is being solved. These data sets are used as inputs to the third program, called RMSERR (Fig. 4). A root mean square (RMS) error is computed between solutions of two systems ( $S_1, S_2$ ) which are specified interactively. Finally, program RMSERR displays tables and graphs of the RMS errors. Graphs are also produced to display the range of model input parameters for which the errors in the solutions are acceptable.

### 3.0 COMPENSATION THEORY

In this section, the different components of the hybrid loop contributing to the time delay are summarized. It is shown how this delay affects the hybrid solutions and how it can be compensated from the point of view of Taylor Series expansions. Finally, the relationship between theory, digital correction and analog compensation is established.

A source of error inherent in sampled-data systems is the sample and hold process whereby the digital computer samples the analog output at discrete time intervals and holds the analog input constant during this interval. A second error,

known as digital computation error or transport lag, is due to the computational delay between sampling and updating of the analog computer. The cycle of calculations, or hybrid loop, is shown in Figure 5 illustrating the associated component delays. The total delay  $T_C$ , which will be referred to in the sequel as the digital time of computation, is given by

$$T_C = T_1 + T_2 + T_3 \quad (1)$$

where  $T_1$  is the analog to digital (A/D) conversion time,  $T_2$  is the digital calculation time and  $T_3$  is the digital to analog (D/A) conversion time.

In 1963, Miura and Iwata<sup>2</sup> applied the Taylor Series extrapolation scheme to modify the analog integrator input. This method requires that the sample and hold delay be fixed. The previous year, Korn<sup>12</sup> had shown the importance of a constant time interval when using digital compensation. Thus a fixed digital computation time  $T_C$  and a fixed sampling and update interval  $T$  were specified by Miura and Iwata. They then compared the actual input  $W(t)$ , a staircase function (Fig. 6(a)), with the ideal function  $Y(t)$ , (Fig. 6(b)). The function  $W(t)$  is first delayed by a constant time  $\tau$ . This fixed  $\tau$  is the amount of time from the instant the integrators start operating with their initial conditions to the instant they receive their first input value. Usually,  $\tau$

is equal to the total digital time of computation  $T_C$ . The analog input is held constant until it is updated by the result of the next new digital computation and so on. Since the true input  $W(t)$  is shifted from the ideal input  $Y(t)$ , a compensation scheme is needed which will make both functions equivalent.

Miura and Iwata proved that when the update interval  $T$  is small, the integral of the step function  $W(t)$  is equivalent to the integral of the smooth curve shown in Figure 6(c) passing through the middle of the steps. Since this smooth curve is parallel to  $Y(t)$  with a phase shift of  $\tau + T/2$ , they have shown that

$$\int W(t) dt = \int Y(t - (\tau + T/2)) dt \quad (2)$$

Thus, it is seen that the input to the analog integrator should be  $W(t + (\tau + T/2))$  as shown in Figure 6(d). This can be expanded for small  $(\tau + T/2)$  in a Taylor Series

$$W(t + (\tau + T/2)) = W(t) + W'(t)(\tau + T/2) + \frac{W''(t)(\tau + T/2)^2}{2!} + \dots \quad (3)$$

Thus, a first order digital correction would include the first two terms of (3) and higher order corrections would include higher order terms. For a first order correction, an approximation for  $W(t)$  in the interval  $[iT, (i+1)T]$ ,  $i=1, 2, 3, \dots$ , is the slope between the outputs of the digital

computer at sampling times  $(i-1)T$  and  $iT$  computed as:

$$W(t) = \frac{W(iT) - W((i-1)T)}{T}, \quad t \in [iT, (i+1)T] \quad (4)$$

Replacing (4) into (3) gives a corrected input to the analog integrator and performing the integration on the first two terms of (3) for one step interval  $T$  gives the incremental input to the digital computer as:

$$X((i+1)T) - X(iT) = \int_0^T \left\{ W(iT) + \frac{[W(iT) - W((i-1)T)](\tau + T/2)}{T} \right\} dt \quad (5)$$

or equivalently,

$$X((i+1)T) = X(iT) + \int_0^T W(iT) dt + (\tau + T/2)[W(iT) - W((i-1)T)] \quad (6)$$

keeping in mind that  $W(iT)$  and  $W((i-1)T)$  are constants in the  $T$  interval.

It can be shown that the analog compensation method is also based on a first order Taylor Series expansion. Figure 7 is a simplified diagram of the continuous operations performed by the analog computer in the hybrid loop. The diagram illustrates the equation

$$X(t) = \int W(t) dt + \theta W(t) \quad (7)$$

where time functions  $W(t)$ ,  $\theta W(t)$  and  $X(t)$  are displayed in

Figure 8. The input to the analog computer is  $W(t)$  and since the constant  $W((i+1)T)$  is set before  $X((i+1)T)$  is read, the approximation for  $W(t)$  in the interval  $[iT, (i+1)T]$  is an interpolation in analog compensation rather than an extrapolation as in the digital correction case. The approximation is:

$$W(t) = \frac{W((i+1)T) - W(iT)}{T}, \quad t \in [iT, (i+1)T] \quad (8)$$

Thus, a result similar to (5) is obtained with analog compensation factor  $\theta$  over the interval  $[iT, (i+1)T]$ , i.e.,

$$X((i+1)T) - X(iT) = \int_0^T \left\{ W(iT) + \frac{\theta[W((i+1)T) - W(iT)]}{T} \right\} dt \quad (9)$$

and since  $W((i+1)T)$ ,  $W(iT)$  and  $\theta$  are constants, the input to the digital computer at  $t=(i+1)T$ , is

$$X((i+1)T) = X(iT) + \int_0^T W(iT) dt + \theta[W((i+1)T) - W(iT)] \quad (10)$$

The best value for  $\theta$  in the Taylor Series sense is thus  $(T+T/2)$  as it was for the digital prediction case.

The updating interval  $T$  is the time interval during which the analog input is held constant. But it is usually held constant during the period of conversions and digital

computations  $T_C$ . As mentioned above,  $\tau$  is also usually equal to  $T_C$  which means that according to the Taylor Series, the value of  $\theta$  for the best analog compensation is

$$\theta = (T_C + T_C/2) = 1.5T_C \quad (11)$$

Indeed, in this study, both  $\tau$  and  $T$  were set equal to  $T_C$ . Furthermore it was important to fix the loop time  $T_C$  accurately because of its role in the computation of  $\theta$ .

As Deiters et. al.<sup>10</sup>, the analog compensation method yields a larger stability region in the space of parameters but a smaller accuracy region than their first order digital correction method. They used the Gregory-Newton extrapolation formula in a similar way than the Taylor Series to derive the digital correction equations. However their tests were conducted for only one analog compensation case, i. e.,  $\theta = 1.5T_C$ . This might not be the best value for every set of parameters. An objective of this thesis project was to determine ranges of parameter values where  $1.5T_C$  is not the optimum value of  $\theta$ .

An advantage of the analog compensation method is that it does not require additional digital programming in the hybrid loop which would increase the computation time. Furthermore, it is easy to implement on the analog computer.

#### 4.0 MATHEMATICAL MODELS

This section describes the four mathematical models that were used in computerized models as seen in Figure 1. These models were implemented in computer programs in order that their solutions could be compared and their performance analysed. In this thesis, a mathematical model is defined to be either 1) a conceptual model or 2) a mathematical equivalent of a conceptual model or 3) a mathematical equivalent of another mathematical model. A conceptual model is a mathematical representation of reality. A mathematical equivalent is defined to be a set of equations whose solution approximates the solution of another mathematical model.

A second-order linear differential equation (SOLDE) was chosen as a continuous-time conceptual model representing a real system such as a mass-spring-damper system and was solved in synchronous time on an analog computer.

A discrete-time analytical model consisting of equations which generate the solution of the SOLDE was solved asynchronously for very small time intervals on a digital computer. Its solution was the exact solution of the SOLDE used as reference to determine the solution errors of computerized mathematical equivalents.

A third mathematical model was a sampled-data model (i. e., a combination of a continuous-time and discrete-time sub-models) which was implemented on a hybrid computer in such a way that all computations were performed in the digital computer except for compensated integrations which were done in the analog computer. A main objective was to produce results comparing its solutions with those of other models.

The fourth mathematical model was a discrete-time equivalent to the sampled-data (DTESD) model consisting of a set of difference equations. The DTESD model was solved asynchronously on a digital computer to determine the range of parameter values over which equivalence with the hybrid model implementation could be ascertained. With this comparison, the assumptions of perfect equivalence made by Deiters et al.<sup>10</sup> could be verified. Results were then obtained for extrapolated parameter values to predict the accuracy of hybrid implementations in parameter ranges exceeding the capabilities of the available hybrid facility (e.g.,  $T_C \leq 5$  ms).

#### 4.1 Continuous-Time

The continuous-time model is the conceptual model represented by a second-order linear constant-coefficient differential equation with step input:

$$\ddot{x}(t) + 2\zeta\omega_n^* \dot{x}(t) + \omega_n^{*2} x(t) = \omega_n^{*2} u(t) \quad (12a)$$

$$\zeta \geq 0 \quad (12b)$$

$$\omega_n^* > 0 \quad (12c)$$

where  $t$  is clock time identified as real time, parameters  $\zeta$  and  $\omega_n^*$  respectively are the damping ratio and natural undamped frequency of the system and  $u(t)$  is the unit step function occurring at time  $t=0$ . This second-order system can be solved in real time but it can also be solved in synchronous time by defining a time-scaled equivalent

$$\ddot{x}(t') + 2\zeta\omega_n \dot{x}(t') + \omega_n^2 x(t') = \omega_n^2 u(t') \quad (13)$$

where

$$t' = \beta t \quad (14)$$

is model time and

$$\omega_n = \omega_n^* / \beta \quad (15a)$$

$$\beta > 0 \quad (15b)$$

is natural undamped frequency in model time, and  $\beta$  is a time-scale factor.

A variation in parameter value  $\beta$  results in a variation in solution speed of the system.<sup>11</sup> Precisely, when:

$\beta = 1$ , solution is in real time (i. e. corresponds to solution of system (12)),

$\beta > 1$ , solution is slower than real time,

$0 < \beta < 1$ , solution is faster than real time.

The conversion of system (12) from real-time to model-time can be visualized in the diagram of Figure 9 where it is seen that

$$\dot{x}(t) = \frac{dx(t)}{dt} = \beta \frac{dx(t')}{dt'} = \beta \dot{x}(t') \quad (16)$$

Likewise,

$$\ddot{x}(t) = \beta^2 \ddot{x}(t') \quad (17)$$

Replacing equations (16) and (17) into equation (12) leads to:

$$\beta^2 \ddot{x}(t') + 2\zeta \omega_n^* \beta \dot{x}(t') + \omega_n^{*2} x(t') = \omega_n^{*2} u(t') \quad (18)$$

Dividing by  $\beta^2$  and using (15) gives system (13).

Since factor  $\beta$  affects only the time scale of the solution, equation (13) can be used to study the system represented by equation (12).

## 4.2 Discrete-Time Analytical Solution

The analytical solution  $x(t)$  of system (12) is computed at discrete time  $t^i$ , where  $i=0, 1, 2, \dots$ , starting with  $t^0=0$ . Let the response data point  $x(t^i)$  simply be  $x^i$ . The equations of the solution and its derivative depend on damping ratio  $\zeta$  as follows:<sup>13</sup> If  $0 < \zeta < 1$ , the response is oscillatory:

$$x^i = u(t^i) - \frac{e^{-\zeta \omega_n^* t^i}}{\sqrt{1 - \zeta^2}} \sin(\omega_n^* \sqrt{1 - \zeta^2} t^i + \phi) \quad (19)$$

$$\dot{x}^i = \omega_n^* e^{-\zeta \omega_n^* t^i} \left[ \frac{\zeta \sin(\omega_n^* \sqrt{1 - \zeta^2} t^i + \phi)}{\sqrt{1 - \zeta^2}} - \cos(\omega_n^* \sqrt{1 - \zeta^2} t^i + \phi) \right] \quad (20)$$

where

$$\tan \phi = \sqrt{1 - \zeta^2} / \zeta \quad (21)$$

If  $\zeta > 1$ , the response is nonoscillatory:

$$x^i = u(t^i) + ce^{-at^i} + de^{-bt^i} \quad (22)$$

$$\dot{x}^i = -ace^{-at^i} - bde^{-bt^i} \quad (23)$$

where

$$a = \omega_n^* (\zeta - \sqrt{\zeta^2 - 1}) \quad (24)$$

$$b = \omega_n^* (\zeta + \sqrt{\zeta^2 - 1}) \quad (25)$$

$$c = -(\zeta + \sqrt{\zeta^2 - 1}) / 2\sqrt{\zeta^2 - 1} \quad (26)$$

$$d = -(-\zeta + \sqrt{\zeta^2 - 1}) / 2\sqrt{\zeta^2 - 1} \quad (27)$$

If  $\zeta=1$ , the system is critically damped and the response is nonoscillatory:

$$x^i = u(t^i) - e^{-\omega_n^* t^i} (1 + \omega_n^* t^i) \quad (28)$$

$$\dot{x}^i = \omega_n^{*2} e^{-\omega_n^* t^i} \quad (29)$$

#### 4.3 Sampled-Data

The sampled-data model consists of the three subsystems shown in Figure 10: discrete-time, sample and hold, and continuous-time. Algebraic computations are performed in the discrete-time subsystem at every constant time interval of length  $T_C$ . This time interval includes the computation time in the discrete subsystem and the data conversion time between continuous and discrete subsystems. As the output  $X(t')$  of the continuous subsystem is sampled at times  $iT_C$ , i.e.,

$$x^i = X(t'^i) \quad (30)$$

to become the input to the discrete subsystem, the output of the discrete subsystem becomes the input to the continuous subsystem at times  $(i+1)T_c$ , i.e.,

$$W(t') = W^i, \quad t' \in [t'^i, t'^{i+1}) \quad (31)$$

$$t'^{i+1} = t'^i + T_c, \quad i=0, 1, 2, \dots \quad (32)$$

The input  $W(t')$  is a staircase function remaining constant over each sampling period.

The continuous-time subsystem performs the integrations on its input with respect to time and also compensates for the time delay  $T_c$  as discussed in Section 3. Its operations are illustrated in Figure 7 representing a standard configuration of a set of  $n$  integrators and  $n$  compensators. Thus, variables  $W$ ,  $Z$ ,  $V$  and  $X$  in the figure are  $n$ -vectors and  $\theta$  is an  $n \times n$  diagonal matrix. The equations describing these operations are the following

$$\dot{Z}(t') = W(t') \quad (33)$$

$$V(t') = \theta W(t') \quad (34)$$

$$X(t') = Z(t') + V(t') \quad (35)$$

where  $Z$  is the integration output,  $V$  is the compensation vector and  $\theta$  is the matrix of compensation factors.

The operations of the discrete-time subsystem consists in the calculation of a discrete n-order linear equation expressed in vector notation as

$$W^{i+1} = AX^i + BF^i \quad (36)$$

where A and B are nxn coefficients matrices and F is the forcing function vector. The special case of the second-order linear differential equation (13) may be expressed in the form of equation (36) by

$$X = (x_1 \quad x_2)^T \quad (37a)$$

$$W = (w_1 \quad w_2)^T \quad (37b)$$

$$A = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\zeta\omega_n \end{bmatrix} \quad (37c)$$

$$B = \begin{bmatrix} 0 & 0 \\ 0 & \omega_n^2 \end{bmatrix} \quad (37d)$$

$$F = (0 \quad u)^T \quad (37e)$$

$$x_1 = x \quad (37f)$$

$$x_2 = w_1 = \dot{x} \quad (37g)$$

$$w_2 = \ddot{x} \quad (37h)$$

or

$$\begin{bmatrix} w_1 \\ w_2 \end{bmatrix}^{i+1} = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\zeta\omega_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}^i + \begin{bmatrix} 0 & 0 \\ 0 & \omega_n^2 \end{bmatrix} \begin{bmatrix} 0 \\ u \end{bmatrix}^i \quad (38)$$

In scalar notation, this is:

$$w_1^{i+1} = x_2^i \quad (39)$$

and

$$w_2^{i+1} = -\omega_n^2 x_1^i - 2\omega_n x_2^i + \omega_n^2 u^i \quad (40)$$

#### 4.4 Discrete-Time Equivalent Of Sampled-Data

The sampled-data model can be represented by a discrete-time model since the operations in its discrete-time subsystem are discrete and the input to its continuous-time subsystem are constant over fixed intervals permitting the analytical computation of the latter's outputs. The objective is to develop a difference equation for the solution  $X(t)$  representing the operations of the sampled-data model.

Function  $X(t)$  is being discretized at every sampling instant  $t^i = iT_c$ ,  $i=0, 1, 2, \dots$ . Thus equation (35) leads to the following equation for the difference of two consecutive discretized value of  $X(t)$ .

$$X^{i+1} - X^i = (Z^{i+1} - Z^i) + (V^{i+1} - V^i) \quad (41)$$

Similarly, from equation (34) and since  $\theta$  is constant, the difference of two consecutive discretized value of

the compensation function  $V(t)$  is

$$V^{i+1} - V^i = \theta(W^{i+1} - W^i) \quad (42)$$

The discrete-time difference of the integrator output  $Z(t)$  is obtained by integrating equation (33) over the sampling interval  $T$ :

$$Z^{i+1} - Z^i = \int_0^{T_C} W^i dt = W^i T_C \quad (43)$$

where  $W^i$  is constant over the interval  $(t^i, t^{i+1})$ .

Substitution of equations (42) and (43) into (41) yields:

$$X^{i+1} - X^i = T_C W^i + \theta(W^{i+1} - W^i) \quad (44)$$

and substituting for  $W^i$  from equation (36) gives

$$\begin{aligned} X^{i+1} = X^i + T_C (AX^{i-1} + BF^{i-1}) + \theta(AX^i + BF^i) \\ - \theta(AX^{i-1} + BF^{i-1}) \end{aligned} \quad (45)$$

or

$$\begin{aligned} X^{i+1} = (I + \theta A)X^i + (T_C - \theta)AX^{i-1} \\ + \theta BF^i + (T_C - \theta)BF^{i-1} \end{aligned} \quad (46)$$

a matrix equation which is a discrete-time equivalent to the sampled-data model.

The corresponding second-order model can be derived from equation (46) as follows. Let matrices A, B and F be as in equations (37c) to (37e). Thus equation (46) becomes:

$$\begin{bmatrix} \dot{x} \\ \dot{x} \end{bmatrix}^{i+1} = \begin{bmatrix} 1 & 0 \\ -\theta\omega_n^* & 1-2\theta\zeta\omega_n^* \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix}^i + (T_C - \theta) \begin{bmatrix} 0 & 1 \\ -\omega_n^* & -2\zeta\omega_n^* \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix}^{i-1} \\ + \theta \begin{bmatrix} 0 & 0 \\ 0 & \omega_n^* \end{bmatrix} \begin{bmatrix} 0 \\ u \end{bmatrix}^i + (T_C - \theta) \begin{bmatrix} 0 & 0 \\ 0 & \omega_n^* \end{bmatrix} \begin{bmatrix} 0 \\ u \end{bmatrix}^{i-1} \quad (47)$$

In scalar notation, this is :

$$x^{i+1} = x^i + \theta x^i + (T_C - \theta)x^{i-1} \quad (48)$$

and

$$\begin{aligned} \dot{x}^{i+1} &= -\theta\omega_n^* x^i + (1 - 2\theta\zeta\omega_n^*) \dot{x}^i \\ &+ (T_C - \theta)(-\omega_n^* x^{i-1} - 2\zeta\omega_n^* \dot{x}^{i-1}) \\ &+ \theta\omega_n^* u^i + (T_C - \theta)\omega_n^* u^{i-1} \end{aligned} \quad (49)$$

## 5.0 COMPUTERIZED MODELS

A computerized model is a computer program which implements a mathematical model on a particular computer. The four computerized models are identified as Systems A, B, C and D in Figure 1. This section describes the computer implementation of the mathematical models of Section 4.

## 5.1 System A

The discrete-time analytical solution mathematical model is implemented on a VAX 11/780 digital computer. This computerized model, System A, is implemented as FORTRAN subroutine SYSTMA which uses data set DSA as input, solves the analytical equations, and produces data set DSR as output. Its documentation is given in Appendix C.

Subroutine SYSTMA starts by establishing a final solution time  $T_F$  and a data computation/storage period  $T_S$ . These variables are computed as:

$$T_F = 2\pi N_T / \omega_n^* \quad (50)$$

and

$$T_S = 2\pi / N_S \omega_n^* \quad (51)$$

where  $N_T$  is the required number of cycles for the whole solution and  $N_S$  is the required number of data points per cycle to be computed and stored. The remaining operations of SYSTMA depend on whether the damping ratio is less than, equal to, or greater than unity to solve the appropriate equations among (19) to (29) iteratively. Data points  $x^i$ ,  $\dot{x}^i$  and  $t^i$  where  $t^i$  is incremented by  $T_S$  at each iteration, are stored in data set DSR.

## 5.2 System B

The continuous-time model is implemented on an EAI 680 analog computer. The analog computer is an electronic computing machine whose operation is quite different from that of a digital computer. Numerical values on an analog computer are established by the measurement of electrical voltages on which mathematical operations are performed. An analog computer operates in a parallel manner whereas a digital computer operates sequentially. Parallel operation means that all variables in a problem are simultaneously updated as time evolves. Consequently, the time required to generate problem solutions on an analog computer is independent of problem complexity. Also, an analog computer solves differential equations synchronously. Furthermore, in this investigation every solution of System B is done in real time ( $B=1$ ).

An analog computer is made of electronic components such as integrators, summers, etc. It is programmed by linking these components together with electrical connections. Furthermore, the analog computer operates with values smaller than or equal to 1 at all times. For that purpose, the model's time-dependent variables must be scaled with 'amplitude scaling factors' to prevent

'overloading' the analog components. Figure 11 illustrates a scaled analog circuit for System (13) where,  $x_M$ ,  $x_M$  and  $x_M$  are the scale factors corresponding to variables  $x$ ,  $\dot{x}$  and  $\ddot{x}$ , respectively.  $x^0$  and  $\dot{x}^0$  are the initial conditions of the system. On the circuit diagram, the symbol numbered 16 represents a summer whereas symbols 20 and 25 represent integrators. A DCA (Digitally Controlled Attenuator), or a potentiometer, has the function of multiplying its own constant coefficient by its input value. DCA's are represented by the circular symbols numbered 15, 20, 22, 23, 25, 27 and 28. The expressions in square brackets are scaled variables whereas the curved brackets indicate DCA coefficients. Since the maximum value of a DCA coefficient is also unity, it is sometimes necessary to introduce an 'amplifier gain'  $G$ . Such a gain is shown associated with integrators 20 and 25, allowing the coefficient of DCA's 22 and 27 to be divided by the same factor.

When the analog computer is in operate mode, that is when the model is being solved, variables  $x$  and  $\dot{x}$  are integrated. Also, variables  $x$  and  $\dot{x}$ , multiplied respectively by the coefficients of DCA's 28 and 23, are added to the forcing term from DCA 15 to produce a new

value for  $x$ . Each of these steps is executed continuously.

The analog program of System B is controlled by digital computer subroutine SYSTMB whose documentation is contained in Appendix D. There are two main parts in the subroutine. The first one sets the analog computer components; the second stores data (Fig. 12).

The first part of SYSTMB loads program VAXHYB on the PACER 100 digital computer. This program is part of the VAX/HYBRID system and provides for data transfer between the VAX digital computer and the analog computer through the PACER digital computer. SYSTMB then computes the final solution time  $T_f$  and the data storage sampling period  $T_S$  by equations (50) and (51). It also computes the following scale factors:

$$x_M = 2 u \quad (52)$$

$$x_M = u \omega_n \quad (53)$$

$$\ddot{x}_M = u \omega_n^2 \quad (54)$$

The amplifier gain  $G$  is determined depending on the natural undamped frequency  $\omega_n$  as follows:

$$G = \begin{cases} 1, & 0 < \omega_n \leq 1 \\ 10, & 1 < \omega_n \leq 10 \\ 100, & 10 < \omega_n \leq 100 \end{cases} \quad (55)$$

Gain  $G$  is then set on the integrators by analog mode control using VAX/HYBRID system subroutines (Q Routines). The first part of SYSTMB concludes by computing the DCA values  $D_K$ , where  $K$  is the DCA number, and sets them on the analog computer. DCA values are computed as follows:

$$D_{15} = u \omega_n^2 / 10 x_M \quad (56)$$

$$D_{20} = x^0 / x_M = 0 \quad (57)$$

$$D_{25} = x^0 / x_M = 0 \quad (58)$$

$$D_{22} = x_M / G x_M \quad (59)$$

$$D_{27} = x_M / G x_M \quad (60)$$

$$D_{23} = -2\zeta \omega_n x_M / 10 x_M \quad (61)$$

$$D_{28} = -\omega_n^2 x_M / 10 x_M \quad (62)$$

The second part of subroutine SYSTMB is performed by calling subroutine HILOOPB. It puts the analog computer in operate mode and reads variables  $x_S$  and  $x_S$  respectively at a high rate from the analog-to-digital (A/D) converters, unscaling them each time by

$$x = x_S x_M \quad (63)$$

and

$$x = x_S \quad x_M \quad (64)$$

An accurate clock on the VAX computer determines the time  $t^J$  when variables are read from D/A converters. Solution data points are stored in data set DSR as  $x^i$ ,  $x^j$  and  $t^i$  when  $t^J$  is larger than or equal to the last time of storage  $t^{i-1}$  plus the data storage sampling period  $T_S$ .

The solution stops when

$$t^J \geq T_F \quad (65)$$

The iterative logic is shown in Figure D-5.

### 5.3 System C

The sampled-data model is implemented on the hybrid computer as System C in Figure 1. The continuous-time subsystem is implemented on the EAI 680 analog computer while the discrete-time subsystem depends upon two digital computers: the DEC VAX 11/780 and the EAI PACER 100 (Fig. 13). System C is controlled by subroutine SYSTM C on the VAX computer. Program PACMAN (PACER MAIN) on the PACER provides for data transfer between SYSTM C and the analog computer as well as reading the analog computer clock. Data conversion between the PACER and the analog computer is performed by A/D and D/A converters in the sample and hold subsystem. The

documentation for SYSTM C and PACMAN can be found in Appendices E and G respectively.

The circuit diagram of the continuous-time subsystem is illustrated in Figure 14. The symbolic figures in this diagram have the same meaning as in the analog circuit of Figure 11. For each integration, this subsystem continuously integrates the D/A converter values, implements analog compensation by adding a fraction  $\theta$  thereof to the integrator output and delivers the sum to an A/D converters.

Subroutine SYSTM C is implemented in such a way that with minor changes and the standard analog patchboard, it would allow up to fifteen integrators with compensation to be used simultaneously. This would permit, for example, the performance study of other mathematical models such as higher order linear or nonlinear systems or combinations thereof. Furthermore, with relays  $R_{34}$  and  $R_{39}$  positioned as shown in Figure 14, the integrators operate independently. Suppose that  $R_{34}$  would be switched to its alternative position, then the integrators would be connected in series. Different compensation factors would probably be required in this case. Such alternatives bear investigation but are not considered here.

Since the hybrid system exchanges data between the VAX computer and the analog computer, the hybrid facility used was such that a program similar to program VAXHYB for System B was required on the PACER computer to allow these transfers to occur. As a replacement for the general-purpose program VAXHYB, program PACMAN was implemented for the particular application of the computerized model of System C. This program has two main functions and performs no important calculations. The first one is to receive data from the VAX into a buffer, set the analog components and D/A converters, read A/D converters and send back the buffer containing new values to the VAX; The second is to fix the required loop-time  $T_C$  by looping on one if-statement until the elapsed time since the last reading of D/A converters does not exceed  $T_C$ .

Transfer program VAXHYB could have been used for System C as it had been for System B. However, SYSTM C was done before SYSTM B and the accurate clock of the VAX was not available then. Thus, PACMAN remains as a special-purpose alternative to VAXHYB with the advantage that looping to fix computation time  $T_C$  is done on the dedicated PACER rather than the multi-user VAX computer, thereby liberating the latter for other users.

The operations of SYSTM C are now summarized. First, the final solution time and data storage period are computed using the same equations as in Systems A and B, i. e., equations (50) and (51). Amplitude scale factors are computed by:

$$x_M = (1.2)^2 u \quad (66)$$

$$x_M = (1.2) u \omega_n \quad (67)$$

$$x_M = (1.2) u \omega_n^2 \quad (68)$$

The scale factors are set larger than in System B since many solutions tend to be less accurate with System C. The scale factors are adjusted further, as follows, if the coefficients of compensation DCA's (32 and 37 in Figure 14) exceed unity:

$$x_M = \begin{cases} 1.2 \theta x_{MP} & \theta x_{MP} / x_M \geq 1 \\ x_{MP} & \theta x_{MP} / x_M < 1 \end{cases} \quad (69)$$

$$x_M = \begin{cases} 1.2 \theta x_{MP} & \theta x_{MP} / x_M \geq 1 \\ x_{MP} & \theta x_{MP} / x_M < 1 \end{cases} \quad (70)$$

where  $x_{MP}$  and  $x_{MP}$  respectively are the past values of  $x_M$  and  $x_M$ . Then, the amplified gain  $G$  is given a value such that DCA's 31 and 36 do not exceed unity. This is

achieved by first determining the maximum value of  $G$ ,

i.e.,

$$G_M = \text{MAX} \left( x_M / x_M, x_M / x_M \right) \quad (71)$$

Gain  $G$  is then set depending on  $G_M$  as follows:

$$G = \begin{cases} 1, & G_M \leq 1 \\ 10, & 1 < G_M \leq 10 \\ 100, & 10 < G_M \leq 100 \\ 1000, & 100 < G_M \leq 1000 \end{cases} \quad (72)$$

Relay variables  $R_{34}$  and  $R_{39}$ , which are used to define the analog circuit, are given values of zero such that the relays will remain open as shown in Figure 14 for the duration of the solution. The DCA values  $D_K$ , where  $K$  represents the DCA number, are computed as follows:

$$D_{30} = x^0 / x_M = 0 \quad (73)$$

$$D_{35} = x^0 / x_M = 0 \quad (74)$$

$$D_{32} = \theta x_M / x_M \quad (75)$$

$$D_{37} = \theta x_M / x_M \quad (76)$$

$$D_{31} = -x_M / x_M G \quad (77)$$

$$D_{36} = -x_M / x_M G \quad (78)$$

In order to set up the analog computer for a particular solution, program PACMAN needs the necessary data. As mentioned above, the data are transmitted from the VAX to the PACER through a buffer. At this point of SYSTM C, the buffer is filled with the values of the following variables:  $D_{30}$ ,  $D_{35}$ ,  $D_{32}$ ,  $D_{37}$ ,  $D_{31}$ ,  $D_{36}$ ,  $G$ ,  $T_C$ ,  $R_{34}$ ,  $R_{39}$  and an integer value specifying the number of integrations. The buffer data are received from the VAX as soon as the execution of program PACMAN begins on the PACER computer.

Then the solution of System C begins with the execution of subroutine HILOOP called by SYSTM C. It is solved in a high speed iterative loop which includes the transfer of hybrid data (VAX-Analog-VAX through PACER). The high-speed-loop includes the following operations (Figure E-4):

- (1) The A/D converter variables  $x_S$  and  $x_M$  are received in the buffer from the PACER and unscaled:

$$x = x_S x_M \quad (79)$$

$$x = x_S x_M \quad (80)$$

- (2) The discrete time solution  $(t^J, x^J, x^J)$  is stored in data set DSR as discrete data  $(t^i, x^i, x^i)$  in a similar manner as SYSTM B (Fig. E-6), where  $t^J$  and  $t^i$

are the solution and data storage times respectively incremented by

$$t^J = t^{J-1} + T_C \quad (81)$$

and

$$t^i = t^{i-1} + T_S \quad (82)$$

(3) Model equation (13) is solved for  $x$  and variables  $x$  and  $x$  are scaled by

$$x_S = x / x_M \quad (83)$$

and

$$x_S = x / x_M \quad (84)$$

These variables are sent to the D/A converters via the PACER.

The VAX/PACER interface system is such that data transferred in either direction must be integers. However, most of the hybrid data are fractions. To overcome this problem, the fractions are multiplied by the largest PACER integer (i.e., 32768) and then converted into integers by the FORTRAN function ININT. For example, variables  $x_S$  and  $x_S$  are transformed by the following FORTRAN statements before being sent to the PACER:

$$XDS = \text{ININT}(XDS * 32768.) \quad (85)$$

$$XDDS = \text{ININT}(XDDS * 32768.) \quad (86)$$

The inverse transformation (i. e., division by 32768) is then performed by subroutine VXPBUF of program PACMAN to revert back to scaled fractions for D/A conversion purposes. The same idea applies for PACER to VAX transfers. In the PACER, fractions  $x_S$  and  $x_S$  are transformed into integers by subroutine PVXBW and inverse transformed in the VAX by:

$$XS = \text{FLOATI}(XS) / 32768. \quad (87)$$

$$XDS = \text{FLOATI}(XDS) / 32768. \quad (88)$$

where the FORTRAN function FLOATI converts integer variables into real variables.

System C uses a FLAG variable with six possible values to control whether the program should stop or continue:

FLAG = 1 :

This is the normal value indicating that the solution must continue.

FLAG = 2 :

Indicates that the solution must stop because either the final solution time is reached or the solution is growing indefinitely large.

FLAG = 3 :

Indicates a time constraint. It means that the required time of computation  $T_C$  is too small and the operations in the high-speed-loop could not be achieved completely during that period.

FLAG = 4 :

Indicates that for some reason, the VAX was unable to send the buffer data to the PACER. This case and the case of FLAG=5 should never happen unless the hybrid system is not functioning properly.

FLAG = 5 :

Indicates that for some reason, the VAX was unable to receive the buffer data from the PACER (see FLAG=4).

FLAG = 6 :

Indicates that an overload on the analog computer is about to be or has already been detected. The data going to the D/A converters and coming from the A/D converters are checked to prevent them from getting too close to unity. If an overload is detected, the amplitude scale factors are multiplied by 1.5 and the high-speed-loop is restarted.

#### 5.4 System D

The discrete-time equivalent of sampled-data computerized model is implemented digitally by FORTRAN subroutine SYSTMD whose documentation appears in Appendix F. Subroutine SYSTMD uses the model parameters of DSA and DSB as input and solves equations (48) and (49). It first computes a final solution time  $T_F$  (eq. 50) and a

data storage sampling period  $T_S$  (eq. 51). As in System C, the equations are solved at every instant  $t^J$  and incremented as in equation (81) and data corresponding to instants  $t^i$  (eq. 82) are stored in data set DSR. The solution stops when  $t^J \geq T_F$ .

## 6.0 PERFORMANCE CRITERIA

Solution errors are defined as departures from a reference solution. Several criteria such as amplitude error, gain error and root mean square error have been used in the literature to establish the accuracy of dynamic system solutions.

The criterion adopted in this report is a normalized root mean square error of a normal distance approximation. The overall error between a given function  $x(t)$  and a reference function  $x_R(t)$  (Fig. 15a) is determined as follows. At any given value of time  $t$  where both functions exist, the normal distance is approximated by

$$\xi = \Delta x \cos \alpha \quad (89)$$

where

$$\Delta x = x - x_R \quad (90)$$

is the difference in amplitude and

$$\alpha = \tan^{-1} \frac{x}{x_R} \quad (91)$$

is the slope angle of  $x_R$ . Furthermore, defining line L to be parallel to the tangent  $L_R$  of  $x_R$  and intersecting  $x$  at the given value of  $t$ , the derivative may be expressed as

$$\dot{x}_R = \Delta x / \Delta t \quad (92)$$

where

$$\Delta t = t - t_1 \quad (93)$$

is the difference in time between the given value of  $t$  and  $t_1$ , the time corresponding to the horizontal projection of  $x_R(t)$  onto L.

The distance  $\delta$  is normalized by normalizing the differences  $\Delta x$  and  $\Delta t$  respectively to the maximum absolute amplitude  $x_{MAX}$  and the time domain  $T_1$  of the functions. Specifically,

$$x_{MAX} = \text{MAX} \left[ \text{MAX}(|x(t)|), \text{MAX}(|x_R(t)|) \right], t \in [0, T_1] \quad (94)$$

where  $T_1$  is the minimum of both total solution times. In order to be consistent, every model was solved for a fixed period corresponding to  $N_T=3$  cycles of undamped natural frequency  $F_{n1} = \omega_n / 2\pi$  except when a system was severely unstable. Thus the normalized differences are computed by

$$\Delta x_N = \Delta x / x_{MAX} \quad (95)$$

and

$$\Delta t_N = \Delta t / T_1 \quad (96)$$

and the normalized derivative is

$$\dot{x}_{RN} = \Delta x_N / \Delta t_N = \Delta x T_1 / \Delta t x_{MAX} = \dot{x}_R T_1 / x_{MAX} \quad (97)$$

The normalization of Figure 15a to 15b is completed by:

$$\alpha_N = \tan^{-1} \dot{x}_{RN} \quad (98)$$

$$\delta_N = \Delta x_N \cos \alpha_N \quad (99)$$

$$x_{RN} = x_R / x_{MAX} \quad (100)$$

$$x_N = x / x_{MAX} \quad (101)$$

$$L_{RN} = L_R / x_{MAX} \quad (102)$$

$$L_N = L / x_{MAX} \quad (103)$$

$$t_{1N} = t_1 / T_1 \quad (104)$$

and

$$t_N = t / T_1 \quad (105)$$

Finally, the root mean square error criterion is given

by:

$$\epsilon_N = \left[ \frac{1}{T_1} \int_0^{T_1} \delta_N^2 dt \right]^{1/2} = \left[ \int_0^1 \delta_N^2 dt_N \right]^{1/2} \quad (106)$$

In the case when one of the solutions grows indefinitely,  $\epsilon_N$  is given a large value of unity since the borderline of practical acceptability will be in the vicinity of 0.0075.

This error value ( $\epsilon_N$ ) represents a normalized approximation to the average normal distance between two solutions. In order to gain insight into the significance of  $\epsilon_N$ , a set of graphs displaying errors between various SOLDE solutions is presented in Appendix A. These curves are all solutions of the analytical model for different values of damping ratio ( $\zeta = .01, .1, .5, 1, 2, 5$ ) and a natural undamped frequency of 1 Hz for the reference solutions. In Figures A-1 to A-6, the damping ratio was varied until the illustrated errors ( $\epsilon_N = .0075, .01, .1$ ) were obtained. Similarly, in Figures A-7 to A-12, the undamped natural frequency was varied to achieve the same errors. It is seen that  $\epsilon_N = .0075$  to .01 would likely be acceptable as a figure of merit for many practical engineering applications but that  $\epsilon_N = .1$  would definitely be too large. This normal error criterion was chosen over a simple amplitude error criterion because the latter was too intolerant of frequency deviations, especially for the low damping solutions.

The error criterion was used to determine regions of accuracy in the space of system parameters. Damping ratio  $\zeta$  and natural undamped frequency  $\omega_n$  are the two parameters of model equation (13) whereas computation time  $T_C$  and compensation factor  $\theta$  are hybrid computer implementation parameters.

It can be shown by analysis that parameters  $\omega_n$  and  $T_C$  can be combined into one, i. e.,  $\omega_n T_C$  radians/sample. Other authors<sup>8-10</sup> have also used this parameter in accuracy studies. Furthermore, it was verified by experiment in the course of this work that accuracy is a function of this combined parameter. However, the equivalent 'sampling rate' parameter

$$R = (F_n T_C)^{-1} = 2\pi / \omega_n T_C \quad (107)$$

expressed in samples per cycle, was found to be more meaningful and is used in the presentation of results throughout this report.

The same authors<sup>8-10</sup> presented their results only for  $\theta = 1.5T_C$ , which is the optimum value of  $\theta$  in the Taylor Series sense. Vichnevetsky,<sup>7</sup> however, is one of the few authors who presented results for other values of  $\theta$ , but only for stability studies. An objective in this project was to identify regions of improved accuracy with values of  $\theta$  other than  $1.5T_C$ . Also, a 'modified compensation factor'

$$\theta' = \theta / 1.5T_C$$

(108)

was defined such that its optimum compensation value in the Taylor Series sense is unity whereas  $\theta'=0$  corresponds to the uncompensated hybrid simulation case.

## 7.0 PERFORMANCE ANALYSIS PROGRAMS

Three programs were developed on the VAX 11/780 digital computer for the performance analysis of the previously defined computerized models. Program RESPLT simply plots the time response of a system which is specified interactively by one of the characters A, B, C or D. The input parameters in DSA and DSB are also entered by the user. Program RESPONS also accepts a character (A, B, C, D) from the user and produces time responses of the specified system. It then solves the system for every combination of input parameters included in Table 3. The data are then stored in disk files. The performance analysis of a system compared to another system with the same input parameter values is executed by program RMSERR where the root mean square (RMS) error is computed between both. This program asks the user to specify two systems to be compared and then performs the analysis on the corresponding solution data produced by program RESPONS. The RMS errors are tabulated and displayed on graphs. Run examples of the three programs are given in Appendix K.

## 7.1 Program RESPLT

Program RESPLT is an interactive program in which the user is asked to specify one of the four systems (A, B, C, D) and a set of values for the input parameters  $S$ ,  $F_0$ ,  $\theta'$  and  $T_C$ . The documentation of program RESPLT is contained in Appendix H. The program uses a plotting package<sup>14</sup> to plot time response solutions. It uses the solution data in data set DSR generated by the four computerized models (subroutines SYSTMA, SYSTMB, SYSTM C and SYSTMD) to plot the curves. The abscissa and ordinate are scaled automatically. Furthermore, it displays a fixed number of cycles of oscillation depending on the value of  $N_T$  read from disk file DSC.DAT which also contains the value for  $N_S$ , i.e., the number of data points to be stored per cycle of solution. The user is required to specify one of several possible output devices, such as a screen terminal, an X-Y plotter or a printer-plotter.

## 7.2 Program RESPNS

Program RESPNS is documented in Appendix I. Briefly, the user is asked to supply a letter (A to D) corresponding to the system to be solved. The whole range of values of the input parameters in data sets DSA and DSB (Tables 1 and 3) are read from disk files DSA.DAT

and DSB.DAT as well as file DSC.DAT containing the values of  $N_T$  and  $N_S$ . For the case when System C or D is to be solved, the values of  $\theta'$  are displayed on the screen and the user is requested to choose one, whereupon the model is solved for every combination of  $\xi$ ,  $F_N$  and  $T_C$  for the chosen value of  $\theta'$ . The user may then choose another value of  $\theta'$ . On the other hand, Systems A and B, are solved for every combination of the only two applicable parameters, i.e.,  $\xi$  and  $F_N$ . The solution data points temporarily stored by the computerized models in data set DSR are then stored in disk files. The solutions of Systems A and B are stored in files DSRA.DAT and DSRB.DAT, respectively. System C data are stored in files DSRC1.DAT to DSRC5.DAT where integers 1 to 5 correspond to the values  $\theta'$ ,  $i=1, \dots, 5$ . Likewise, for System D, the files are DSRD1.DAT to DSRD5.DAT.

### 7.3 Program RMSERR

Program RMSERR is documented in Appendix J. The user is requested interactively to enter two characters corresponding to two of the four systems A, B, C and D. The user's response is checked and an error message is issued if there is an inconsistency. Then, as in program RESPON, if one of the systems entered is C or D, the user has to supply a number  $i=1, \dots, 5$  corresponding to a

desired value  $\theta'$  so that the program can read the appropriate disk files containing the solution data points. Depending on the systems upon which the performance analysis is to be performed, two of the following twelve data files are read into program arrays: DSRA.DAT, DSRB.DAT, DSRC1.DAT to DSRC5.DAT and DSRD1.DAT to DSRD5.DAT. The normalized RMS error  $\epsilon_N$  (eq. 106) is then computed for every time response contained in the above files. The time responses are taken in the same order in which they were created by program RESPONS. The values of  $\epsilon_N$  are stored in an array which is organized to be tabulated and plotted, ~~in~~ one of two alternative ways.

The first alternative produces a table and a graph of  $\epsilon_N$  values. When System C or D is involved, the table gives the error as a function of the normalized sampling rate  $R$  and damping ratio  $\zeta$ . The values of  $R$  displayed in the table are entered by the user as their corresponding values of  $F_n T_C$  in file DSD.DAT (data set DSD). The associated graphs plot  $\epsilon_N$  against  $\zeta$  for several predetermined values of  $R$ . For Systems A and B, where  $T_C$  is zero,  $R$  is replaced by the natural period  $T_n = 1/F_n$ . The table is stored in disk file DSE'IJ'.TBL, where System 'I' is compared to reference System 'J'. Such tables and graphs are presented in Appendix B.

The second alternative produces a different graph but, first, the user is asked to supply an acceptable error value  $\epsilon_{NA}$ . Appropriate computations are made to find the sampling rate  $R$  for which the error is smaller than  $\epsilon_{NA}$  for a given value of  $\xi$ . The graph axes are  $R$  against  $\xi$ . For every specified combination of  $R$  and  $\xi$  a dot is plotted on the graph if the error is acceptable. Again, if Systems A and B are involved,  $R$  is replaced by  $T_0$ . Such graphs appear in Figures 18 to 36 where the dots have been replaced by regions of accuracy.

## 8.0 PERFORMANCE OF COMPUTERIZED MODELS

The performance analysis programs described in the previous section were implemented to determine the accuracy of the computerized model solutions. In this section the performance of Systems B, C and D are discussed and the correspondence between Systems C and D is established. The stability of sampled-data systems has been studied by several authors<sup>7,15,16,19</sup>. The regions of stability established by these authors are also discussed in more detail in this section. However, the main objective is to determine regions of accuracy within the regions of stability. It is also interesting to find the values of  $\theta'$  which increase the regions of accuracy and stability.

The computerized models were solved for a practical range of their input parameters. Damping ratio  $\zeta$  was varied from .002 (negligible damping) to 5 (high damping). The performances of the sampled-data model, System C, and its digital equivalent, System D, were observed for sampling rate  $R=(F_n T_C)^{-1}$  values varying from one to 10 thousand samples per natural period. For these two Systems, results were also obtained for the following discrete values of  $\theta'$ : 0, .5, 1, 1.5, 2. However, some results are also given for other values of  $\theta'$ . Since the analog computer system, System B, does not involve a computation time  $T_C$ , the errors are simply observed as a function of the natural period  $T_n (=F_n^{-1})$ .

The analysis programs produce graphs and tables as output. On the first series of graphs which are accompanied by a table of the exact values, the normalized root mean square error ( $\epsilon_N$ ) is plotted against  $\zeta$  with a curve for different values of the sampling rate  $R$ . Such graphs and tables are produced for each predetermined value of  $\theta'$ . In the case of System B, the curves are plotted for different values of  $T_n$  only. These tables and graphs are displayed in Appendix B and they serve the purpose of giving a precise value of the error for a fixed set of input parameter values.

With a different objective, the second series of graphs produced by program RMSERR, displays the region of the parameters  $R$  vs  $\xi$  where the error is considered acceptable ( $\epsilon_N \leq .0075$  and  $.01$ ). In other words, the region indicates the allowable sampling rate that will produce a small error for a given damping ratio and compensation factor. Each graph is produced for a constant value of  $\theta'$  and  $\epsilon_{NA}$ . However, for purposes of condensing and comparing results, several curves have been judiciously included in each graph of Figures 18 to 36. The dashed line 'window' in these graphs defines the range of parameters investigated. In the graphs of Figures 20 to 35, different regions of the window can be identified. One is a region of small error (or high accuracy) indicated by  $\epsilon_N \leq .0075$ . Another is a region of larger error (or intermediate accuracy) indicated by the cross-hatched areas where  $.0075 \leq \epsilon_N \leq .01$ . The region below the lower line (short and long dashes) is the DTESD model stability boundary under which the solutions grow increasingly large with time. An interesting comment can be made concerning the intermediate region of accuracy. The width of the intermediate region is an indication of the rate at which the error varies when varying the damping ratio or sampling rate. When this region is large, for a fixed  $\xi$ , it can be shown that the error increases smoothly for decreasing sampling rates. However, the intermediate error region is non-existent along some

segments of the high accuracy boundaries indicating a more radical variation in the error as the sampling rate or damping ratio varies. Thus some care has to be taken when simulating with these parameters. This is often seen in the region of large  $\zeta$  where relatively small variations in damping can produce disproportionately large solution errors or even destabilize the system completely, as seen by the proximity of the high accuracy boundary to the stability boundary of the DTESD model.

#### 8.1 System D Relative To A

Vichnevetsky<sup>7</sup> studied the theoretical limit of stability for the solution of an n'th order linear differential equation with constant coefficients using a hybrid computer where the integrations and compensations are done on the analog computer. He derived stability contours in the complex plane of the characteristic roots of the simulated system and plotted these contours for no compensation ( $\theta'=0$ ) and optimum compensation in the Taylor Series sense ( $\theta'=1$ ). Such stability contours can be quite different for other values of  $\theta'$  as shown by Allison and Johnson<sup>15</sup> for  $\theta'=.5, .75$  and  $1.5$ .

To facilitate the comprehension of the stability contours in the case of a SOLDE, they were transformed to the ( $\zeta$ , R) plane (viz. Appendix L) in Figure 16 where the stable region lies above the stability boundary for each value of  $\theta' = 0, .5, 1, 1.5$  and  $2$ . The boundaries for  $\theta' = .5, .75, 1$  and  $1.25$  are shown in Figure 17. These stability boundaries were verified with the DTESD computerized model (System D) solutions. It is clear from this graph that, for a given value of damping ratio,  $\theta' = 1$  is not necessarily the optimum value for stability with minimum sampling rates. In the curves of Figure 17, it is seen that  $\theta' = 1$  is optimum only for a small range of damping ratio, i. e.,  $\zeta \in (.1, .4)$ . In fact, it can be shown by plotting the stability curves of  $\theta'$  values between  $.75$  and  $1.25$  that the  $\theta' = 1$  boundary is practically never the lower curve even for  $\zeta \in (.1, .4)$ . Furthermore, it was verified that  $\theta' = 0.5$  is optimum for  $\zeta \geq 1$  and  $\theta' = 1.25$  is optimum for  $\zeta \leq 0.1$ . For example, however, it is seen that the system is stable for  $\zeta \in (.1, 1)$  with  $\theta' = 1$  and  $R \geq 10$  samples per cycle.

As for the stability boundaries, the accuracy boundaries defining the regions wherein  $\epsilon_N \leq .0075$  (good accuracy) are presented in Figure 18. There is a curve for each of the five  $\theta'$  values of interest. From this

graph, it is clear that  $\theta'=1$  and  $\theta'=0.5$  are optimum respectively for  $\zeta < 2$  and  $\zeta \geq 2$ . Since  $\theta'=1$  is optimum for a large range of damping ratios, it is interesting to look at accuracy curves for values of  $\theta'$  in the vicinity of unity. Some of these are shown in Figure 19. It seems that the accuracy regions, unlike stability, cannot be improved if  $\theta' > 1$ . However, the curves tend to show that the optimum value of  $\theta'$  for  $\zeta > 1$  lies in the semi-closed interval  $[0.5, 1)$ .

The two different levels of accuracy of the DTESD model and the stability boundaries are illustrated in Figures 20 to 24. It is seen that the region of high accuracy sometimes lies below the limit of stability for low damping. This is understandable since low damping implies marginal stability and, although a System D solution might be slightly unstable, its error relative to the analytical solution may satisfy  $\epsilon_N \leq 0.0075$ .

The smallest allowable sampling rate that can be found in these figures is approximately 20 samples/cycle. It occurs when  $\theta'=0.5$  (Fig. 21), with  $\zeta \approx 5$  and when  $\theta'=1$  (Fig. 22) with  $\zeta \approx 1$ . For example, this means that with  $\theta'=1$ ,  $\zeta=1$  and  $T_C=10$  msec, the highest allowable frequency for good accuracy is approximately 5 hertz, or 10 hertz if  $T_C=5$  msec. Also, with  $\theta'=1$ , good accuracy can be

obtained for  $\xi \in (.002, 2)$  with a sampling rate  $R \geq 50$  samples/cycle and the range can be extended to include  $\xi \in (2, 5)$  with  $R \geq 90$ . However, the same extension can be obtained with  $\theta' = 0.5$  and  $R \geq 32$ .

## 8.2 System C Relative To A

Accuracy boundaries of System C relative to System A and the digital equivalent stability boundaries are presented in Figures 25 to 29. It can be assumed that these stability curves are not too different from the actual stability limits of System C since the regions of accuracy follow a similar pattern as those of System D. This can be seen by superimposing the graphs of Figures 20 to 24 on those of Figures 25 to 29 respectively. However, there are a few exceptions where the regions of accuracy do not correspond. One of them is the case of  $\theta = 1$  (Figs. 22 and 27) and  $\xi \in (.5, 2)$  where the  $\epsilon_N = .0075$  boundary is somewhat lower for System C than for System D. However, the general discussion of System D relative to A is equally applicable to System C. In addition, Figure 30 demonstrates the effect of increasing the acceptable accuracy by decreasing  $\epsilon_N$  from .0075 to .005.

### 8.3 System C Relative To D

For the comparison of the sampled-data computerized model and its discrete-time equivalent, it is more appropriate to talk about regions of equivalence ( $\epsilon_N \leq 0.0075$ ) rather than accuracy. The graphs of equivalence regions are shown in Figures 31 to 35.

It is observed that for small values of compensation factor ( $\theta' = 0, .5$ ), both systems are equivalent somewhat beyond the stability boundary in the low damping and high sampling rate region. Otherwise, the equivalence curves all follow the stability boundaries very closely on the stable side. This means that as long as the solutions are stable, System D is equivalent to System C. This total equivalence supports the assumption made by Deiters, Kano and Inoue<sup>10</sup> on the basis of a few verification tests.

### 8.4 System B Relative To A

Since there is no time-delay in the analog computer solution of the continuous-time model, only one graph of results is required. Two accuracy regions ( $\epsilon_N \leq 0.0075$  and  $\epsilon_N \geq 0.01$ ) of System B are separated by a single boundary in the natural period versus damping ratio plane of Figure 36. The lack of any shaded area along the

boundary indicates a rapid deterioration of accuracy from one side to the other. To maintain good accuracy, the natural frequency  $F_n$  of the SOLDE must be less than 15 hertz ( $T_n = 0.067s$ ) if  $\xi \in [0.002, .5]$  and less than 30 hertz ( $T_n = 0.033s$ ) if  $\xi \in [2, 5]$ . The range  $\xi \in (.5, 2)$  is transitional as far as the upper bound of  $F_n$  is concerned. Furthermore, these upper limits of frequency for good accuracy represent a sort of ideal which could only be approached with System C by reducing  $T_c$  as much as possible.

## 9.0 CONCLUSION

Four mathematical models describing different methods of solution of a linear second order system were defined. A computerized model corresponding to each mathematical model was implemented and documented. One of the computerized models was a discrete-time analytical solution implemented on a digital computer as System A. A second, System B, was a real-time model solved continuously on an analog computer. System C was an implementation of a real-time sampled-data mathematical model on a hybrid computer. The well-known computational time delay in hybrid loops and a method compensating for it were discussed. The fourth computerized model solved the equations for a discrete-time equivalent of the sampled-data model and was implemented on a digital

computer as System D.

A performance criterion, defined to measure the root mean square of a normal distance approximation between the solutions of any two computerized models, gave an overall idea of the difference between two solutions.

A set of three general programs for the performance analysis of the computerized models were described and documented. With some minor changes, these programs could be used to investigate other systems such as nonlinear or higher order linear systems.

Useful results were obtained concerning the accuracy of the computerized models. These results are not only useful for the continuing work of this research but can also be useful to the hybrid programmer who would want to specify, for example, a safe value of sampling rate or the optimum compensation factor for a given SOLDE application. Although it is risky to extrapolate, they can at least serve as a starting point for second order dominant systems. Accuracy and stability boundaries for the DTESD model showed that the optimum value of analog compensation factor is a function of damping ratio and is, in general, different from the optimum value in the Taylor series sense. Also, it was found that System D is equivalent to System C in the stable region of parameters. The upper limits of frequency for good accuracy

of the analog computer model (System B) were determined. These limits represent, in a sense, the limits of System C when the hybrid time-delay tends to zero.

The programs developed in this work can serve as basic tools in the performance analysis of other computerized models. One interesting model would be to connect the integrators in series rather than independently as in Systems C and D. For this, a different compensation scheme would probably be needed. It is the ultimate goal of this continuing research to produce a hybrid computer programming package which would automate analog computer programming for the user. Such a package might include optimization of analog compensation factors. The option of using digital as well as analog integration would be provided. For example, in case of shortage of analog integrators, an equivalent to sampled-data model similar to System D could be used as a supplement. Its equations would thus be solved synchronously on the digital computer. Variables would be computed at every hybrid computation interval  $T_C$  and compensation parameter  $\theta$  would be adjusted accordingly.

## REFERENCES

1. Kleinert, W. (1982). "The New Hybrid Time-Sharing System MACHYS", EDP Centre, Technical University of Vienna, No. 19, December 1982, 18 pages.
2. Miura, T., and Iwata, J. (1963). "Effects of Digital Execution Time in a Hybrid Computer", Proceedings AFIPS Fall Joint Computer Conference, Vol. 24, 1963, pp. 251-266.
3. Gilbert, E. G. (1966). "Dynamic-Error Analysis of Digital and Combined Analog-Digital Computer Systems", Simulation, Vol. 6, No. 4, April 1966, pp. 241-257.
4. Matlock, David L. (1966). "Pulsed Prediction Filters Applied to Digital and Hybrid Simulation", Simulation, Vol. 6, No. 3, March 1966, pp. 153-157.
5. Deiters, Robert M., and Nomura, Tamiya (1967). "Circle Test Evaluation of a Method of Compensating Hybrid Computing Error by Predicted Integral", Simulation, Vol. 8, No. 1, January 1967, pp. 33-40.
6. Karplus, Walter J. (1966). "Error Analysis of Hybrid Computer Systems", Simulation, Vol. 6, No. 2, February 1966, pp. 120-136.
7. Vichnevetsky, R. (1969). "Stability Contours for the Analysis of Analog/Digital Hybrid Simulation Loops", Proceedings AFIPS Spring Joint Computer Conference, Vol. 34, 1969, pp. 859-866.
8. Curry, W. H. (1977). "An Evaluation of a Correction Method for Digital Computer Lag in Hybrid Systems", Proceedings Summer Computer Simulation Conference,

Chicago, July 1977, pp. 94-101.

9. Howe, Robert M. (1975). "Frame-Rate Requirements for Digital Function Generation in Hybrid Computing Loops", Winter Computer Simulation Conference, Sacramento, December 1975, pp. 457-461.
10. Deiters, R. M., Kano, K., and Inoue, K. (1971). "Practical Stability Error Charts for some Commonly Used Methods of Hybrid Computing Error Compensation", Proceedings AICA Symposium Simulation Complex Systems, Tokyo, September 1971, pp. D2.1-6.
11. Amyot, J. R. (1982). "Defining a Real-Time Model", Simulation, Vol. 38, No. 1, January, 1982.
12. Korn, G. A. (1962). "Approximations of Variable Time Delays Require Caution", Transactions of IRE on Electronic Computers, Vol EC-11, No. 1, February 1962, p. 82.
13. Gille J-C, Pelegrin M.J., Decaulne P., 'Feedback Control System', McGraw-Hill 1959.
14. 'PLOT 10 ADVANCED GRAPHING II, USER'S MANUAL', Tektronix, 1977
15. Allison, J. S., and Johnson H. M. (1979). "Stability of Hybrid Simulation of Dynamic Systems", Mathematics and Computers in Simulation XXI, North-Holland Publishing Company, 1979, pp. 289-303.
16. Little, Warren D. (1973). "Serial Hybrid Computation and Errors in Hybrid Loops", Transactions of IEEE on Computers, Vol. C-22, No. 4, April 1973, pp. 367-370.
17. El-Sherif, A. K., Kamal, A. A., and Bilial, A. Y. (1976). "Error Analysis in Hybrid Computer Simulation of

Dynamic Systems", Transactions IMACS (Annales de l' AICA), Vol. 18, No. 3, pp. 141-147.

18. Kemp, N. H. (1969). "Extensions and Analysis of Use of Derivatives for Compensation of Hybrid Solution of Linear Differential Equations", Proceedings AFIPS Fall Joint Computer Conference, Vol. 35, 1969, pp. 761-770.
19. Vansteenkiste, G. C. (1973). "Precision and Efficiency of Some Hybrid Algorithms", Proceedings 7th AICA Conference, Part 1, Prague, August 1973, pp. 94-97.
20. Bekey, G. A., and Karplus, W. J. (1968). "Hybrid Computation", John Wiley and Sons Inc., New York, 1968.
21. Boullart, Dr. I. L. (1982). "Hybrid Computing, Evaluation of 10 Years Experience in a University Environment", Tenth IMACS World Congress Proceedings, Vol. 2, Montreal, August 1982, pp. 9-12.
22. Connely, Marc E. (1961). "Real-Time Analog-Digital Computation", IRE Convention Record, Part 2, 1961, pp. 182-195.
23. Crosbie, Roy E., and Hay, John L. (1976). "Experience in Using the HCS-1 Hybrid Compiler", Simulation, Vol. 6, No. 2, December 1976, pp. 127-131.
24. Crosbie, Roy E., and Hay, John L. (1982). "Towards New Standards for Continuous System Simulation Languages", Proceedings Summer Computer Simulation Conference, Denver, July 1982, pp. 186-190.
25. Danilin, A. B., Spiro, A. G., and Yadykin, I. B. (1981). "Accuracy of Simulation of Hybrid Control Systems with a Digital Controller", Autom. and Remote Control, 42(11, Part 2), November 1981, pp 1577-81.

26. Deiters, Robert M., and Nomura, Tamiya (1967). "Predicted Integral Method of Compensating for Sampling and Time-Delay Errors in a Hybrid Computing System", Proceedings 5th AICA Conference, Lausanne, August 1967, pp. 181-190.
27. El-Sherif, A. K., Kamal, A. A., and Bilial, A. Y. (1975). "An Improved Scheme for Hybrid Computer Simulation of Dynamic Systems", Proceedings 6th Conference on Modeling and Simulation, Pittsburgh, April 1975, pp. 249-252.
28. Fleischer, Paul E. (1972). "Digital Realization of Complex Transfer Functions", Simulation, Vol. 6, No. 3, March 1966, pp. 171-180.
29. Gelman, Robert (1963). "Corrected Inputs--A Method for Improved Hybrid Simulation", Proceedings AFIPS Fall Joint Computer Conference, Vol. 24, 1963, pp. 267-276.
30. Genin, J., and Genin, R. (1973). "Etudes Analogiques des Equations", Annales de l' AICA, Vol. 15, No. 3, July 1973, pp. 104-114.
31. Gibson, J. A., and Gibbard, R. W. (1980). "Hybrid Serial-Parallel Digital Computation", Computer and Electrical Engineering, Vol. 7, 1980, pp. 25-34.
32. Gilbert, E. G., and Vansteenkiste, G. C. (1970). "Dynamic Error Analysis of Hybrid Computer Loops", Proceedings 6th AICA Conference, Munich, August 1970, pp. 227-234.
33. Gilbert, E. G. (1967). "Error Analysis of Hybrid Computer Loops", Annales de l' AICA, Vol. 9, No. 1, January 1967, pp. 35-36.

34. Giloi, W. (1967). "Error Corrected Operation of Hybrid Computer Systems", Proceedings 5th AICA Conference, Lausanne, August 1967, pp. 172-180.
35. Grierson, W. O., Lipski, D. B., and Tiffany, N. O. (1980). "Simulation Tools: Where can we go? ", Proceedings Summer Computer Simulation Conference, Seattle, August 1980, pp. 3-6.
36. Hammond, J. L., and Alford C. O. (1969). "Sampling Errors in Closed-Loop Hybrid Computer", Simulation, Vol. 13, No. 6, December 1969, pp. 307-313.
37. Howe, R. M. (1971). "The Future of Automatically Patched Hybrid Computers", Proceedings AICA Symposium Complex Systems, Tokyo, September 1971, pp. A1.1-8.
38. Howe, R. M., Holstien, R. B., and Moran, R. A. (1972). "Hardware/Software Considerations in the AD/FOUR Electronic Patched Hybrid Computer", Information Processing 71, North-Holland Publishing Company, 1972, pp. 668-674.
39. Howe, R. M., and Landauer, J. P., "A Quantitative Method of Speed Comparison Between Analog/Hybrid and Digital Computers", Computer, July 1976.
40. Howe, R. M. (1967). "Some Techniques for Accuracy Improvement in Analog Computation", Simulation, Vol. 9, No. 4, October 1967, pp. 173-179.
41. Justice, Harold R. (1981). "Programming an Analog Computer with a High Level Language", Proceedings Summer Computer Simulation Conference, Washington D. C., July 1981, pp. 166-169.
42. Karplus, Walter J., and Wood, Roger C. (1965). "Error

Analysis of Digital-Computer-Oriented Hybrid Computer Systems", Proceedings IFIP Conference, New York, May 1965, pp. 428-429.

43. Katz, S., and Neumann, D. (1980). "A Novel Approach to Real-Time Hybrid Simulation", Simulation of Systems 79, North-Holland Publishing Company, 1980.
44. Kerckhoffs, E. J. H., Dekker, L., and van Gelderen, J. A. (1973). "A Block-Iteration Method for the Hybrid Solution of Large Systems of Ordinary Differential Equations", Proceedings 7th AICA Conference, Part 1, Prague, August 1973, pp. 125-129.
45. Kerckhoffs, E. J. H. (1978). "On the Analog Computation of Integrals", Simulation, Vol. 30, No. 5, May 1978, pp. 169-170.
46. Korn, G. A. (1967). "Automated Computing-Error Studies in Fast Hybrid Computations", Annales de l' AICA, Vol. 19, No. 1, January 1967, p. 34.
47. Korn, G. A. (1978). "Digital Continuous-System Simulation", Prentice-Hall, 1978.
48. Korn, G. A. (1963). "Parameter-Perturbation Generator for Analog-Computer Error and Optimization Studies", Annales de l' AICA, Vol. 5, No. 2, April 1963, pp. 93-95.
49. Korn, G. A. (1964). "A Simple First-Order Hold Circuit", Simulation, Vol. 2, No. 2, February 1964, p. 17.
50. Korn, G. A. (1969). "Variable Time-Delay Simulation", Simulation, Vol. 13, No. 4, October 1969, p. 218.

51. Kuo, B. C. (1962). "Automatic Control Systems", Prentice-Hall, 1962.
52. Maslo, Ronald M. (1982). "A survey of Hybrid Computer Uses in Control Systems Design", Proceedings Summer Computer Simulation Conference, Denver, July 1982, pp. 83-85.
53. Mitchell, E. E. L. (1975). "Advanced Continuous Simulation Language User Guide/Reference Manual", Mitchell and Gauthier Associates Inc., Concord, Massachusetts, 1975.
54. Mitchell, E. E. L. (1982). "Advanced Continuous Simulation Language (ACSL): An Update", Tenth IMACS World Congress Proceedings, Vol. 1, Montreal, August 1982, pp. 462-464.
55. Mitchell, E. E. L. (1967). "The Effect of Digital Compensation for Computation Delay in a Hybrid Loop", Proceedings AFIPS Fall Joint Computer Conference, Vol. 31, 1967, pp. 103-108.
56. Miura, T. (1964). "Hybrid Computation Techniques for Differential Equations", Proceedings 4th International AICA Meeting, Brighton, September 1964, pp. 47-58.
57. Miura, T., and Iwata, J. (1965). "Study on Time-Shared Analog Computation Technique" Simulation, Vol. 5, No. 5, November 1965, pp. 318-327.
58. Paul, J. F. (1980). "The Effect of Recent Developments in Hybrid Simulation on Modern Scientific Computation", Proceedings Summer Computer Simulation Conference, Seattle, August 1980, pp. 7-8.
59. Phillips, Robert A. (1980). "Getting Productivity from a

- Hybrid Computer Facility", Proceedings Summer Computer Simulation Conference, Seattle, August 1980, pp. 9-11.
60. Van Remoortere, P. (1982). "Introduction to the Session on the User's Experience in Hybrid Computation", Tenth IMACS World Congress Proceedings, Vol. 2, Montreal, August 1982, pp. 1-2.
  61. Saydam, Tuncay (1982). "Systems Simulations and Computer Graphics Interface Issues", Tenth IMACS World Congress Proceedings, Vol. 4, Montreal, August 1982, pp. 216-218.
  62. Sheppard, Sallie (1983). "Applying Software Engineering to Simulation", pp. 13-19.
  63. Strauss, Jon C. (1967). "The SCI Continuous System Simulation Language", Simulation, Vol. 9, No. 6, December 1967, pp. 281-303.
  64. Trier, Reinhold (1982). "The Operation of a Hybrid Computer System Using a Simulation Language", Tenth IMACS World Congress Proceedings, Vol. 2, Montreal, August 1982, pp. 7-8.
  65. Valisalo, P. (1982). "Hybrid Computation--Today and Tomorrow", Tenth IMACS World Congress Proceedings, Vol. 2, Montreal, August 1982, p. 13.
  66. Vansteenkiste, G. C. (1971). "Analog or Digital Compensation for the Simulation of Complex Systems in a Hybrid Way", Proceedings AICA Symposium Simulation Complex Systems, Tokyo, September 1971, pp. D2.1-6.
  67. Vansteenkiste, G. C. (1976). "Mixed Data Processing Using Parallel Compensation", \*\*\*( UNKNOWN )
  68. Vansteenkiste, G. C. (1969). "Study of the Dynamic

Errors Introduced by the Delays Inherent on Combined Analog-Digital Computation in Hybrid Systems", Annales de l' AICA, Vol. 11, No. 4, October 1969, pp. 226-232.

69. Vichnevetsky, Robert (1967). "Error Analysis in the Computer Simulation of Dynamic Systems: Variational Aspects of the Problem", Transactions of IEEE on Computers, Vol. EC-16, No. 4, August 1967, pp. 403-411.
70. Walli, C. R. (1964). "Quantizing and Sampling Errors in Hybrid Computation", Proceedings AFIPS Fall Joint Computer Conference, Vol. 26, Part 1, October 1964, pp. 545-558.

TABLES

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Table 1: Data Set Definitions

Data set name	Contents*
DSA	$\xi, F_n$
DSAU	$\xi, F_n$ specified interactively by user
DSB	$\theta', T_c$
DSBU	$\theta', T_c$ specified interactively by user
DSC	$N, N_T, N_S$
DSD	$F_n T_c$ values to be displayed in error tables
DSE	$\epsilon_N$ table
DSEBA	$\epsilon_N$ table for System B relative to A
DSECA	$\epsilon_N$ table for System C relative to A
DSECD	$\epsilon_N$ table for System C relative to D
DSEDA	$\epsilon_N$ table for System D relative to A
DSR	$x, t$
DSR1	DSR used in program RMSERR to compare solutions of $S_1$ and $S_2$
DSR2	DSR used in program RMSERR to compare solutions of $S_1$ and $S_2$
DSRA	$x, t$ of System A
DSRB	$x, t$ of System B
DSRC 'k'	$x, t$ of System C corresponding to k'th value of $\theta'$ in DSB
DSRD 'k'	$x, t$ of System D corresponding to k'th value of $\theta'$ in DSB

\* Contents are defined in terms of parameter names. The sets of values associated with these parameters constitute the data set.

Table 2: Symbol Definitions

SYMBOL	FORTTRAN NAME	DEFINITION
A		System coefficient matrix
B		Forcing function coefficient matrix
D <sub>k</sub>	DCA(k)	Value of DCA number k
F		Forcing function vector
F <sup>i</sup>		Value of F at time t <sup>i</sup>
F <sub>n</sub>	FN	Natural undamped frequency, hertz
G	G	Integrator gain
i	NPOINT	Discretization index for solution storage
J		Discretization index for solution computation
L		Line parallel to L <sub>R</sub> and intersecting x <sub>R</sub> at a given time t
L <sub>N</sub>		Line L normalized
L <sub>R</sub>		Line tangent to x <sub>R</sub> at a given time t
L <sub>RN</sub>		Line L <sub>R</sub> normalized
N <sub>S</sub>	NS	Total number of samples per cycle to be stored
N <sub>T</sub>	NT	Number of cycles per solution
R		Normalized sampling rate (samples/cycle)
R <sub>k</sub>	RELAY(k)	Relay number k; state (0/1)
S	SYSTEM	User specified system
S <sub>1</sub>	SYSTEM	User specified system
S <sub>2</sub>	SYSTEM	User specified reference system
t	TIME	Clock time
T		Sampling and update time interval
t'	TIME	Model time
T <sub>C</sub>	TC	Computation and conversion time in hybrid loop

SYMBOL	FORTRAN NAME	DEFINITION
T	FINALTIME	Final solution time
F		
t <sup>i</sup>	RESTIME	Discrete time for storage of solution
t <sup>j</sup>	TIME	Discrete time for computation of solution
T <sub>n</sub>		Undamped natural period of a SOLDE
T <sub>S</sub>	SAVINCTIM	Sampling period for storage of solution data
T <sub>1</sub>	T1	Time period over which $\epsilon_N$ is computed
t <sub>1</sub>		Time corresponding to the horizontal projection of $x_R$ onto L
t <sub>1N</sub>		Normalized value of t <sub>1</sub>
u	STEP	Unit step function
v		Compensation variable
v <sup>i</sup>		Value of v at time t <sup>i</sup>
v <sub>1</sub>		First element of v
v <sub>2</sub>		Second element of v
w		Input vector to continuous-time subsystem in sampled-data model
w <sup>i</sup>	DAC	Value of w at time t <sup>i</sup>
w <sub>1</sub>		First element of w
w <sub>2</sub>		Second element of w
x	X	Response function
X		Response function vector
x	XD	First derivative of x with respect to time
x	XDD	Second derivative of x with respect to time
x <sup>i</sup>	RESPONS	Value of x at time t <sup>i</sup>
X <sup>i</sup>	ADC	Value of X at time t <sup>i</sup>
x <sub>M</sub>	XM	Amplitude scale factor for x

SYMBOL	FORTRAN NAME	DEFINITION
$x$ M	XDM	Amplitude scale factor for $x$
$x$ M	XDDM	Amplitude scale factor for $\dot{x}$
$x$ MAX	RESPM	Maximum amplitude of $x$
$x$ R		Reference response function
$x$ R		Derivative of $x$ R
$x$ RN		Function $x$ normalized R
$x$ RN		Normalized derivative of $x$ R
$x$ S	XS	Scaled value of $x$
$x$ S	XDS, XDAS	Scaled value of $\dot{x}$
$x$ S	XDDAS	Scaled value of $\ddot{x}$
$x$ 0		Initial condition on $x$
$x$ 0		Initial condition on $\dot{x}$
$x$ 1		First element of $X$
$x$ 2		Second element of $X$
Y		Ideal input function to continuous-time subsystem in sampled-data model
Z		Continuous-time integration output vector
$z$ 1		Value of $Z$ at time $t$ <sup>1</sup>
$z$ 1		First element of $Z$
$z$ 2		Second element of $Z$
$\alpha$		Slope angle of $x$ at a given time $t$ R
$\alpha$ N		Normalized value of $\alpha$
$\beta$	BETA	Time-scale factor
$\epsilon$ N	ERMSN	Normalized root mean square error

SYMBOL	FORTRAN NAME	DEFINITION
$\epsilon_{NA}$	ACCEPT	Acceptable value of $\epsilon_N$
$\zeta$	ZETA	Damping ratio
$\theta$	THETA	Compensation factor
$\theta'$	THETAP	Modified compensation factor
$\theta'_i$	NUMTHETA	i'th $\theta'$ value in data set DSB
$\delta$		Approximate distance in the direction perpendicular to $x_R$
$\delta_N$		Normalized value of $\delta$
$\Delta t$		Approximate distance in horizontal direction between two solutions
$\Delta t_N$		Normalized value of $\Delta t$
$\Delta x$		Difference in amplitude between two solutions
$\Delta x_N$		Normalized value of $\Delta x$
$T_1$		Initial time-delay in the hybrid loop
$T_2$		Analog to digital conversion delay
$T_3$		Digital computation delay
$T_3^*$		Digital to analog conversion delay
$\omega_c$	OMEGAN	Natural undamped frequency in time-scaled systems, rad/sec
$\omega$	OMEGAN	Natural undamped frequency in real systems, rad/sec

**Table 3: Specific Set of Model Parameters  
for which Systems C and D were  
solved in the performance analysis.**

$\theta$	$T_c$	$F_n$	$\zeta$
0.0	0.01	0.01	0.002
0.5	0.025	0.1	0.02
1.0	0.05	0.5	0.05
1.5	0.1	1.0	0.1
2.0	0.2	3.0	0.2
		5.0	0.5
		7.0	1.0
			2.0
			5.0

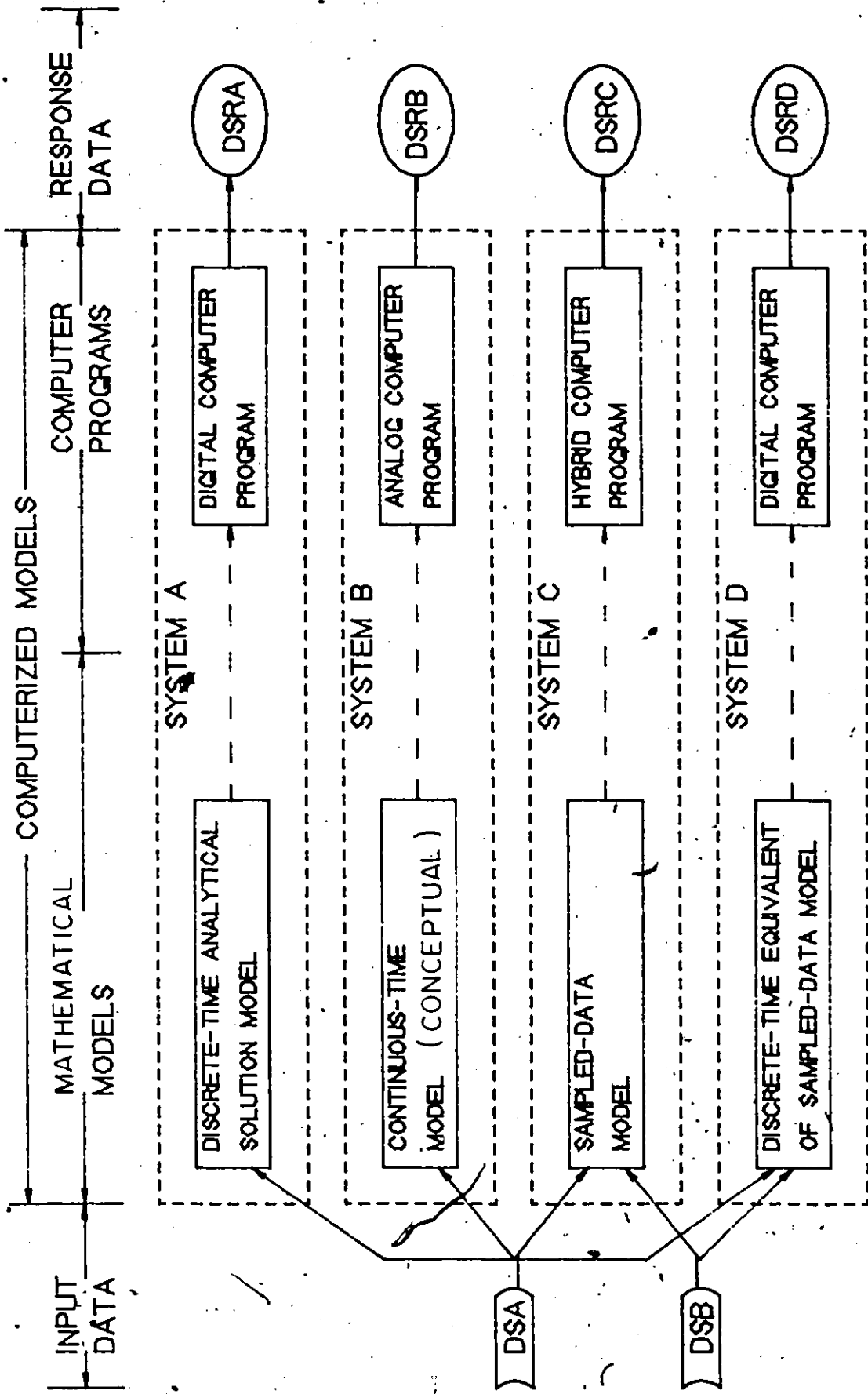


Figure 1 : Input-process-output diagram of computerized models

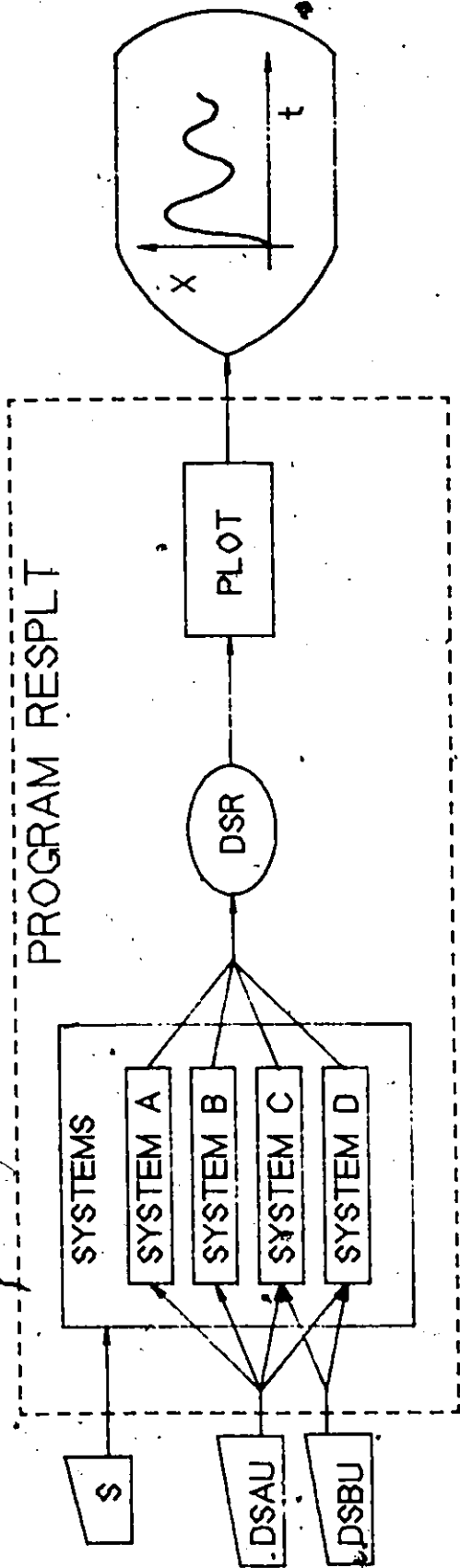


Figure 2 : File flow diagram of program RESULT

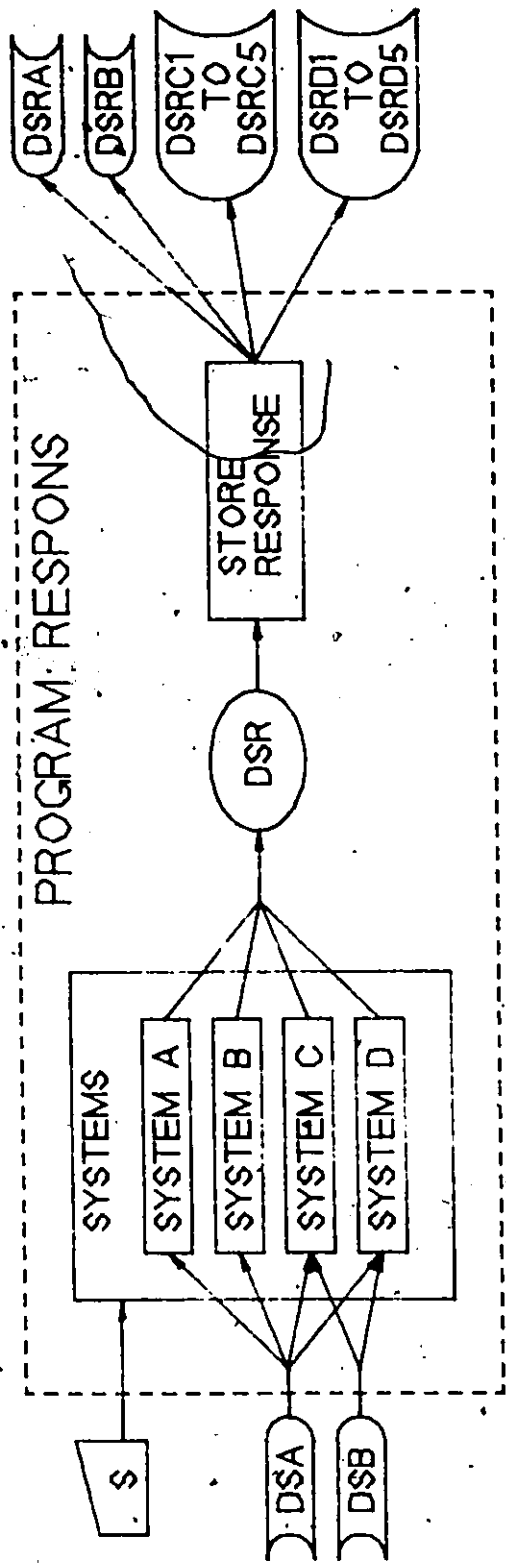


Figure 3 : File flow diagram of program RESPONSES

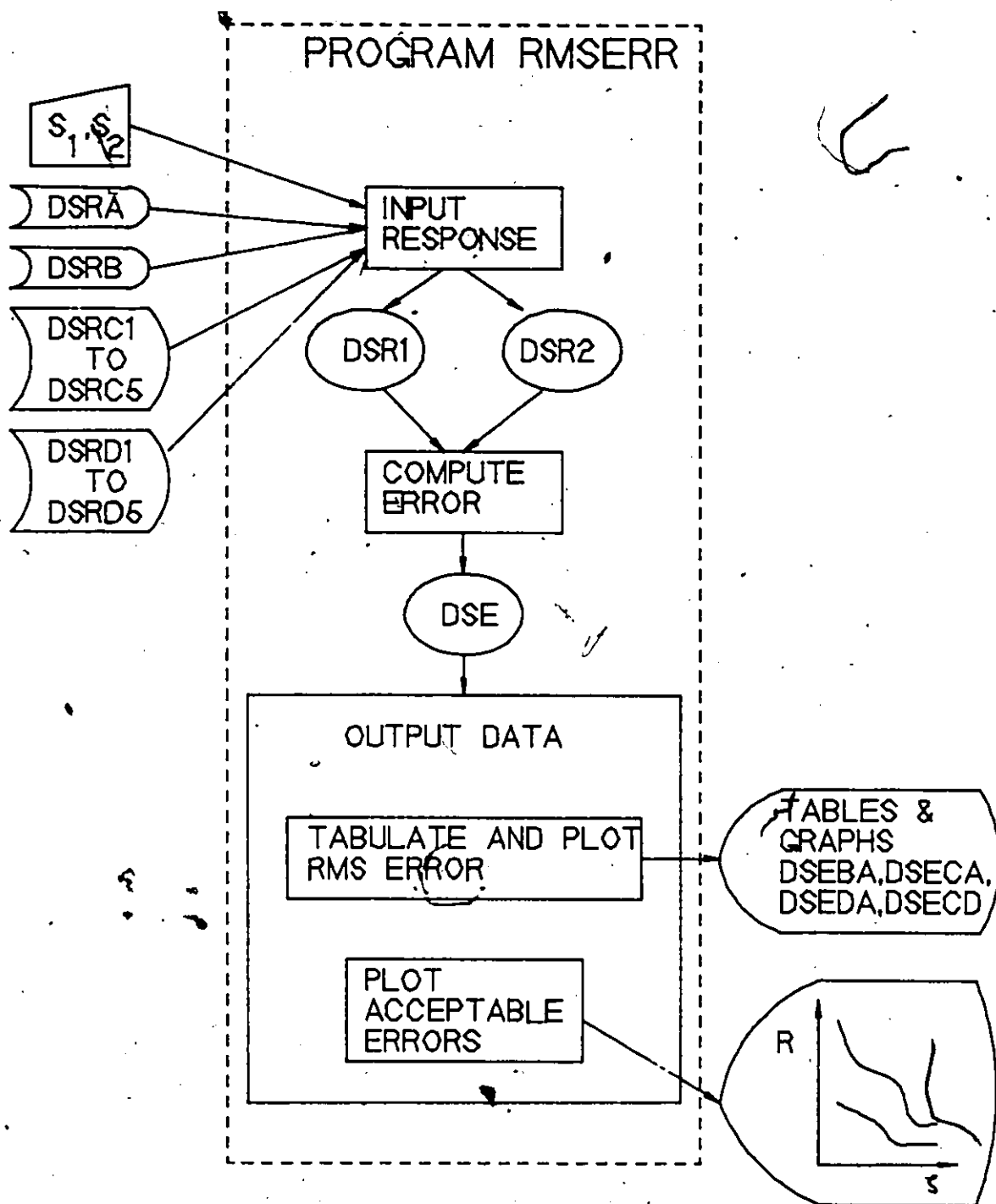


Figure 4 : File flow diagram of program RMSERR

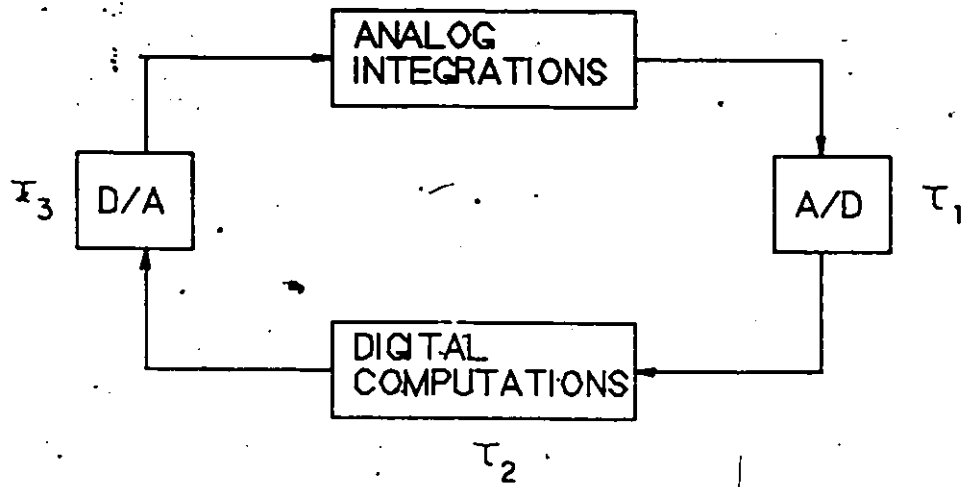


Figure 5 : Hybrid-loop with component delays

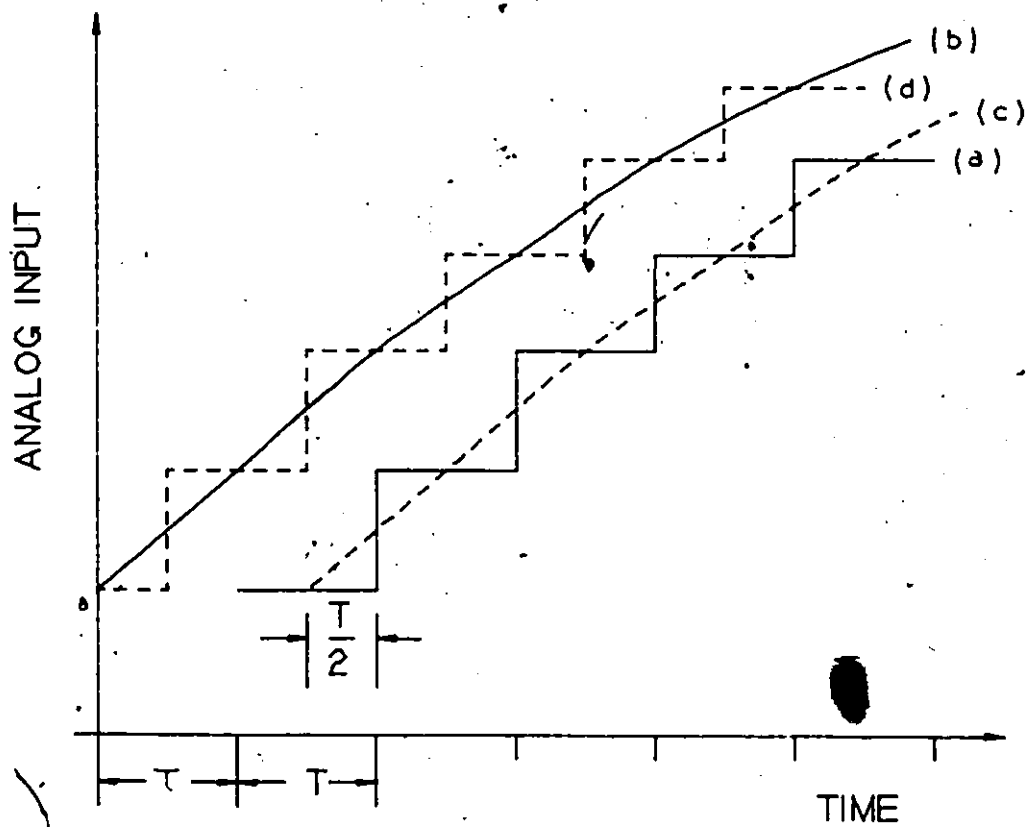
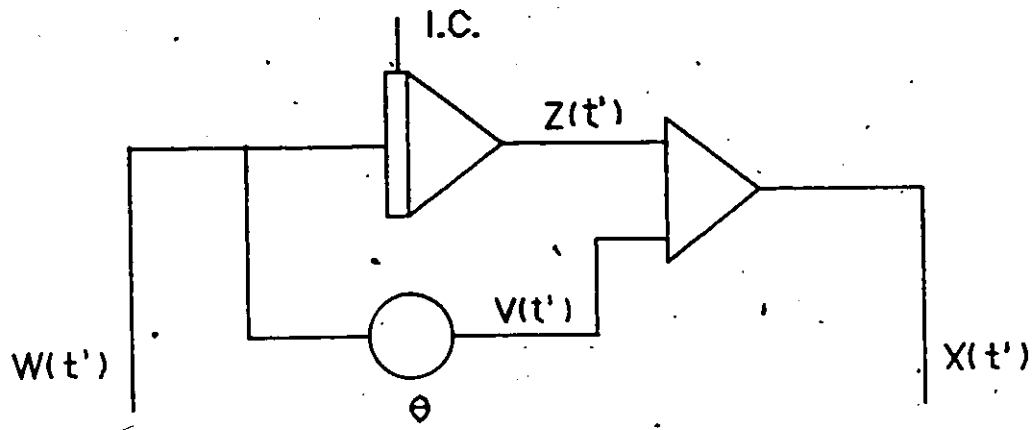


Figure 6 : Analog integrator input functions



$$X(t') = \int W(t') dt + \theta W(t')$$

Figure 7 : Simplified diagram of analog operations in hybrid loop

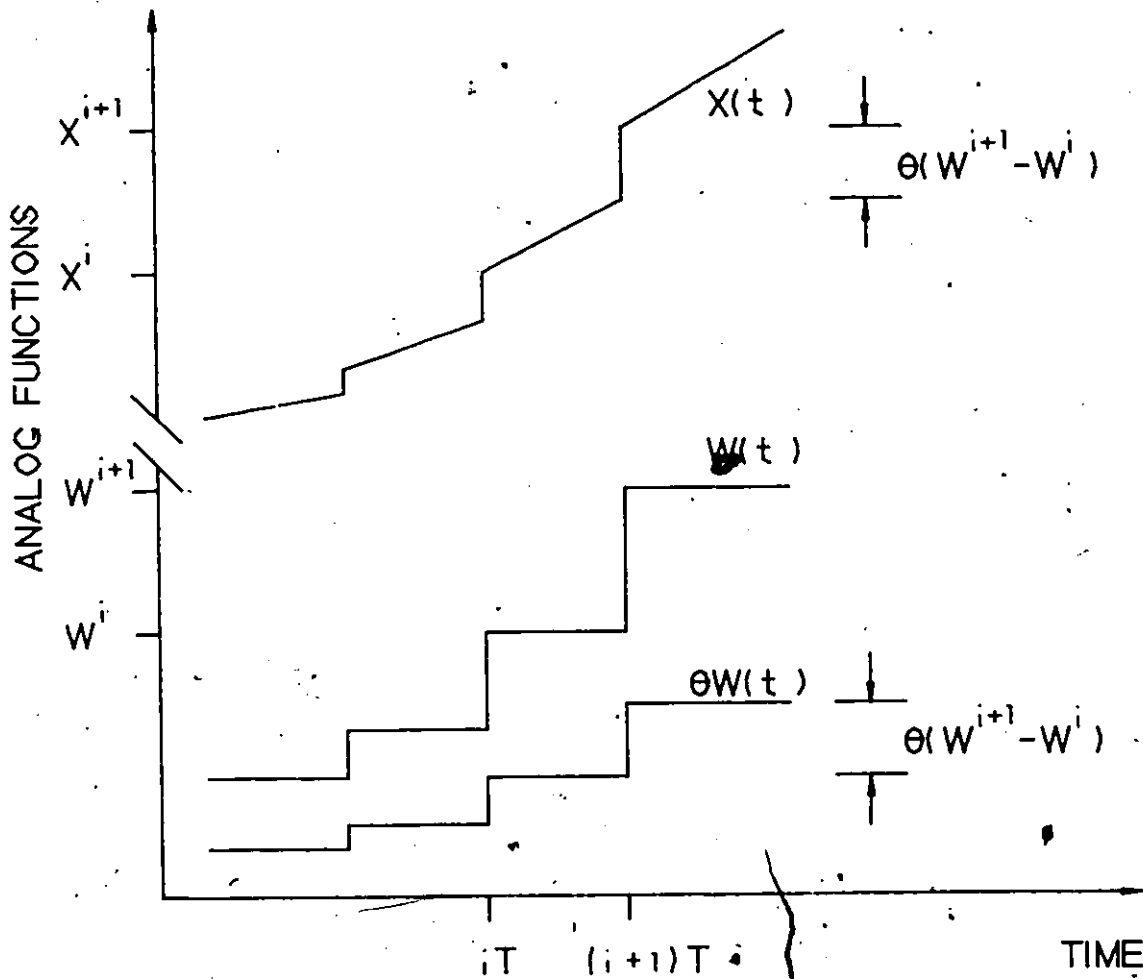


Figure 8 : Analog time functions in hybrid loop

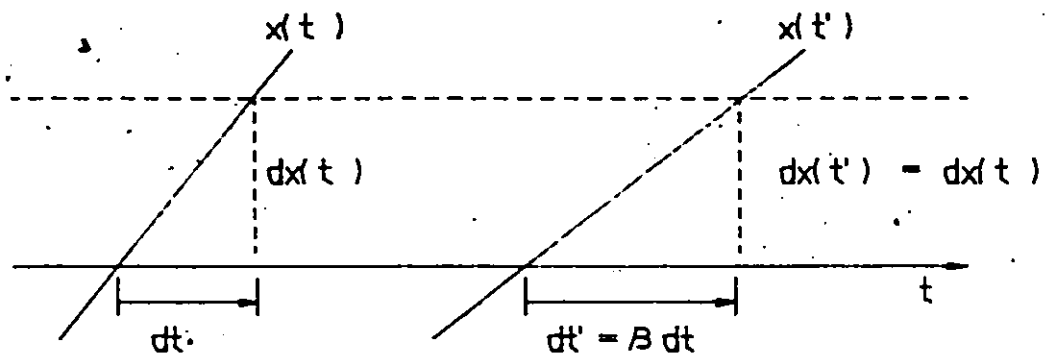


Figure 9 : Real-time to model-time conversion diagram

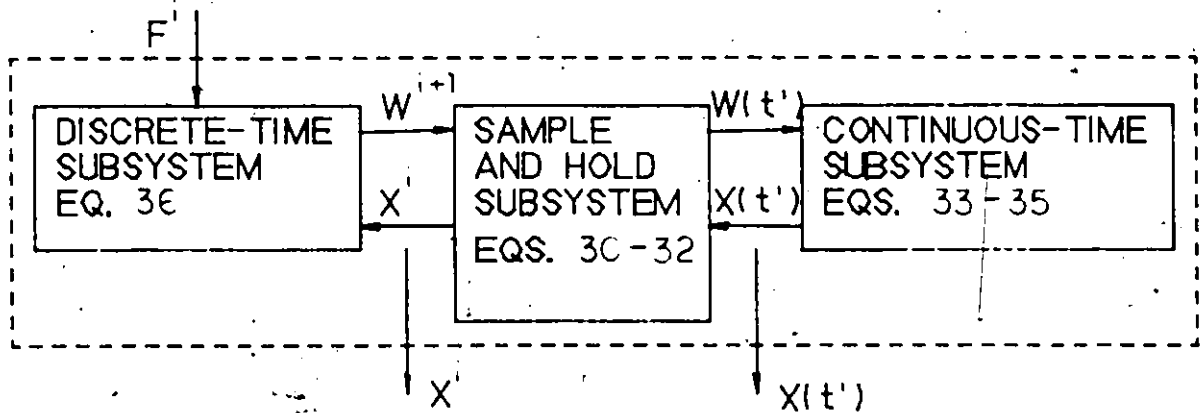


Figure 10 : Sampled-data mathematical model

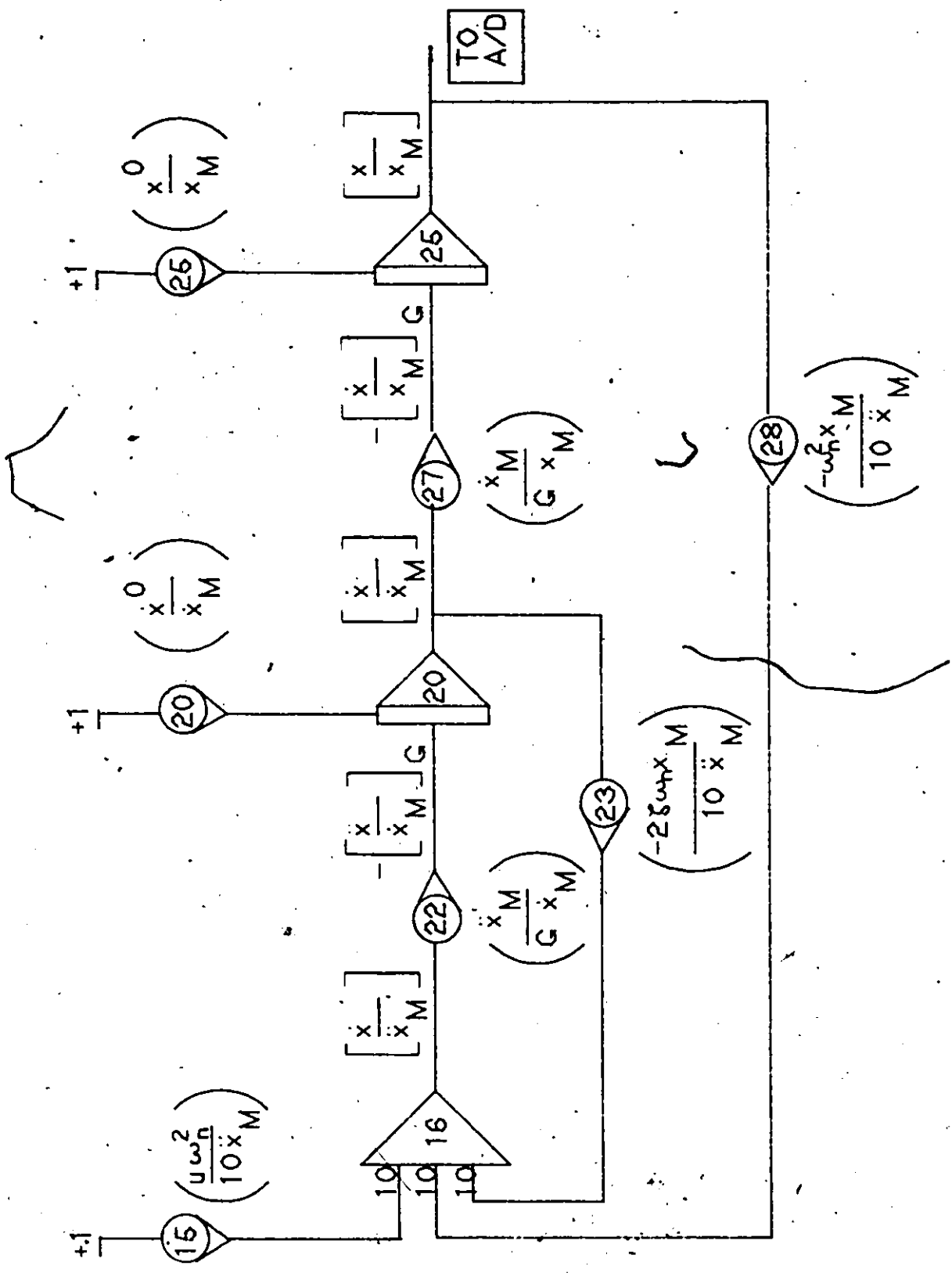


Figure 11 : Analog computer circuit diagram

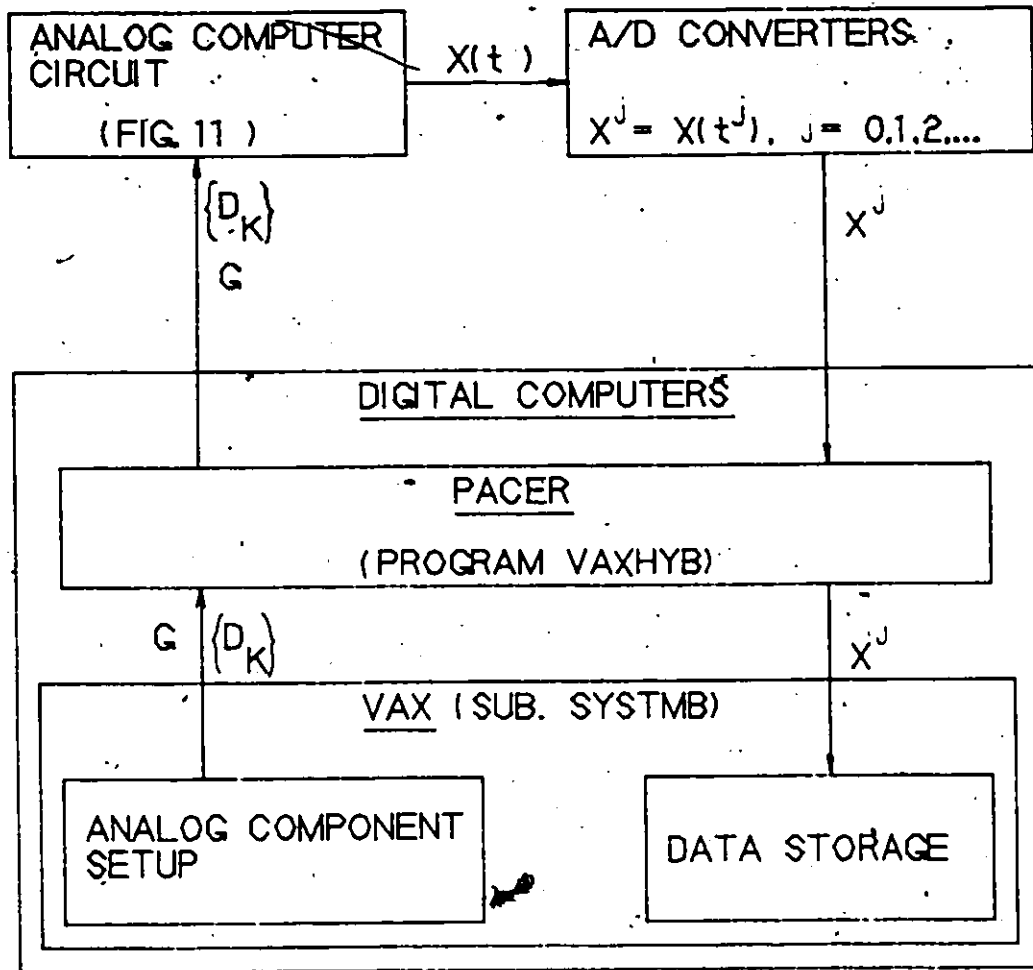


Figure 12 : System B information flow diagram

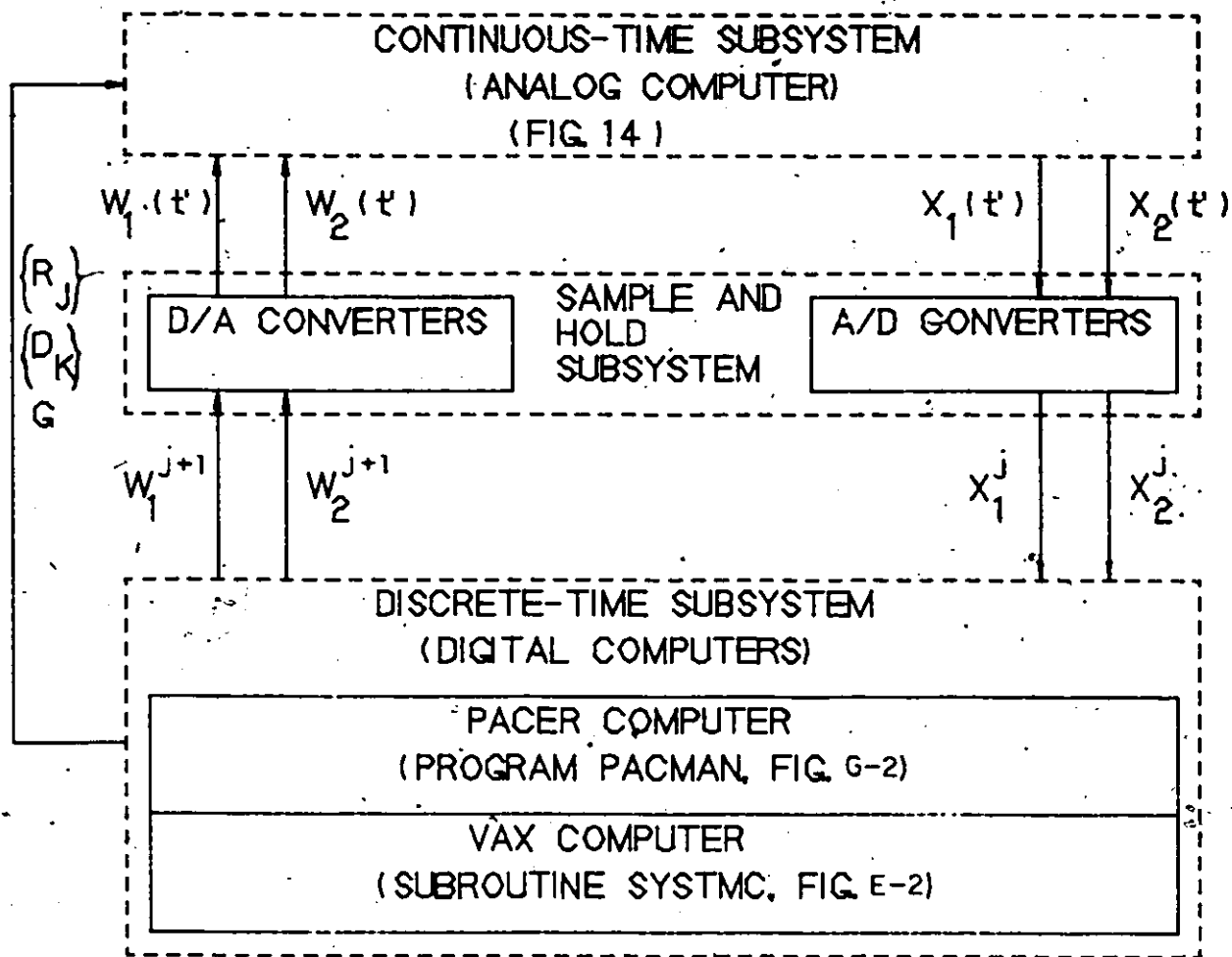


Figure 13 : System C information flow diagram

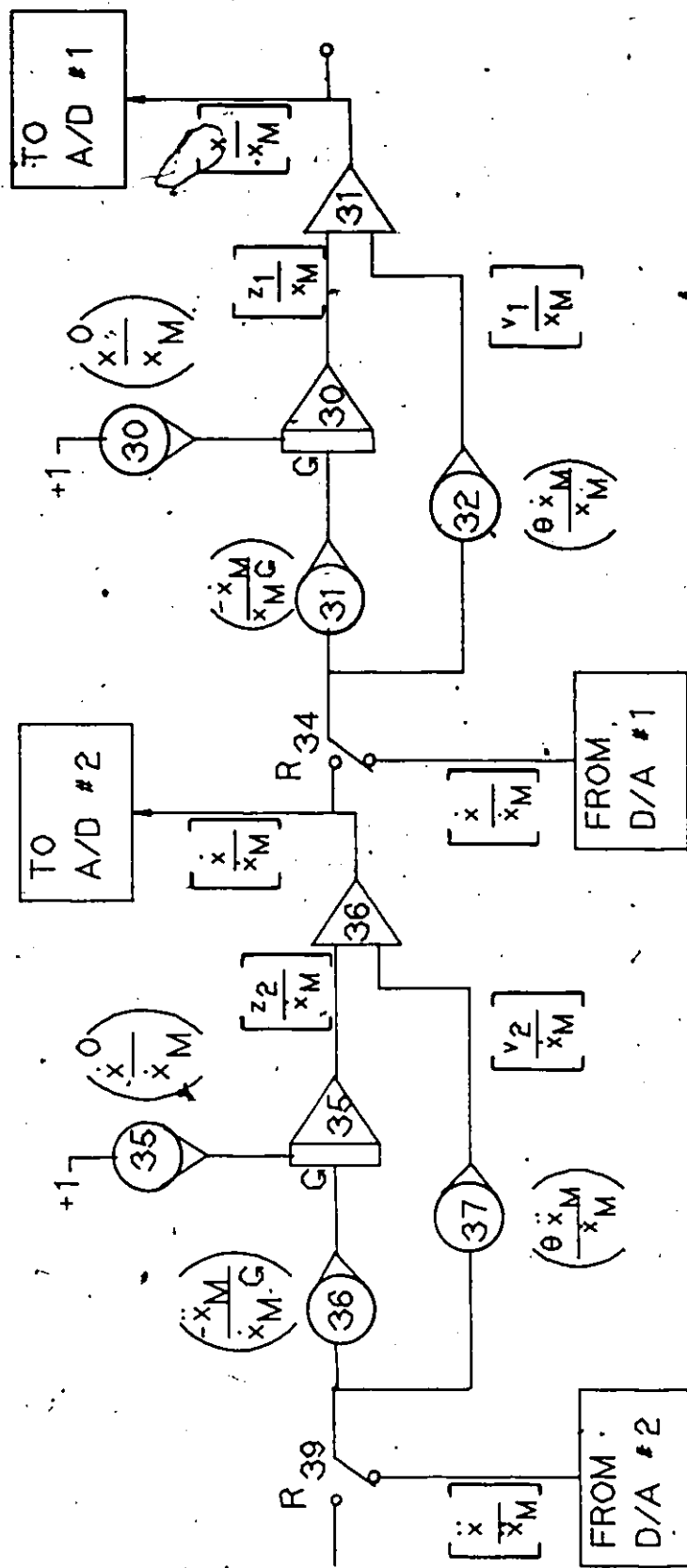


Figure 14 : Continuous-time subsystem circuit diagram of System C

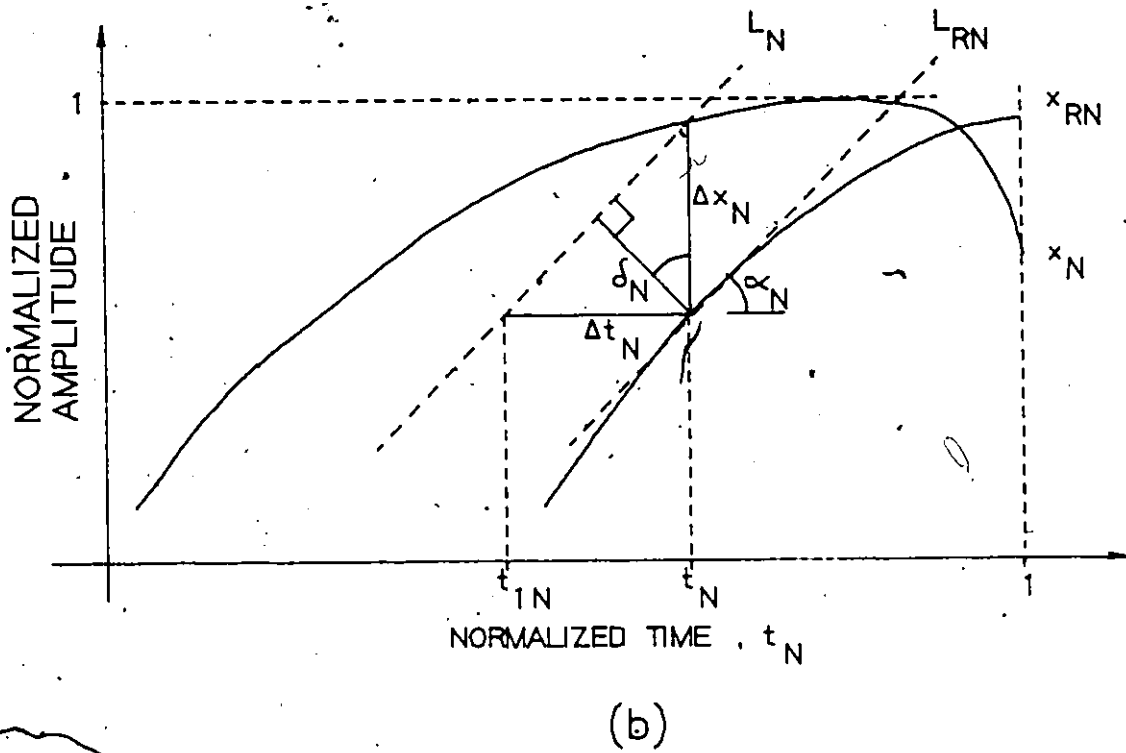
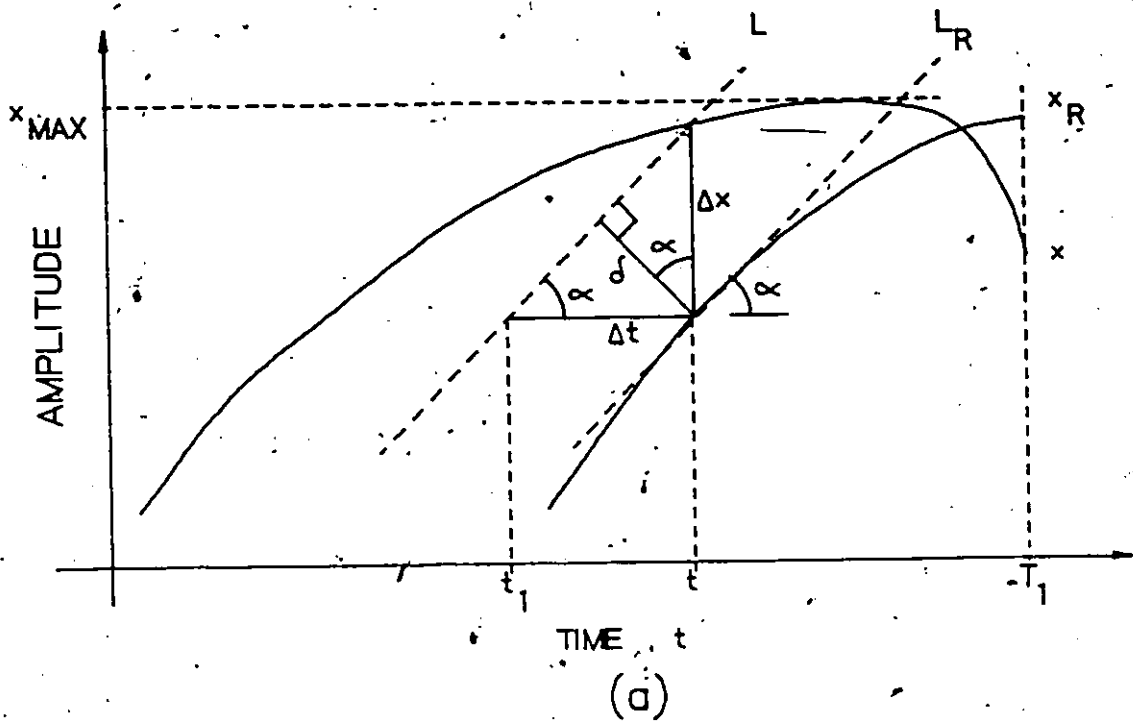


Figure 15 : Normal distance approximation :  
 (a) nominal, (b) normalized

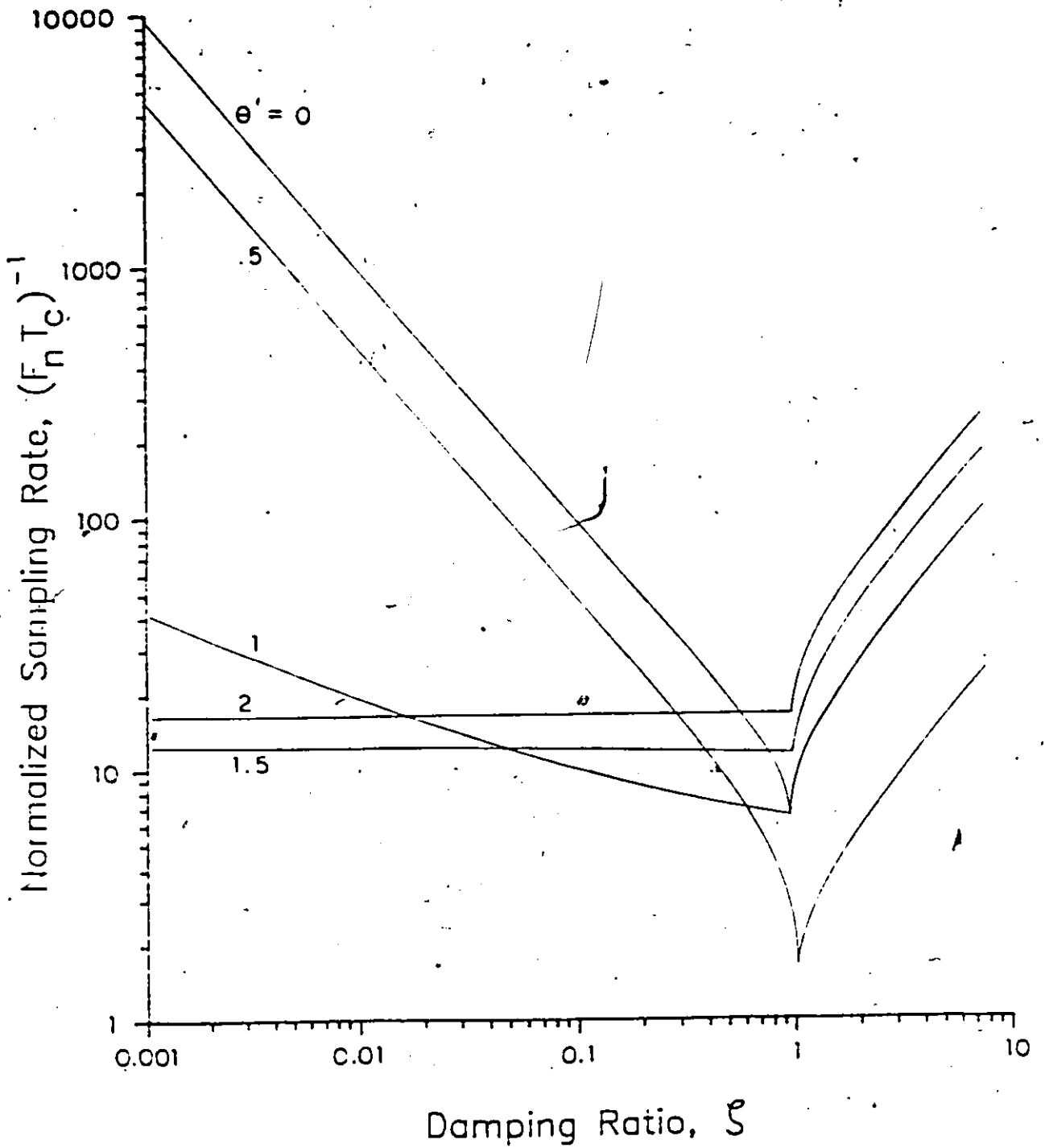


Figure 16 : DTESD model (System D) stability boundaries for  $\theta' = 0, .5, 1, 1.5, 2$

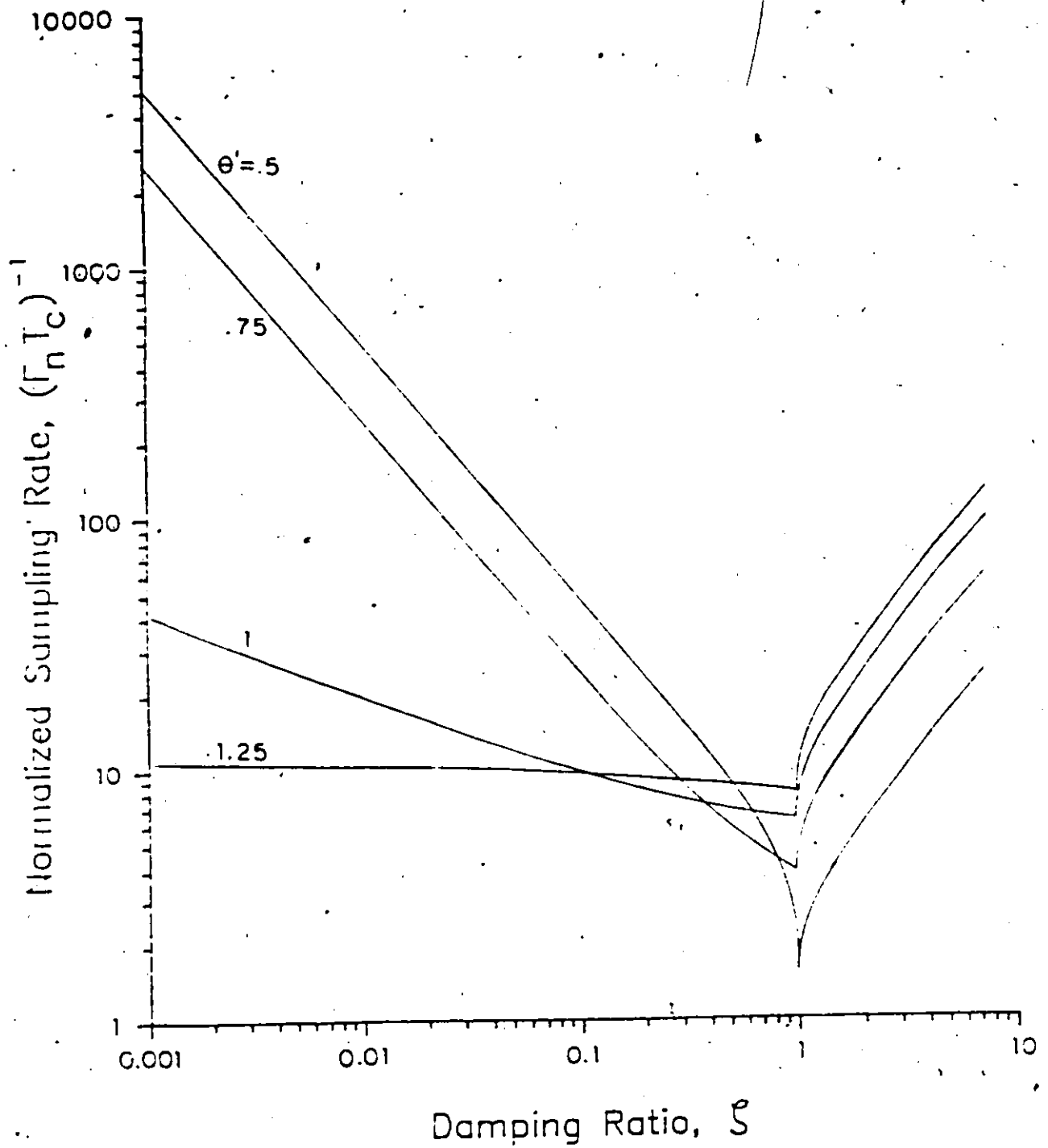


Figure 17 : DTESD model (System D) stability boundaries for  $\theta' = .5, .75, 1, 1.25$

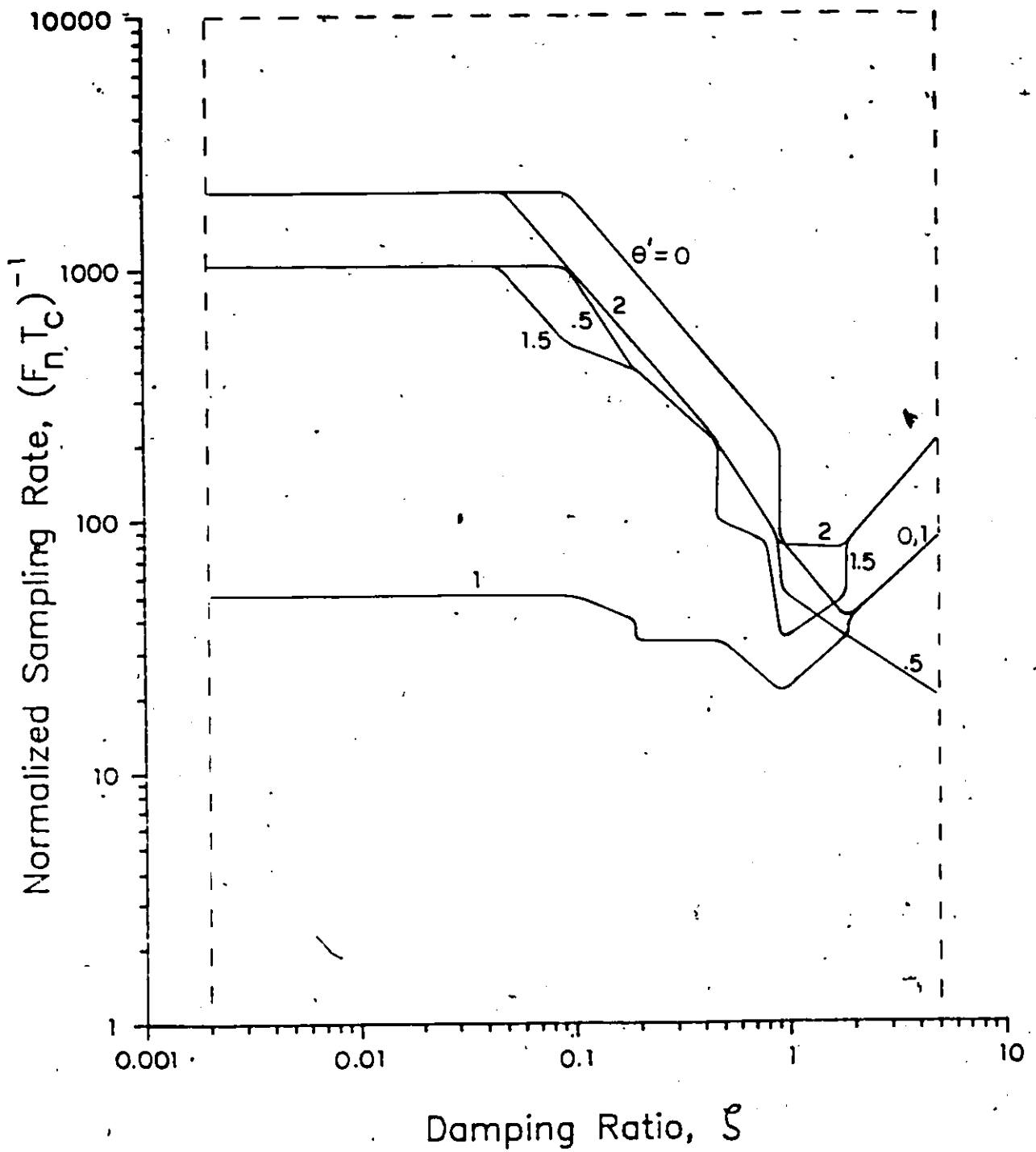


Figure 18 : System D accuracy boundaries ( $\epsilon_N = .0075$ )  
for  $\theta' = 0, .5, 1, 1.5, 2$

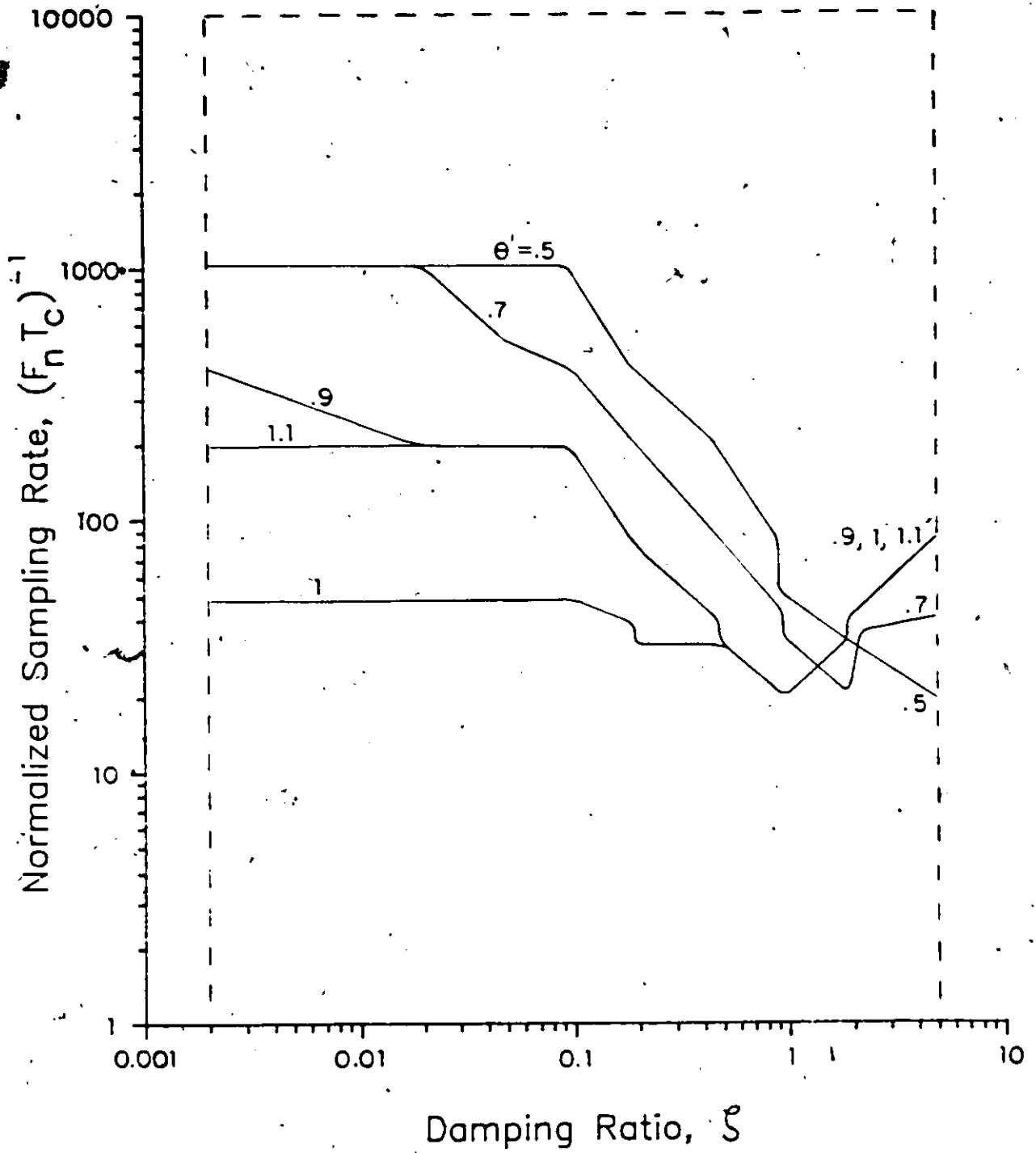


Figure 19 : System D accuracy boundaries ( $\epsilon_N = .0075$ ) for  $\theta' = .5, .7, .9, 1, 1.1$

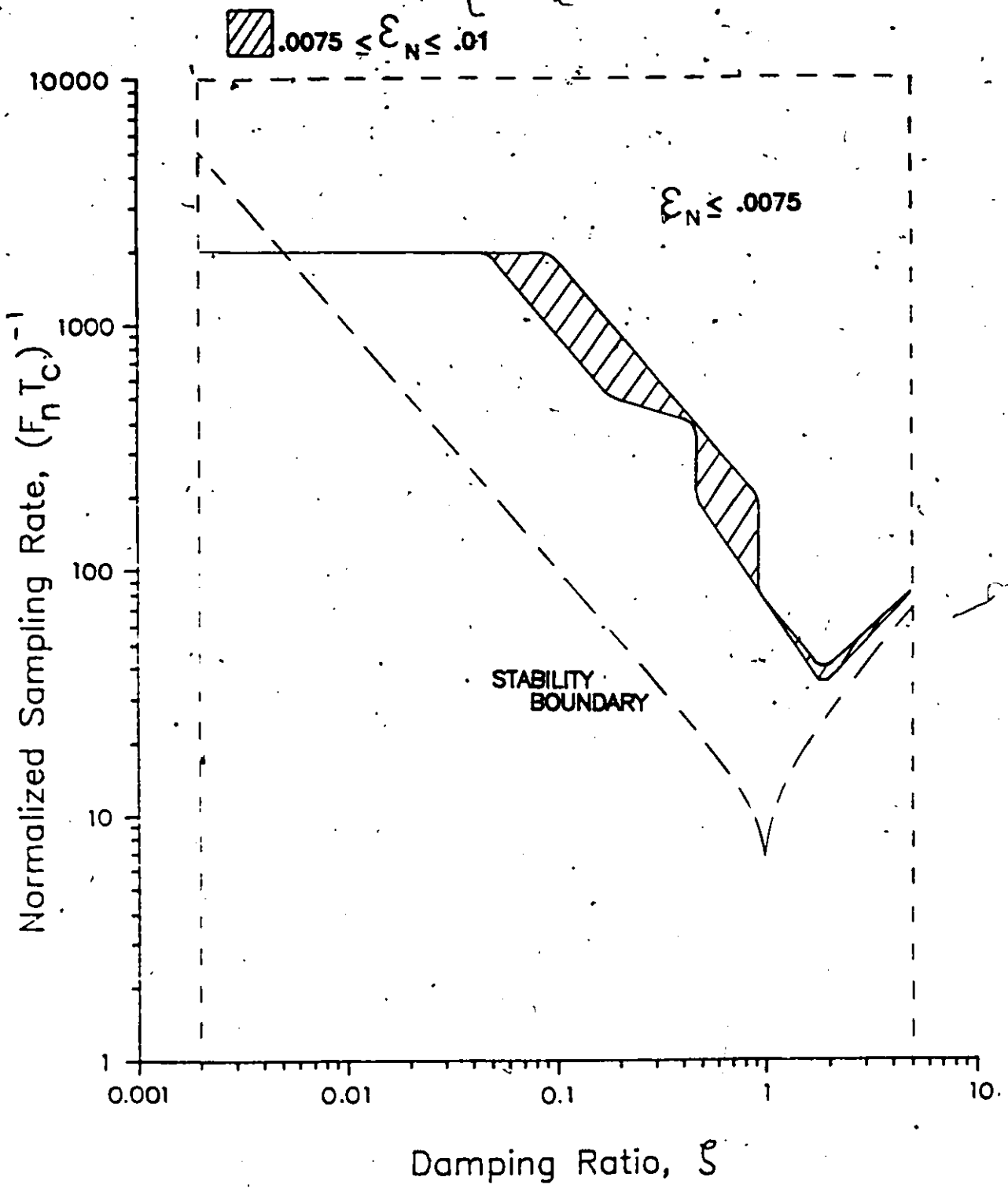


Figure 20 : System D accuracy regions for  $\theta'=0$

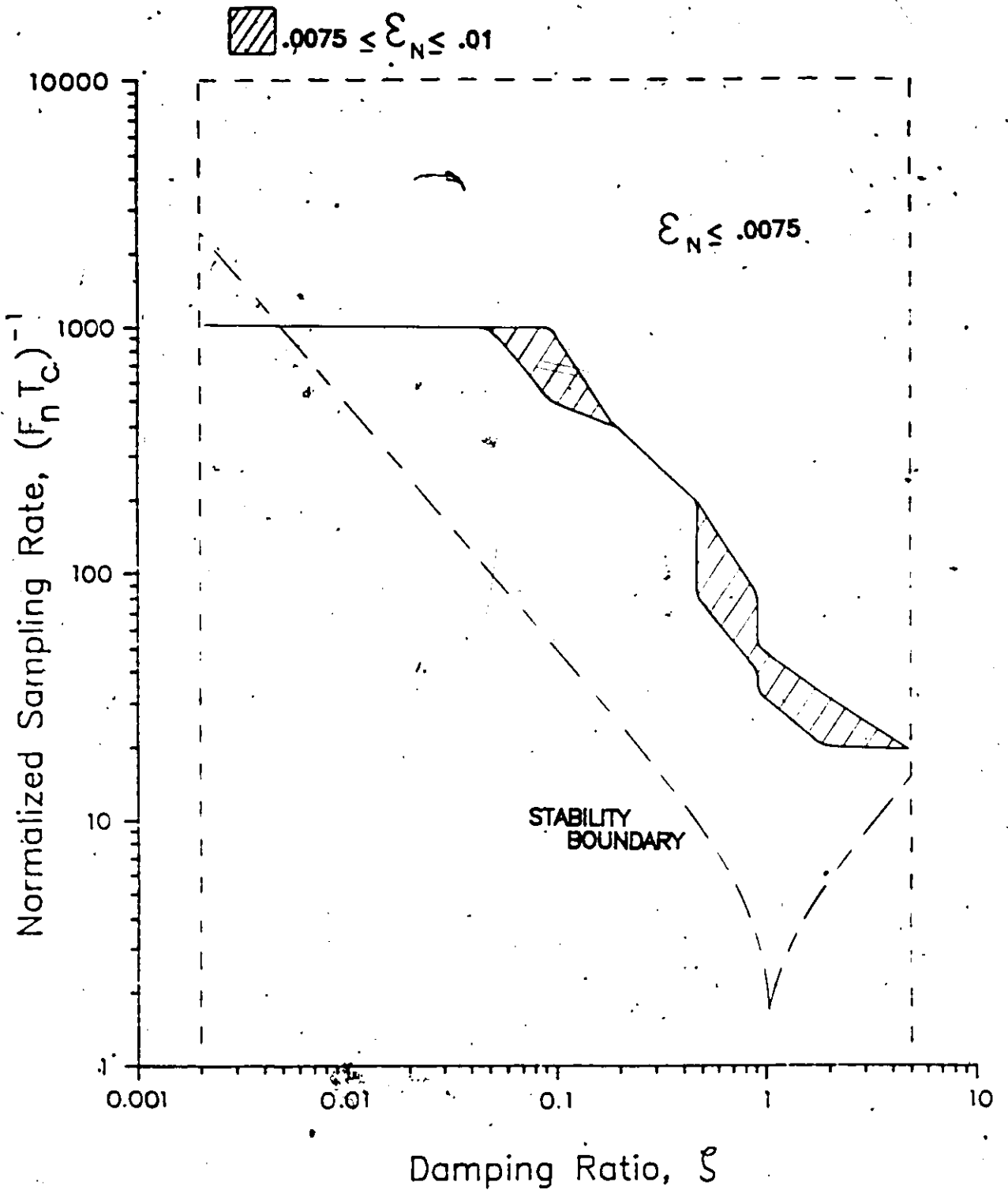


Figure 21 : System D accuracy regions for  $\theta'=.5$

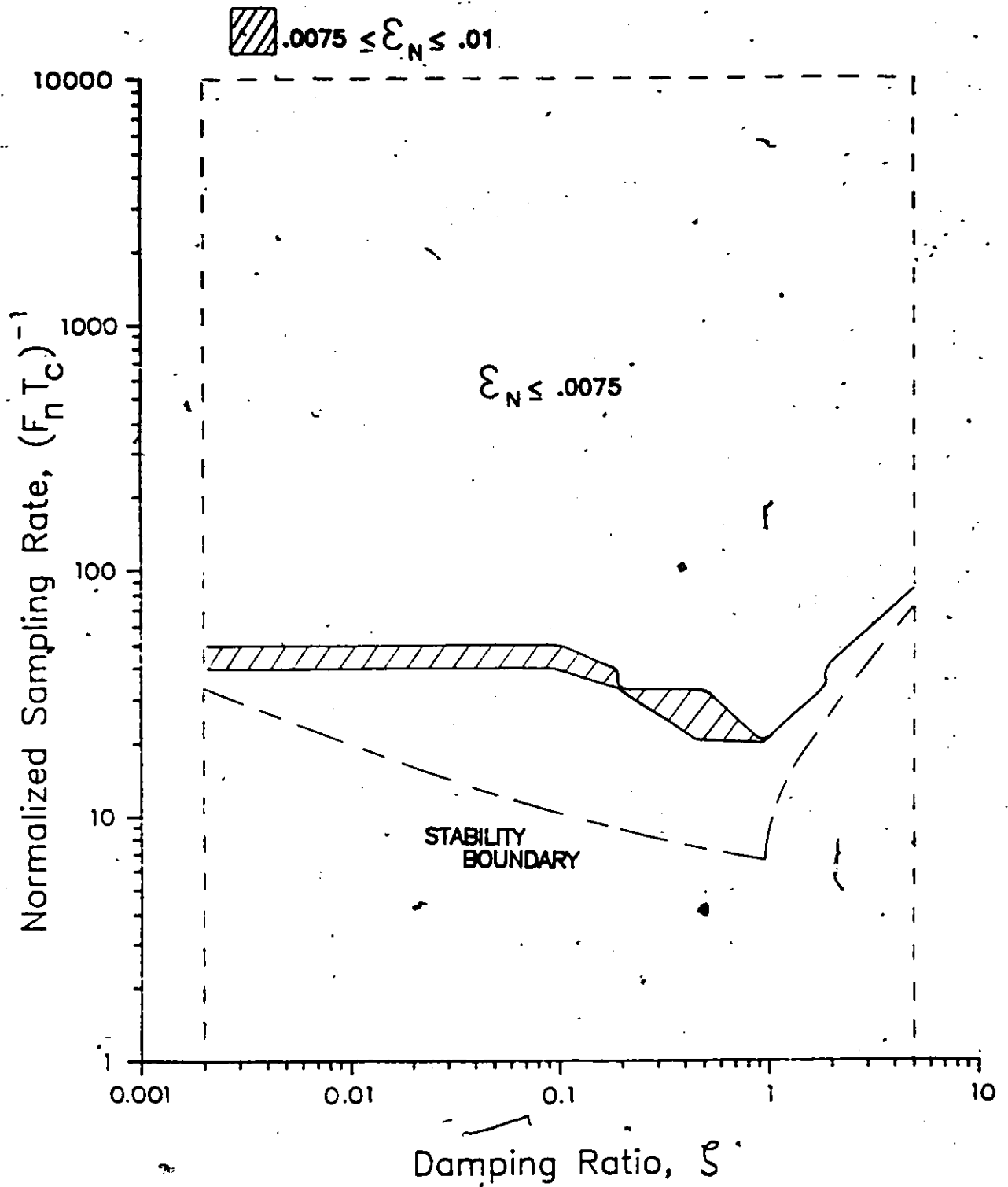


Figure 22 : System D accuracy regions for  $\theta'=1$

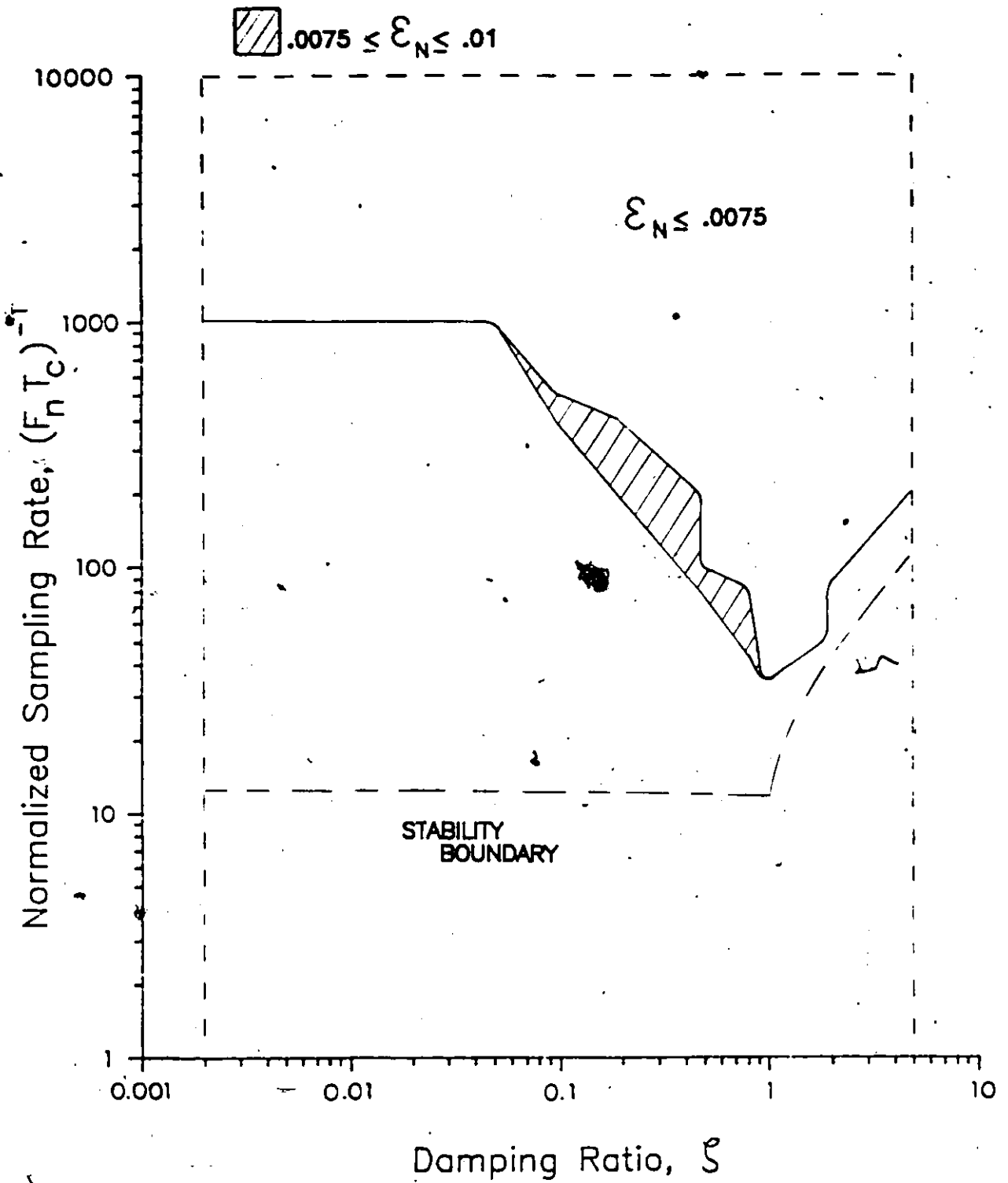


Figure 23 : System D accuracy regions for  $\theta' = 1.5$

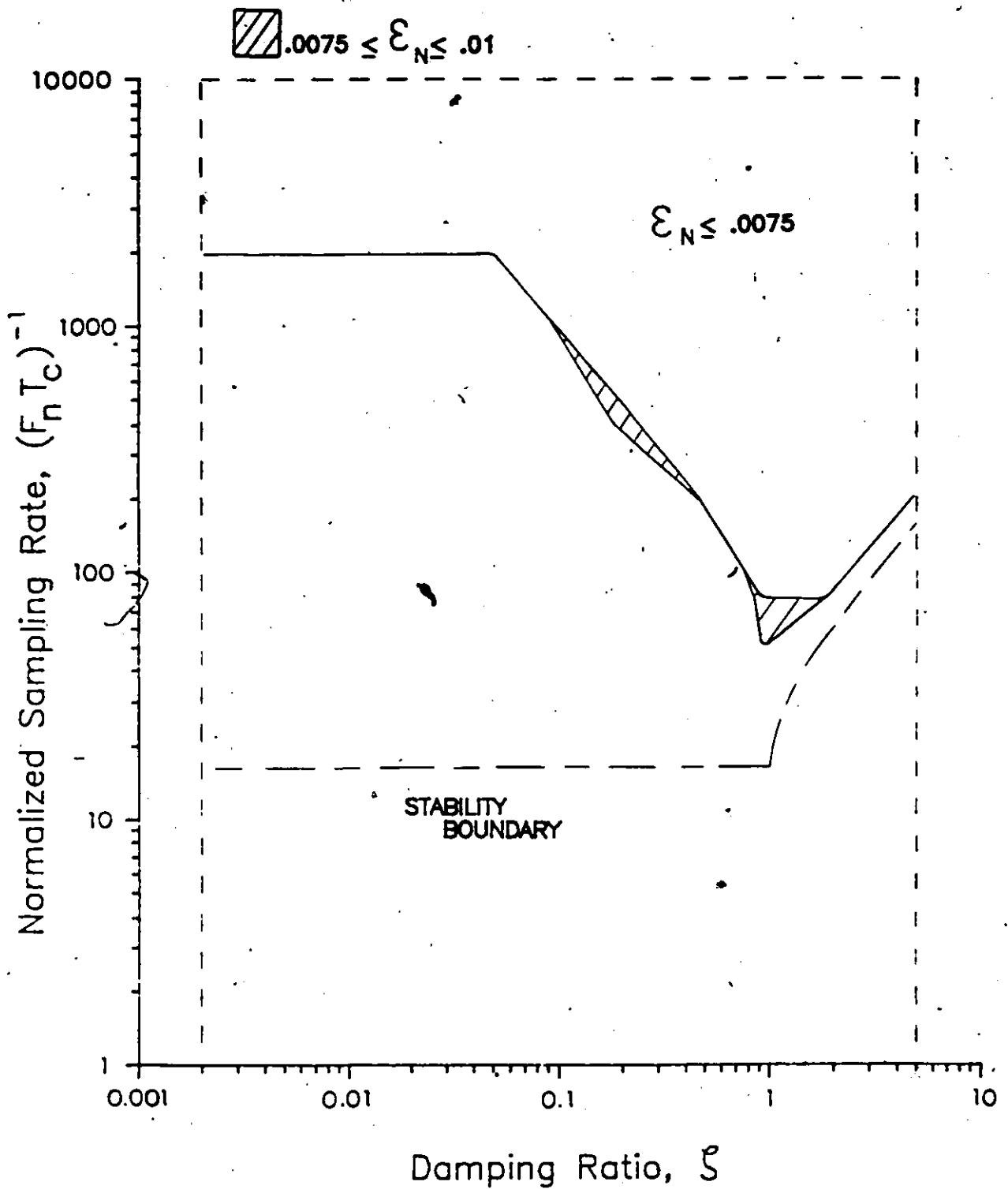


Figure 24 : System D accuracy regions for  $\theta' = 2$

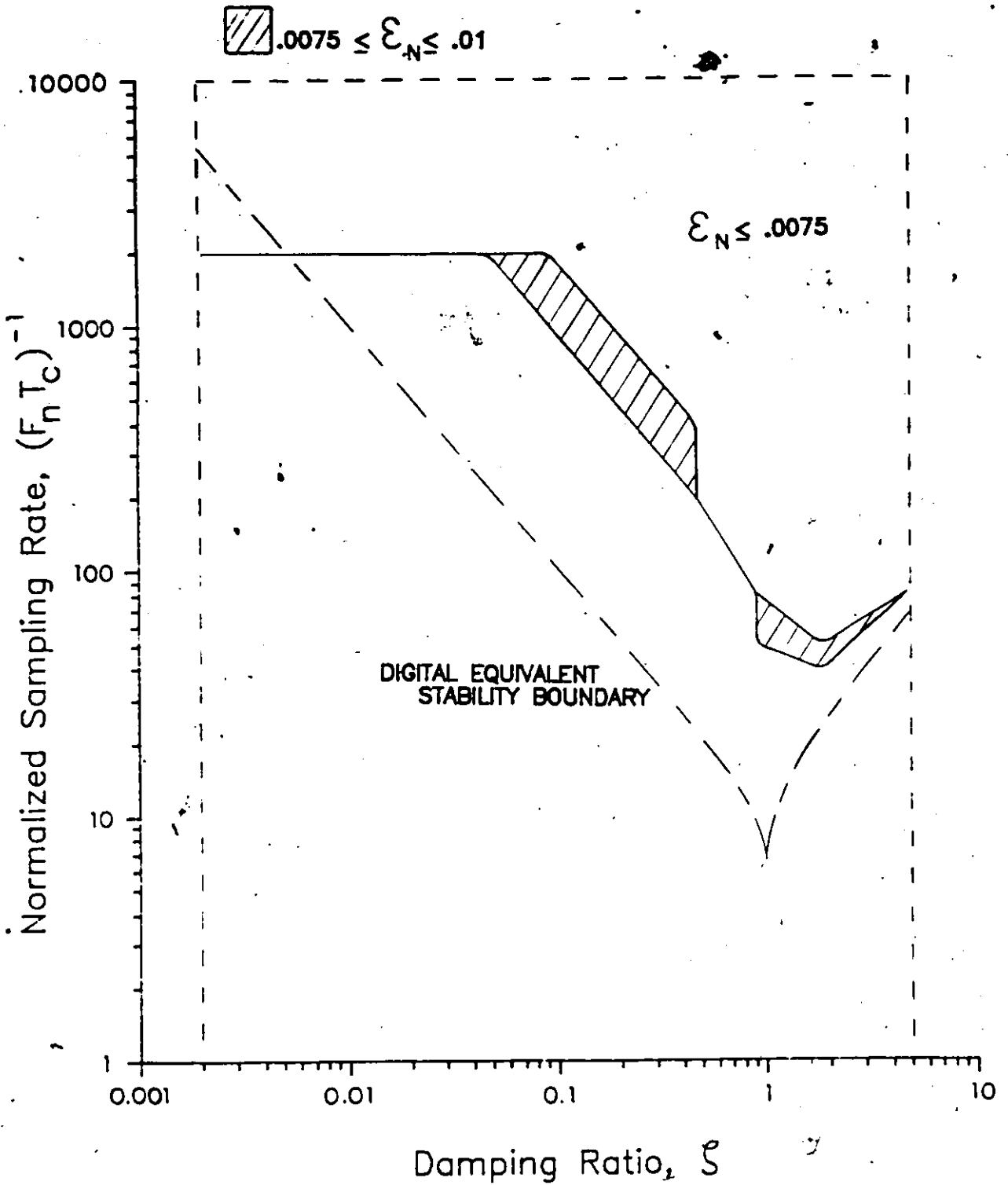


Figure 25 : System G accuracy regions for  $\theta' = 0$

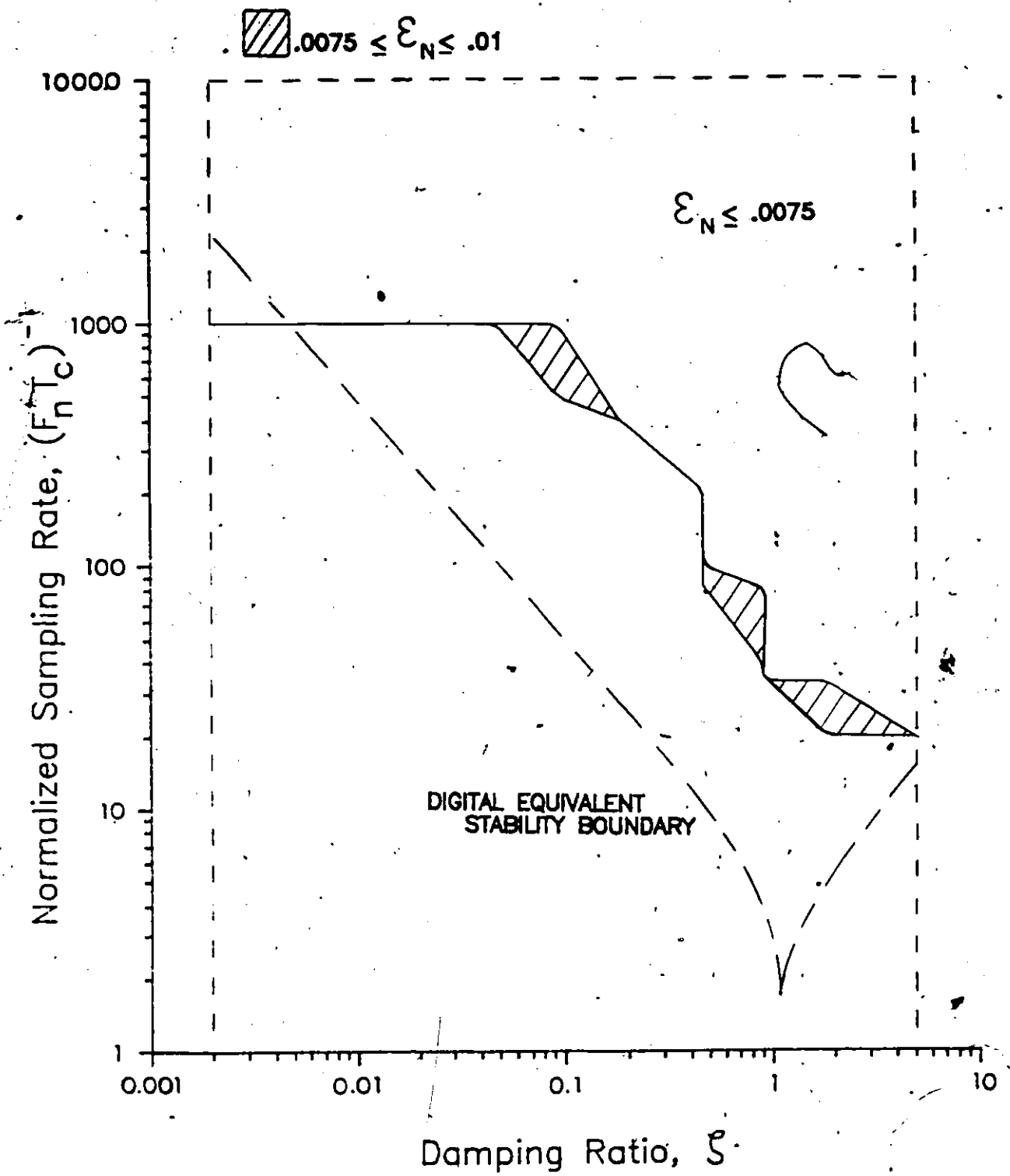


Figure 26 : System C accuracy regions for  $\theta'=.5$

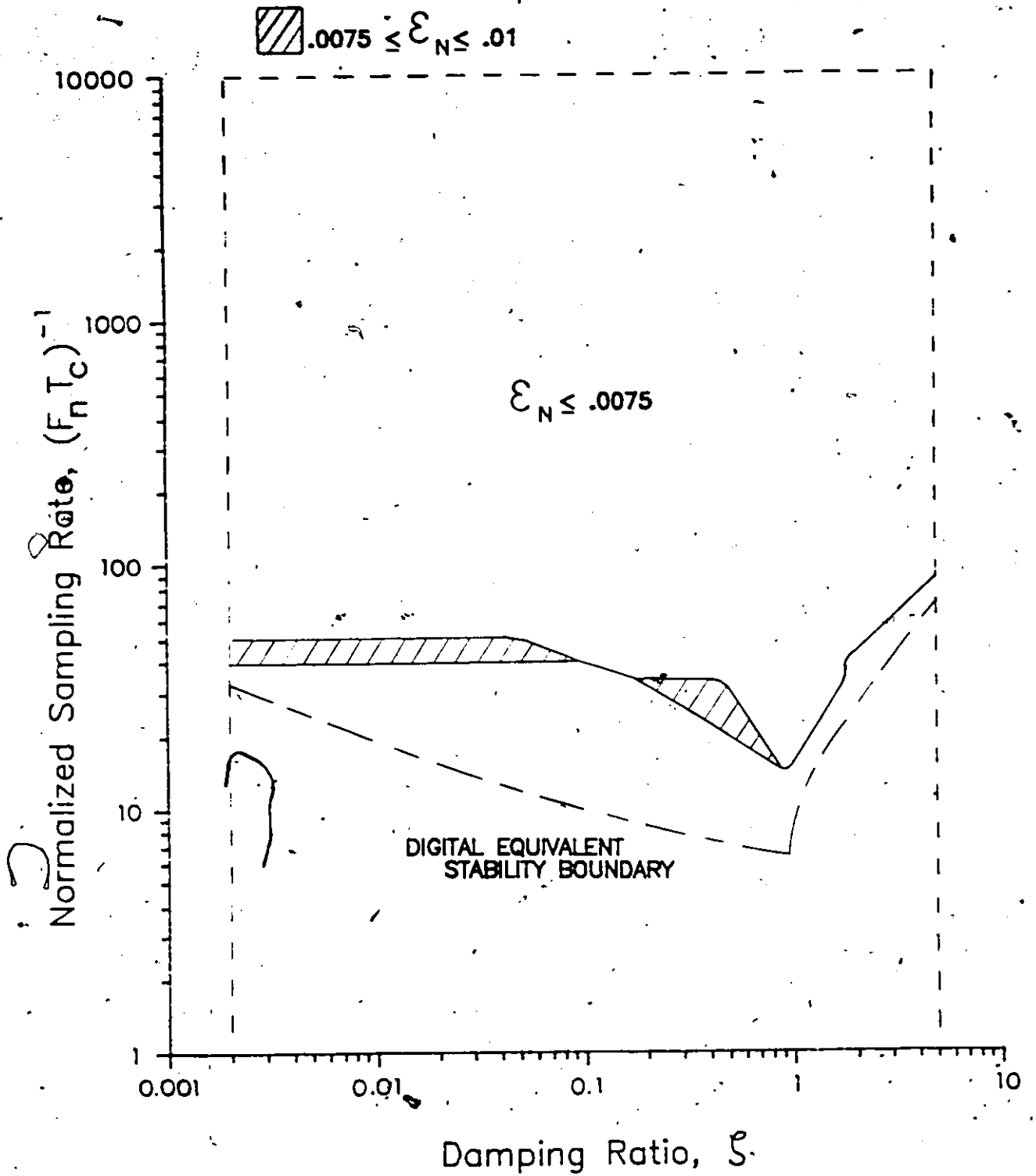


Figure 27.: System C accuracy regions for  $\theta' = 1$

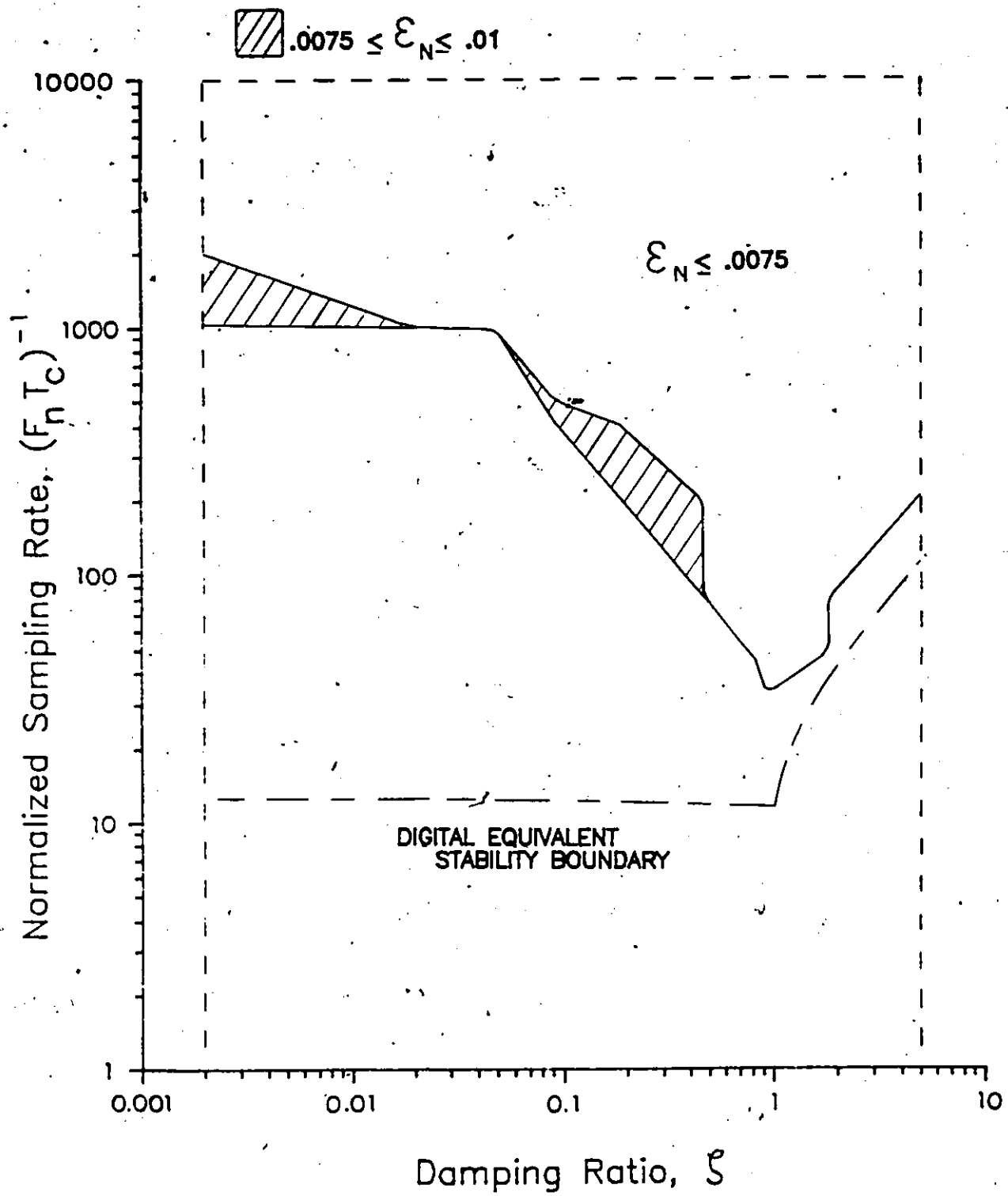


Figure 28 : System C accuracy regions for  $\theta'=1.5$

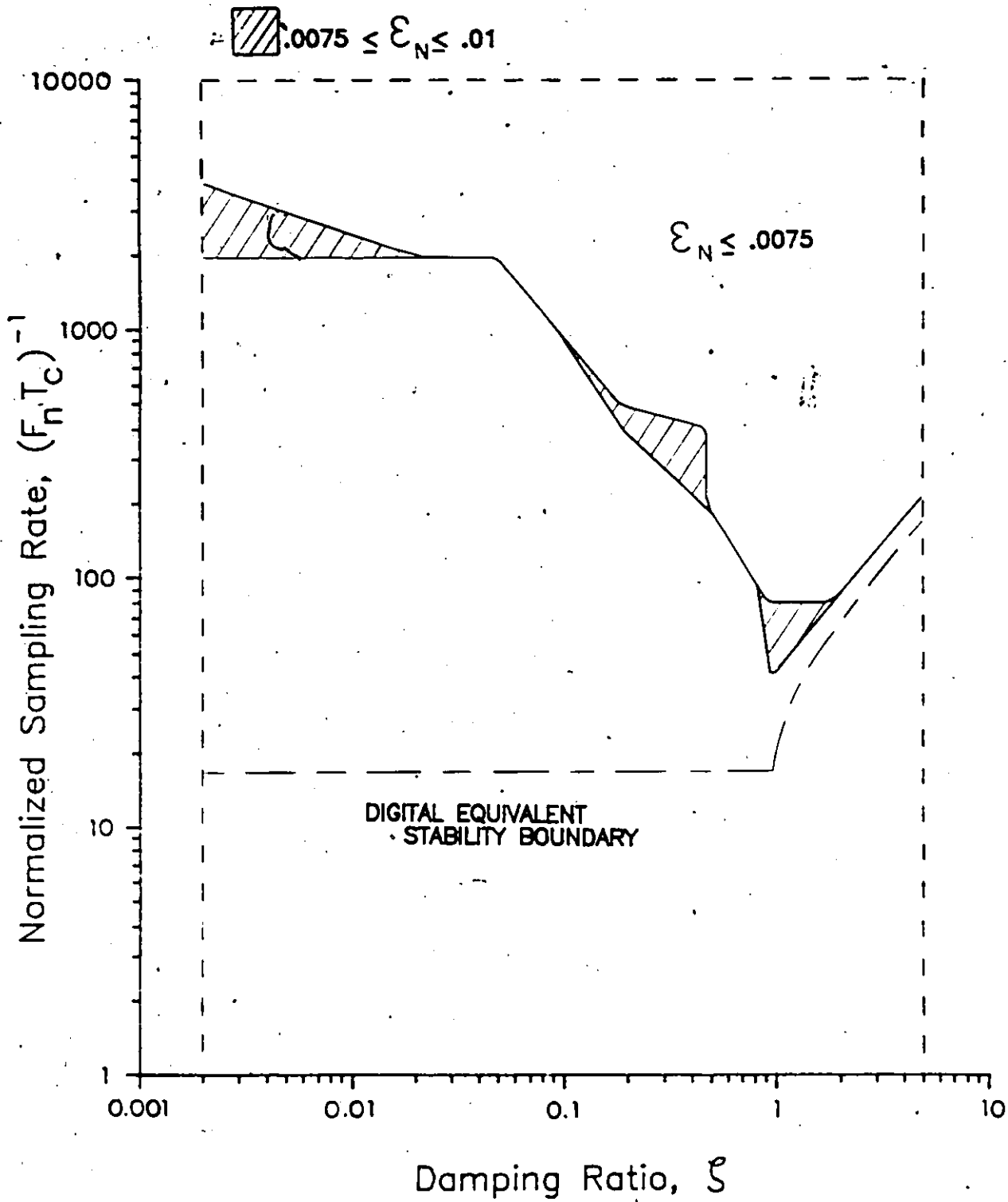


Figure 29 : System C accuracy regions for  $\theta' = 2$

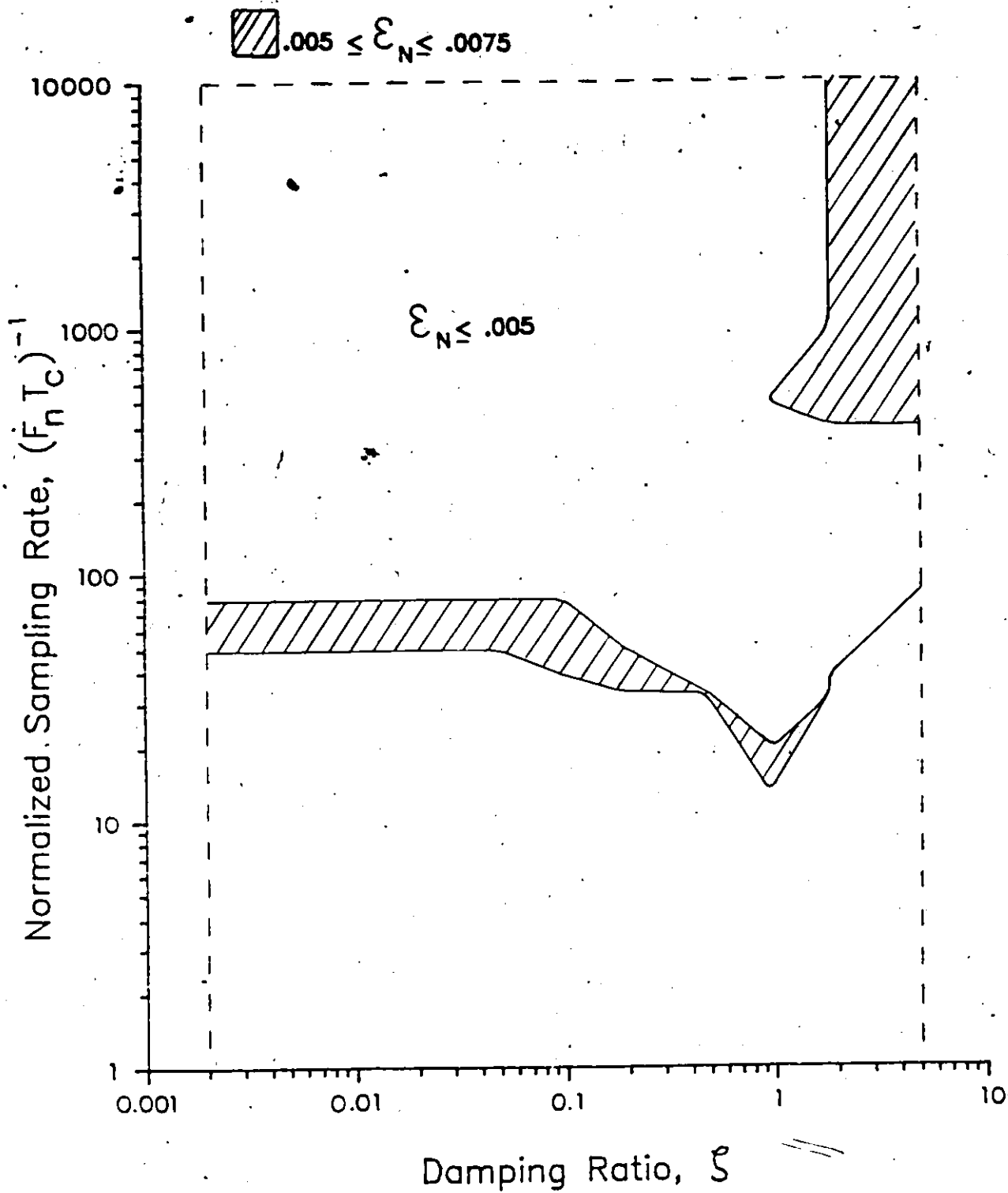


Figure 30 : System C accuracy regions for  $\theta'=1$  and lower acceptable error values

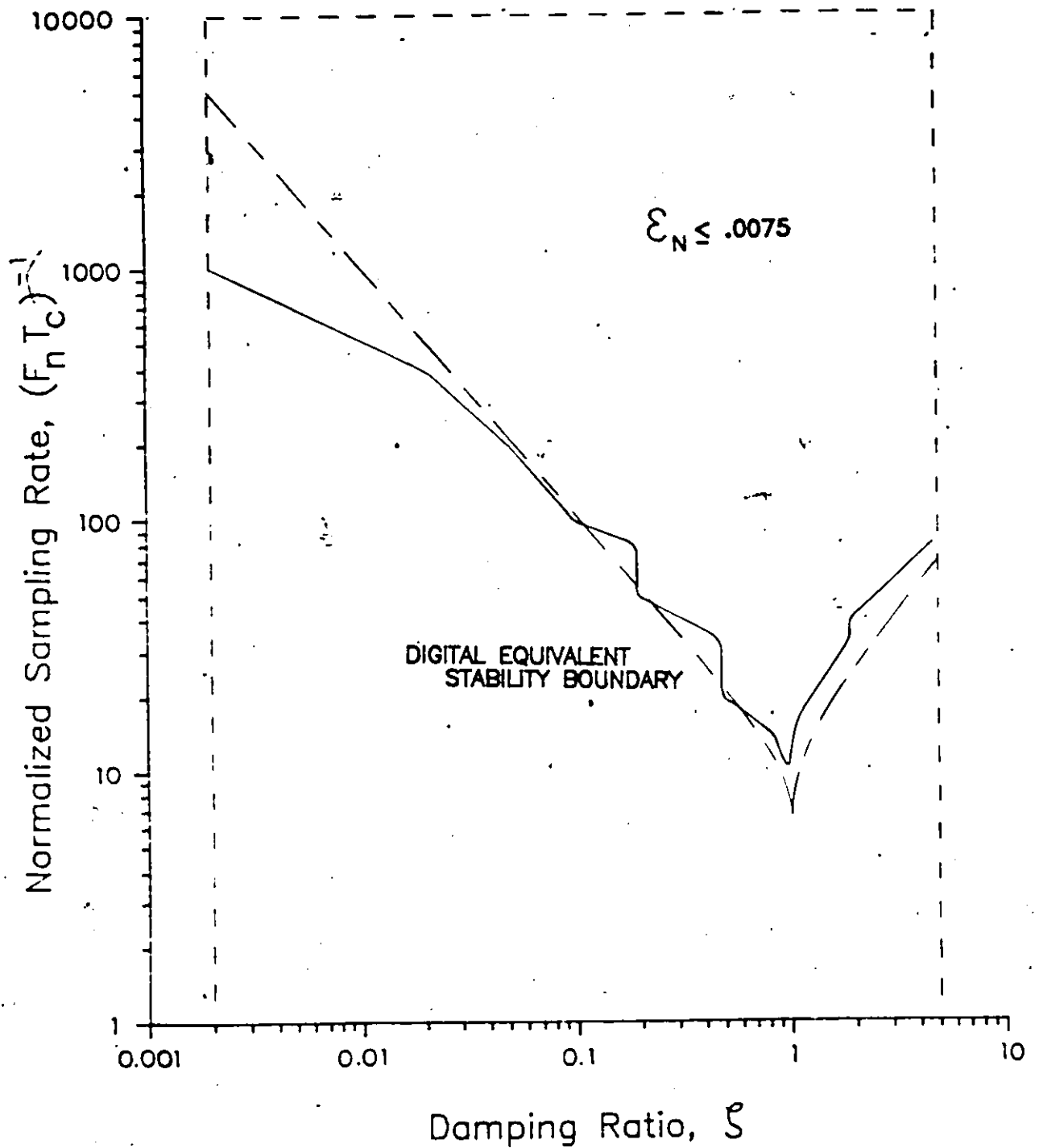


Figure 31 : Equivalence regions between Systems C and D for  $\theta^1=0$

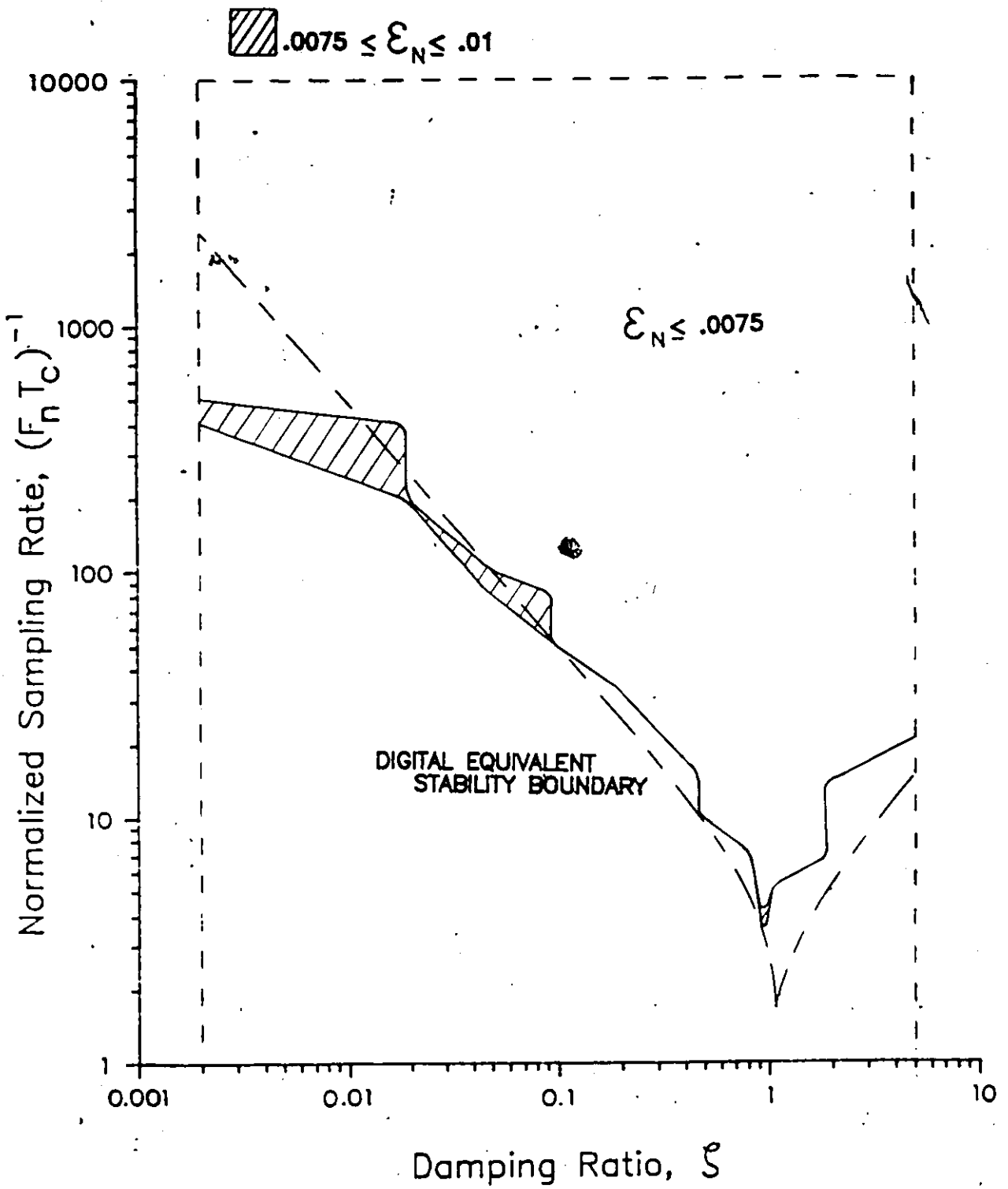


Figure 32 : Equivalence regions between Systems C and D for  $\theta = .5$

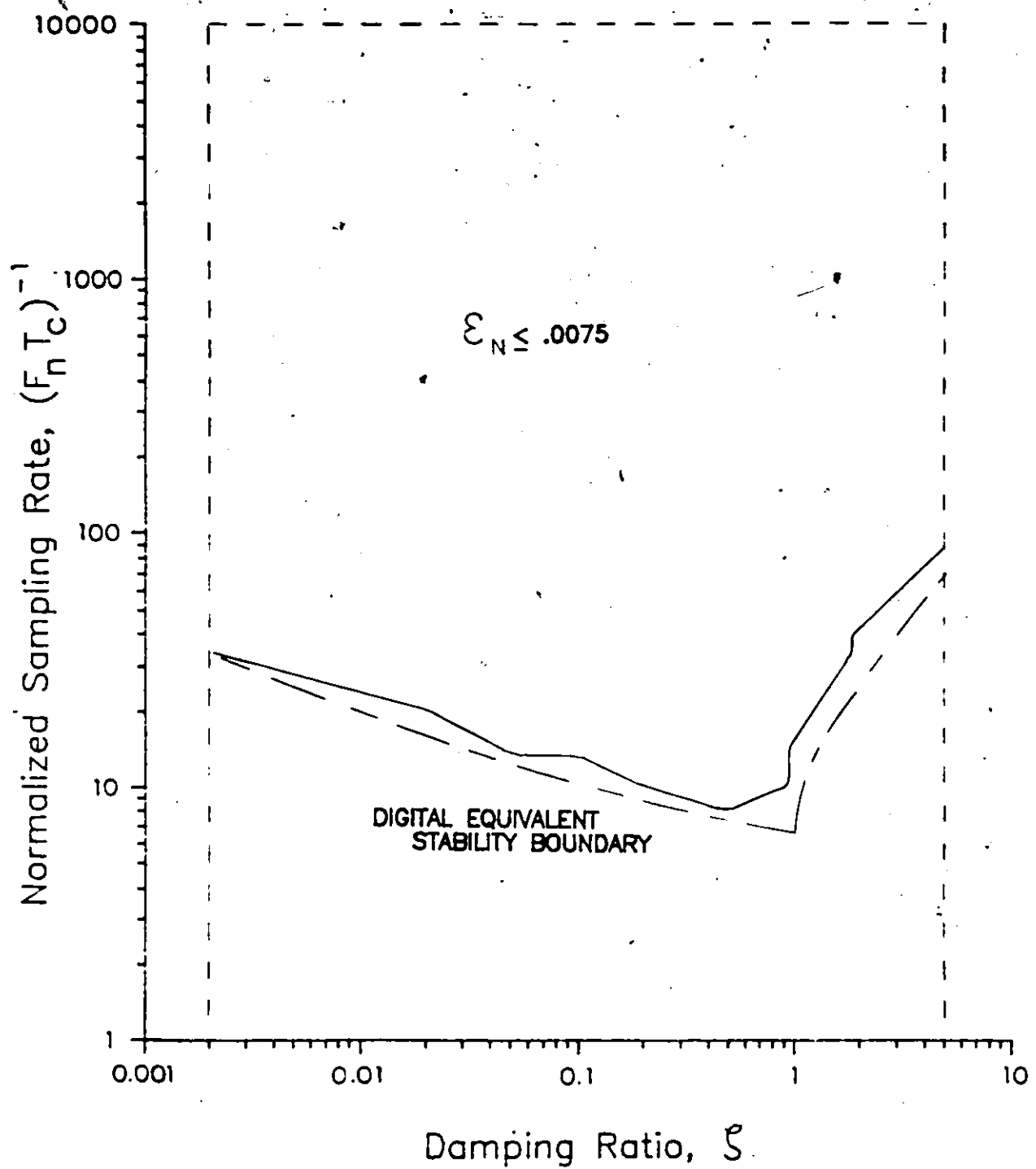


Figure 33 : Equivalence regions between Systems C and D for  $\theta' = 1$

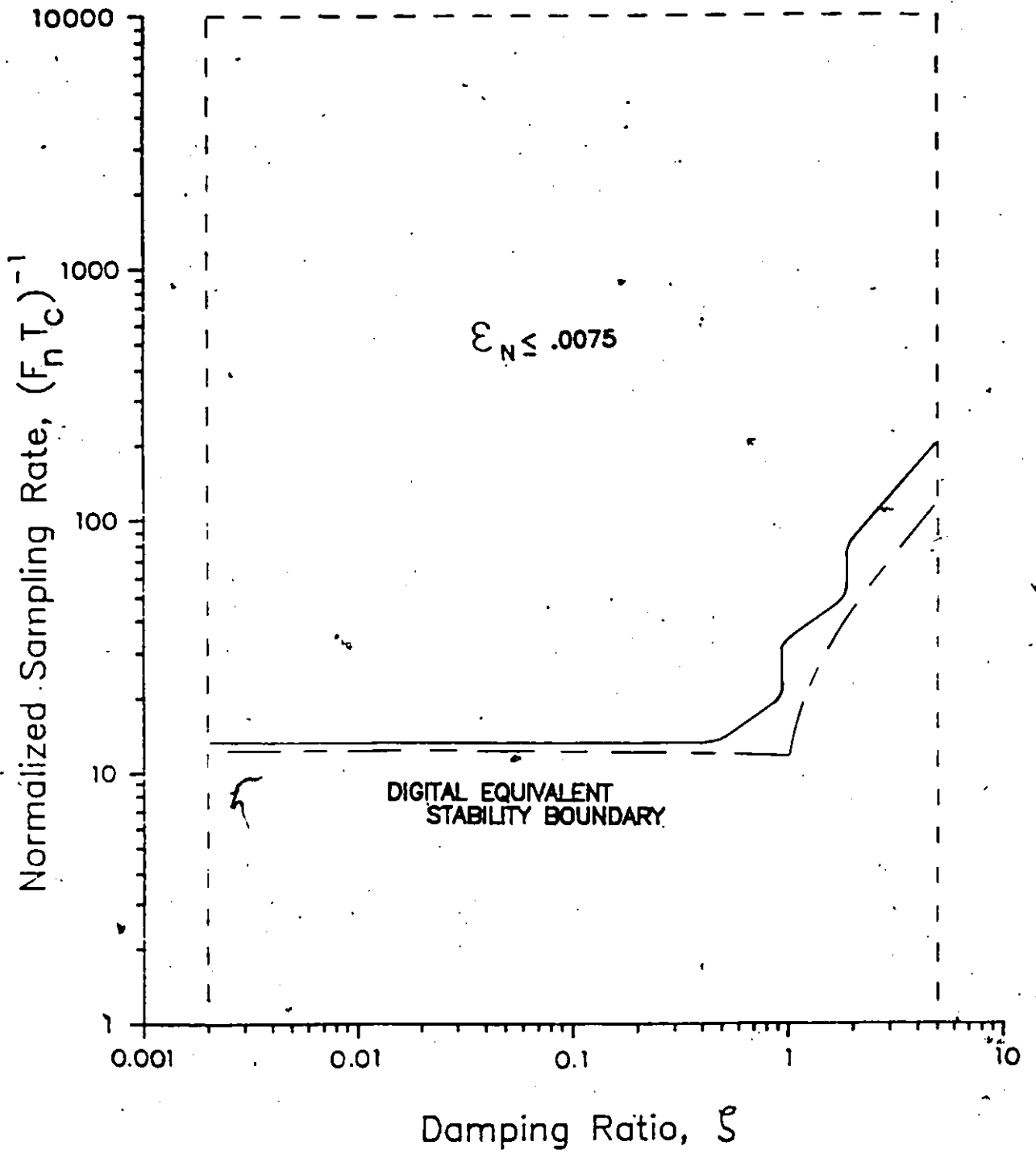


Figure 34 : Equivalence regions between Systems C and D for  $\theta_T=1.5$

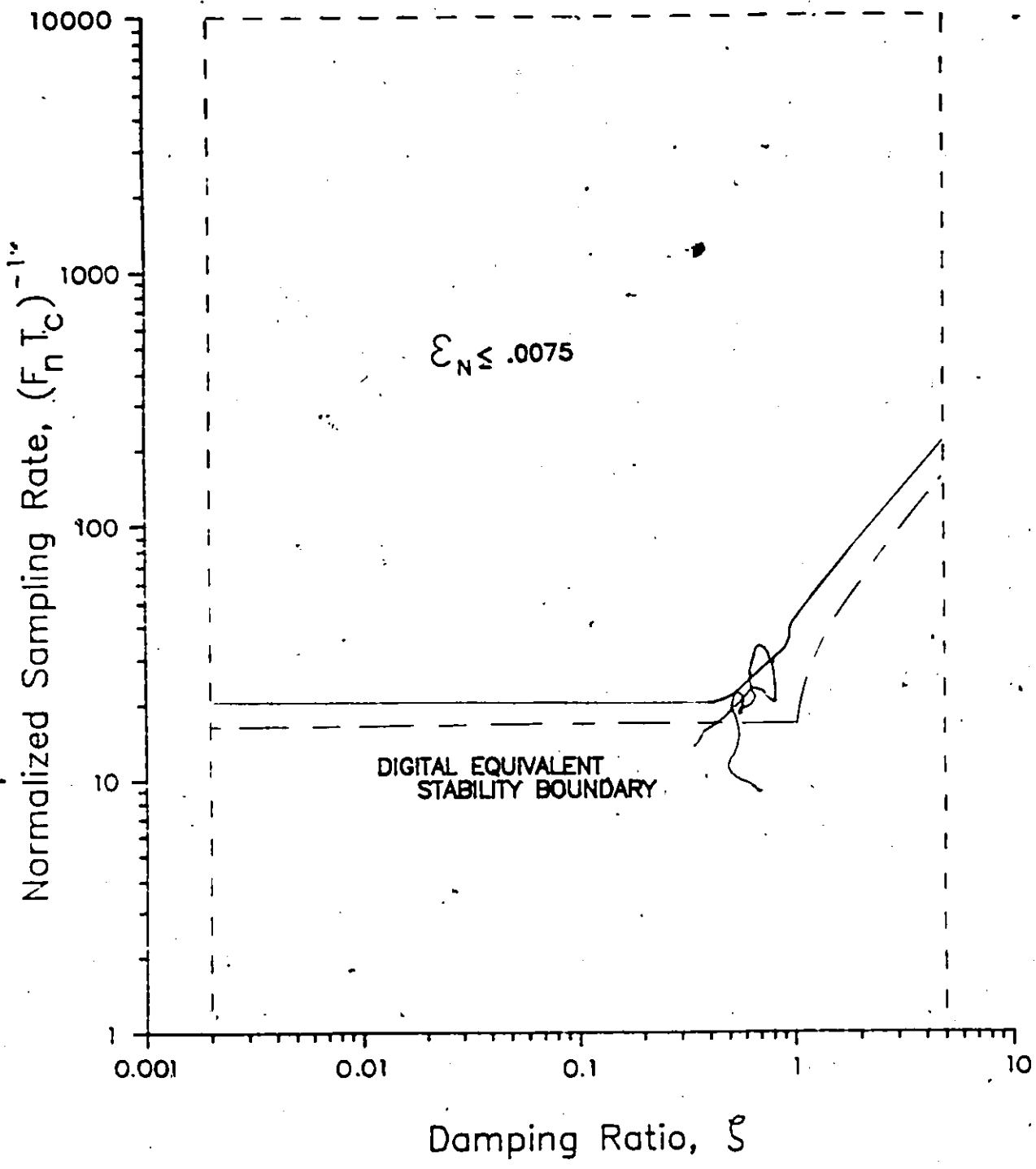


Figure 35 : Equivalence regions between Systems C and D for  $\theta^i=2$

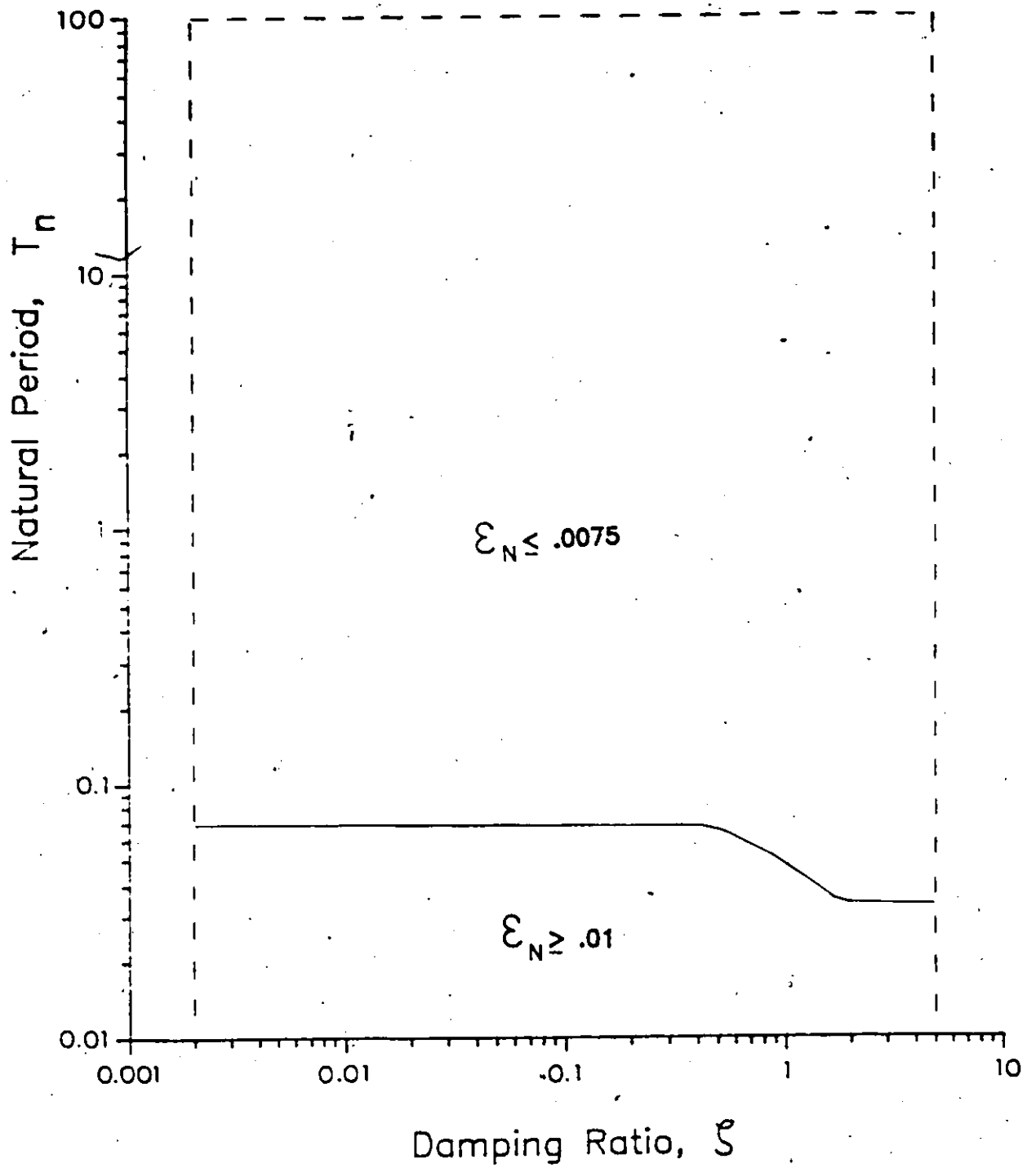


Figure 36 : System B accuracy regions

APPENDIX A

Normalized RMS Error Illustration Curves  
Obtained from SOLDE Analytical Solutions

NOTE : The undamped natural frequency  
of the analytical solution is  
1.0-Hz in all cases.

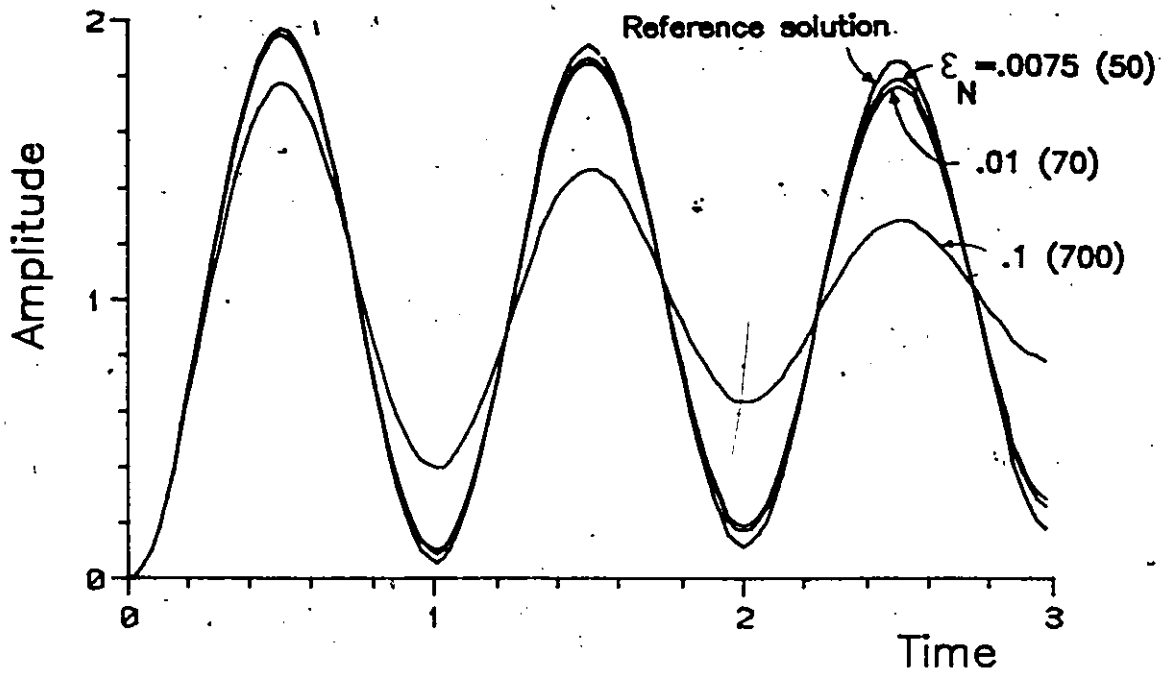


Figure A-1 : Normalized error with damping ratio of .01 for the reference solution (Numbers in brackets are percentage variations in damping ratio)

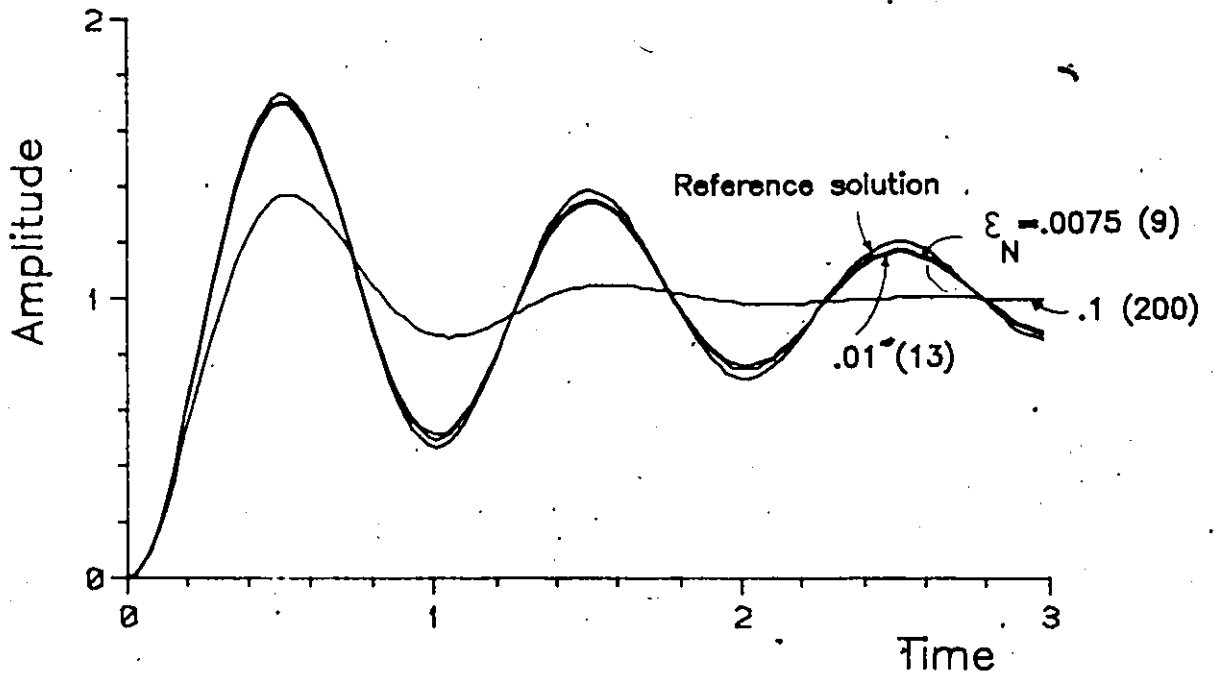


Figure A-2 : Normalized error with damping ratio of .1 for the reference solution (Numbers in brackets are percentage variations in damping ratio)

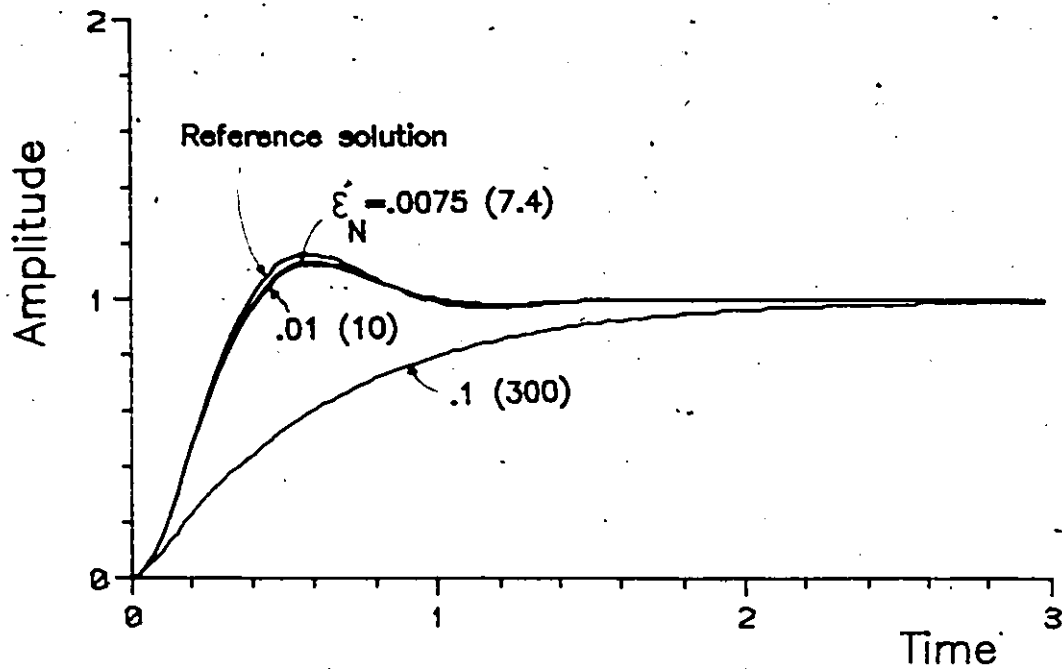


Figure A-3 : Normalized error with damping ratio of .5 for the reference solution (Numbers in brackets are percentage variations in damping ratio)

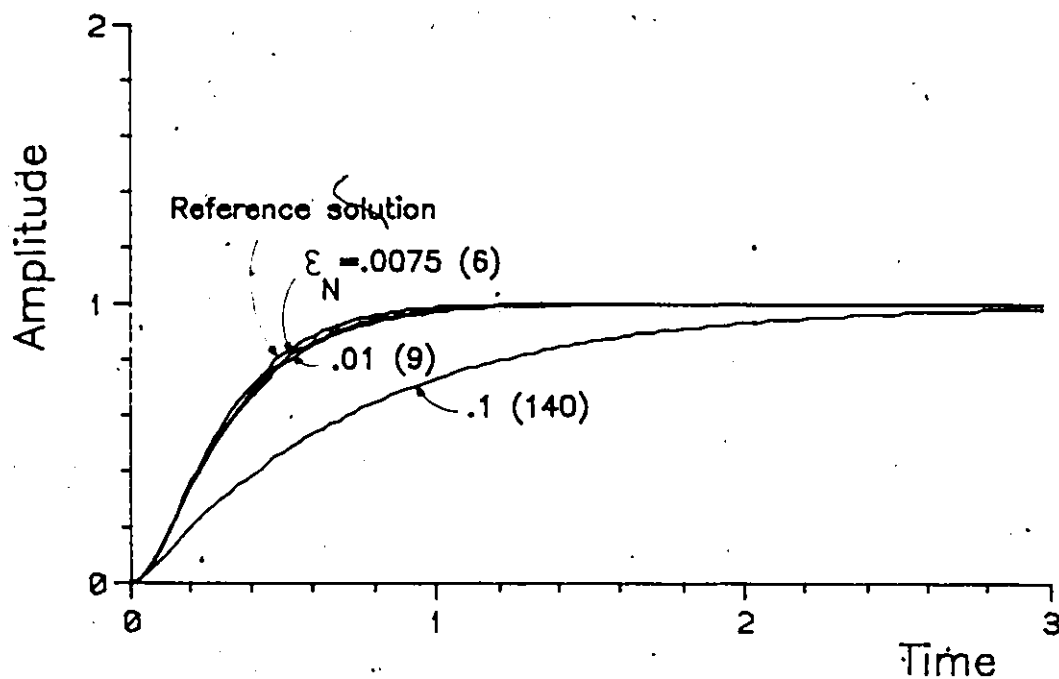


Figure A-4 : Normalized error with damping ratio of 1 for the reference solution. (Numbers in brackets are percentage variations in damping ratio)

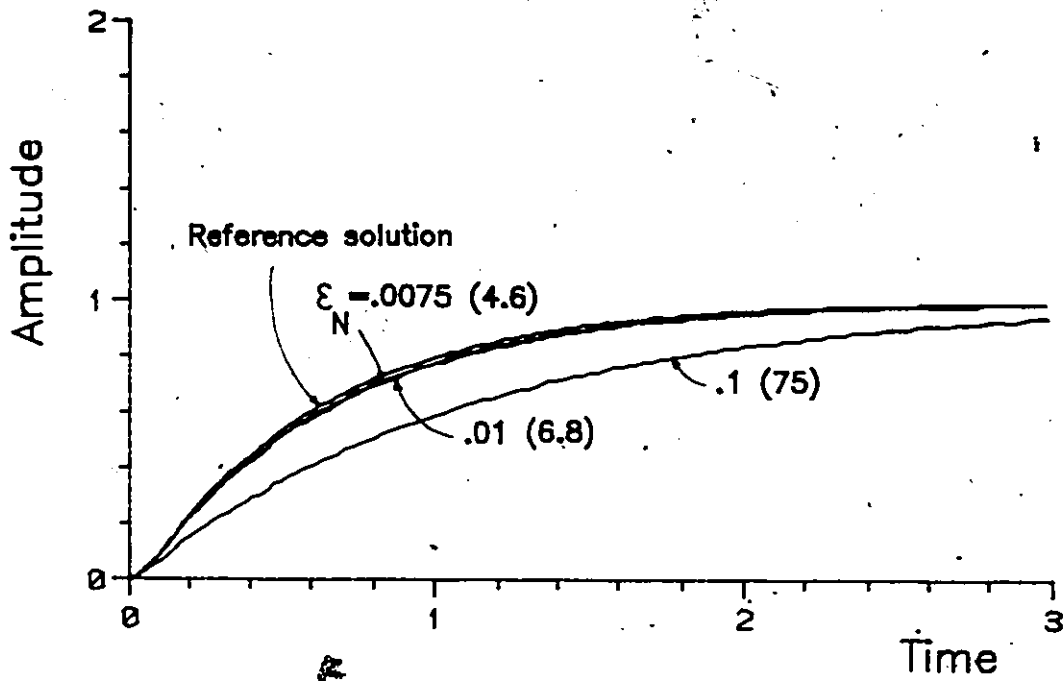


Figure A-5 : Normalized error with damping ratio of 2 for the reference solution (Numbers in brackets are percentage variations in damping ratio)

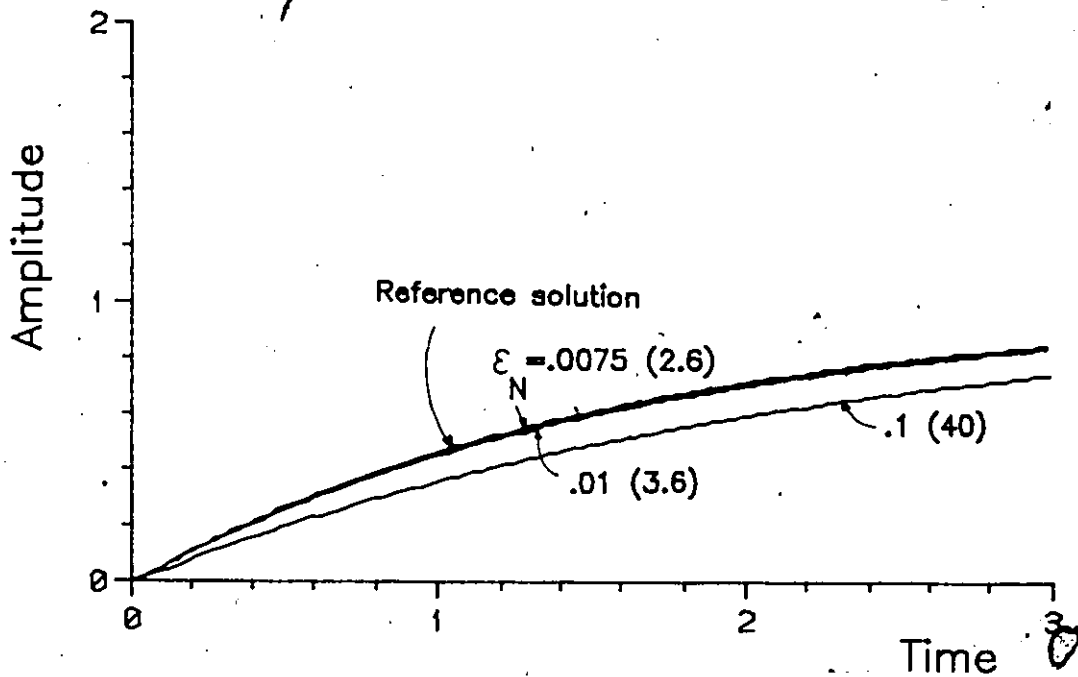


Figure A-6 : Normalized error with damping ratio of 5 for the reference solution (Numbers in brackets are percentage variations in damping ratio)

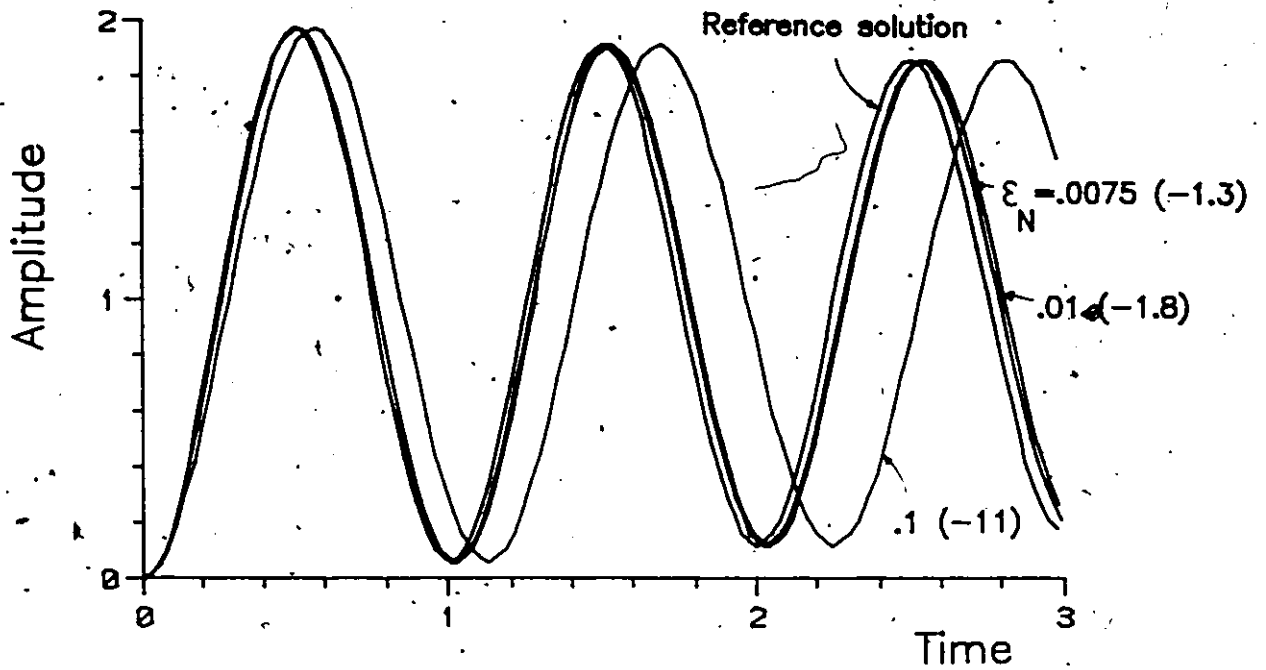


Figure A-7 : Normalized error, with damping ratio of .01 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

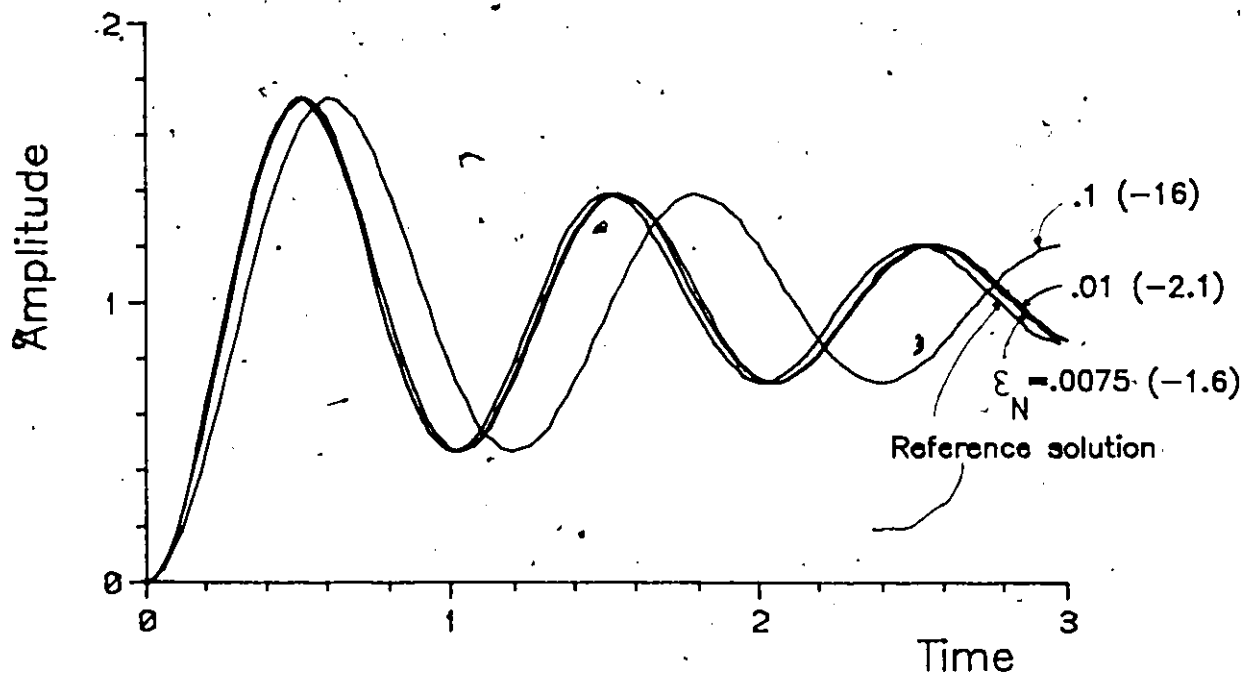


Figure A-8 : Normalized error with damping ratio of .1 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

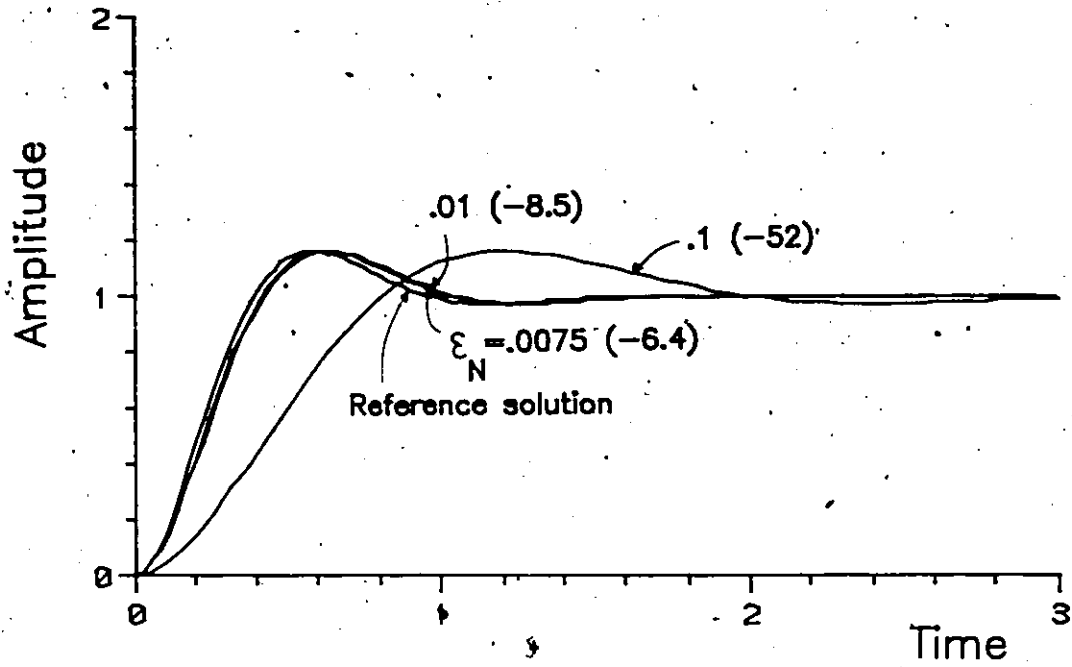


Figure A-9 : Normalized error with damping ratio of .5 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

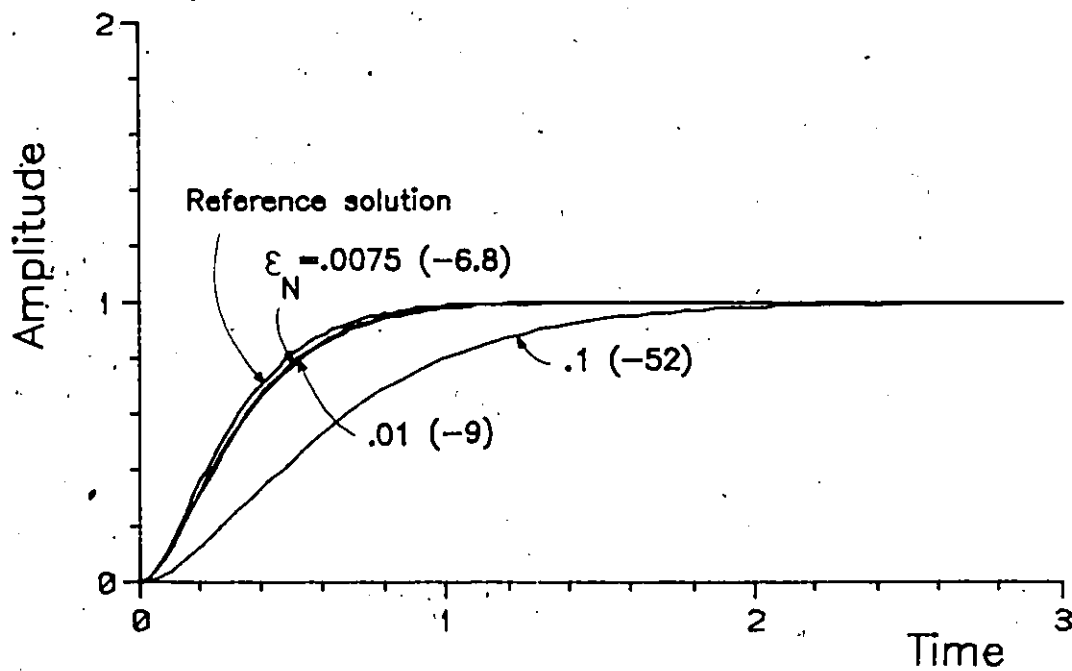


Figure A-10 : Normalized error with damping ratio of 1 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

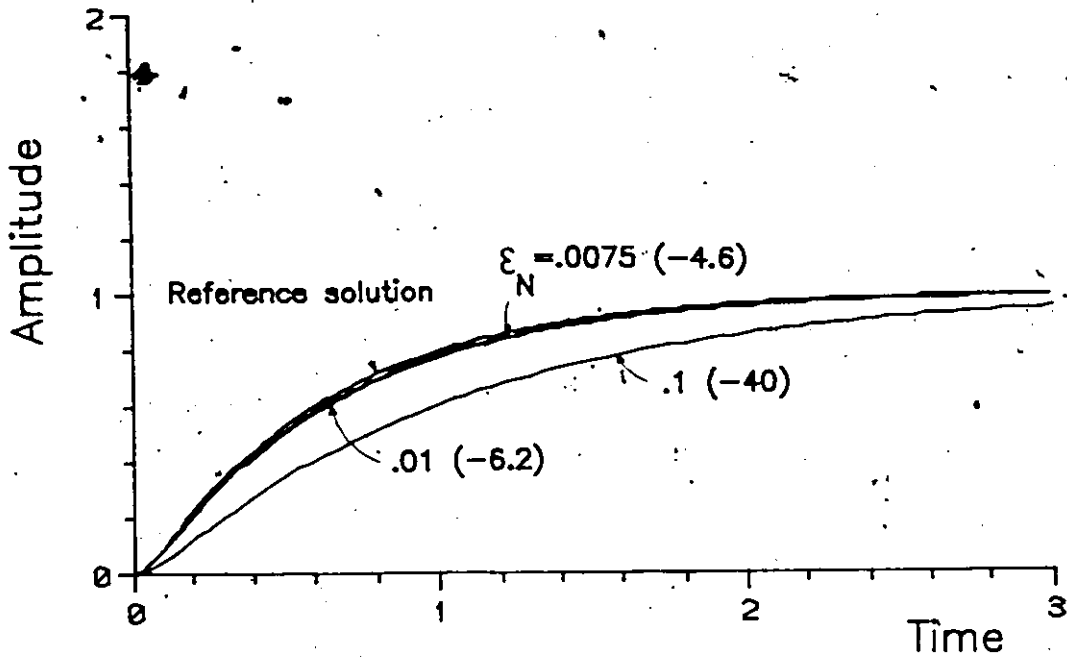


Figure A-11 : Normalized error with damping ratio of 2 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

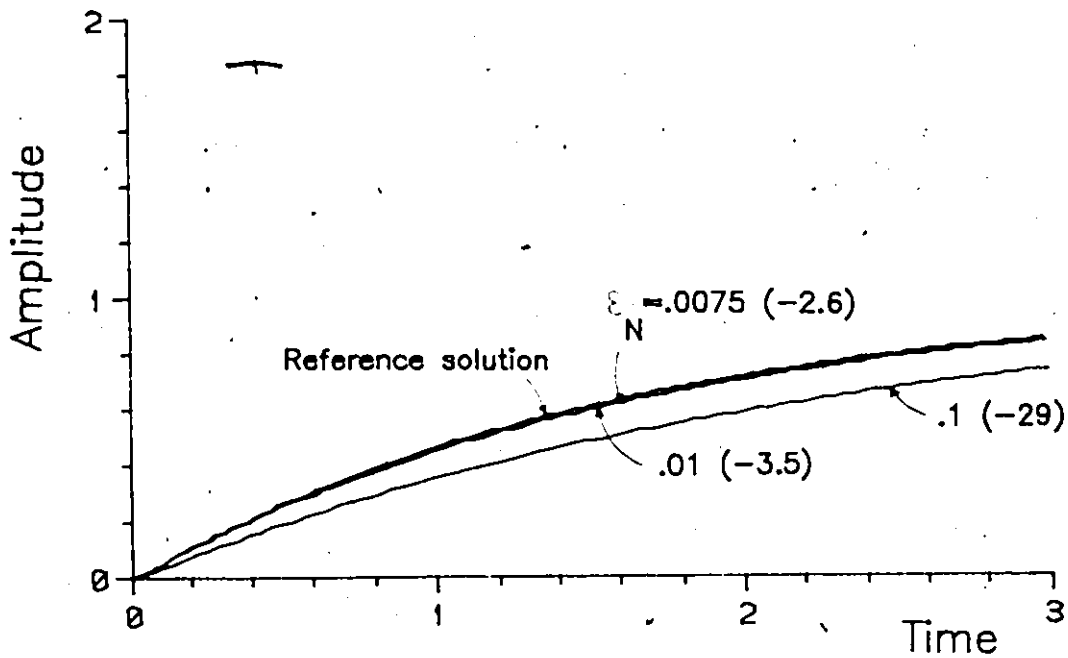


Figure A-12 : Normalized error with damping ratio of 5 for all solutions  
 (Numbers in brackets are percentage variations in undamped natural frequency)

APPENDIX B

Computerized Model Performance Data

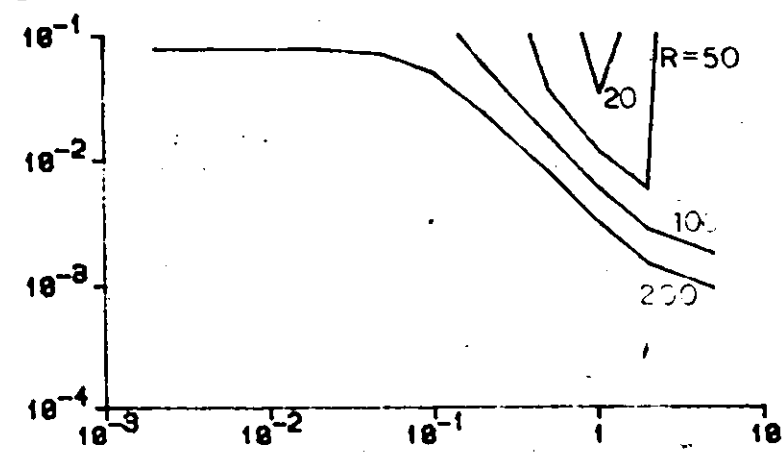
TABLE OF CONTENTS

	Table and Graph	$\theta'$	Page
System D relative to A	DA 1	0	120
	DA 2	0.5	120
	DA 3	1.0	121
	DA 4	1.5	121
	DA 5	2.0	122
System C relative to A	CA 1	0	123
	CA 2	0.5	123
	CA 3	1.0	124
	CA 4	1.5	124
	CA 5	2.0	125
System C relative to D	CD 1	0	126
	CD 2	0.5	126
	CD 3	1.0	127
	CD 4	1.5	127
	CD 5	2.0	128
System B relative to A	BA		129

R	5.	10.	20.	50.	100.	200.	500.
0.0021	.272	.358	.329	.261	.159	.079	.031
0.0201	.278	.358	.276	.262	.159	.077	.030
0.0501	.289	.365	.235	.275	.155	.071	.024
0.1001	.314	.358	.223	.279	.133	.050	.017
0.2001	.393	.224	.290	.206	.059	.024	.008
0.5001	.280	.320	.219	.035	.015	.008	.003
1.0001	.222	.156	.034	.012	.006	.003	.001
2.0001	1.00	1.00	.210	.006	.003	.001	7E-3
3.0001	1.00	1.00	1.00	1.00	.002	.9E-3	.5E-3

TABLE DA 1

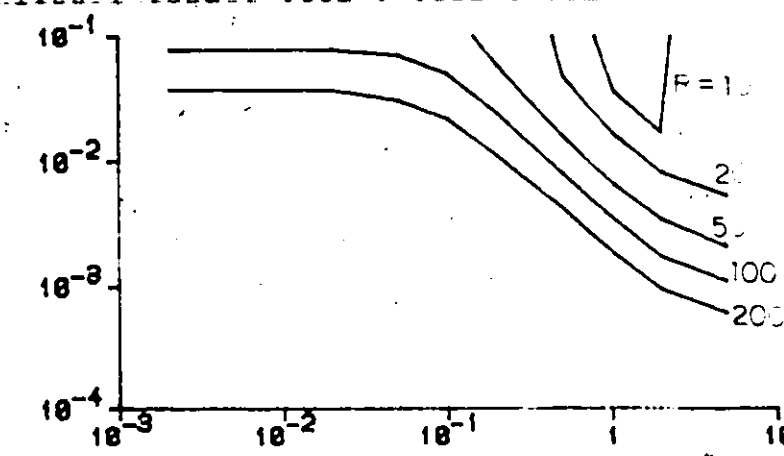
AP = 10.0



R	5.	10.	20.	50.	100.	200.	500.
0.0021	.346	.347	.300	.107	.070	.038	.019
0.0201	.347	.337	.304	.102	.070	.037	.014
0.0501	.351	.290	.300	.113	.070	.031	.012
0.1001	.351	.234	.307	.132	.049	.022	.008
0.2001	.236	.269	.280	.057	.024	.011	.004
0.5001	.381	.195	.048	.015	.002	.004	.002
1.0001	.093	.035	.016	.006	.003	.002	.7E-3
2.0001	.176	.017	.008	.003	.002	.9E-3	.9E-3
3.0001	1.00	1.00	.005	.002	.001	.6E-3	.3E-3

TABLE DA 2

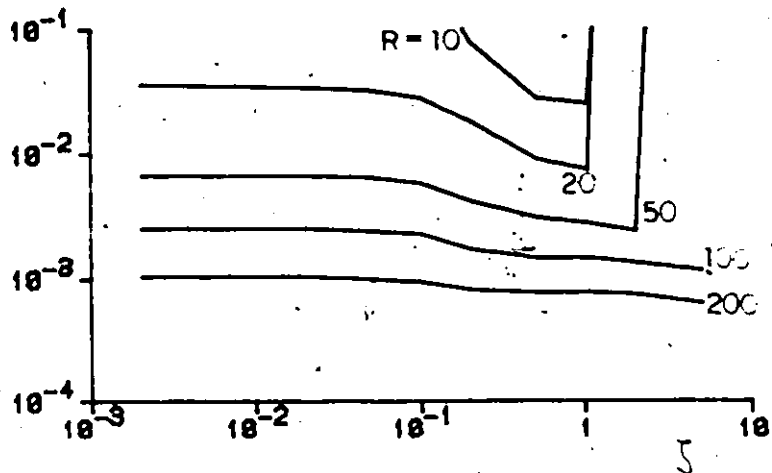
AP = 10.0



R	5.	10.	20.	50.	100.	200.	500.
ZETA							
0.002	1.00	.277	.035	.007	.002	.001	.4E-3
0.020	1.00	.269	.034	.007	.002	.001	.4E-3
0.050	1.00	.266	.032	.006	.002	.1E-2	.4E-3
0.100	1.00	.217	.028	.006	.002	.9E-3	.4E-3
0.200	1.00	.077	.017	.004	.002	.8E-3	.4E-3
0.500	.245	.027	.009	.003	.001	.8E-3	.3E-3
1.000	1.00	.025	.007	.003	.001	.8E-3	.3E-3
2.000	1.00	1.00	1.00	.002	.001	.7E-3	.3E-3
5.000	1.00	1.00	1.00	1.00	.001	.6E-3	.3E-3

TABLE DA 3

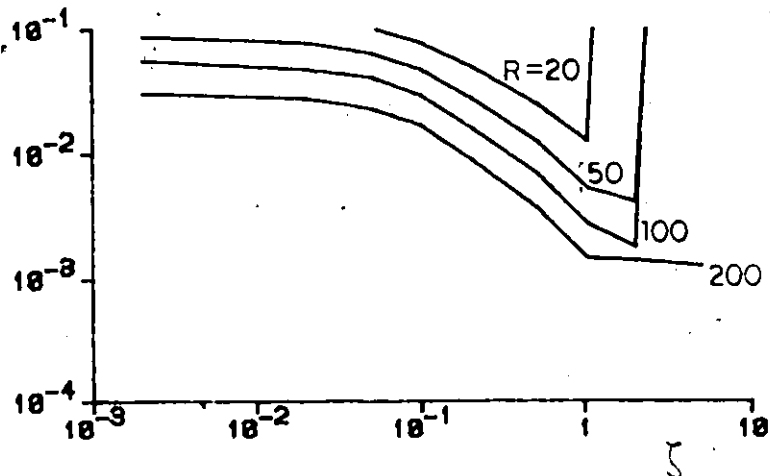
$R^* = 1.0$



R	5.	10.	20.	50.	100.	200.	500.
ZETA							
0.002	1.00	1.00	.130	.085	.054	.031	.014
0.020	1.00	1.00	.118	.077	.048	.028	.012
0.050	1.00	1.00	.101	.065	.041	.023	.010
0.100	1.00	.231	.079	.049	.030	.017	.007
0.200	1.00	.217	.051	.028	.016	.009	.004
0.500	1.00	.235	.026	.012	.007	.004	.002
1.000	1.00	.199	.012	.005	.003	.001	.7E-3
2.000	1.00	1.00	1.00	.004	.002	.001	.6E-3
5.000	1.00	1.00	1.00	1.00	1.00	.001	.6E-3

TABLE DA 4

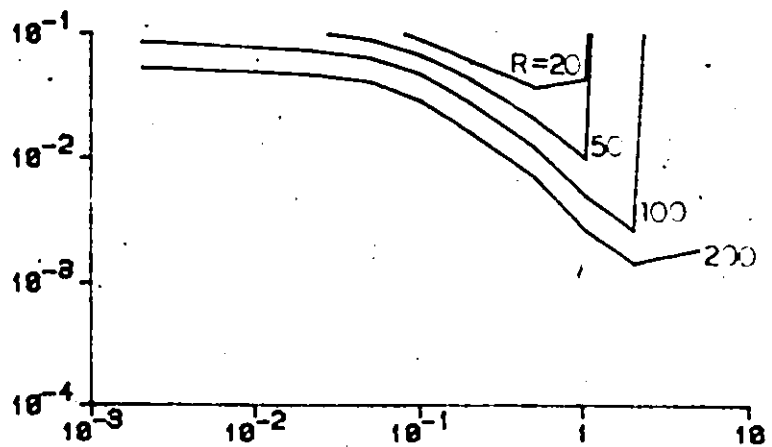
$R^* = 1.5$



NR	5.	10.	20.	50.	100.	200.	500.
0.002	1.00	1.00	.139	.114	.084	.054	.026
0.020	1.00	1.00	.128	.104	.076	.049	.023
0.050	1.00	1.00	.113	.089	.064	.040	.019
0.100	1.00	1.00	.091	.068	.048	.030	.014
0.200	1.00	1.00	.062	.043	.028	.016	.007
0.500	1.00	1.00	.038	.020	.012	.007	.003
1.000	1.00	1.00	.043	.010	.005	.003	.001
2.000	1.00	1.00	1.00	1.00	.003	.001	.8E-3
5.000	1.00	1.00	1.00	1.00	1.00	.002	.8E-3

TABLE IA 5

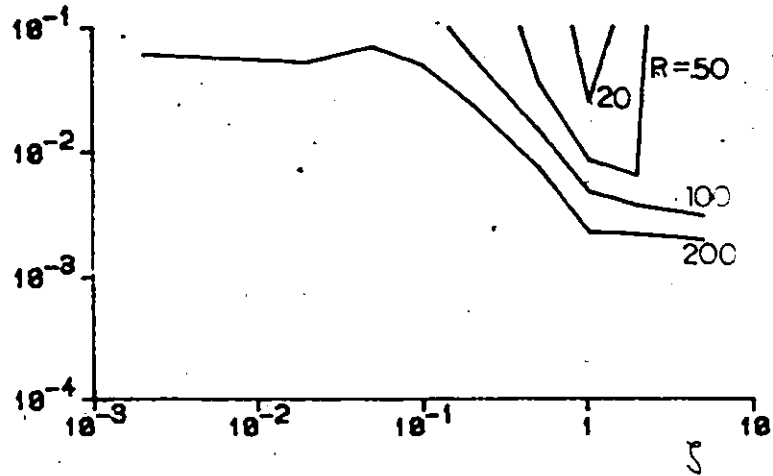
$\epsilon = 2.0$



R	5.	10.	20.	50.	100.	200.	500.
0.002	358	256	142	221	124	060	023
0.020	363	259	146	214	138	053	029
0.050	369	264	173	175	101	069	024
0.100	375	272	265	201	132	049	017
0.200	383	282	288	209	059	023	009
0.500	367	291	217	035	015	007	004
1.000	243	153	025	009	005	002	004
2.000	1.00	1.00	200	006	004	002	006
5.000	1.00	1.00	1.00	1.00	003	002	007

TABLE CA 1

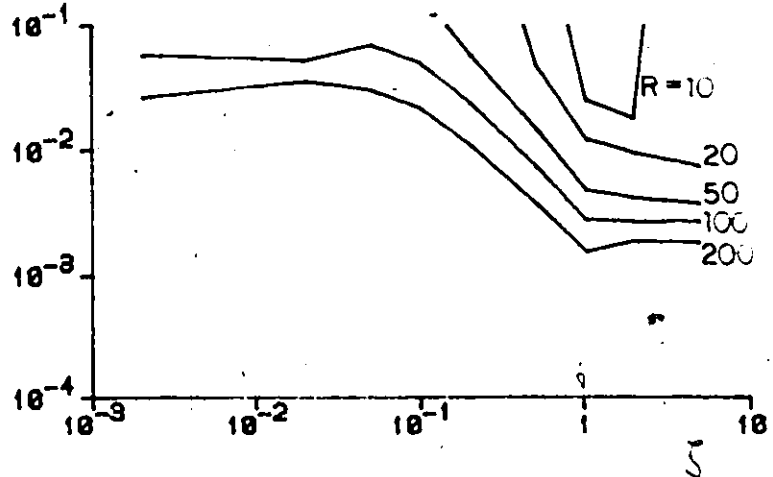
$H = 0.0$



R	5.	10.	20.	50.	100.	200.	500.
0.002	247	141	167	121	057	027	012
0.020	248	150	214	134	053	035	014
0.050	252	217	232	101	069	030	012
0.100	260	260	196	130	049	021	008
0.200	263	285	258	058	024	011	005
0.500	289	191	047	015	007	004	004
1.000	092	026	012	005	003	002	004
2.000	1.00	018	009	004	003	002	005
5.000	1.00	1.00	007	004	003	002	007

TABLE CA 2

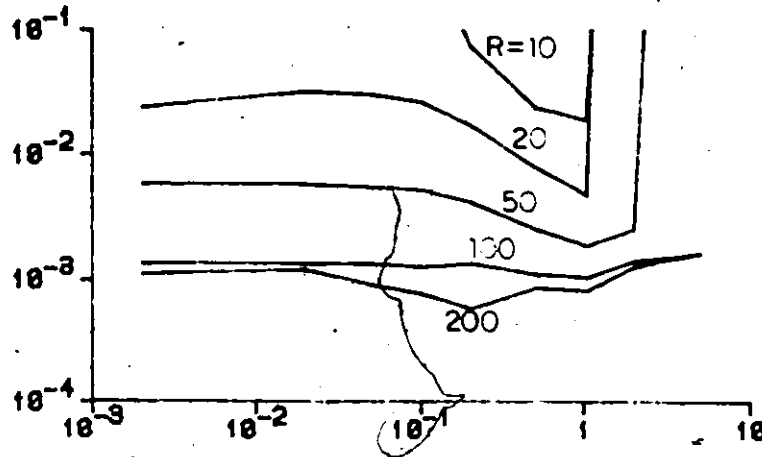
$H = 0.5$



R	.5	10	20	50	100	200	500
0.002	160	121	024	006	001	001	001
0.020	161	120	033	006	001	001	001
0.050	166	119	031	005	001	9E-31	001
0.100	185	189	026	005	001	7E-31	001
0.200	245	025	017	004	001	6E-31	002
0.500	255	024	008	003	001	8E-31	003
1.000	1.00	019	005	002	001	8E-31	004
2.000	1.00	1.00	1.00	002	001	001	005
5.000	1.00	1.00	1.00	1.00	002	002	007

TABLE CA 3

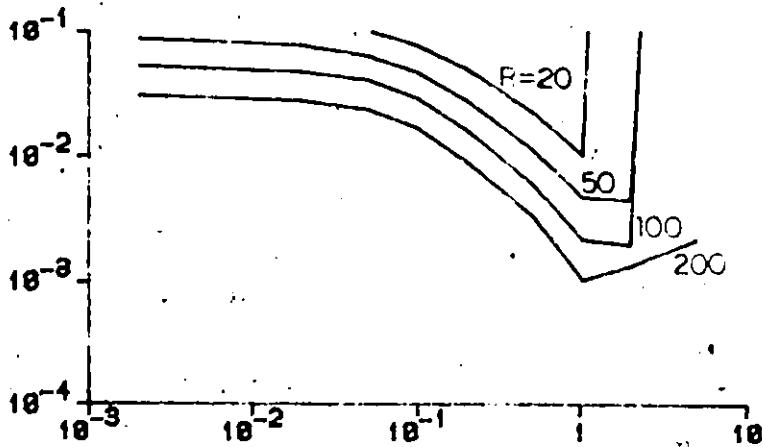
$\eta = 1.0$



R	.5	10	20	50	100	200	500
0.002	207	156	130	085	054	031	014
0.020	208	161	118	072	048	028	013
0.050	209	166	101	065	041	023	010
0.100	229	189	079	048	030	017	007
0.200	230	251	059	028	018	009	004
0.500	228	230	023	011	006	003	003
1.000	1.00	1.00	010	005	002	001	004
2.000	1.00	1.00	1.00	004	002	001	005
5.000	1.00	1.00	1.00	1.00	1.00	002	007

TABLE CA 4

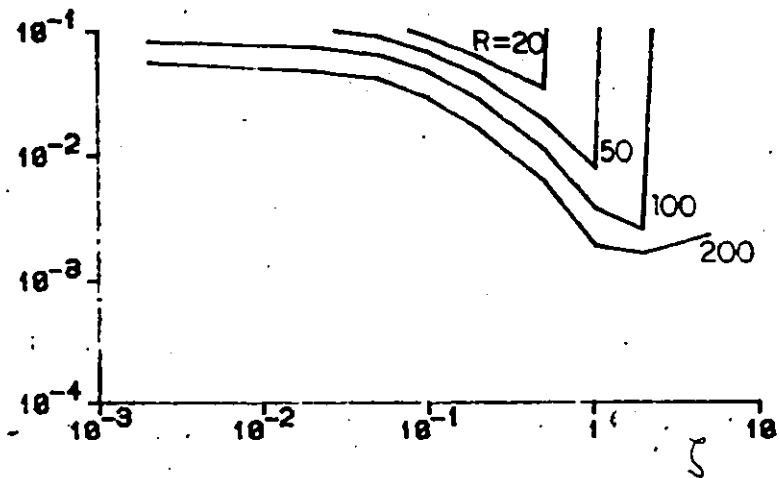
$\eta = 1.5$



\R	5.	10.	20.	50.	100.	200.	500.
ZEI\							
0.002	240	138	139	114	084	054	026
0.020	246	142	128	104	076	049	024
0.050	257	137	112	088	064	041	019
0.100	270	189	090	068	048	030	014
0.200	1.00	224	061	043	028	016	007
0.500	1.00	189	034	019	011	006	004
1.000	1.00	1.00	1.00	008	004	002	004
2.000	1.00	1.00	1.00	1.00	003	002	005
5.000	1.00	1.00	1.00	1.00	1.00	002	002

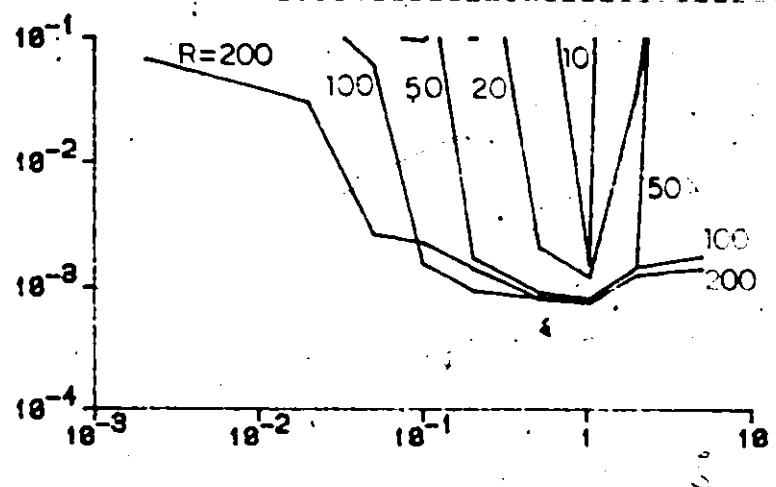
TABLE CA 5

$R' = 2.0$



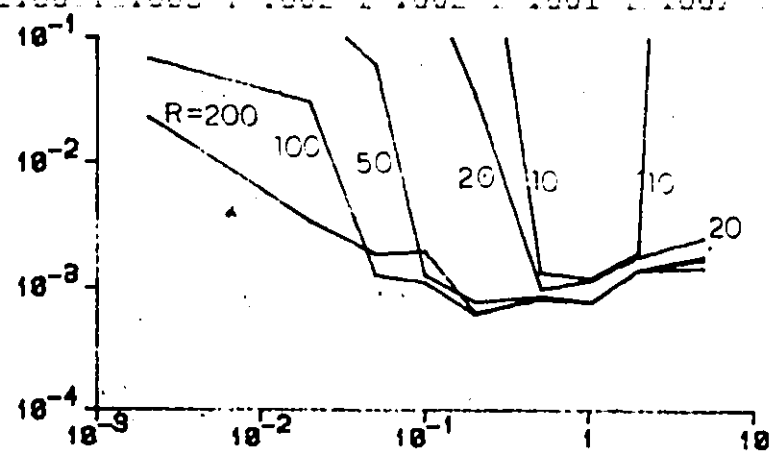
	5.0	10.0	20.0	50.0	100.0	200.0	500.0
0.0020	.153	.153	.134	.166	.133	.067	.015
0.0200	.148	.149	.119	.163	.129	.030	.001
0.0500	.154	.142	.103	.147	.061	.003	1E-2
0.1000	.147	.145	.097	.131	.001	.002	.001
0.2000	.148	.099	.158	.002	9E-3	.001	.002
0.5000	.086	.141	.002	9E-3	9E-3	9E-3	.003
1.0000	.032	.002	.001	8E-3	8E-3	7E-3	.004
2.0000	1.00	1.00	.037	.001	.001	.001	.005
5.0000	1.00	1.00	1.00	1.00	.002	.001	.002

TABLE CD 1



	10.0	50.0	100.0	200.0	500.0
0.0020	.143	.140	.107	.138	.087
0.0200	.143	.138	.108	.132	.030
0.0500	.128	.114	.105	.082	.001
0.1000	.135	.110	.142	.001	.001
0.2000	.103	.153	.035	8E-3	8E-3
0.5000	.137	.001	.1E-3	8E-3	8E-3
1.0000	.001	.001	.001	8E-3	7E-3
2.0000	1.00	.002	.002	.001	.001
5.0000	1.00	1.00	.003	.001	.002

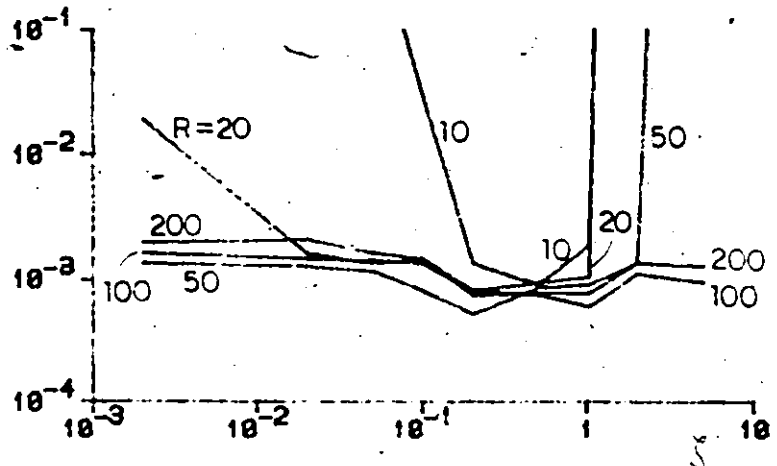
TABLE CD 2



NR	5.	10.	20.	50.	100.	200.	500.
ZETA1							
0.002	1.00	152	012	001	002	002	9E-3
0.020	1.00	142	002	001	001	002	8E-3
0.050	1.00	174	001	001	001	002	9E-3
0.100	1.00	032	001	8E-3	001	001	001
0.200	1.00	001	8E-3	5E-3	8E-3	7E-3	002
0.500	0.75	9E-3	9E-3	8E-3	7E-3	8E-3	003
1.000	1.00	002	001	9E-3	6E-3	8E-3	004
2.000	1.00	1.00	1.00	001	001	001	005
5.000	1.00	1.00	1.00	1.00	9E-3	001	007

TABLE CD 3

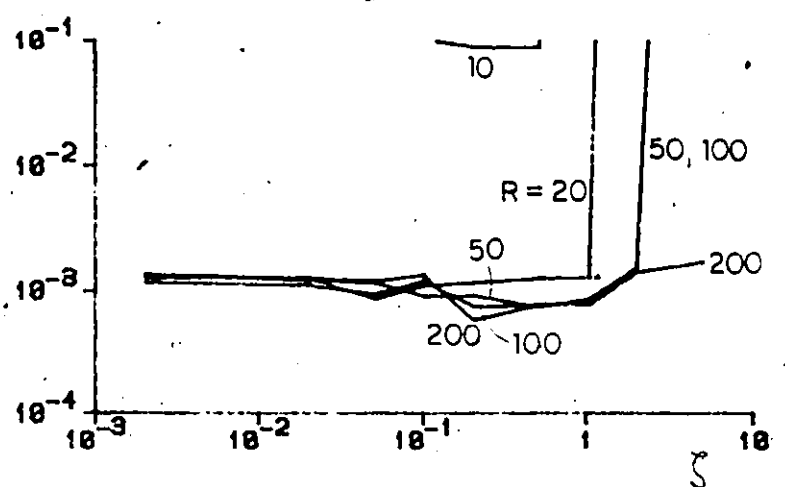
R = 1.0



NR	5.	10.	20.	50.	100.	200.	500.
ZETA1							
0.002	1.00	1.00	001	001	001	001	8E-3
0.020	1.00	1.00	001	001	001	001	8E-3
0.050	1.00	1.00	8E-3	001	9E-3	001	8E-3
0.100	1.00	1.03	001	9E-3	001	001	001
0.200	1.00	089	001	9E-3	7E-3	6E-3	002
0.500	1.00	092	001	7E-3	8E-3	8E-3	003
1.000	1.00	1.00	001	8E-3	8E-3	8E-3	004
2.000	1.00	1.00	1.00	001	001	001	005
5.000	1.00	1.00	1.00	1.00	1.00	002	007

TABLE CD 4

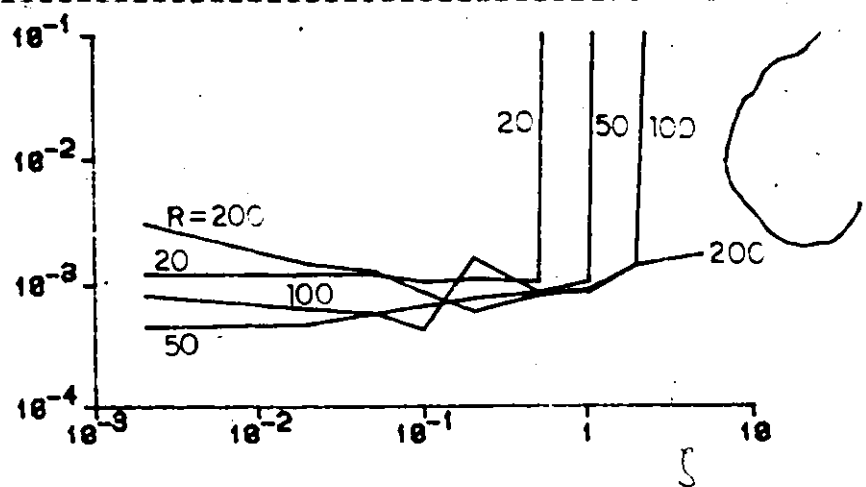
R = 1.5



NR	5.	10.	20.	50.	100.	200.	500.
ZETA							
0.002	1.00	1.00	.001	.4E-3	.8E-3	.003	.9E-3
0.020	1.00	1.00	.001	.5E-3	.6E-3	.001	.1E-2
0.050	1.00	1.00	.001	.6E-3	.6E-3	.001	.001
0.100	1.00	1.00	.001	.7E-3	.4E-3	.9E-3	.001
0.200	1.00	1.00	.001	.8E-3	.002	.6E-3	.002
0.500	1.00	1.00	.001	.8E-3	.8E-3	.8E-3	.003
1.000	1.00	1.00	1.00	.001	.8E-3	.9E-3	.004
2.000	1.00	1.00	1.00	1.00	.001	.001	.005
5.000	1.00	1.00	1.00	1.00	1.00	.002	.007

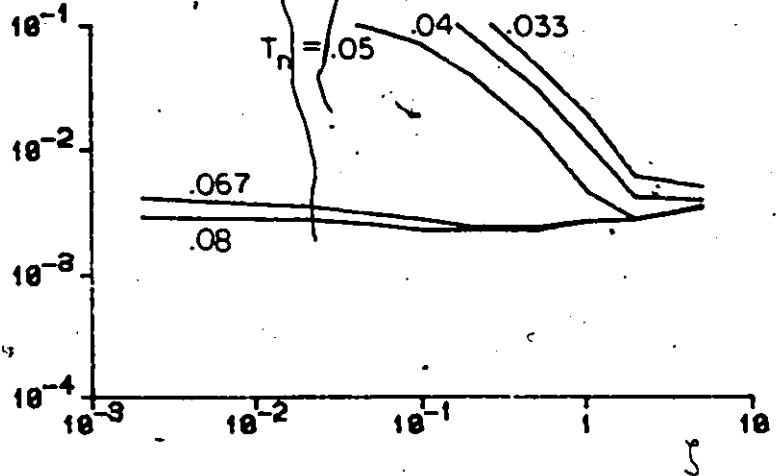
TABLE CD 5

W = 2.00



$\Delta T_n$	0.025	0.033	0.040	0.050	0.067	0.080	0.100
0.002	181	208	203	127	004	003	003
0.020	175	197	189	113	003	003	002
0.050	168	181	168	095	003	002	002
0.100	162	159	135	070	003	002	002
0.200	152	117	083	039	002	002	002
0.500	091	048	031	014	002	002	002
1.000	033	018	011	004	003	003	003
2.000	041	006	004	003	003	003	003
5.000	072	005	004	003	003	003	004

TABLE BA



APPENDIX C

System A Documentation

Contents

- Flowchart
- Listing

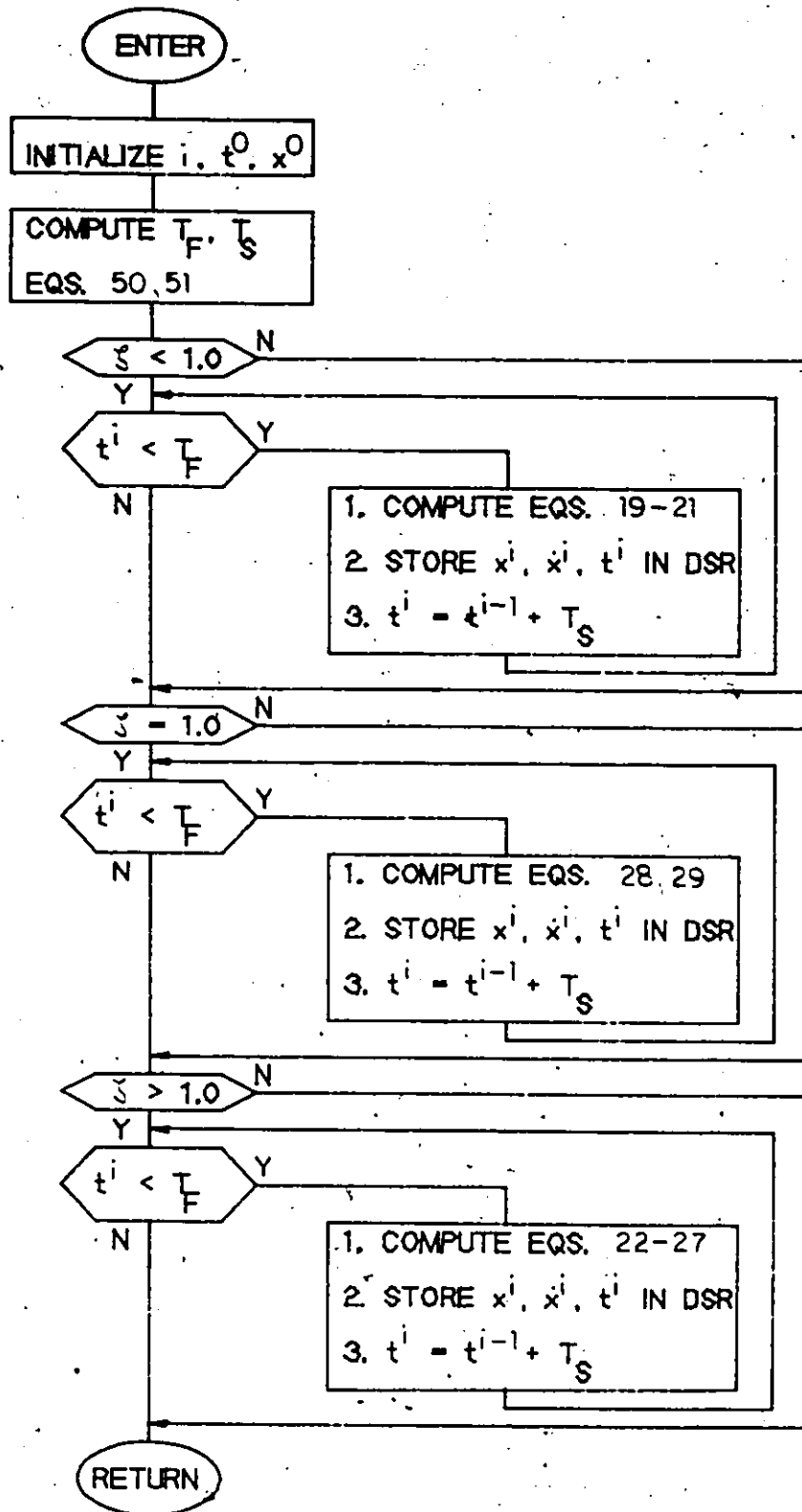


Figure C-1 : Subroutine SYSTMA flowchart

```

C _____ Subroutine SYSTMA
C _____ Computes response data points for the analytical system
SUBROUTINE SYSTMA

C _____ Specification statements
DIMENSION RESPONSE(1000), RESPONSD(1000), RESTIME(1000)

COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /CONSTANTS/ XF, PI
COMMON /FORCE/ STEP
COMMON /NUMTIM/ NT, NS
COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME
COMMON /RESPONSDOT/ RESPONSD

C _____ Initialization
TIME = 0.0
X = 0.0
NPOINT = 0

C _____ Compute final solution time and computation time
C _____ interval
FINALTIME = (NT*2 *PI)/OMEGAN
TIMEINC = (2 *PI)/(NS*OMEGAN)

C _____ Compute response data if ZETA is less than 1
IF(ZETA LT 1.0) THEN

C _____ Initialize constants
SGROOT = SQRT(1 - ZETA**2)
PHI = ATAN(SGROOT/ZETA)

C _____ Compute data points until final solution time
DO WHILE(TIME LE FINALTIME)
  X = STEP - EXP(-ZETA*OMEGAN*TIME)/SGROOT *
    SIN(OMEGAN*SGROOT*TIME + PHI)
  XD = OMEGAN*EXP(-ZETA*OMEGAN*TIME)
    *((ZETA/SGROOT)*SIN(OMEGAN*SGROOT*TIME + PHI)
    - COS(OMEGAN*SGROOT*TIME + PHI))
  NPOINT = NPOINT + 1
  RESPONSE(NPOINT) = X
  RESPONSD(NPOINT) = XD
  RESTIME(NPOINT) = TIME
  TIME = TIME + TIMEINC
END DO
END IF

C _____ Compute response data if ZETA equals 1
IF(ZETA EQ 1.0) THEN

C _____ Compute data points until final solution time
DO WHILE(TIME LE FINALTIME)
  X = STEP - EXP(-OMEGAN*TIME)*(1 + OMEGAN*TIME)
  XD = EXP(-OMEGAN*TIME)*(OMEGAN**2)*TIME
  NPOINT = NPOINT + 1
  RESPONSE(NPOINT) = X
  RESPONSD(NPOINT) = XD
  RESTIME(NPOINT) = TIME
  TIME = TIME + TIMEINC
END DO
END IF

C _____ Compute response data if ZETA is greater than 1
IF(ZETA GT 1.0) THEN

C _____ Compute constant and coefficients
SGROOT = SQRT(ZETA**2 - 1)
CA = OMEGAN*(ZETA - SGROOT)
CB = OMEGAN*(ZETA + SGROOT)
CC = -(ZETA + SGROOT)/(2 *SGROOT)
CD = -(-ZETA + SGROOT)/(2 *SGROOT)

C _____ Compute data points until final solution time
DO WHILE(TIME LE FINALTIME)
  X = STEP + CC*EXP(-CA*TIME) + CD*EXP(-CB*TIME)
  XD = -CA*CC*EXP(-CA*TIME) - CB*CD*EXP(-CB*TIME)
  NPOINT = NPOINT + 1
  RESPONSE(NPOINT) = X
  RESPONSD(NPOINT) = XD
  RESTIME(NPOINT) = TIME
  TIME = TIME + TIMEINC
END DO
END IF

RETURN
END

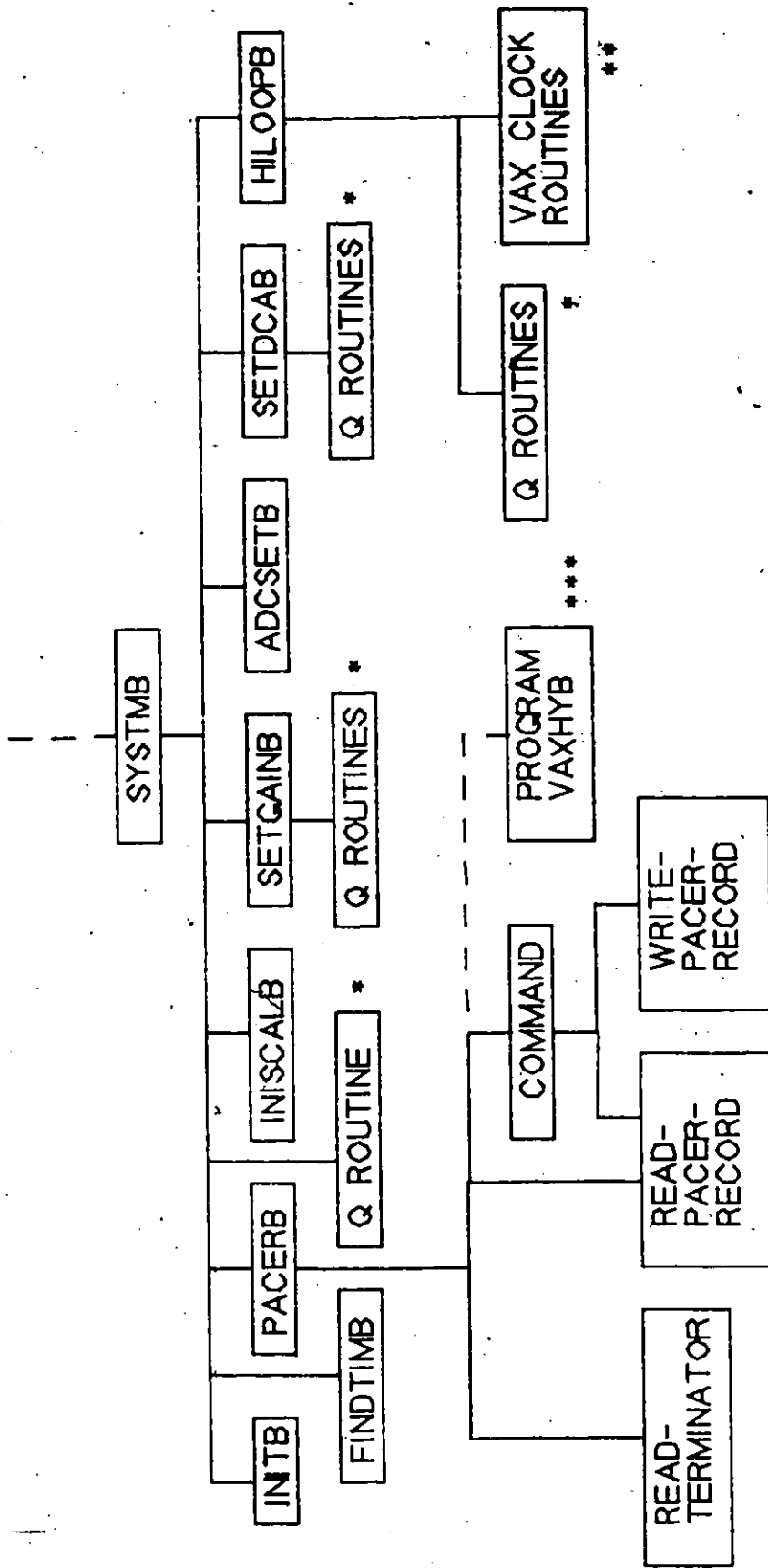
```

APPENDIX D

System B Documentation

Contents

- Subroutine Hierarchical Diagram
- Hierarchy
- Input-Process-Output Table of Subroutines
- Flowcharts
- Listings



- Q ROUTINES ARE VAX/HYBRID SYSTEM SUBROUTINES
- \*\* VAX CLOCK ROUTINES ARE VAX SYSTEM SUBROUTINES
- \*\*\* PROGRAM VAXHYB IS A VAX/HYBRID SYSTEM PROGRAM

Figure D-1 : Subroutine hierarchical diagram of subroutine SYSTMB

## Subroutine SYSTMB Hierarchy

1. Initialize variables	...	sub INITB
2. Compute $T_F$ and $T_S$	...	sub FINDTIMB
3. Prepare PACER computer to run PACER program VAXHYB	...	<u>sub PACERB</u>
4. Establish connection with analog computer	...	sub QSHYIN
5. Initialize $x_M$ , $x_M$ , $x_M$	...	sub INISCALB
6. Set amplifier gain G	...	<u>sub SETGAINB</u>
7. Set A/D channel numbers	...	sub ADCSETB
8. Set DCA channel numbers and set DCA values on analog computer	...	<u>sub SETDCAB</u>
9. Execute high-speed-loop	...	<u>sub HILOOPB</u>
3. <u>Sub PACERB</u>		
3.1 Assign a channel to PACER		
3.2 Set up terminator mask for PACER read operation	...	sub READ-TERMINATOR
3.3 Obtain PACER monitor	...	sub READ-PACER-RECORD
3.4 Load program VAXHYB on PACER and start its execution	...	sub COMMAND
6. <u>Sub SETGAINB</u>		
6.1 Set G=1 on analog integrators	...	sub QSSECN
6.2 Set G=10	...	sub QSSECF

6.3 SET G=100

... sub GSMSN

8. Sub SETDCAB

8.1 Set DCA channel numbers

8.2 Set DCA values

8.3 Establish number of DCA's used

8.4 Set DCA values on analog computer

... sub QWRPTR

9. Sub HILOOPB

9.1 Initialize time variable

9.2 Put analog computer in IC mode

... sub GINIT

9.3 Read starting time on VAX clock

... fctn USER-  
GET-  
REALTIME

9.4 Put analog computer in operate (OP) mode

... sub GOPER

9.5 Read data from A/D converters

... sub GRBADS

9.6 Descale A/D data

9.7 Compute time since start of solution

... sub SUBGUAD

9.8 Store response solution data

9.9 Put analog computer in IC mode

... sub GINIT

Input-Process-Output Table of Subroutines

Subroutine	Inputs	Process	Outputs
SYSTMB	$\zeta, \omega_n, \pi, u, N_T, N_S$	Fig. D-2	DSR
FINDTIMB	$\omega_n, \pi, N_T, N_S$	Eqs. 50, 51	$T_F, T_S$
INISCALB	$\omega_n, u$	Eqs. 52-54	$x_M, x_M, x_M$
SETGAINB	$\omega_n$	Fig. D-4	$\theta$
SETDCAB	$\omega_n, \zeta, u, \theta, x_M^0, x_M^0$	Eqs. 56-62	$D_{15}, D_{20}, D_{25}, D_{22}$ $D_{27}, D_{23}, D_{28}$
HILOOPB	$T_F, T_S, x_M, x_M$ $x_S, x_S$	Fig. D-5	DSR

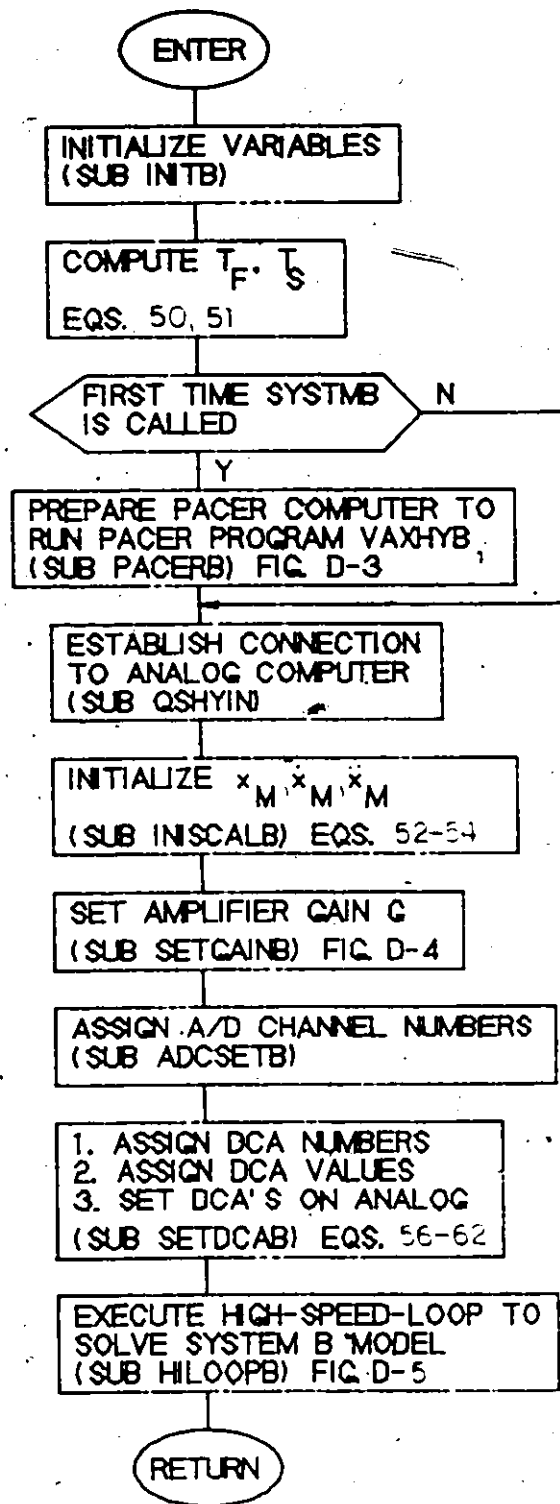


Figure D-2 : Subroutine SYSTM B-flowchart

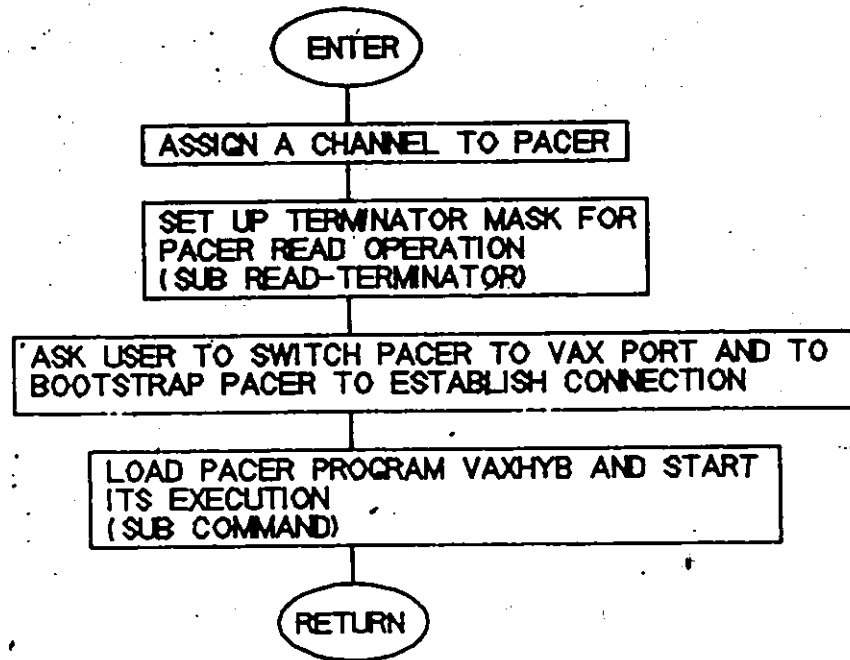


Figure D-3 : Subroutine PACERB flowchart

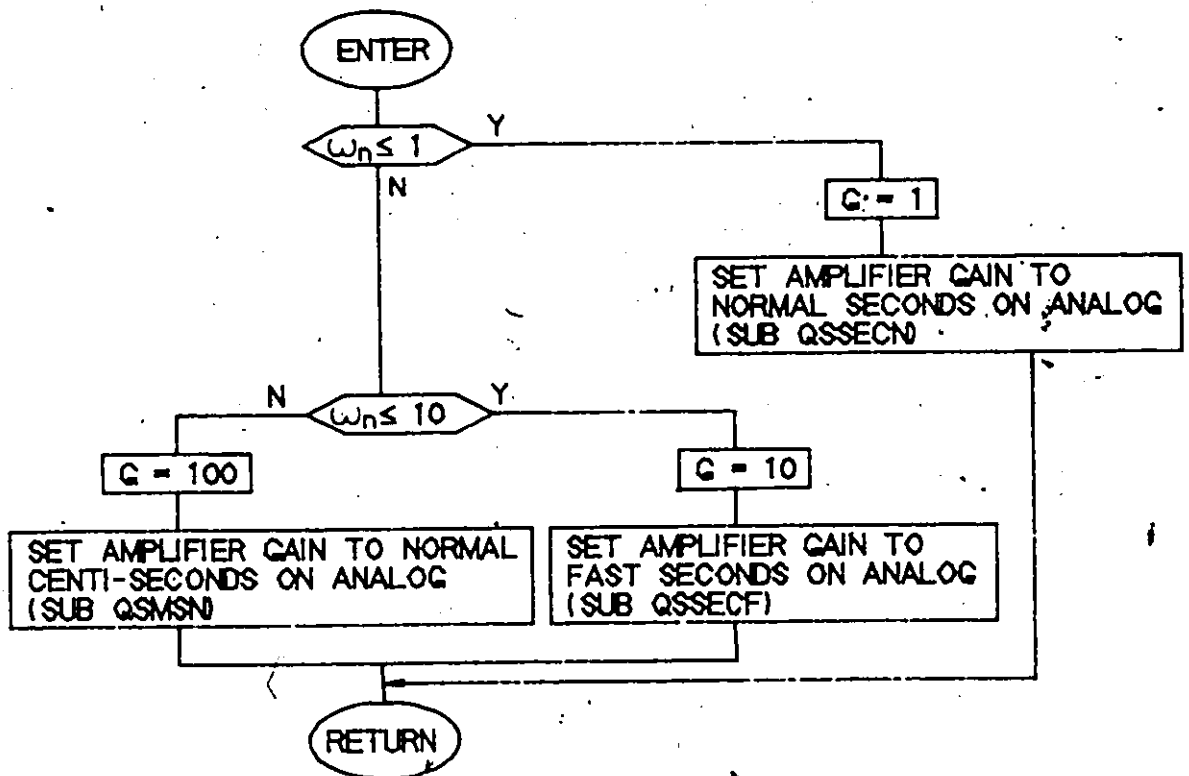


Figure D-4 : Subroutine SETGAINB flowchart

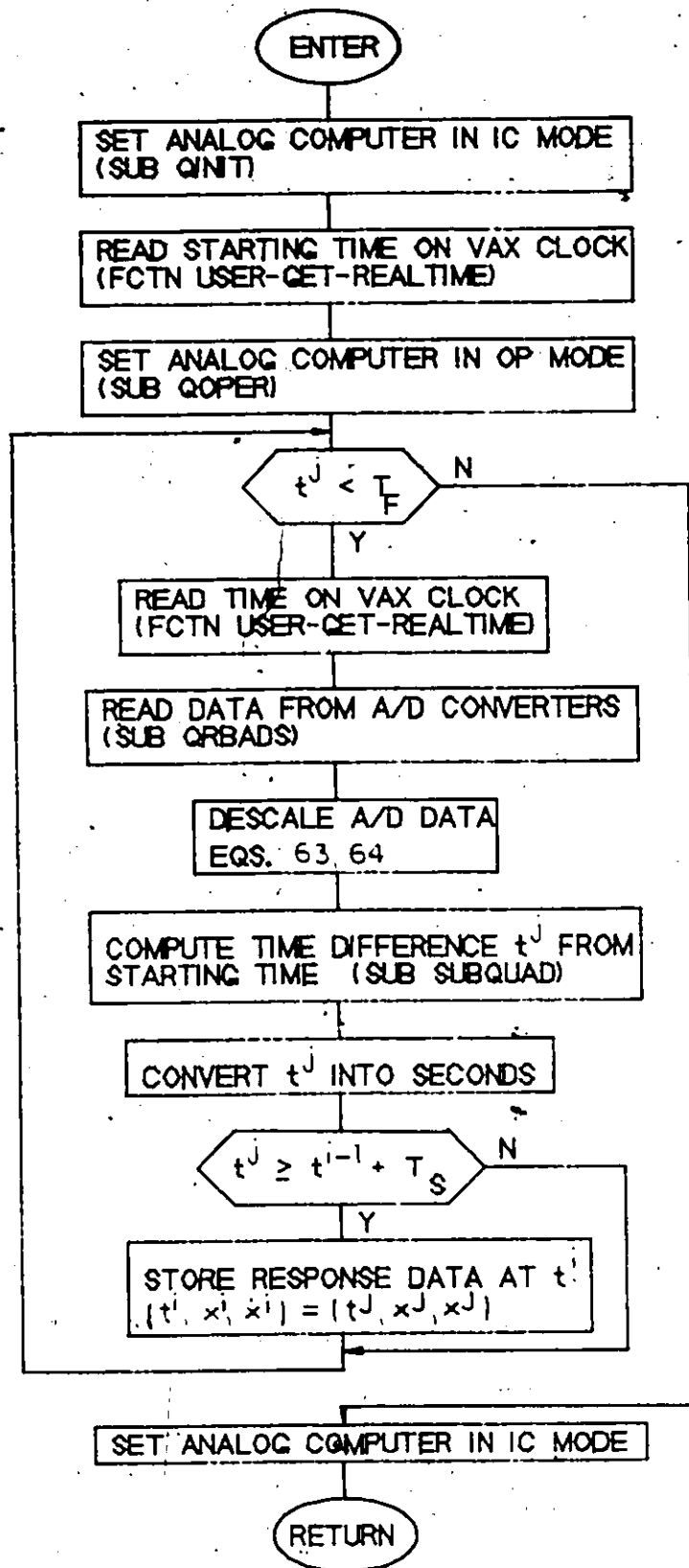


Figure D-5 : Subroutine HILOOPB flowchart

```

C _____ Subroutine SYSTM8
C _____ Computes response data points for the continuous-time
C _____ system (Analog computer)
C _____ SUBROUTINE SYSTM8

C _____ Specification statements
LOGICAL FIRSTRUNB, FIRSTRUNC

COMMON /FIRSTRUN/ FIRSTRUNB, FIRSTRUNC

C _____ Prepare the PACER to enable VAX/HYBRID running
C _____ if it is the first time subroutine SYSTM8 is called or
C _____ if subroutine SYSTM8 has been called in the same main
C _____ program run
C _____ IF(FIRSTRUNB) THEN
C _____ CALL PACERB
C _____ END IF

C _____ Establish connection to analog computer
C _____ CALL OSHYIN(IER,680,680)

C _____ Initialize constants
C _____ CALL INITB

C _____ Compute final solution time and data storage sampling
C _____ period
C _____ CALL FINDTIMR

C _____ Initialize scaling variables
C _____ CALL INISCALB

C _____ Set amplifier gain value for analog integrators
C _____ CALL SETGAINB

C _____ Assign A/D channel numbers
C _____ CALL ADCSETB

C _____ Assign DCA numbers, assign DCA values and set DCA's
C _____ on analog computer
C _____ CALL SETDCAB

C _____ Execute high-speed-loop to solve System B model
C _____ CALL HILOOPB

C _____ CALL RELEASE_DR11B

C _____ RETURN
C _____ END

```

```

C _____ Subroutine INITB
C _____ Initializes constants
C _____ SUBROUTINE INITB

C _____ Specification statements
REAL LASTSAVTIM

DIMENSION RESPONSE(1000), RESPONSD(1000), RESTIME(1000)

COMMON /CONSOLE/ NOCNLS
COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME
COMMON /RESPONSDOT/ RESPONSD
COMMON /TIM/ TIME, FINALTIM, SAVINCTIM, LASTSAVTIM

C _____ Initialize console number
C _____ NOCNLS= 1

C _____ Initialize response data pointer
C _____ NPOINT= 1

C _____ Initialize first time data
C _____ TIME = 0.0

C _____ Store first response and time data
C _____ RESPONSE(NPOINT) = 0.0
C _____ RESPONSD(NPOINT) = 0.0
C _____ RESTIME(NPOINT) = 0.0

C _____ Initialize last time data that has been stored
C _____ LASTSAVTIM = 0.0

C _____ RETURN
C _____ END

```

C \_\_\_\_\_ Subroutine FINDTIMB  
 C \_\_\_\_\_ Finds final solution time for a fixed number (NT) of cycles  
 C \_\_\_\_\_ and finds the data storage sampling period  
 SUBROUTINE FINDTIMB

C \_\_\_\_\_ Specification statements  
 REAL LASTSAVTIM

COMMON /CONSTANTS/ XF, PI  
 COMMON /NUMTIM/ NT, NS  
 COMMON /INPUTPARAM/ THETA, TC, ZETA, DMEGAN  
 COMMON /TIM/ TIME, FINALTIM, SAVINCTIM, LASTSAVTIM

C \_\_\_\_\_ Compute final solution time  
 FINALTIM = (NT\*2\*PI)/DMEGAN

C \_\_\_\_\_ Compute data storage sampling period  
 SAVINCTIM = (2\*PI)/(NS\*DMEGAN)

RETURN  
 END

C \_\_\_\_\_ Subroutine PACERB  
 C \_\_\_\_\_ Prepares the PACER to enable VAX/HYBRID runing for  
 C \_\_\_\_\_ System B  
 SUBROUTINE PACERB

C \_\_\_\_\_ Specification statements  
 EXTERNAL SSB\_NORMAL

INTEGER\*4 SYS\$ASSIGN, SYS\$ALLOD  
 INTEGER\*2 CHANNEL2, LENGTH

CHARACTER RECORD\_STRING\*80, TERM\_MASK\*32

COMMON/GIO/CHANNEL2, LENGTH/MESSAGE/RECORD\_STRING, TERM\_MASK

C \_\_\_\_\_ Assign a channel to PACER  
 I=SYS\$ASSIGN('PACER100', CHANNEL2,.)  
 IF (I NE %LOC(SSB\_NORMAL)) THEN  
 TYPE 100, I  
 END IF

C \_\_\_\_\_ Set up terminator mask for PACER read operation  
 CALL READ\_TERMINATOR

C \_\_\_\_\_ Give instructions to user on how to obtain PACER monitor  
 TYPE \*, 'Switch PACER to VAX port and press <RETURN>'  
 ACCEPT \*  
 TYPE \*  
 TYPE \*, 'Bootstrap PACER to establish connection'  
 TYPE \*, '(message when connection established)'  
 CALL READ\_PACER\_RECORD  
 IF (RECORD\_STRING(1:2) EQ 'M\_') THEN  
 TYPE \*  
 TYPE \*, ' \* PACER CONNECTION ESTABLISHED \*'  
 END IF

C \_\_\_\_\_ Load VAX/HYBRID program on PACER and start execution  
 CALL COMMAND('ML,VAXHYB,21', .12, 'LD', .2, .6)  
 CALL COMMAND('BR, 45000, 70000', .15, . . . . . 0, .3)  
 CALL COMMAND('MG, 1000', .7, . . . . . 0, .2)

TYPE \*  
 TYPE \*, ' \* VAX/PACER NOW RUNING \*'  
 TYPE \*

C \_\_\_\_\_ Format statement  
 100 FORMAT(' CANNOT ASSIGN A CHANNEL TO PACER, STATUS = ', Z8)

RETURN  
 END

```

C _____ Subroutine WRITE_PACER_RECORD
C _____ Sends a record to PACER
SUBROUTINE WRITE_PACER_RECORD
EXTERNAL SS%_NORMAL, IOS%_WRITEVBLK, IOS%_NOFORMAT

C _____ Set up storage
COMMON/QIO/CHANNEL2, LENGTH/MESSAGE/RECORD_STRING, TERM_MASK
INTEGER*4 SYSSQIOW
INTEGER*2 CHANNEL2, LENGTH, CHAR_VALU, BIT_EIGHT, IOSB(4)
BYTE RECORD(80)
CHARACTER RECORD_STRING*80, TERM_MASK*32
EQUIVALENCE (RECORD(1), RECORD_STRING(1:1))
DATA BIT_EIGHT/'FF80'X/

C _____ Insure record is in 8 bit ASCII code
DO I=1,LENGTH
CHAR_VALU=RECORD(I)
CHAR_VALU=IIOR(CHAR_VALU, BIT_EIGHT)
RECORD(I)=CHAR_VALU
END DO

C _____ Add eight bit carriage return
LENGTH=LENGTH+1
RECORD(LENGTH)='BD'X

C _____ Send record to PACER
I=SYSSQIOW(, ZVAL(CHANNEL2), ZVAL(ZLOC(IOS%_WRITEVBLK) OR
- ZLOC(IOS%_NOFORMAT)), IOSB,... RECORD, ZVAL(LENGTH),...)
IF (I NE ZLOC(SS%_NORMAL)) THEN
TYPE 100, I
END IF

C _____ Format statement
100 FORMAT(' QIO WRITE FUNCTION TO PACER FAILED, STATUS= ',Z8)

RETURN
END

```

```

C _____ Subroutine READ_TERMINATOR
C _____ This routine establishes the terminator
C _____ mask for PACER read function
SUBROUTINE READ_TERMINATOR

C _____ Set up storage
COMMON/MESSAGE/RECORD_STRING, TERM_MASK
INTEGER*2 LINE_FEED, CAR_RET, BYTEND, SHIFT
BYTE BYTEVAL, BYTEVAL1
CHARACTER RECORD_STRING*80, TERM_MASK*32, DUMYCHAR
EQUIVALENCE (DUMYCHAR, BYTEVAL)
DATA LINE_FEED, CAR_RET/'00BA'X, '00BD'X/

C _____ First for the eight bit line feed
BYTEND=LINE_FEED/8+1
SHIFT=LINE_FEED-(BYTEND-1)*8
BYTEVAL1=2**SHIFT

C _____ Now for the eight bit carriage return
BYTEND=CAR_RET/8+1
SHIFT=CAR_RET-(BYTEND-1)*8
BYTEVAL=2**SHIFT+BYTEVAL1
TERM_MASK(BYTEND:BYTEND)=DUMYCHAR

RETURN
END

```

```

C _____ Subroutine READ_PACER_RECORD
C _____ Reads a record from PACER
SUBROUTINE READ_PACER_RECORD

EXTERNAL SSS_NORMAL, IOS_READVBLK

C _____ Set up storage
COMMON/GID/CHANNEL2, LENGTH/MESSAGE/RECORD_STRING, TERM_MASK
INTEGER*4 SSSQIOW
INTEGER*2 CHANNEL2, LENGTH, CHAR_VALU, BIT_EIGHT, IOSB(4)
BYTE RECORD(80)
CHARACTER RECORD_STRING*80, TERM_MASK*32
EQUIVALENCE (RECORD(1), RECORD_STRING(1:1))
DATA BIT_EIGHT/7F'X/

C _____ Get record from PACER
I=SSSQIOW(, ZVAL(CHANNEL2), ZVAL(ZLOC(IOS_READVBLK)
), IOSB... RECORD, ZVAL(B1), ZVAL(10), TERM_MASK...)
IF (IOSB(1) NE ZLOC(SSS_NORMAL)) THEN
RECORD_STRING='e'
RETURN
END IF

C _____ Convert record to 7 bit ASCII code
LENGTH=IOSB(2)
DO I=1, LENGTH
CHAR_VALU=RECORD(I)
CHAR_VALU=IAND(CHAR_VALU, BIT_EIGHT)
RECORD(I)=CHAR_VALU
END DO

RETURN
END

C _____ Subroutine COMMAND
C _____ Processes a PACER command
SUBROUTINE COMMAND(STATEMENT, STAT_LEN, ANSWER, ANS_LEN, NREADS)

C _____ Set up storage
COMMON/GID/CHANNEL2, LENGTH/MESSAGE/RECORD_STRING, TERM_MASK
INTEGER*2 CHANNEL2, LENGTH, ANS_LEN, STAT_LEN, NREADS
CHARACTER RECORD_STRING*80, TERM_MASK*32, STATEMENT*80, ANSWER*80

C _____ Send command to PACER
RECORD_STRING=STATEMENT
LENGTH=STAT_LEN
CALL WRITE_PACER_RECORD

C _____ Read responses from PACER
DO J=1, NREADS
CALL READ_PACER_RECORD
END DO

C _____ Check if response is correct
IF (RECORD_STRING(1:ANS_LEN) NE ANSWER(1:ANS_LEN)) THEN
TYPE = 'ERROR OCCURED DURING EXECUTION OF PACER COMMAND'
TYPE = STATEMENT(1:STAT_LEN)
STOP
END IF

RETURN
END

C _____ Subroutine INISCALB
C _____ Initializes scaling variables
SUBROUTINE INISCALB

C _____ Specification statements
COMMON /INPUTPARAM/ THETA, IC, ZETA, OMEGAN
COMMON /FORCE/ STEP
COMMON /SCALMAX/ XM, XDM, XDDM

C _____ Initialize maximum values of X, XD, XDD
XM = 2 * STEP
XDM = STEP * OMEGAN
XDDM = STEP * OMEGAN ** 2

RETURN
END

```

C \_\_\_\_\_ Subroutine SETGAINB  
 C \_\_\_\_\_ Sets amplifier gain value for analog integrators  
 SUBROUTINE SETGAINB

C \_\_\_\_\_ Specification statements  
 COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN  
 COMMON /AMPLISCALB/ GAIN

C \_\_\_\_\_ Assign amplifier gain value depending on natural  
 C \_\_\_\_\_ undamped frequency (OMEGAN) and set gain value on  
 C \_\_\_\_\_ analog integrators  
 IF(OMEGAN.LE.1.0) THEN  
 GAIN = 1.0  
 CALL OSSECN(1ER)  
 ELSE IF(OMEGAN.LE.10.0) THEN  
 GAIN = 10.0  
 CALL OSSECF(1ER)  
 ELSE  
 GAIN = 100.0  
 CALL GSMSN(1ER)  
 END IF  
  
 RETURN  
 END

C \_\_\_\_\_ Subroutine ADCSETB  
 C \_\_\_\_\_ Assigns A/D channel numbers  
 SUBROUTINE ADCSETB

C \_\_\_\_\_ Specification statements  
 DIMENSION ADC(2), IADC(2)  
  
 COMMON /ADCONVER/ ADC, IADC, NADC

C \_\_\_\_\_ Assign A/D channel numbers  
 IADC(1) = 22  
 IADC(2) = 23

C \_\_\_\_\_ Establish how many A/D channels  
 NADC = 2  
  
 RETURN  
 END

C \_\_\_\_\_ Subroutine SETDCAB  
 C \_\_\_\_\_ Assigns DCA number, assigns DCA value and sets DCA's  
 C \_\_\_\_\_ on analog computer  
 SUBROUTINE SETDCAB

C \_\_\_\_\_ Specification statements  
 DIMENSION DCA(7), IDCA(7)  
  
 COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN  
 COMMON /AMPLISCALB/ GAIN  
 COMMON /FORCE/ STEP  
 COMMON /SCALMAX/ XM, XDM, XDDM

C \_\_\_\_\_ Assign DCA number  
 IDCA(1) = 15  
 IDCA(2) = 20  
 IDCA(3) = 25  
 IDCA(4) = 22  
 IDCA(5) = 27  
 IDCA(6) = 23  
 IDCA(7) = 28

C \_\_\_\_\_ Assign DCA values  
 DCA(1) = STEP\*(OMEGAN\*\*2)/(10 \*XDDM)  
 DCA(2) = 0.0  
 DCA(3) = 0.0  
 DCA(4) = XDDM/(GAIN\*XDM)  
 DCA(5) = XDM/(GAIN\*XM)  
 DCA(6) = -2 \*ZETA\*OMEGAN\*XDM/(10 \*XDDM)  
 DCA(7) = -(OMEGAN\*\*2)\*XM/(10 \*XDDM)

C \_\_\_\_\_ Establish how many DCA's used  
 NDCA = 7

C \_\_\_\_\_ Set DCA's on analog computer  
 CALL QWRPTR(DCA, IDCA, NDCA, 1, 1ER)  
  
 RETURN  
 END

```

C _____ Subroutine HILOOPB
C _____ Executes high-speed-loop
SUBROUTINE HILOOPB

C _____ Specification statements
INTEGER STARTIM(2), PRESENTIM(2), DATATIM(2)
INTEGER USER_GET_REALTIME

REAL LASTSAVTIM

DIMENSION ADC(2), IADC(2)
DIMENSION RESPONSE(1000), RESPNSD(1000), RESTIME(1000)

COMMON /TIM/ TIME, FINALLTIME, SAVINCTIM, LASTSAVTIM
COMMON /ADCONVER/ ADC, IADC, NADC
COMMON /CONSOLE/ NOCNLS
COMMON /SCALMAX/ XM, XDM, XDDM
COMMON /RESPNSDATA/ NPOINT, RESPONSE, RESTIME
COMMON /RESPNSDOT/ RESPNSD

EQUIVALENCE(XS, ADC(1))
EQUIVALENCE(XDS, ADC(2))

C _____ Type final solution time on terminal screen
TYPE *, 'Solution time = ', FINALLTIME, ' Sec'

C _____ Initialize saving time variable
TIMSAVE = 0.0

C _____ Put Analog computer in initial condition (IC) mode
CALL QINIT(NOCNLS)

C _____ Read the starting time of solution on VAX clock
MM = USER_GET_REALTIME(STARTIM)

C _____ Compute response data until final solution time is reached
NLOOP = 0
DO WHILE(TIME LT FINALLTIME)

C _____ Put analog computer in operate mode and read starting
C _____ time only in the second loop because the VAX takes more
C _____ time to execute the first loop
NLOOP = NLOOP + 1
IF(NLOOP EQ 2) THEN

C _____ Put Analog computer in operate (OP) mode
CALL QOPER(NOCNLS)

C _____ Read the starting time of solution on VAX clock
MM = USER_GET_REALTIME(STARTIM)

END IF

C _____ Read data from A/D converters
CALL GRBADS(ADC, IADC, NADC, IER)

C _____ Read present time of solution on clock
MM = USER_GET_REALTIME(PRESENTIM)

C _____ Descal A/D values
X = XS*XM
XD = XDS*XDM

C _____ Compute time difference from now to starting time
C _____ Computation is DATATIM = PRESENTIM - STARTIM
CALL SUBQUAD(PRESENTIM, STARTIM, DATATIM)

C _____ Convert DATATIM into seconds
TIME = TIMSAVE + DATATIM(1)/10000000

C _____ At every 200 seconds of solution time (TM), save
C _____ present time in variable TIMSAVE and re-initialize
C _____ the starting time. This is to overcome the
C _____ possibility for array DATATIM to get numbers much
C _____ larger than 2.0E9
IF(DATATIM(1)/10000000.0 GE 200.) THEN
TIMSAVE = TIME
STARTIM(1) = PRESENTIM(1)
STARTIM(2) = PRESENTIM(2)
END IF

```

```
C _____ Store response data and time data if time is past
C _____ * the last saved time plus the data storage sampling
C _____ period
      IF((TIME GE LASTSAVTIM+SAVINCTIM). AND. (NLOOP. GT. 1)) THEN
          NPOINT = NPOINT + 1
          RESPONSE(NPOINT) = X
          RESPONSD(NPOINT) = XD
          RESTIME(NPOINT) = TIME
          LASTSAVTIM = TIME
      END IF,
```

```
      END DO
```

```
C _____ Put Analog computer in IC mode
      CABL GINIT(NOCNLS)
```

```
      RETURN
      END
```

APPENDIX E

System C Documentation

Contents

- Subroutine Hierarchical Diagram
- Hierarchy
- Input-Process-Output Table of Subroutines
- Flowcharts
- Listings

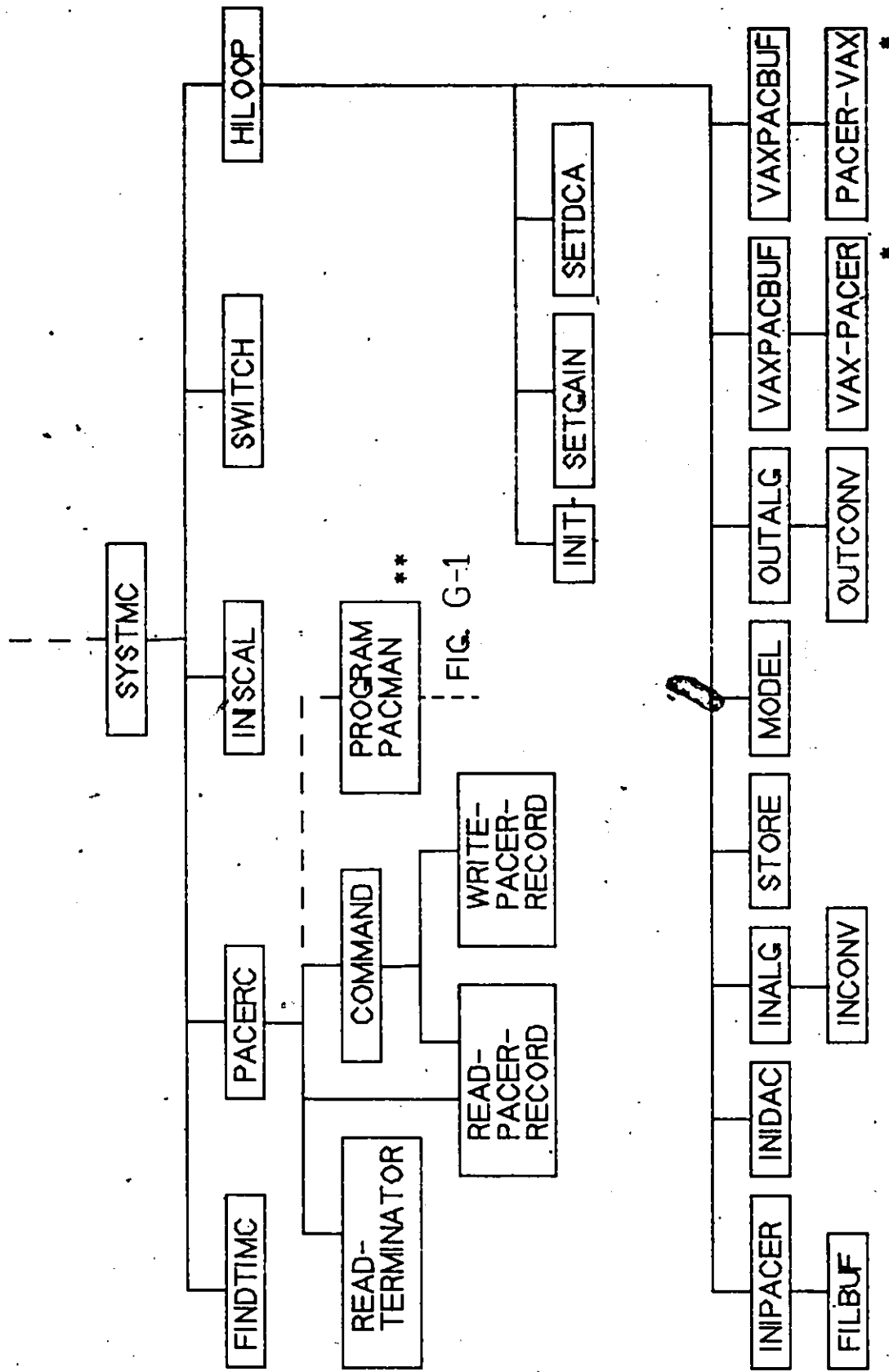


FIG. G-1

\* VAX-PACER AND PACER-VAX ARE VAX/HYBRID SYSTEM SUBROUTINES  
 \*\* PROGRAM PACMAN RUNS ON PACER COMPUTER

Figure E-1 : Subroutine hierarchical diagram of subroutine SYSTMTC

## Subroutine SYSTEMC Hierarchy

- |  |     |                       |
|--|-----|-----------------------|
| 1. Compute $T_F$ and $T_S$                               | ... | sub FINDTIMC          |
| 2. Prepare PACER computer to run PACER program PACMAN    | ... | sub <u>PACERC</u>     |
| 3. Initialize $x_M, x_M, x_M$                            | ... | sub INISCAL           |
| 4. Set value (0/1) to relay switches $R_K$ 's            | ... | sub SWITCH            |
| 5. Execute high-speed-loop                               | ... | sub <u>HILOOP</u>     |
|  |     |                       |
| 2. <u>Sub PACERC</u>                                     |     |                       |
|  |     |                       |
| 2.1 Assign a channel to PACER                            |     |                       |
| 2.2 Set up terminator mask for PACER read operation      | ... | sub READ-TERMINATOR   |
| 2.3 Obtain PACER monitor                                 | ... | sub READ-PACER-RECORD |
| 2.4 Load program PACMAN on PACER and start its execution | ... | sub COMMAND           |
|  |     |                       |
| 5. <u>Sub HILOOP</u>                                     |     |                       |
|  |     |                       |
| 5.1 Initialize time variables                            |     |                       |
| 5.2 Set amplifier gain $G$                               | ... | sub SETGAIN           |
| 5.3 Set DCA values                                       | ... | sub SETDCA            |
| 5.4 Set up PACER buffer                                  | ... | sub INIPACER          |

5.5 Assign initial conditions for D/A channels	...	sub INIDAC
5.6 Convert A/D data from integers to reals and descale data	....	sub INALC
5.7 Store response solution data	...	sub STORE
5.8 Compute model equation	...	sub MODEL
5.9 Scale D/A data and convert them from reals to integers	...	sub OUTALC
5.10 Send buffer to PACER	...	sub VAXPACBUF
5.11 Read buffer from PACER	...	sub PACVAXBUF
5.12 Communication message if end of solution was not a normal stop		

Input-Process-Output Table of Subroutines

Subroutine	Inputs	Process	Outputs
SYSTM	$\zeta, \omega_n, \pi, u, N_T, N_S$ $\theta, T_c$	Fig. E-2	DSR
FINDTMC	$\omega_n, \pi, N_T, N_S$	Eqs. 50, 51	$T_F, T_S$
INISCAL	$\omega_n, u$	Eqs. 66-68	$x_M, x_M, x_M$
SWITCH		$R=0, K=34, 39$ $K$	$R_{34}, R_{39}$
HILOOP	$T_F$	Fig. E-4	DSR
SETGAIN	$\theta, x_M, x_M, x_M$	Fig. E-5	$\theta$
SETDCA	$\theta, u, G, x^0, x^0$ $x_M, x_M, x_M$	Eqs. 73-78	$D_{30}, D_{31}, D_{32}$ $D_{35}, D_{36}, D_{37}$
INALG	$x_S, x_S, x_M, x_M$	Eqs. 79, 80	$x, x$
INCONV	$x_S, x_S, x_M, x_M$	Eqs. 87, 88, $x_M = 1.5x_M$ $x_M = 1.5x_M$	$x_S, x_S, x_M, x_M$
STORE	$T_S, x, t^J, T_c$	Fig. E-6	DSR
MODEL	$\omega_n, \zeta, u, x, x$	Equ. 13	$x$
OUTALG	$x, x, x_M, x_M$	Eqs. 83, 84	$x_S, x_S$
OUTCONV	$x_S, x_S, x_M, x_M$	Eqs. 85, 86, $x_M = 1.5x_M$ $x_M = 1.5x_M$	$x_S, x_S, x_M, x_M$

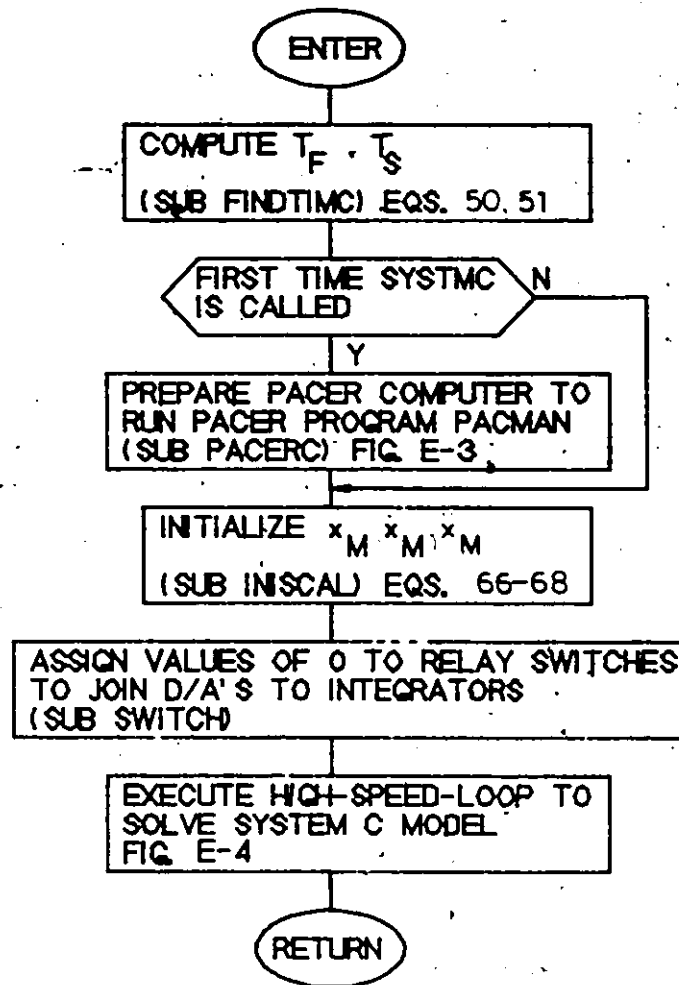


Figure E-2 : Subroutine SYSTMTC flowchart

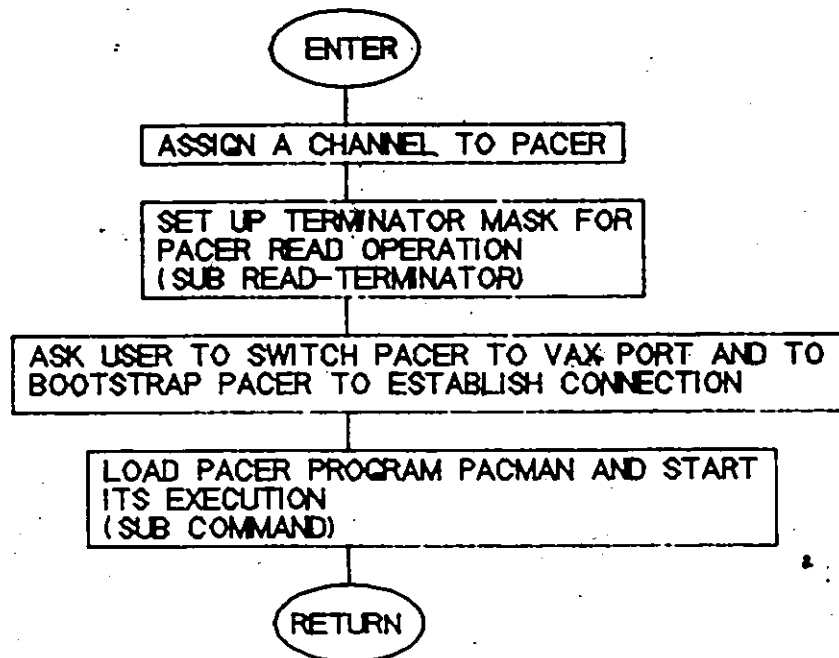


Figure E-3 : Subroutine PACERC flowchart

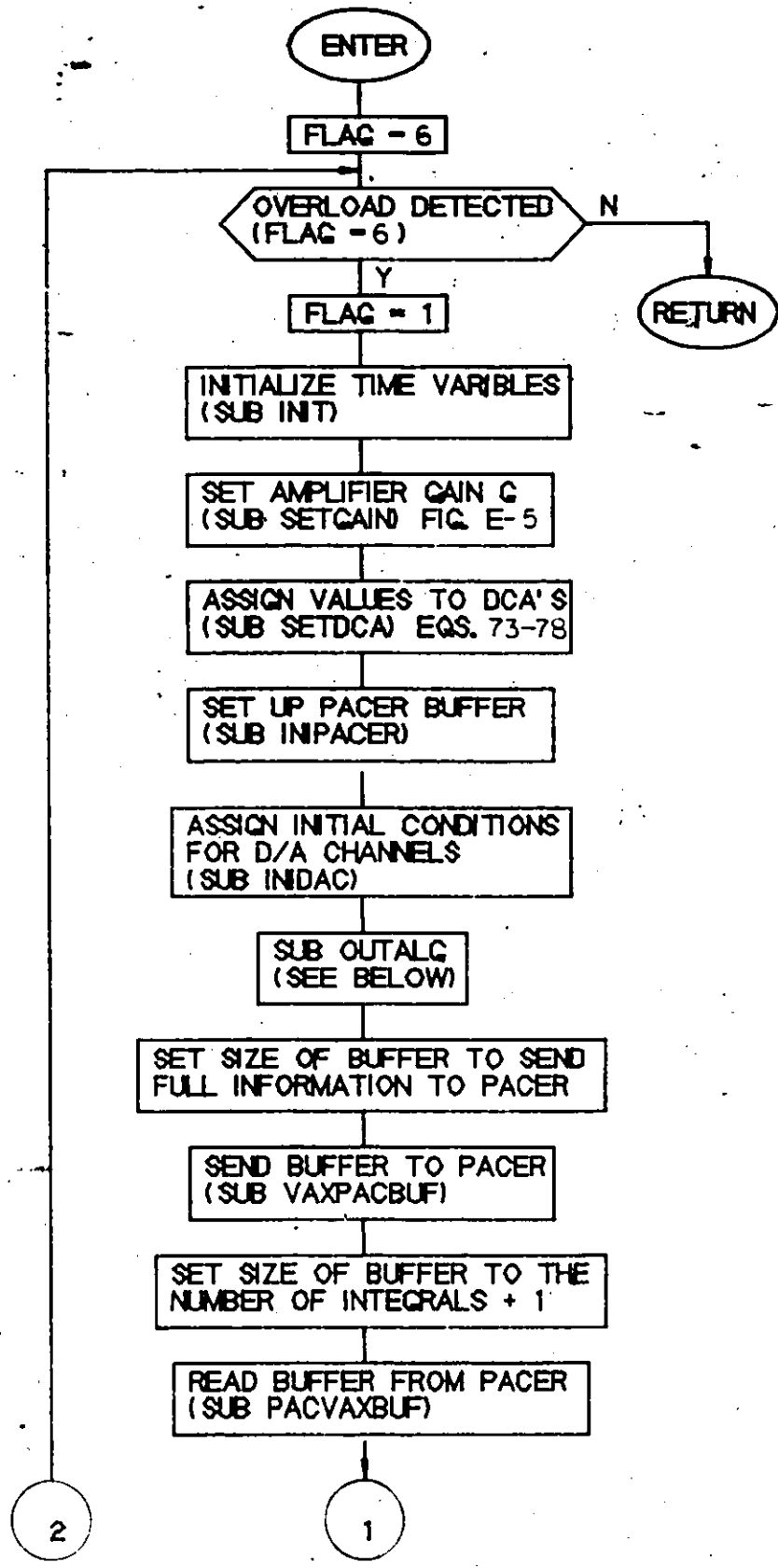


Figure E-4 : Subroutine HILOOP flowchart

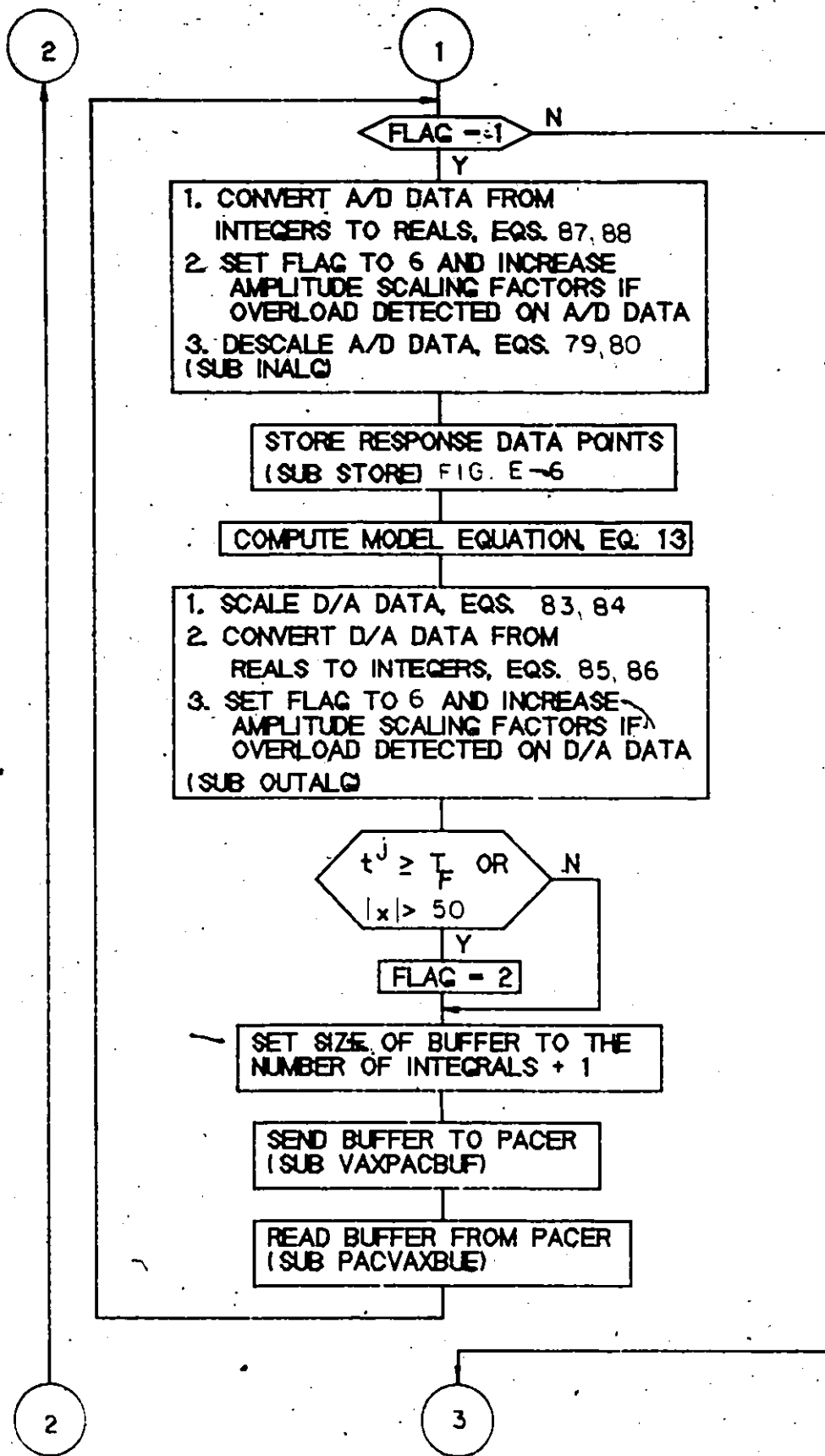


Figure E-4 : (cont'd)

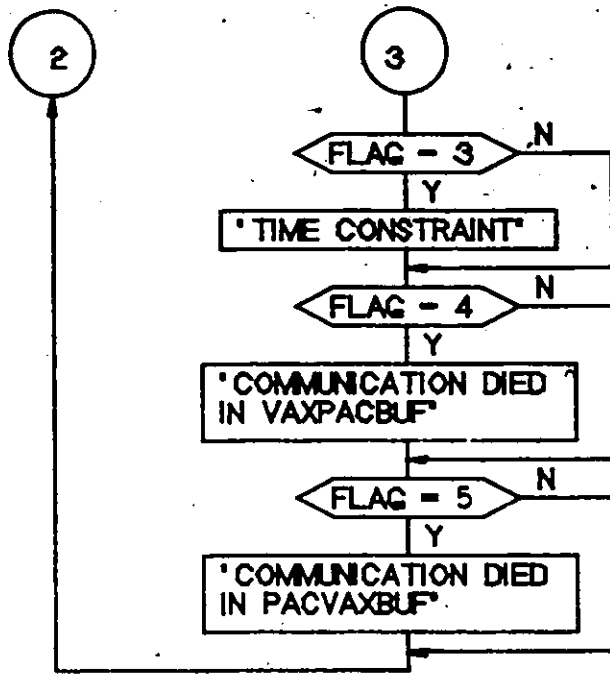


Figure E-4 : (End)

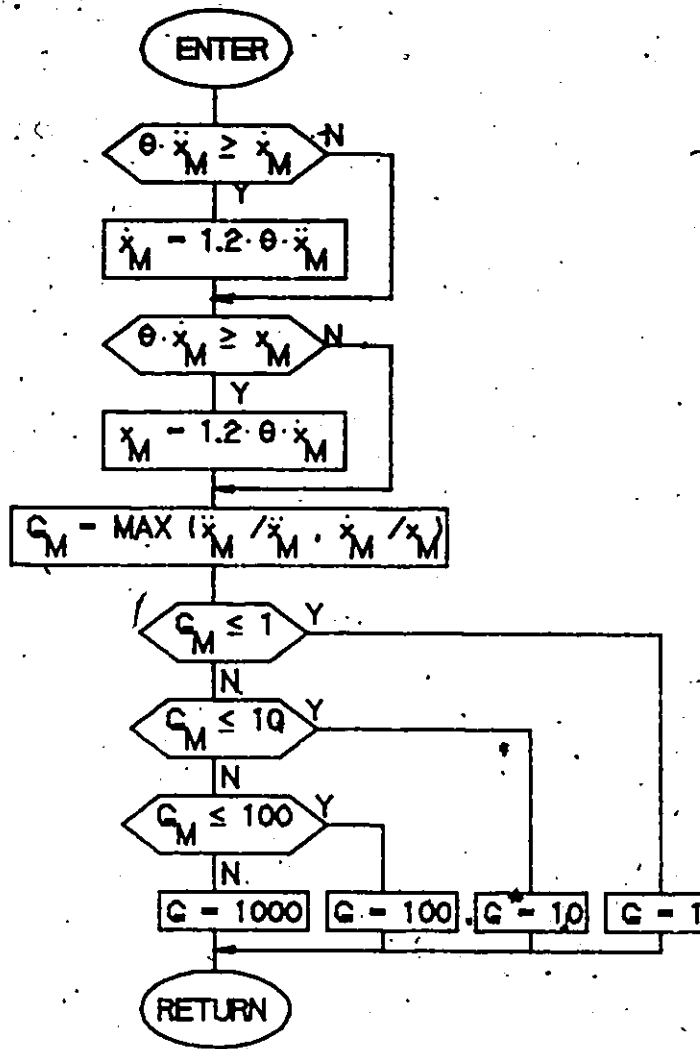


Figure E-5 : Subroutine SETGAIN flowchart

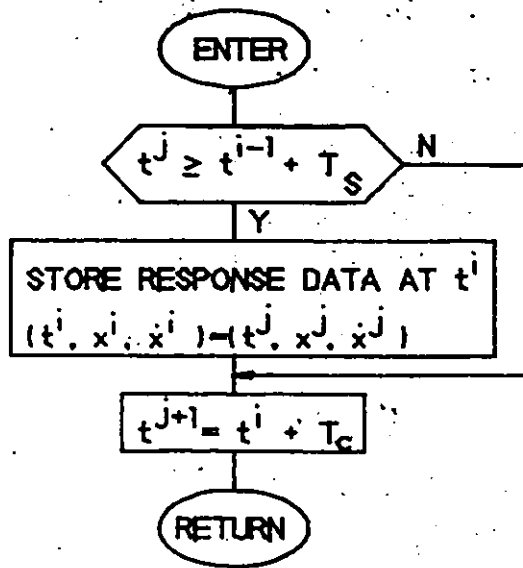


Figure E-6 : Subroutine STORE flowchart

```

C _____ Subroutine SYSTM
C _____ Computes response data points for the sampled-data
C _____ system (Hybrid computer)
SUBROUTINE SYSTM

C _____ Specification statements
LOGICAL FIRSTRUNB, FIRSTRUNC

COMMON /FIRSTRUN/-FIRSTRUNB, FIRSTRUNC

C _____ Start PACER program PACMAN the first time subroutine
C _____ SYSTM is called or if subroutine SYSTM has been
C _____ called in the same main program run
CALL SETUP_DR11B
IF (FIRSTRUNC) THEN
  CALL PACERC
END IF

C _____ Compute final solution time and data storage sampling period
CALL FINDTIM

C _____ Initialize scaling variables
CALL INISCAL

C _____ Assign values to relay switches (0/1) to define
C _____ the circuit on analog patchboard
CALL SWITCH

C _____ Execute high-speed-loop to solve System C model
CALL HILOOP

CALL RELEASE_DR11B

RETURN
END

C _____ Subroutine FINDTIM
C _____ Computes final solution time for a fixed number (NT) of cycles
C _____ and computes data storage sampling period
SUBROUTINE FINDTIM

C _____ Specification statements
REAL LASTSAVTIM

COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /CONSTANTS/ XF, PI
COMMON /NUMTIM/ NT, NS
COMMON /TIM/ TIME, FINALLTIME, SAVINCTIM, LASTSAVTIM

C _____ Compute final solution time
FINALLTIME = (NT*2 *PI)/OMEGAN

C _____ Compute data storage sampling period
SAVINCTIM = (2 *PI)/(NS*OMEGAN)

RETURN
END

C _____ Subroutine PACERC
C _____ Loads program PACMAN on PACER and starts its execution
C _____ to enable VAX/HYBRID runing for System C
SUBROUTINE PACERC

C _____ Specification statements
EXTERNAL SS%_NORMAL
INTEGER*4 SYS%ASSIGN, SYS%ALLOC
INTEGER*2 CHANNEL2, LENGTH
CHARACTER RECORD_STRING*80, TERM_MASK*32

COMMON/GIO/CHANNEL2, LENGTH/MESSAGE/RECORD_STRING, TERM_MASK

C _____ Assign a channel to PACER
I=SYS%ASSIGN('PACER100', CHANNEL2,.)
IF (I.NE.XLOC(SS%_NORMAL)) THEN
  TYPE 100, I
END IF

C _____ Set up terminator mask for PACER read operation
CALL READ_TERMINATOR

```

```

C Give instructions to user on how to obtain PACER monitor
TYPE * 'Switch PACER to VAX port and press (RETURN)'
ACCEPT *
TYPE *
TYPE * 'Bootstrap PACER to establish connection'
TYPE * '(message when connection established);'
CALL READ_PACER_RECORD
IF (RECORD_STRING(1:2) EQ 'M_') THEN
  TYPE *
  TYPE * '          * PACER CONNECTION ESTABLISHED *'
END IF

```

```

C Load PACER program (PACMAN) and start execution
CALL COMMAND('WL.PACMAN,21' ,12,'LD' ,2.6)
CALL COMMAND('BR.,60000,65000' ,15,' ' ,0.3)
CALL COMMAND('EG,1000' ,7,' ' ,0.2)

TYPE *
TYPE * '          * VAX/PACER NOW RUNNING *'
TYPE *

```

```

C Format statement
100 FORMAT(' CANNOT ASSIGN A CHANNEL TO PACER. STATUS = ',ZB)

RETURN
END

```

```

C Subroutine INISCAL
C Initialises scaling variables
SUBROUTINE INISCAL

```

```

C Specification statements
COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /FORCE/ STEP
COMMON /SCALMAX/ XM, XDM, XDDM

```

```

C Initialize maximum values of X, XD and XDD.
C Set XM smaller for a large damping for better scaling
IF(ZETA GE. 1.0) THEN
  XM = 1.2*STEP
ELSE
  XM = 1.2*(2.*STEP)
END IF

XDM = 1.2*(STEP*OMEGAN)
XDDM = 1.2*(STEP*OMEGAN**2.)

RETURN
END

```

```

C Subroutine SWITCH
C Assigns values to relay switches (0/1) to define
C the circuit on analog patchboard For System C.
C every switches are opened (0) to connect every D/A's
C to the integrators
SUBROUTINE SWITCH

```

```

C Specification statements
INTEGER*2 RELAY(15)

```

```

COMMON /RELAYCHANL/ RELAY

```

```

C Subroutine statements
DO I=1,15
  RELAY(I) = 0
END DO

RETURN
END

```

```

C _____ Subroutine HILOOP
C _____ Executes high-speed-loop
SUBROUTINE HILOOP

C _____ Specification statements
REAL LASTSAVTIM
INTEGER*2 MAXINT, NUMINT
INTEGER*4 LINK_BLOCK(3), IERR
INTEGER*2 OUT_SIZE, IN_SIZE, OUT_BUFFER(256), IN_BUFFER(256)
INTEGER*2 FLAG, CHANNEL, END_BLOCK

COMMON /DRIB_BUF/ LINK_BLOCK, OUT_SIZE, IN_SIZE,
OUT_BUFFER, IN_BUFFER, IERR, CHANNEL,
END_BLOCK
COMMON /NUMINTGRL/ NUMINT, MAXINT
COMMON /FUNCTIONS/ X, XD, XDD
COMMON /FLG/ FLAG
COMMON /TIM/ TIME, FINALTIME, SAVINCTIM, LASTSAVTIM

C _____ Type final solution time on terminal screen
TYPE *, 'Solution time =', FINALTIME, ' Sec'

C _____ Execute high-speed-loop as often as there is an overload
C _____ detected
FLAG = 6
DO WHILE(FLAG EQ 6),

C _____ Set FLAG to 1 to indicate to PACER that data
C _____ will be transmitted
FLAG = 1

C _____ Initialize constants
CALL INIT

C _____ Determine amplifier gain value for analog integrators
CALL SETGAIN

C _____ Assign values to DCA's
CALL SETDCA

C _____ Set up BUFFER to send to PACER and start PACER program
CALL INIPACER

C _____ Assign initial conditions for D/A channels
CALL INIDAC

C _____ Scale D/A data and convert real values to scaled fractions
C _____ before sending them to PACER
CALL OUTALG

C _____ Set size of buffer to send the full information
C _____ to PACER
OUT_SIZE = 5*MAXINT + 4

C _____ Send BUFFER to PACER
CALL VAXPACBUF

C _____ Set size of buffer to the number of integrals + 1
IN_SIZE = NUMINT + 1

C _____ Read BUFFER from PACER
CALL PACVXIBUF

C _____ Execute high-speed-loop while FLAG is 1
DO WHILE(FLAG EQ 1)

C _____ Convert PACER values from scaled fractions
C _____ to real values and descale A/D data
CALL INALG

C _____ Store response data points and increment time
C _____ variable
CALL STORE

C _____ Compute model equation
CALL MODEL

C _____ Scale D/A data and convert real values to scaled
C _____ fractions before sending them to PACER
CALL OUTALG

```

```

C _____ Test if time has reached final solution time
C _____ or if response data are getting to large and set
C _____ FLAG to 2 to indicate a normal stop of the solution
      IF((TIME.GT.FINALTIME).OR.(X.GT.500.).OR.
        (X.LT.-500.)) THEN
          FLAG = 2
        END IF

C _____ Set size of buffer to the number of integrals + 1
      OUT_SIZE = NUMINT + 1

C _____ Send BUFFER to PACER
      CALL VAXPACBUF

C _____ Set size of buffer to the number of integrals + 1
      IN_SIZE = NUMINT + 1

C _____ Read BUFFER from PACER
      CALL PACVAXBUF

      END DO

C _____ The value of FLAG=3 comes from the PACER program. It means
C _____ that the high-speed-loop took more time than required time
C _____ of computation (TC)
      IF(FLAG.EQ.3) THEN
        TYPE *
        TYPE *      ***** TIME CONSTRAINT *****
        TYPE *

C _____ The value of FLAG=4 comes from subroutine VAXPACBUF.
C _____ The value of FLAG=5 comes from subroutine PACVAXBUF.
C _____ It means that for some unknown exact reason, the buffer
C _____ cannot be sent to PACER or read from PACER
      ELSE IF(FLAG.EQ.4 OR FLAG.EQ.5) THEN
        TYPE *
        TYPE *      ***** COMMUNICATION DIED IN VAX TO PACER *****
        TYPE *      ***** OR PACER TO VAX TRANSFER. *****
        TYPE *

      END IF

      END DO

      RETURN
      END

```

```

C _____ Subroutine INIT
C _____ Initializes constants
      SUBROUTINE INIT

C _____ Specification statements
      REAL LASTSAVTIM

      DIMENSION RESPONSE(1000), RESTIME(1000)

      COMMON /TIM/ TIME, FINALTIME, SAVINCTIM, LASTSAVTIM
      COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME

C _____ Initialize response data pointer
      NPOINT = 0

C _____ Initialize time variable
      TIME = 0.0

C _____ Initialize to a very small value, the variable
C _____ representing the last time data that has been stored
      LASTSAVTIM = -1.0E30

      RETURN
      END

```

```

C _____ Subroutine SETGAIN
C _____ Determines amplifier gain value C for analog integrators
SUBROUTINE SETGAIN

C _____ Specification statements
INTEGER*2 GAIN

COMMON /SCALMAX/ XM, XDM, XDDM
COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /AMPLISCAL/ GAIN, GAINA

C _____ Adjust XM and XDM if compensation DCA's are overscaled
IF(THETA*XDDM GE XDM) THEN
  XDM = 1 2*THETA*XDDM
END IF

IF(THETA*XDM GE XM) THEN
  XM = 1 2*THETA*XDM
END IF

C _____ Determine maximum of ratios in front of integrators
GAINMAX = MAX(XDDM/XDM, XDM/XM)

C _____ Set amplifier gain depending on GAINMAX
IF(GAINMAX LE 1 0) THEN
  GAIN = 1
ELSE IF(GAINMAX LE 10 0) THEN
  GAIN = 10
ELSE IF(GAINMAX LE 100 0) THEN
  GAIN = 100
ELSE
  GAIN = 1000
END IF

RETURN
END

```

```

C _____ Subroutine SETDCA
C _____ Assign values to DCA's
SUBROUTINE SETDCA

C _____ Specification statements
INTEGER*2 GAIN

DIMENSION IDCA(6)
DIMENSION DCA(45)

COMMON /SCALMAX/ XM, XDM, XDDM
COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /AMPLISCAL/ GAIN, GAINA
COMMON /DCACHAN./ DCA, NDCA

C _____ Assign initial conditions on DCA's
DCA(1) = 0 0
DCA(4) = 0 0

C _____ Assign compensation factor values on DCA's
DCA(3) = THETA*XDM/XM
DCA(6) = THETA*XDDM/XDM

C _____ Assign values to DCA's in front of integrators
DCA(2) = -XDM/(XM*GAIN)
DCA(5) = -XDDM/(XDM*GAIN)

C _____ Assign the rest of the 45 DCA's to zero
DO I = 7, 45
  DCA(I) = 0 0
END DO

RETURN
END

```

```

C _____ Subroutine INIPACER
C _____ Initializes some constants and fills the BUFFER
SUBROUTINE INIPACER

C _____ Specification statements
INTEGER*2 MAXINT, NUMINT

DIMENSION DAC(15), ADC(15), DCA(45)

COMMON /NUMINTGRL/ NUMINT, MAXINT
COMMON /DACCHANL/ DAC, NDAC
COMMON /ADCHANL/ ADC, NADC
COMMON /DCACHANL/ DCA, NDCA

C _____ Set maximum number of integrators, set number of
C _____ integrators used for System C, set number of
C _____ D/A and A/D channels for this problem and set
C _____ number of DCA
MAXINT = 15
NUMINT = 2
NDAC = NUMINT
NADC = NUMINT
NDCA = 3*NUMINT

C _____ Fill the BUFFER to send to PACER
CALL FILBUF

RETURN
END

C _____ Subroutine FILBUF
C _____ Fills the BUFFER with variables that are to be
C _____ sent to PACER
SUBROUTINE FILBUF

C _____ Specification statements
INTEGER*2 MAXINT, NUMINT, GAIN, RELAY(15)
INTEGER*4 LINK_BLOCK(5), IERR
INTEGER*2 OUT_SIZE, IN_SIZE, OUT_BUFFER(256), IN_BUFFER(256)
INTEGER*2 CHANNEL, END_BLOCK

DIMENSION DCA(45)

COMMON /DR11B_BUF/ LINK_BLOCK, OUT_SIZE, IN_SIZE,
OUT_BUFFER, IN_BUFFER, IERR, CHANNEL,
END_BLOCK
COMMON /NUMINTGRL/ NUMINT, MAXINT
COMMON /DCACHANL/ DCA, NDCA
COMMON /AMPLISCAL/ GAIN, GAINA
COMMON /INPUTPARAM/ THETA, TC, ZETA, DMEGAN
COMMON /RELAYCHANL/ RELAY

C _____ Fill the BUFFER except for D/A and A/D channel values,
C _____ convert real variables DCA and TC to scaled fraction values
DO I=1,MAXINT
OUT_BUFFER(I+1) = 0
END DO
DO I=1,3*MAXINT
OUT_BUFFER(I+MAXINT+1) = ININT(DCA(I)*32768.)
END DO
OUT_BUFFER(4*MAXINT+2) = ININT(TC*32768.)
OUT_BUFFER(4*MAXINT+3) = NUMINT
OUT_BUFFER(4*MAXINT+4) = GAIN
DO I=1,MAXINT
OUT_BUFFER(I+4*MAXINT+4) = RELAY(I)
END DO

RETURN
END

C _____ Subroutine INIDAC
C _____ Assigns initial conditions for D/A channels
SUBROUTINE INIDAC

C _____ Specification statements
COMMON /FUNCTIONS/ X,XD,XDD

C _____ Assign initial conditions for D/A channels
XD = 0.0
XDD = 0.0

RETURN
END

```

C \_\_\_\_\_ Subroutine INALG  
 C \_\_\_\_\_ Converts PACER values from scaled fractions  
 C \_\_\_\_\_ to real values and descales A/D data  
 SUBROUTINE INALG

C \_\_\_\_\_ Specification statements  
 DIMENSION ADC(15)  
  
 COMMON /ADCHANL/ ADC, NADC  
 COMMON /SCALMAX/ XM, XDM, XDDM  
 COMMON /FUNCTIONS/ X, XD, XDD  
  
 EQUIVALENCE(ADC(1),XS)  
 EQUIVALENCE(ADC(2),XDS)

C \_\_\_\_\_ Convert PACER values from scaled fractions  
 C \_\_\_\_\_ to real values  
 CALL INCONV

C \_\_\_\_\_ Descale A/D data  
 X = XS\*XM  
 XD = XDS\*XDM

RETURN  
 END

C \_\_\_\_\_ Subroutine INCONV  
 C \_\_\_\_\_ Converts PACER values from scaled fractions  
 C \_\_\_\_\_ to real values and checks if one of these values are  
 C \_\_\_\_\_ overloading (>1) or close to  
 SUBROUTINE INCONV

C \_\_\_\_\_ Specification statements  
 INTEGER\*4 LINK\_BLOCK(5), IERR  
 INTEGER\*2 OUT\_SIZE, IN\_SIZE, OUT\_BUFFER(256), IN\_BUFFER(256)  
 INTEGER\*2 FLAG, CHANNEL, END\_BLOCK

DIMENSION ADC(15)

COMMON /DR11B\_BUF/ LINK\_BLOCK, OUT\_SIZE, IN\_SIZE,  
 OUT\_BUFFER, IN\_BUFFER, IERR, CHANNEL,  
 END\_BLOCK

COMMON /ADCHANL/ ADC, NADC  
 COMMON /SCALMAX/ XM, XDM, XDDM  
 COMMON /FLG/ FLAG

C \_\_\_\_\_ Convert A/D values  
 ADC(1) = FLOATI(IN\_BUFFER(2))/32768 0  
 ADC(2) = FLOATI(IN\_BUFFER(3))/32768 0

C \_\_\_\_\_ Set FLAG to 6 and adjust scaling factors if an  
 C \_\_\_\_\_ overload is detected  
 IF((ADC(1).GT 0 95) OR (ADC(1).LT -0 95)) THEN  
 XM = 1 5\*XM  
 FLAG = 6  
 END IF  
 IF((ADC(2).GT 0 95) OR (ADC(2).LT -0 95)) THEN  
 XDM = 1 5\*XDM  
 FLAG=6  
 END IF

RETURN  
 END

```

C _____ Subroutine STORE
C _____ Store response data points and increment time variable
SUBROUTINE STORE

C _____ Specification statements
REAL LASTSAVTIM

      DIMENSION RESPONSE(1000), RESPONSD(1000), RESTIME(1000)

      COMMON /FUNCTIONS/ X, XD, XDD
      COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
      COMMON /TIM/ TIME, FINALTIME, SAVINCTIM, LASTSAVTIM
      COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME
      COMMON /RESPONSDOT/ RESPONSD

C _____ Store response data and time data if time
C _____ is past the last saved-time plus the data-storage
C _____ sampling period
      IF (TIME GE LASTSAVTIM + SAVINCTIM) THEN
        NPOINT = NPOINT + 1
        RESPONSE(NPOINT) = X
        RESPONSD(NPOINT) = XD
        RESTIME(NPOINT) = TIME
        LASTSAVTIM = TIME
      END IF

C _____ Increment time variable
      TIME = TIME + TC

      RETURN
      END

```

```

C _____ Subroutine MODEL
C _____ Computes model equation
SUBROUTINE MODEL

C _____ Specification statements
COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /FORCE/ STEP
COMMON /FUNCTIONS/ X, XD, XDD

C _____ Compute equation
      XDD = -(OMEGAN**2) * X - 2 * ZETA * OMEGAN * XD
            + (OMEGAN**2) * STEP

      RETURN
      END

```

```

C _____ Subroutine OUTALC
C _____ Scales D/A data and converts real values to scaled fractions
C _____ before sending them to PACER
SUBROUTINE OUTALC

C _____ Specification statements
DIMENSION DAC(15)

      COMMON /FUNCTIONS/ X, XD, XDD
      COMMON /SCALMAX/ XM, XDM, XDDM
      COMMON /DACHANL/ DAC, NDAC

      EQUIVALENCE(XDAS, DAC(1))
      EQUIVALENCE(XDDAS, DAC(2))

C _____ Scale D/A data
      XDAS = -XD/XDM
      XDDAS = -XDD/XDDM

C _____ Convert real values to scaled fractions
C _____ before sending them to PACER and check for an
C _____ overload on analog computer
      CALL OUTCONV

      RETURN
      END

```

```

C_____ Subroutine OUTCONV
C_____ Converts real values to scaled fractions before
C_____ sending them to PACER and checks if one of these
C_____ values are overloading (>1) or close to
SUBROUTINE OUTCONV

C_____ Specification statements
INTEGER*4 LINK_BLOCK(5), IERR
INTEGER*2 OUT_SIZE, IN_SIZE, OUT_BUFFER(256), IN_BUFFER(256)
INTEGER*2 FLAG, CHANNEL, END_BLOCK

DIMENSION DAC(15)

COMMON /DR11B_BUF/ LINK_BLOCK, OUT_SIZE, IN_SIZE,
OUT_BUFFER, IN_BUFFER, IERR, CHANNEL,
END_BLOCK
COMMON /DACCHANL/ DAC, NDAC
COMMON /SCALMAX/ XM, XDM, XDDM
COMMON /FLG/ FLAG

C_____ Set FLAG to 6 and adjust scaling factors if an
C_____ overload is detected
IF(FLAG NE 6) THEN
  IF((DAC(1) GT 0.95) OR (DAC(1) LT -0.95)) THEN
    XDM = 1.5*XDM
    FLAG = 6
  END IF
  IF((DAC(2) GT 0.95) OR (DAC(2) LT -0.95)) THEN
    XDDM = 1.5*XDDM
    FLAG=6
  END IF
END IF

C_____ Convert D/A values if no overload detected
IF(FLAG NE 6) THEN
  OUT_BUFFER(2) = ININT(DAC(1)*32768.)
  OUT_BUFFER(3) = ININT(DAC(2)*32768.)
END IF

RETURN
END

```

```

C_____ Subroutine VAXPACBUF
C_____ Sends a block of data (OUT_BUFFER) to PACER
SUBROUTINE VAXPACBUF

C_____ Specification Statements
EXTERNAL SSS_NORMAL

INTEGER*4 LINK_BLOCK(5), IERR
INTEGER*2 OUT_SIZE, IN_SIZE, OUT_BUFFER(256), IN_BUFFER(256)
INTEGER*2 FLAG, CHANNEL, END_BLOCK

COMMON /DR11B_BUF/ LINK_BLOCK, OUT_SIZE, IN_SIZE,
OUT_BUFFER, IN_BUFFER, IERR, CHANNEL,
END_BLOCK
COMMON /FLG/ FLAG

C_____ Assign FLAG value to the first element of the buffer
OUT_BUFFER(1) = FLAG

C_____ Send BUFFER to PACER and check if PACER was ready
C_____ Set FLAG to 4 if no success
CALL VAX_PACER
IF(IERR NE XLOC(SSS_NORMAL)) THEN
  FLAG = 4
END IF

RETURN
END

```

C \_\_\_\_\_ Subroutine PACVAIBUF  
C \_\_\_\_\_ Reads a block of data (IN\_BUFFER) from PACER  
SUBROUTINE PACVAIBUF

C \_\_\_\_\_ Specification Statements  
EXTERNAL SSS\_NORMAL

INTEGER\*4 LINK\_BLOCK(5), IERR  
INTEGER\*2 OUT\_SIZE, IN\_SIZE, OUT\_BUFFER(256), IN\_BUFFER(256)  
INTEGER\*2 FLAG, CHANNEL, END\_BLOCK

COMMON /DR118\_BUF/ LINK\_BLOCK, OUT\_SIZE, IN\_SIZE,  
OUT\_BUFFER, IN\_BUFFER, IERR, CHANNEL,  
END\_BLOCK

COMMON /FLG/ FLAG

C \_\_\_\_\_ Read BUFFER from PACER and check if PACER was ready.  
C \_\_\_\_\_ Set FLAG to 5 if no success  
CALL PACER\_VAX  
IF (IERR NE. ZLOC(SSS\_NORMAL)) THEN  
FLAG = 5  
ELSE

C \_\_\_\_\_ Assign the first element of the buffer to FLAG  
FLAG = IN\_BUFFER(1)

END IF

RETURN  
END

APPENDIX F

System D Documentation

Contents

- Flowchart
- Listing

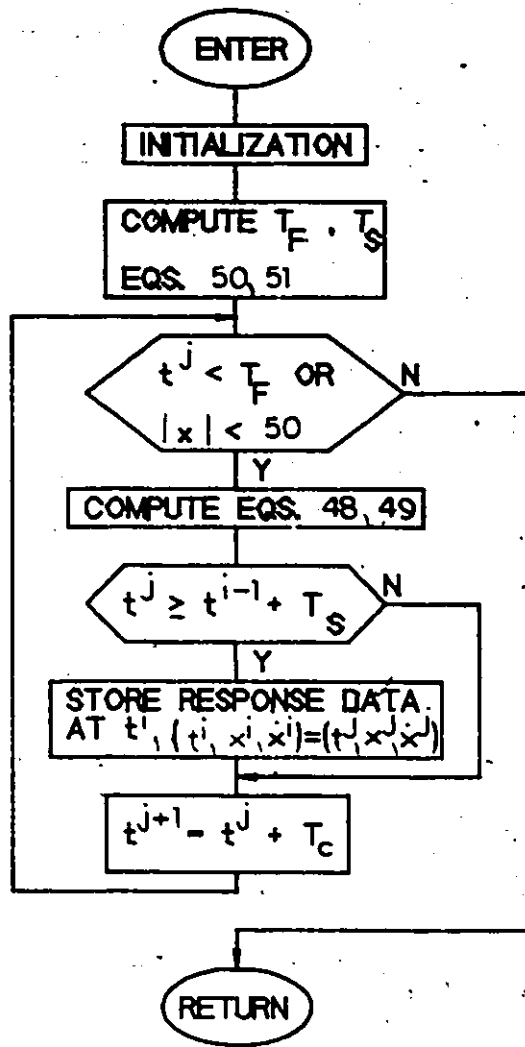


Figure F-1 : Subroutine SYSTMD flowchart

```

C _____ Subroutine SYSTND
C _____ Computes response data points for the
C _____ discrete-time equivalent to sampled-data system
SUBROUTINE SYSTND

C _____ Specification statements
DOUBLE PRECISION X, XD, X1, X2
DOUBLE PRECISION LASTSAVTIM, TIME
DIMENSION RESPONSE(1000), RESPOND(1000), RESTIME(1000)
DIMENSION X1(0:1), X2(0:1)

COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /CONSTANTS/ XF, PI
COMMON /FORCE/ STEP
COMMON /NUNTIM/ NT, NS
COMMON /RESPONSEDATA/ NPOINT, RESPONSE, RESTIME
COMMON /RESPONSDOT/ RESPOND

C _____ Initialization
STEP0 = 0
X = 0.0
XD = 0.0
X1(0) = 0.0
X2(0) = 0.0
X1(1) = 0.0
X2(1) = 0.0
NPOINT = 1
TIME = TC

C _____ Compute final solution time and data storage sampling
C _____ period and initialize last time data value that has
C _____ been stored
FINALTIME = (NT*2.*PI)/OMEGAN
SAVINCTIM = (2.*PI)/(NS*OMEGAN)
LASTSAVTIM = 0.0

C _____ Store first response data point and first time data
RESPONSE(NPOINT) = 0.0
RESPOND(NPOINT) = 0.0
RESTIME(NPOINT) = 0.0

C _____ Compute response data until final solution time or until
C _____ gets too large
DO WHILE((TIME.LE.FINALTIME).AND.(ABS(X).LT.500.))

C _____ Compute model equations
X = X1(1) + THETA*X2(1) + (TC - THETA)*X2(0)
XD = -THETA*(OMEGAN**2.)*X1(1) + (1 - 2.*THETA
-      *ZETA*OMEGAN)*X2(1) + (TC - THETA)
-      *(-OMEGAN**2.)*X1(0) - 2.*ZETA*OMEGAN
-      *X2(0) + STEP*(OMEGAN**2.)*THETA
-      + STEP*(TC - THETA)*(OMEGAN**2.)

C _____ Update temporary variables
STEP0 = STEP
X1(0) = X1(1)
X1(1) = X
X2(0) = X2(1)
X2(1) = XD

C _____ Store response data and time data if time is
C _____ past the last saved time plus the data storage
C _____ sampling period
IF((TIME.GE.LASTSAVTIM + SAVINCTIM) THEN
  NPOINT = NPOINT + 1
  RESPONSE(NPOINT) = X
  RESPOND(NPOINT) = XD
  RESTIME(NPOINT) = TIME
  LASTSAVTIM = TIME
END IF

C _____ Increment time variable
TIME = TIME + TC

END DO

RETURN
END

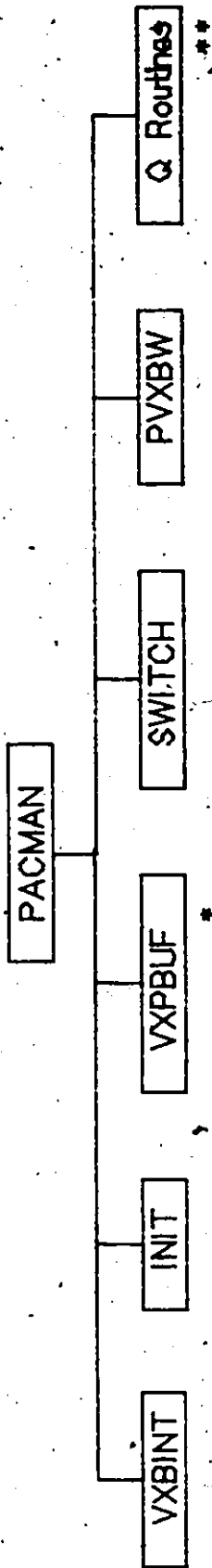
```

APPENDIX C

Program PACMAN Documentation

Contents

- Subroutine Hierarchical Diagram
- Flowchart
- Listings



• VXPBUF IS AN INTERRUPT SUBROUTINE

•• Q ROUTINES ARE PACER/HYBRID SYSTEM SUBROUTINES

Figure G-1 : Subroutine hierarchical diagram of program PACMAN

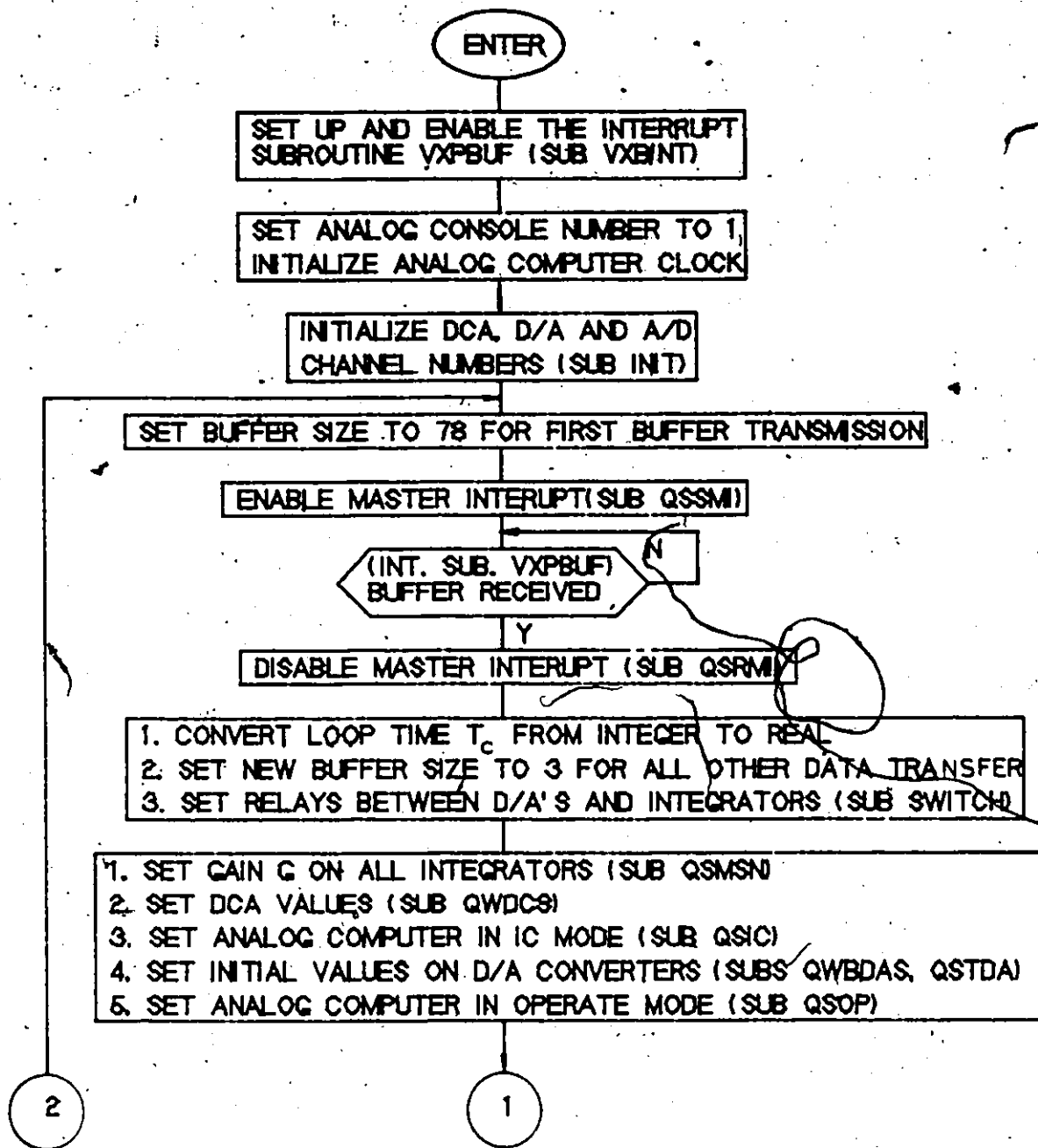


Figure G-2 : Program PACMAN flowchart

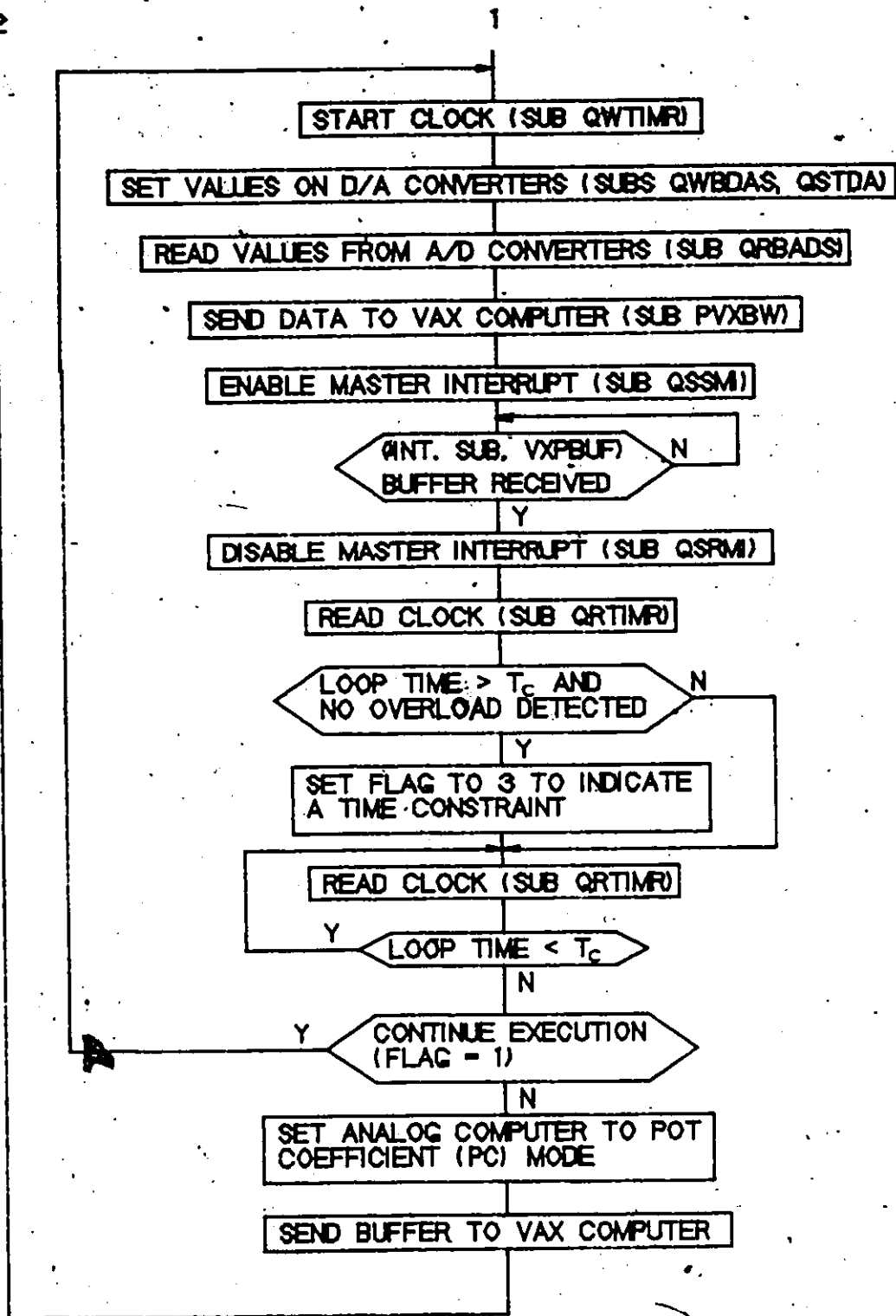


Figure G-2 : (End)

```

C _____ Program PACMAN
C _____ This program sets up the analog computer to run the System C
C _____ model, then within a loop, it receives data from the VAX
C _____ program, sets D/A converters, reads A/D converters
C _____ and sends data to the VAX. It also sets a constant high-
C _____ speed-loop time (TC)

C _____ Specification statements
INTEG ER FLAG, GAIN, RELAY(15), DUMMY(177)
SCALED FRACTION BUFFER, DCA, DAC, ADC
LOGICAL INTFLG

DIMENSION BUFFER(79)
DIMENSION IDCA(45), IDAC(15), IADC(15)
DIMENSION DCA(45), DAC(15), ADC(15)

COMMON /VAXPAC/ INTFLG, NUMBUF, FLAG, DAC, DCA, ITC,
NUMINT, GAIN, RELAY, DUMMY
COMMON /CHANEL/ IDCA, IDAC, IADC

EQUIVALENCE(BUFFER(1), FLAG)
EQUIVALENCE(DAC(1), ADC(1))

C _____ Set, up and enable the interrupt subroutine VXPBUF as
C _____ the only interrupt allowed on PACER
CALL VXBINT

C _____ Set an initial value for the analog computer clock
TSET=50000

C _____ Initialize the DCA channel numbers, the D/A channel
C _____ numbers and the A/D channel numbers
CALL INIT

C _____ Start program loop. The program starts from here when
C _____ subroutine SYSTM C is called the second time or more in
C _____ the same VAX program
5 CONTINUE

C _____ Set-BUFFER size to 79. The first buffer of data
C _____ transmitted from VAX to PACER contains a maximum of
C _____ 79 numbers
NUMBUF = 79

C _____ Set INTFLG .FALSE. to indicate that data have not
C _____ been transmitted from VAX to PACER. INTFLG is set .TRUE.
C _____ in subroutine VXPBUF when data are received
INTFLG = .FALSE.

C _____ Enable master interrupt and loop until the buffer is
C _____ received, then disable master interrupt. This means
C _____ that no interrupt can occur
CALL QSSM
10 IF( NOT INTFLG) GO TO 10
CALL QSRMI

C _____ Convert computation-time (loop-time) from integer to real
TC = FLOAT(ITC)/32768 0

C _____ Adjust TC such that the error of setting and reading the
C _____ clock is compensated
TC = TC - 0.00055

C _____ Set new buffer size for high-speed loop Buffer size is
C _____ the number of integrators used + 1
NUMBUF = NUMINT + 1

C _____ Set appropriate relays between D/A's and integrators
CALL SWITCH(RELAY)

C _____ Set amplifier gain on integrators
CALL SETGAN(GAIN)

C _____ Set DCA values on analog computer
CALL QWDCS(IDCA, DCA, 45, IER)

C _____ Set analog computer to initial condition mode
CALL QSIC( IER)

C _____ Set initial values on D/A converters
CALL QWBDAS(DAC, IDAC, 15, IER)
CALL GSTDA

C _____ Set analog computer in operate mode
CALL QSOP( IER)

```

```

C _____ Start high-speed-loop. Stop when the VAX program sends
C _____ a FLAG value other than 1 or when the loop-time is
C _____ larger than the required value TC

C _____ Set the timer on analog computer. The timer counts downward
CALL QWTIMR(TSET, IER)

20 CONTINUE

C _____ Set values on D/A converters. The array DAC is a
C _____ COMMON part of the array BUFFER
CALL GWBDAS(DAC, IDAC, IS, IER)
CALL GSTDA

C _____ Read values from A/D converters. The array ADC is a
C _____ COMMON part of the array BUFFER
CALL GRBADS(ADC, IADC, NUMINT, IER)

C _____ Send data to VAX through BUFFER
CALL PVXBW(BUFFER, NUMBUF)

C _____ Set INTFLC FALSE to indicate that data have not been
C _____ received from VAX
INTFLC = FALSE

C _____ Enable master interrupt and loop until the buffer is
C _____ received, then disable master interrupt.
CALL GSSMI
30 IF (NOT INTFLC) GO TO 30
CALL GSRMI

C _____ Read timer and test if there was a time-constraint
C _____ (i.e. if loop-time is greater than TC required) Test
C _____ also if the VAX program has detected an overload on
C _____ the analog computer. If there is a time-constraint
C _____ without an overload then set FLAG to 3 to indicate
C _____ this fact to the VAX program
CALL QRTIMR(TREAD, IER)
IF(((TSET-TREAD)/100000 GT TC) AND (FLAG NE 6)) FLAG=3

C _____ Loop until loop-time has reached the constant value TC
40 CONTINUE
CALL QRTIMR(TREAD, IER)
IF((TSET-TREAD)/100000 LT TC) GO TO 40

C _____ Set the timer on analog computer. The timer counts downward
CALL QWTIMR(TSET, IER)

C _____ End of loop
IF(FLAG EQ 1) GO TO 20

C _____ Set analog computer to Pot Coefficient (PC) mode
CALL GSPC(IER)

C _____ Write a message on PACER printer if there is a time constraint
IF(FLAG EQ 3) WRITE(6,100)

C _____ Send buffer to VAX with a FLAG value other than 1
C _____ indicating that program is stopping
CALL PVXBW(BUFFER, NUMBUF)

C _____ Go back to statement labeled 5 to be ready to start
C _____ a new solution for SYSTEM C
GO TO 5

C _____ Format Statement
100 FORMAT(30H ##### TIME CONSTRAINT #####)

END

```

C \_\_\_\_\_ Subroutine INIT  
C \_\_\_\_\_ Initializes the DCA channel numbers, the D/A channel  
C \_\_\_\_\_ numbers and the A/D channel numbers  
SUBROUTINE INIT

C \_\_\_\_\_ Specification statements  
DIMENSION IDCA(45), IDAC(15), IADC(15)  
COMMON /CHANEL/ IDCA, IDAC, IADC

C \_\_\_\_\_ Initialize DCA numbers  
DO 10 I=1,45,3  
IDCA(I) = ((I-1)/3)\*5 + 30  
IDCA(I+1) = ((I-1)/3)\*5 + 31  
IDCA(I+2) = ((I-1)/3)\*5 + 32  
10 CONTINUE

C \_\_\_\_\_ Initialize D/A Converter numbers  
DO 20 I=1,15  
IDAC(I) = 1  
20 CONTINUE

C \_\_\_\_\_ Initialize A/D converter numbers  
DO 30 I=1,15  
IADC(I) = 1  
30 CONTINUE

RETURN  
END

C \_\_\_\_\_ Subroutine SWITCH  
C \_\_\_\_\_ Sets appropriate relays between D/A converters and  
C \_\_\_\_\_ integrators  
SUBROUTINE SWITCH(RELAY)

C \_\_\_\_\_ Specification statement  
INTEGER RELAY(15), IRELAY(15)

C \_\_\_\_\_ Assign relay numbers  
DO 5 I=1,15  
IRELAY(I) = 34 + (I-1)\*5  
5 CONTINUE

C \_\_\_\_\_ Set relays  
DO 10 I=1,15  
IF (RELAY(I) EQ 0) CALL QWFRL(IRELAY(I), FALSE, IER)  
IF (RELAY(I) EQ 1) CALL QWFRL(IRELAY(I), TRUE, IER)  
10 CONTINUE

RETURN  
END

C \_\_\_\_\_ Subroutine SETGAN  
C \_\_\_\_\_ Sets gain on all integrators. The value of gain  
C \_\_\_\_\_ depends on integer value GAIN sent from VAX  
SUBROUTINE SETGAN(GAIN)

C \_\_\_\_\_ Specification statement  
INTEGER GAIN

C \_\_\_\_\_ Test for gain value and set it on integrators  
IF (GAIN EQ 1) CALL OSSECN( IER )  
IF (GAIN EQ 10) CALL OSSECF( IER )  
IF (GAIN EQ 100) CALL OSMSN( IER )  
IF (GAIN EQ 1000) CALL OSMSF( IER )

RETURN  
END

APPENDIX H

Program RESPLT Documentation

Contents

- Subroutine Hierarchical Diagram
- Flowcharts
- Listings

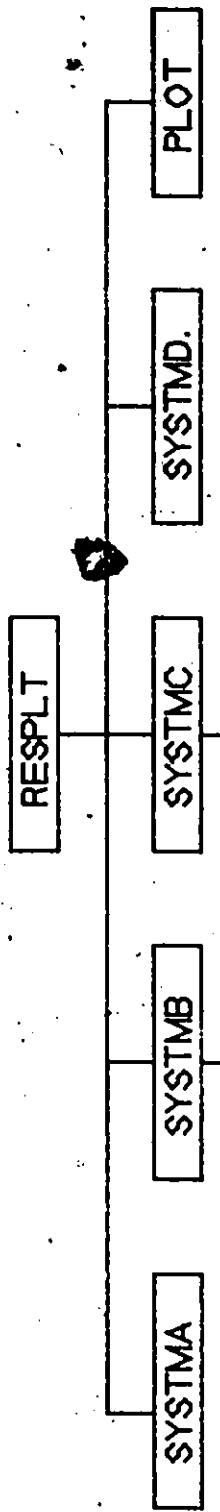


FIG. D-1

FIG. E-1

Figure H-1 : Subroutine hierarchical diagram of program RESPLT

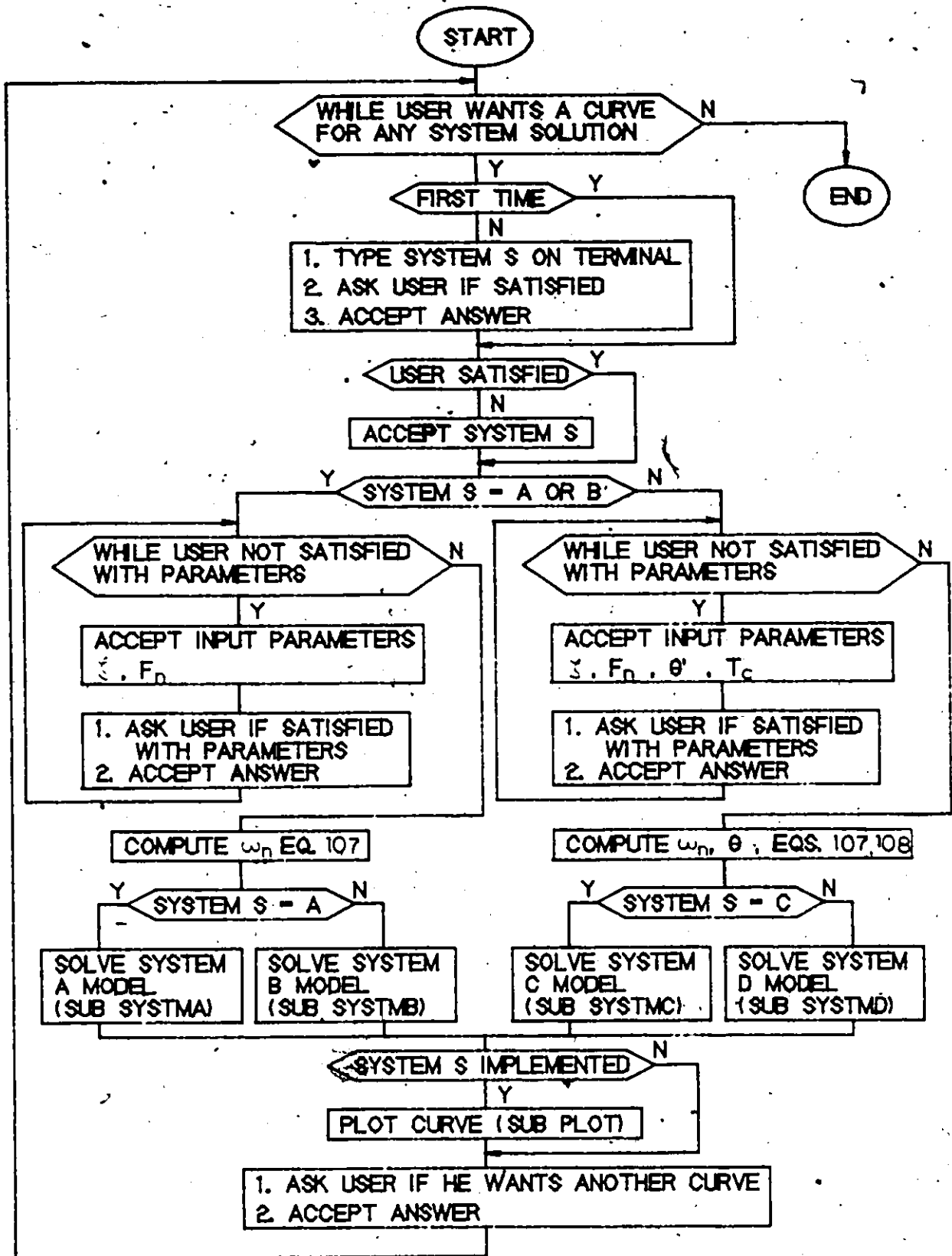


Figure H-2 : Program RESPLT flowchart

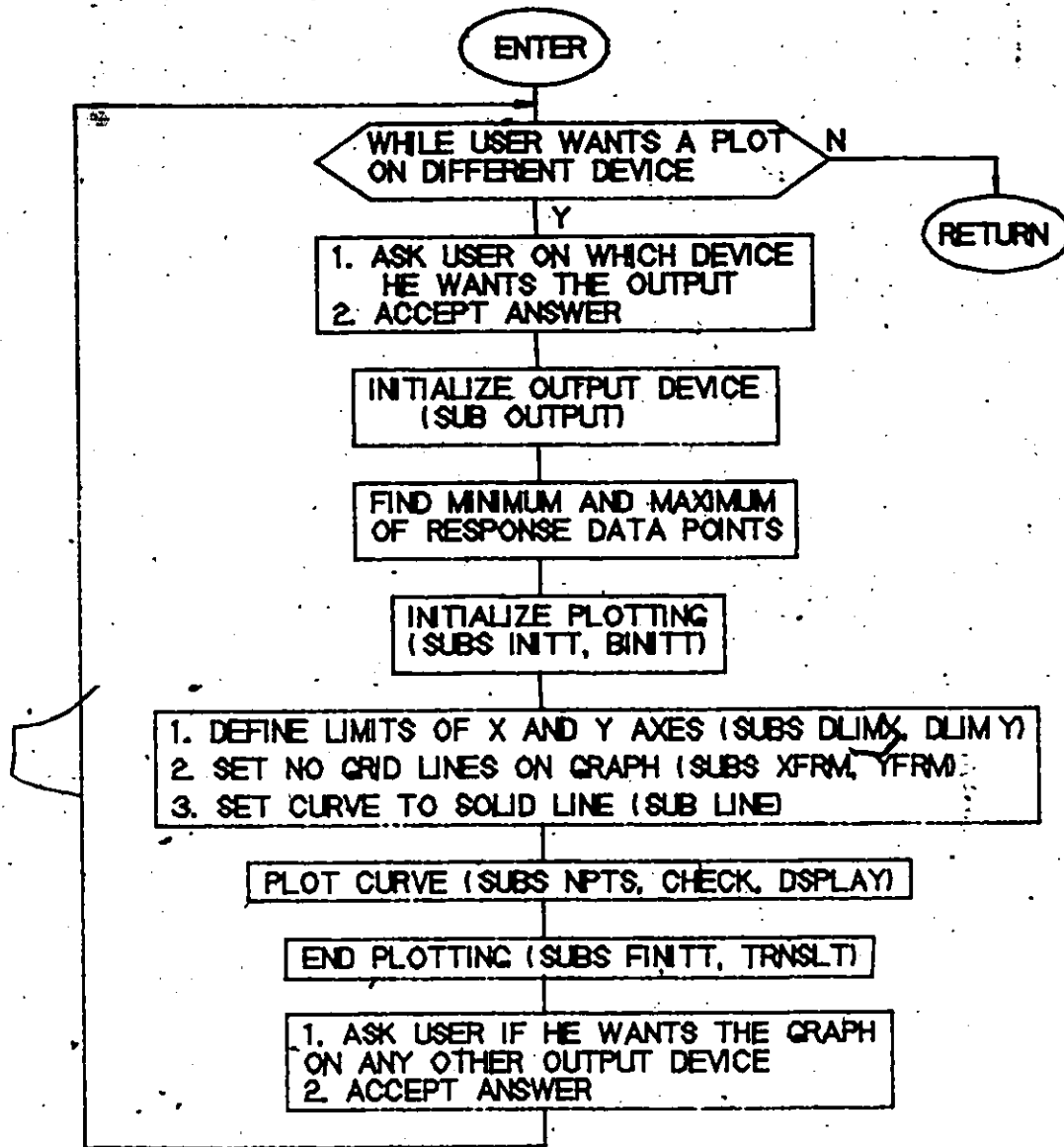


Figure H-3\*: Subroutine PLOT flowchart

```

C _____ Program RESPLT
C _____ Plots response curve of any system. System
C _____ letters and system input parameters are specified
C _____ interactively

C _____ Specification statements
CHARACTER ANSRMORE, INPUTOK, ANRSYS, SYSTM

LOGICAL FIRSTIME, CURVE, FIRSTRUNB, FIRSTRUNC

DIMENSION RESPONSE(1000), RESTIME(1000)

COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /CONSTANTS/ XF, PI
COMMON /FORCE/ STEP
COMMON /NURTIM/ NT, NS
COMMON /FIRSTRUN/ FIRSTRUNB, FIRSTRUNC
COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME

C _____ Open data set DSC DAT
OPEN(30, FILE='(GAC.ERR)DSC DAT', STATUS='OLD')

C _____ Initialize constants
PI=3.1415927
IF=1 0
STEP=1 0

C _____ Read number of cycles per solution and data storage
C _____ sampling period
READ(30,*) NT, NS

C _____ Initialize flags to indicate the first run of
C _____ System B or C
FIRSTRUNB = TRUE
FIRSTRUNC = TRUE

C _____ Plot as many curves as requested by user
CURVE= TRUE
FIRSTIME= TRUE
ANRSYS='N'
DO WHILE(CURVE)
  IMPLEMENTED= FALSE

C _____ If not the first curve, ask user if satisfied with
C _____ system entered. If not, accept system from user
  IF( NOT FIRSTIME) THEN
    TYPE *
    TYPE *, 'System = ', SYSTM
    TYPE *
    TYPE *, 'Satisfied with system ? (Y/N) '
    READ(6,100) ANRSYS
  END IF

C _____ Accept system letter from user if he is not satisfied or if
C _____ first time
  IF(ANRSYS EQ 'N') THEN
    TYPE *
    TYPE *, 'Enter System A, B, C or D '
    READ(6,200) SYSTM
  END IF

C _____ Test which system, accept input parameters
C _____ and compute response data for System A or B
  IF(SYSTM EQ 'A' OR SYSTM EQ 'B') THEN

C _____ Accept input parameters
  IMPLEMENTED= TRUE
  INPUTOK='N'
  DO WHILE(INPUTOK EQ 'N')
    TYPE *
    TYPE *, 'Enter input parameters '
    TYPE *, ' Damping Ratio, ZETA '
    TYPE *, ' Natural Frequency, Fn '
    READ(6,*) ZETA, FN
    TYPE *
    TYPE *, 'Satisfied with parameters ? (Y/N) '
    TYPE 300, ' ZETA= ', ZETA
    TYPE 300, ' Fn = ', FN
    READ(6,100) INPUTOK
  END DO

```

```

C_____ Compute response data for System A or System B
OMEGAN=2.*PI*FN
IF(SYSTH.EQ.'A') THEN
  CALL SYSTHA
ELSE
  CALL SYSTHB
  FIRSTRUNB = .FALSE.
  FIRSTRUNC = .TRUE.
END IF

C_____ Test which system, accept input parameters
and compute response data for System C or D
C_____ ELSE IF(SYSTH.EQ.'C'.OR.SYSTH.EQ.'D') THEN

C_____ Accept input parameters
IMPLEMENTED=.TRUE.
INPUTOK='N'
DO WHILE(INPUTOK.EQ.'N')
  TYPE *
  TYPE *, 'Enter input parameters : '
  TYPE *, '      Damping Ratio,      ZETA'
  TYPE *, '      Natural Frequency,  Fn'
  TYPE *, '      Compensation Factor, THETA PRIME'
  TYPE *, '      Computation Time,   Tc'
  READ(6,*) ZETA, FN, THETAP, TC
  TYPE *
  TYPE *, 'Satisfied with parameters ? (Y/N):'
  TYPE 400, '      ZETA=      ', ZETA
  TYPE 400, '      Fn =      ', FN
  TYPE 400, '      THETA PRIME= ', THETAP
  TYPE 400, '      Tc =      ', TC
  READ(6,100) INPUTOK
END DO

C_____ Compute response data for System C or System D
OMEGAN=2.*PI*FN
THETA=1.5*TC*THETAP
IF(SYSTH.EQ.'C') THEN
  CALL SYSTHC
  FIRSTRUNC = .FALSE.
  FIRSTRUNB = .TRUE.
ELSE
  CALL SYSTHD
END IF

C_____ Inform user that the system he entered is not implemented
ELSE
  TYPE *
  TYPE *, '**** System ', SYSTH, ' is not implemented ****'
END IF

C_____ Test if system has been implemented. If not,
do not plot
C_____ IF(IMPLEMENTED) THEN
  FIRSTIME=.FALSE.
  CALL PLOT
ELSE
  FIRSTIME=.TRUE.
END IF

C_____ Ask User if he wants plot of another curve
TYPE *
TYPE *, 'Output of another curve ? (Y/N):'
READ(6,100) ANSRMORE
IF(ANSRMORE.EQ.'N') THEN
  CURVE=.FALSE.
END IF

END DO

C_____ Format statements
100  FORMAT(A)
200  FORMAT(A)
300  FORMAT(A9,F7.3)
400  FORMAT(A16,F8.4)

END.

```

```

C _____ Subroutine PLOT
C _____ Plots response data points
SUBROUTINE PLOT

C _____ Specification statements
CHARACTER ANSRDEV1, DEVICE
LOGICAL MOREDEVIC

DIMENSION RESPONSE(1000), RESTIME(1000)

COMMON /RESPNSDATA/ NPOINT, RESPONSE, RESTIME

C _____ Plot curve while user wants output on any device
MOREDEVIC= .TRUE.
DO WHILE(MOREDEVIC)

C _____ Ask user for output device
TYPE *
TYPE *, 'Enter output device:'
TYPE *, '      Enter S. for VGT Screen'
TYPE *, '      P. for Line-Printer'
TYPE *, '      H. for HP Plotter'
READ(6,100) DEVICE

C _____ Initialize output device
IF(DEVICE.EQ.'P') THEN
  CALL OUTPUT('PRINTX', 'JKL', 0)
ELSE IF(DEVICE.EQ.'H') THEN
  CALL OUTPUT('HPPLOT', 'JKL', 0)
ELSE
  CALL OUTPUT('VGTERR', 'JKL', 0)
END IF

C _____ Find minimum and maximum of response data points
YMIN=1.0E30
YMAX=-1.0E30
DO I=1,NPOINT
  YMIN=MIN(YMIN, RESPONSE(I))
  YMAX=MAX(YMAX, RESPONSE(I))
END DO

C _____ Initialize plotting
CALL INITT(30)
CALL BINITT

C _____ If output is going on printer,
C _____ define location on paper and size of graph.
C _____ set density of tic marks, and set software
C _____ characters in order to adjust label sizes
IF(DEVICE.EQ.'P') THEN
  CALL SLIMX(100, 375)
  CALL SLIMY(50, 190)
  CALL YDEN(8)
  CALL SWCHAR(1)
  CALL PLCHAR(30, 50)
END IF

C _____ Define limits of X and Y axes
CALL DLIMX(0, 0, RESTIME(NPOINT))
CALL DLIMY(YMIN, (1.05)*YMAX)

C _____ Set no grid lines
CALL XFRM(2)
CALL YFRM(2)

C _____ Set line to solid
CALL LINE(0)

C _____ Plot curve
CALL NPTS(NPOINT)
CALL CHECK(RESTIME, RESPONSE)
CALL DISPLAY(RESTIME, RESPONSE)

C _____ End plotting
CALL FINITT(0, 0)
CALL TRNSLT(1)

```

```
C_____ Ask user if he wants output on any other device.  
TYPE *  
TYPE *. 'Any other output device ? (Y/N):'  
READ(6,100) ANSRDEVI  
IF(ANSRDEVI.EQ.'N') THEN *  
MOREDEVIC=.FALSE.  
END IF
```

```
END DO
```

```
C_____ Format statement  
100 FORMAT(A)
```

```
RETURN  
END
```

APPENDIX I

Program RESPONS Documentation

Contents:

- Subroutine Hierarchical Diagram
- Input-Process-Output Table of Subroutines
- Flowcharts
- Listings

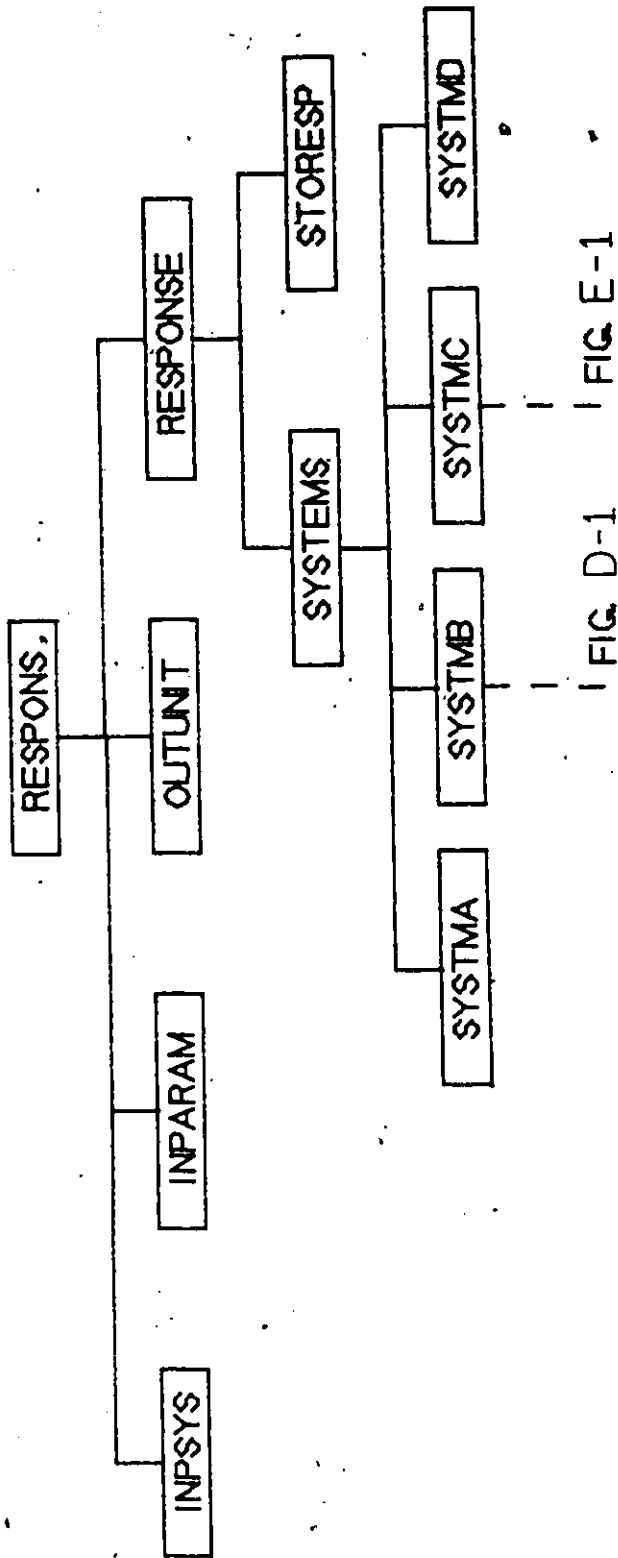


FIG. D-1 | FIG. E-1

Figure I-1 : Subroutine hierarchical diagram of program  
RESPONS

Input-Process-Output Table of Subroutines

Subroutine	Inputs	Process	Outputs
INPSYS	S	Interactivity	S
INPARAM	DSA, DSB, DSC, $\theta'$ i	Interactivity, Read files	DSA, DSB, DSC, $\theta'$ i
RESPONSE	S, DSA, DSB, $\pi$ , $\theta'$ i	Fig. I-3	DSRA, DSRB, DSRC 'i' DSRD 'i'

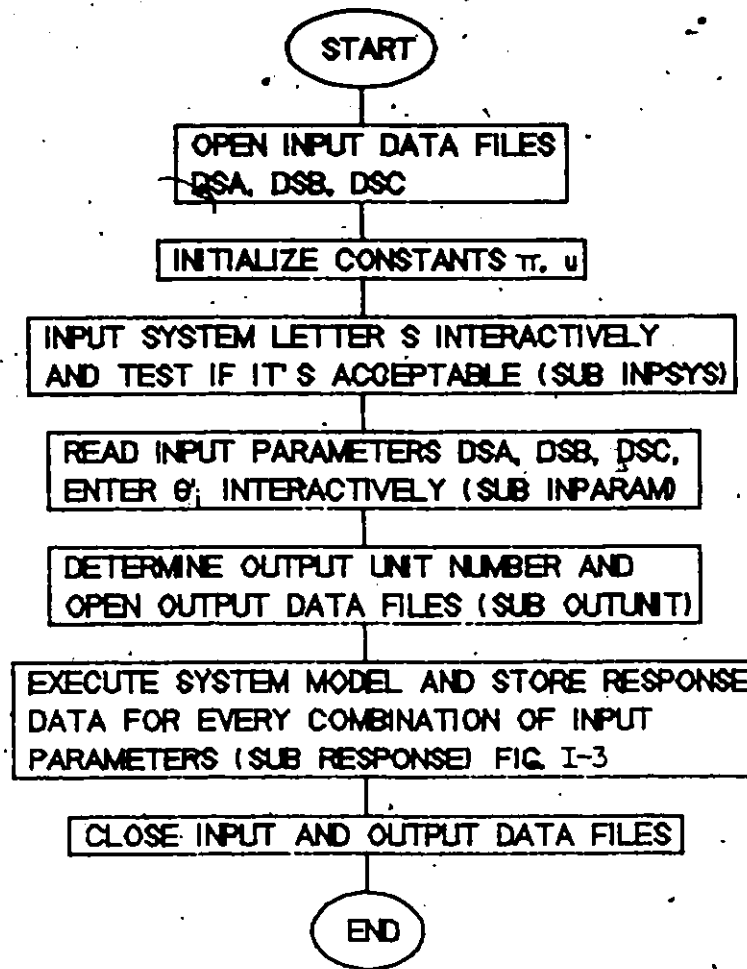


Figure I-2 : Program RESPONS flowchart

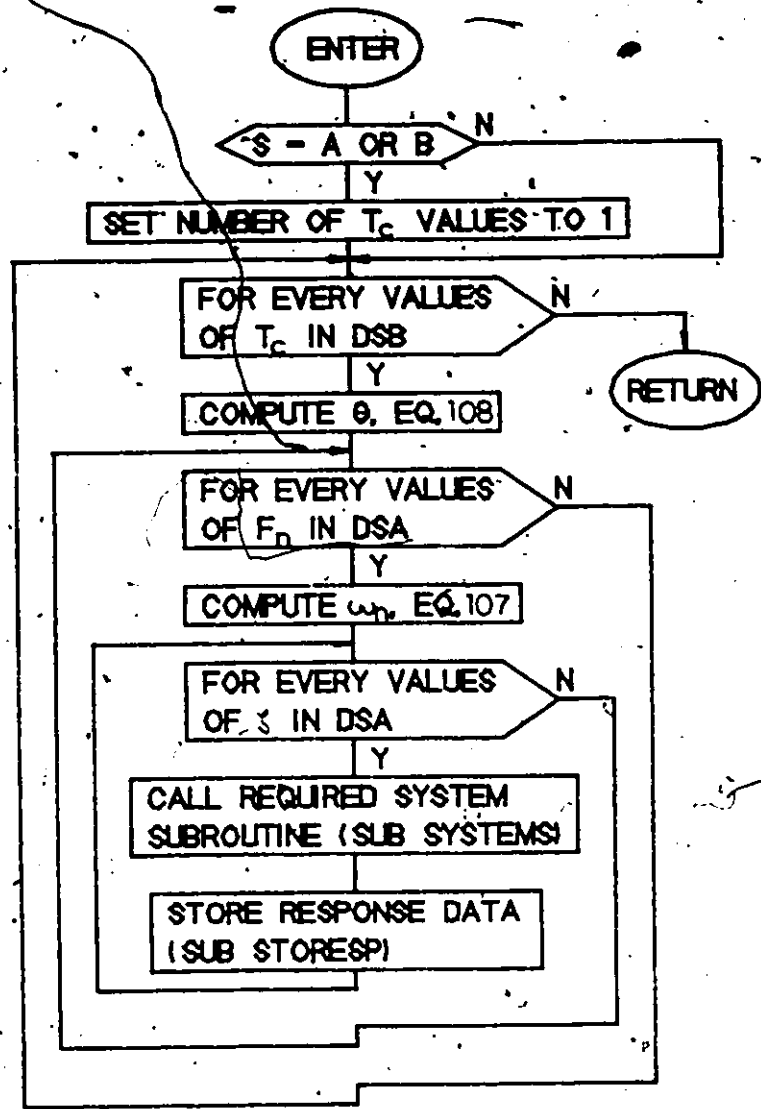


Figure I-3 : Subroutine RESPONSE flowchart

```

C _____ Program RESPONSE
C _____ This program executes a user specified system. It stores
C _____ response data for this system for every set of input
C _____ parameters contained in data sets DSA & DSB

C _____ Specification statements
LOGICAL FIRSTRUNB, FIRSTRUNC

COMMON /FIRSTRUN/ FIRSTRUNB, FIRSTRUNC
COMMON /CONSTANTS/ XF, PI
COMMON /FORCE/ STEP
COMMON /INPOINTER/ NUNTHETA

C _____ Initialize constants
PI = 3.1415927
STEP = 1.0

C _____ Initialize flags indicating the first run of Systems B and C
FIRSTRUNB = .TRUE
FIRSTRUNC = .TRUE

C _____ Input System letter interactively
CALL INPSYS

C _____ Open input parameter data files
OPEN(10, FILE='DSA.DAT', STATUS='OLD')
OPEN(20, FILE='DSB.DAT', STATUS='OLD')
OPEN(30, FILE='DSC.DAT', STATUS='OLD')

C _____ Read input parameters
CALL INPARAM

C _____ Determine output unit number and open output data files
CALL OUTUNIT

C _____ Execute System and store response for every set of input
C _____ parameters
CALL RESPONSE

C _____ Close data files
CLOSE(01)
CLOSE(02)
CLOSE(03)
CLOSE(04)
CLOSE(10)
CLOSE(20)
CLOSE(30)

END

```

```

C _____ Subroutine INPSYS
C _____ Inputs System letter interactively
SUBROUTINE INPSYS

C _____ Specification statements
CHARACTER SYSTM, ANRSYS

LOGICAL GOODSYS

COMMON /SYS/ SYSTM

C _____ Initialize system flag FALSE indicating that the
C _____ inputted system letter is not acceptable
GOODSYS = .FALSE

C _____ Accept System letter until it's a valid one and the user
C _____ is satisfied
DO WHILE (NOT GOODSYS)
  TYPE *, 'Enter System A, B, C OR D'
  READ(6,100) SYSTM
  IF (SYSTM EQ 'A' OR SYSTM EQ 'B' OR SYSTM EQ 'C' OR
    SYSTM EQ 'D') THEN
    GOODSYS = .TRUE
  TYPE *
  TYPE *, 'System = ', SYSTM
  TYPE *
  TYPE *, 'Satisfied with System?'
  READ(6,100) ANRSYS
  IF (ANRSYS EQ 'N') THEN
    GOODSYS = .FALSE
  END IF
ELSE

```

```

      TYPE *
      TYPE * '**** System ***.SYSTM.*** not implemented ****'
      END IF
      END DO

C_____ Format statement,
100  FORMAT(A)

      RETURN
      END

C_____ Subroutine INPARAM
C_____ Read the system's input parameters from files DSA & DSB
SUBROUTINE INPARAM

C_____ Specification statements
CHARACTER SYSTM, ANSRSYS
DIMENSION COMPENSATION(40), COMPUT_TIME(40)
DIMENSION FREQUENCY(40), DAMPING(40)

COMMON /SYS/ SYSTM
COMMON /NUMTIN/ NT, NS
COMMON /INPARAMS/ COMPENSATION, COMPUT_TIME,
                  FREQUENCY, DAMPING
COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
COMMON /INPOINTER/ NUMTHETA

C_____ Read number of cycles per solution and number of sampling
C_____ data per cycle
READ(30,*) NT, NS

C_____ Read system parameters (files DSA & DSB)
READ(10,*) NFREQ, (FREQUENCY(I), I=1,NFREQ)
READ(10,*) NDAMP, (DAMPING(I), I=1,NDAMP)
READ(20,*) NCOMP, (COMPENSATION(I), I=1,NCOMP)
READ(20,*) NTIME, (COMPUT_TIME(I), I=1,NTIME)

C_____ Enter the pointer for THETA_PRIME value
IF((SYSTM EQ 'C') OR (SYSTM EQ 'D')) OR
   (SYSREF EQ 'C') OR (SYSREF EQ 'D')) THEN
  TYPE *
  TYPE * 'Enter Theta Prime number where:'
  TYPE 100, 'Theta Prime number: ', (I, I = 1,NCOMP)
  TYPE 200, 'Theta Prime value: ', (COMPENSATION(I), I = 1,NCOMP)
  READ(6,*) NUMTHETA
END IF

C_____ Format Statements
100  FORMAT(A21,10(I3,4X))
200  FORMAT(A21,10(F5,3,2X))

      RETURN
      END

C_____ Subroutine OUTUNIT
C_____ Determines output unit number and opens output files
SUBROUTINE OUTUNIT

C_____ Specification statements
CHARACTER SYSTM

INTEGER SYSUNIT

COMMON /SYS/ SYSTM
COMMON /INPOINTER/ NUMTHETA
COMMON /UNIT/ SYSUNIT

C_____ Set output unit number and open appropriate output file
IF(SYSTM EQ 'A') THEN
  SYSUNIT = 1
  OPEN(01, FILE='DSRA.DAT', STATUS='UNKNOWN', FORM='UNFORMATTED')
ELSE IF(SYSTM EQ 'B') THEN
  SYSUNIT = 2
  OPEN(02, FILE='DSRB.DAT', STATUS='UNKNOWN', FORM='UNFORMATTED')

```

```

ELSE IF(SYSTH EQ 'C') THEN
  SYSUNIT = 3
  IF(NUMTHETA EQ 1) THEN
    OPEN(03.FILE='DSRC1.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 2) THEN
    OPEN(03.FILE='DSRC2.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 3) THEN
    OPEN(03.FILE='DSRC3.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 4) THEN
    OPEN(03.FILE='DSRC4.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 5) THEN
    OPEN(03.FILE='DSRC5.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  END IF
ELSE IF(SYSTH EQ 'D') THEN
  SYSUNIT = 4
  IF(NUMTHETA EQ 1) THEN
    OPEN(04.FILE='DSRD1.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 2) THEN
    OPEN(04.FILE='DSRD2.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 3) THEN
    OPEN(04.FILE='DSRD3.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 4) THEN
    OPEN(04.FILE='DSRD4.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 5) THEN
    OPEN(04.FILE='DSRD5.DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
  END IF
END IF
RETURN
END

```

C \_\_\_\_\_ Subroutine RESPONSE  
C \_\_\_\_\_ Executes required system for every combination of  
C \_\_\_\_\_ the appropriate input parameters  
SUBROUTINE RESPONSE

C \_\_\_\_\_ Specification statements  
CHARACTER SYSTM

```

DIMENSION COMPENSATION(40), COMPUT_TIME(40)
DIMENSION FREQUENCY(40), DAMPING(40)

```

```

COMMON /SYS/ SYSTM
COMMON /INPARAMS/ COMPENSATION, COMPUT_TIME,
FREQUENCY, DAMPING
COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
COMMON /CONSTANTS/ XF, PI
COMMON /INPUTPARAM/ THETA, TC, ZETA, OMEGAN
COMMON /INPOINTER/ NUMTHETA

```

C \_\_\_\_\_ Set number of Tc values to 1 if System A or B is involved  
IF(SYSTH EQ 'A' OR SYSTM EQ 'B') THEN  
 NTIME = 1  
 NUMTHETA = 1  
 COMPUT\_TIME(1) = 1.0  
END IF

C \_\_\_\_\_ Solve appropriate system for every combination of  
C \_\_\_\_\_ input parameters

```

THETA_PRIME = .COMPENSATION(NUMTHETA)
DO ITC = 1, NTIME
  TC = COMPUT_TIME(ITC)
  THETA = 1.5*TC*THETA_PRIME
  DO IFREQ = 1, NFREQ
    OMEGAN = 2.*PI*FREQUENCY(IFREQ)
    DO IZETA = 1, NDAMP
      ZETA = DAMPING(IZETA)

```

C \_\_\_\_\_ Call required system subroutine  
CALL SYSTEMS

C \_\_\_\_\_ Store response data  
CALL STORESP

```

END DO
END DO
END DO

```

```

RETURN
END

```

C \_\_\_\_\_ Subroutine SYSTEMS

C \_\_\_\_\_ Calls required system subroutine  
SUBROUTINE SYSTEMS

C \_\_\_\_\_ Specification statements  
CHARACTER SYSTM

LOGICAL FIRSTRUNB, FIRSTRUNC

COMMON /FIRSTRUN/ FIRSTRUNB, FIRSTRUNC  
COMMON /SYS/ SYSTM

C \_\_\_\_\_ Check required system, call its subroutine and set  
C \_\_\_\_\_ flags to indicate the first run of Systems B or C

```
IF(SYSTH.EQ.'A')THEN  
  CALL SYSTHA  
ELSE IF(SYSTH.EQ.'B')THEN  
  CALL SYSTHB  
  FIRSTRUNB = .FALSE.  
  FIRSTRUNC = .TRUE.  
ELSE IF(SYSTH.EQ.'C')THEN  
  CALL SYSTM C  
  FIRSTRUNC = .FALSE.  
  FIRSTRUNB = .TRUE.  
ELSE IF(SYSTH.EQ.'D')THEN  
  CALL SYSTM D  
END IF
```

RETURN  
END

C \_\_\_\_\_ Subroutine STORESP

C \_\_\_\_\_ Stores response data  
SUBROUTINE STORESP

C \_\_\_\_\_ Specification statements  
DIMENSION RESPONSE(1000), RESPONSD(1000), RESTIME(1000)

COMMON /RESPONSDATA/ NPOINT, RESPONSE, RESTIME  
COMMON /RESPONSDOT/ RESPONSD

C \_\_\_\_\_ Write response data in file numbered SYSUNIT  
WRITE(SYSUNIT) NPOINT, (RESPONSE(I), I=1,NPOINT),  
(RESTIME(I), I=1,NPOINT),  
(RESPONSD(I), I=1,NPOINT)

RETURN  
END

APPENDIX J

Program RMSERR Documentation

Contents

- Subroutine Hierarchical Diagram
- Input-Process-Output Table of Subroutines
- Flowcharts
- Listings

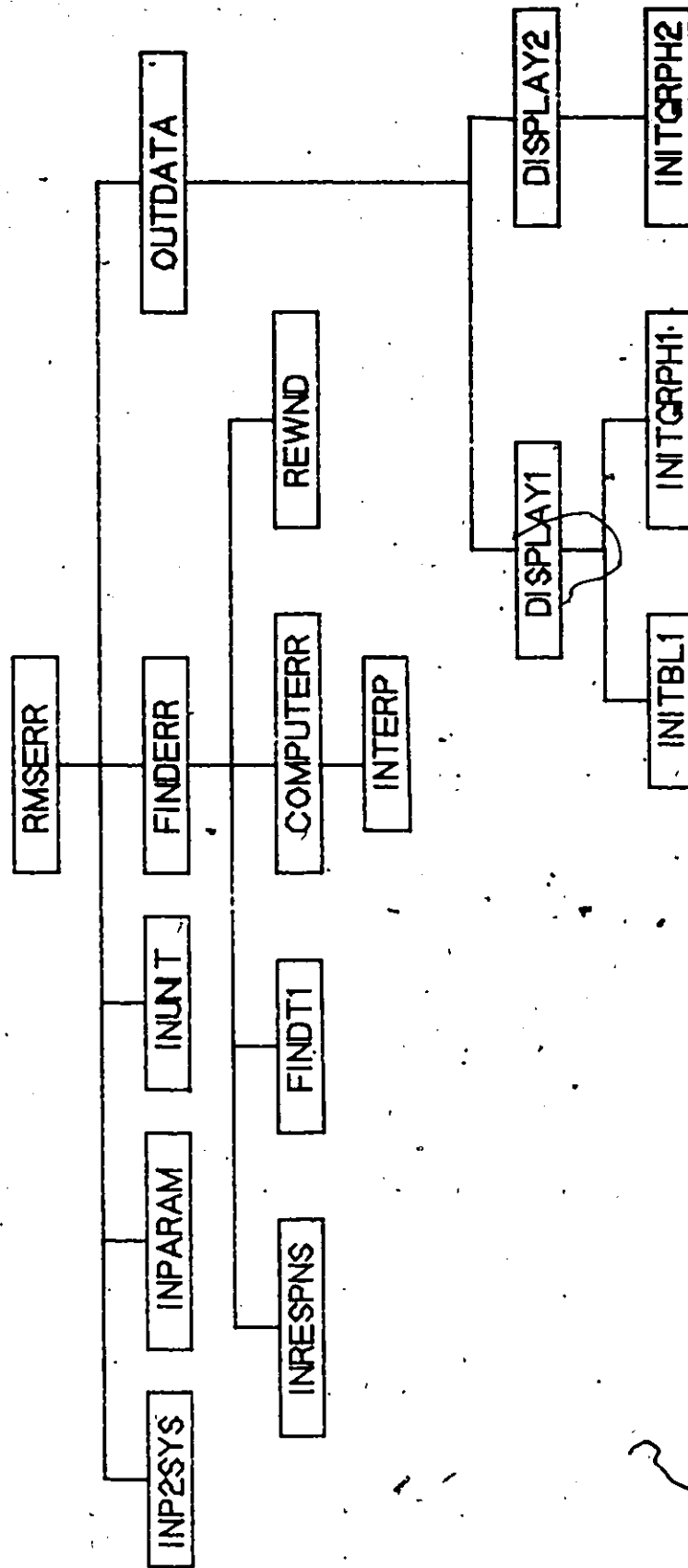


Figure J-1 : Subroutine hierarchical diagram of program  
RMSERR

Input-Process-Output Table of Subroutines

Subroutine	Inputs-	Process	Outputs
INP2SYS	$S_1, S_2$	Interactivity	$S_1, S_2$
INPARAM	DSA, DSB, DSC, $\theta'_i$	Interactivity, Read files	DSA, DSB, DSC, $\theta'_i$
FINDERR	DSA, DSB, $\theta'_i, S_1, S_2$	Fig. J-3	DSE
INRESP	DSR1, DSR2	Read files	DSR1, DSR2
FINDT1	DSR1, DSR2	Find minimum final time of both solutions	$T_1$
COMPUTERR	DSR1, DSR2, $T_1$	Eqs. 90, 94, 95, 97-99, 106	$\epsilon_N$
DISPLAY1	DSA, DSB, DSD, DSE	Fig. J-5	DSEBA, DSECA, DSEDA, DSECD and graphs
DISPLAY2	DSA, DSB, DSE $\epsilon_{NA}$	Fig. J-6	Graphs of $\epsilon_N \leq \epsilon_{NA}$

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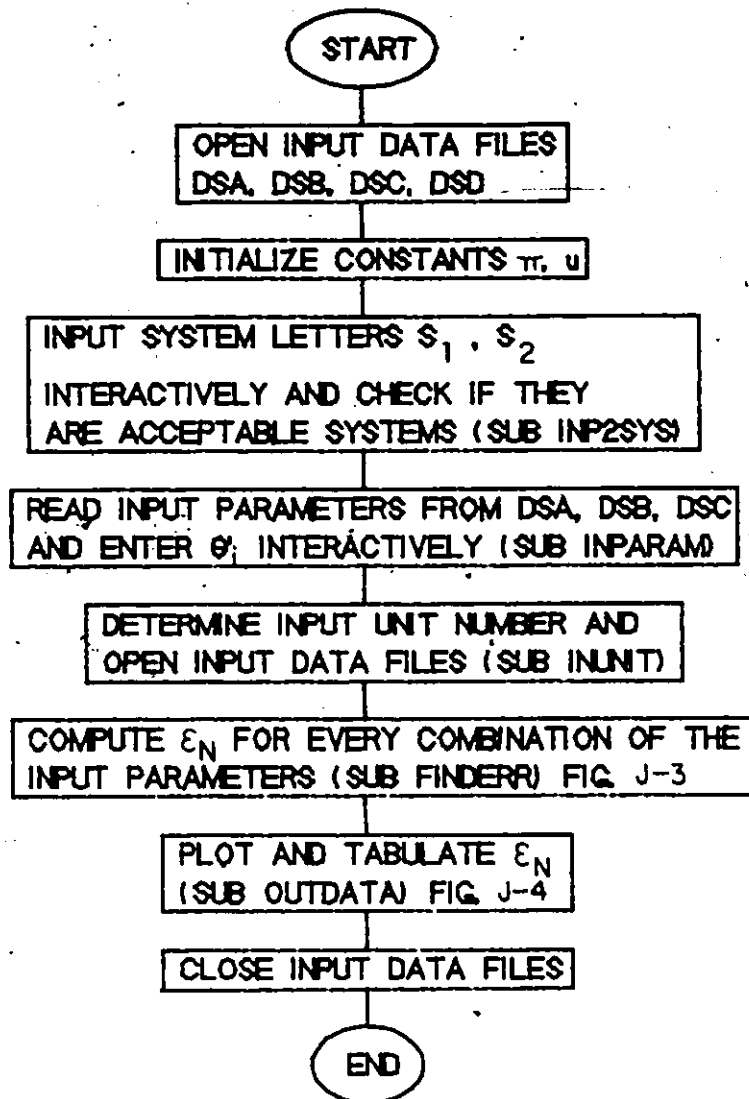


Figure J-2 : Program RMSERR flowchart

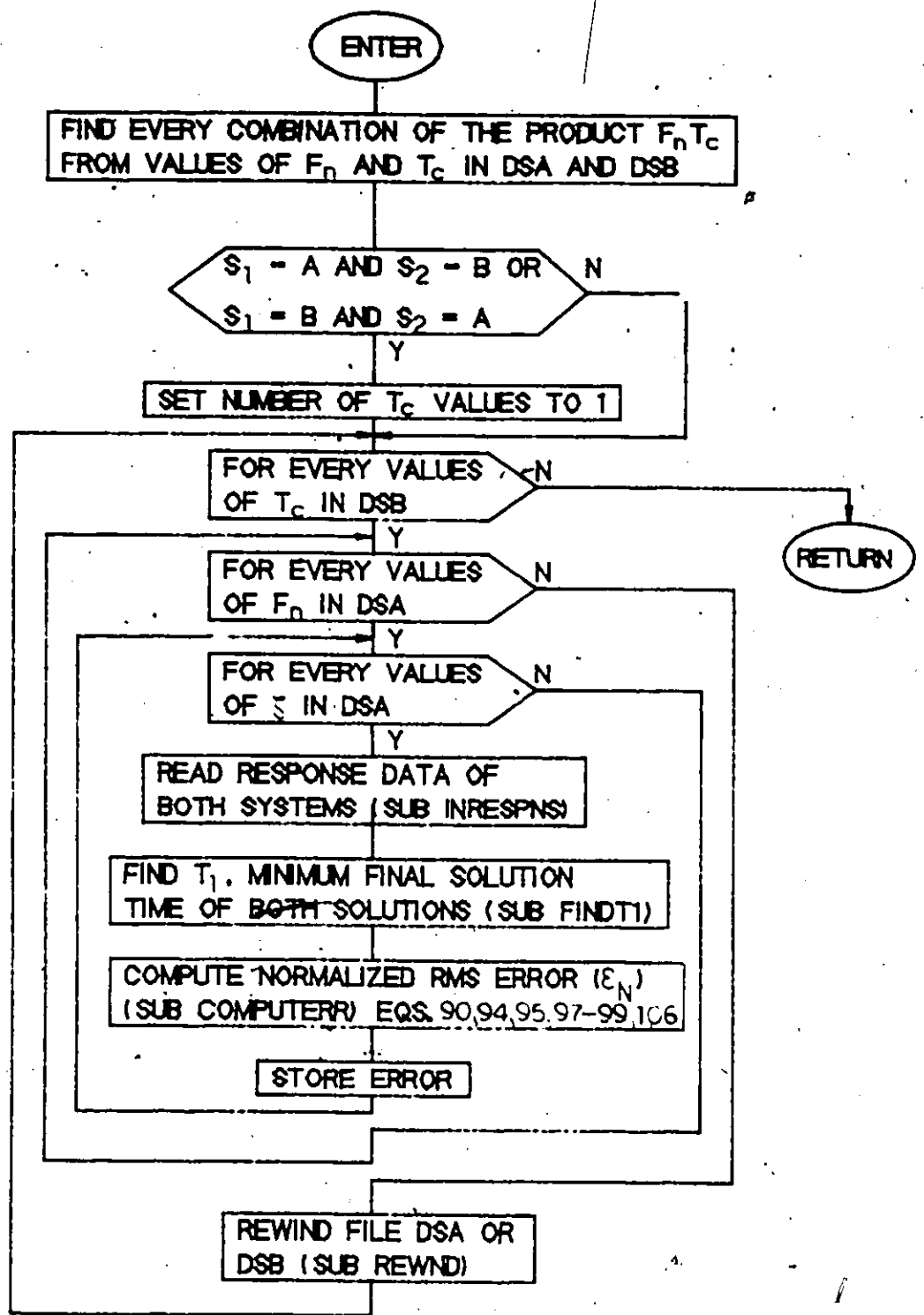


Figure J-3 : Subroutine FINDERR flowchart

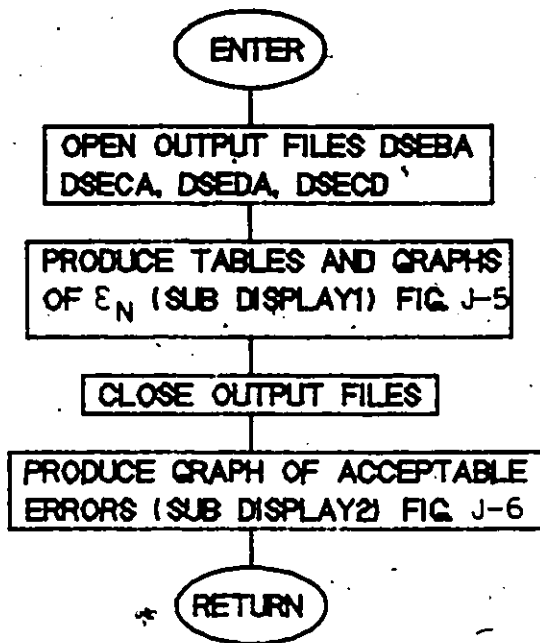


Figure J-4 : Subroutine OUTDATA flowchart

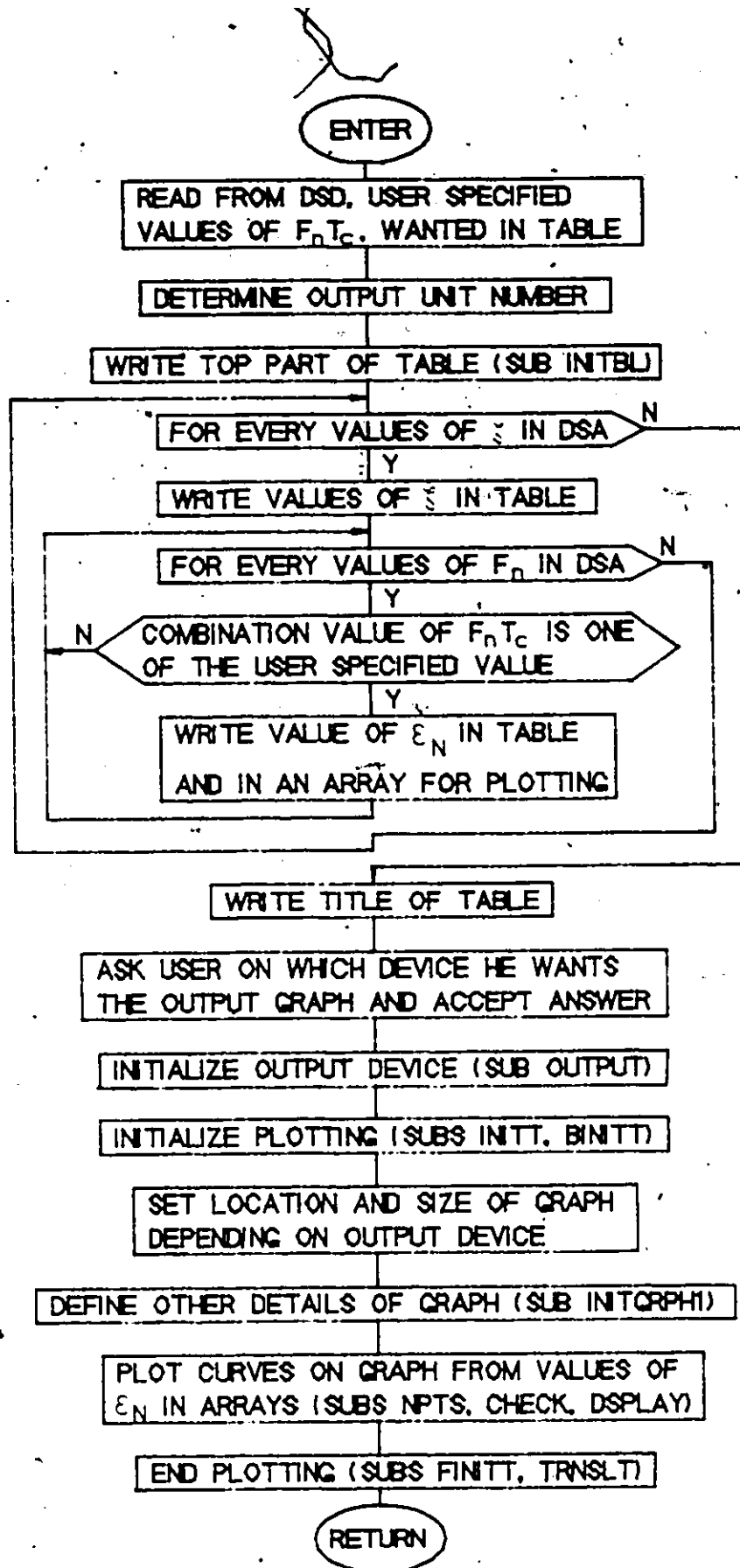


Figure J-5 : Subroutine DISPLAY1 flowchart

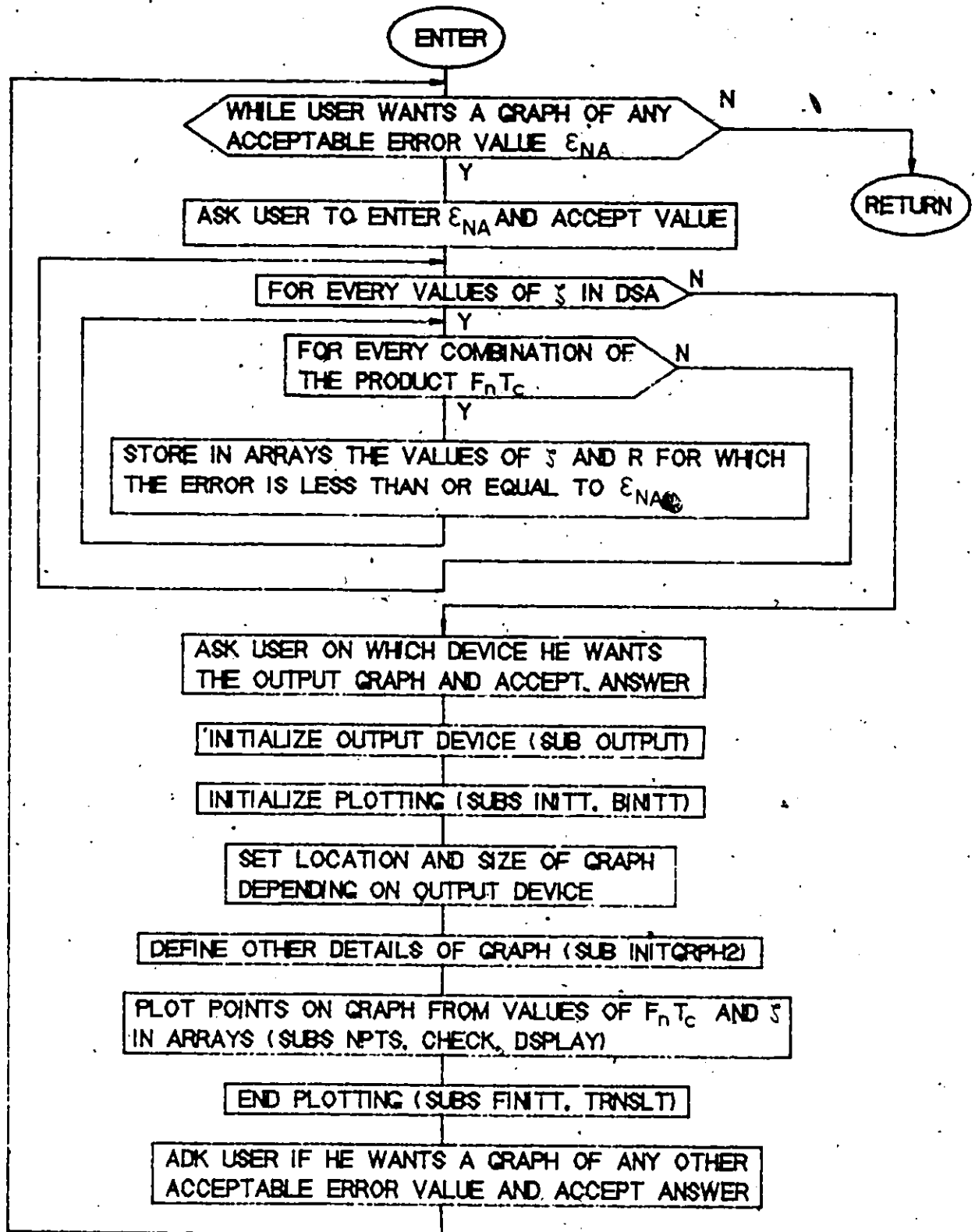


Figure J-6 : Subroutine DISPLAY2 flowchart

```

C _____ Program RMSERR
C _____ This program computes the RMS error between
C _____ the solution of one system to another

C _____ Specification statements
COMMON /CONSTANTS/ IF, PI
COMMON /FORCE/ STEP

C _____ Open input parameter data files
OPEN(10, FILE='DSA DAT', STATUS='OLD')
OPEN(20, FILE='DSB DAT', STATUS='OLD')
OPEN(30, FILE='DSC DAT', STATUS='OLD')
OPEN(40, FILE='DSD DAT', STATUS='OLD')

C _____ Initialize constants
PI = 3.1415927
STEP = 1.0

C _____ Interactively input both systems to be compared
CALL IMP2SYS

C _____ Read input parameters
CALL INPARAM

C _____ Determine the input device unit numbers
CALL INUNIT

C _____ Compute RMS error for every combination of the input
C _____ parameters
CALL FINDERR

C _____ Plot and tabulate RMS errors
CALL OUTDATA

C _____ Close input data files
CLOSE(01)
CLOSE(02)
CLOSE(03)
CLOSE(04)
CLOSE(10)
CLOSE(20)
CLOSE(30)
CLOSE(40)

END

```

```

C _____ Subroutine IMP2SYS
C _____ Interactively inputs both systems to be compared
SUBROUTINE IMP2SYS

C _____ Specification statements
CHARACTER SYSTM, SYSREF, ANSRSYS

LOGICAL GOODSYS

COMMON /SYS/ SYSTM, SYSREF

C _____ Initialize system flag: FALSE indicating that the
C _____ input system letters are not acceptable
GOODSYS = FALSE

C _____ Accept systems until they are valid and the user
C _____ is satisfied
DO WHILE( NOT GOODSYS)
TYPE *
TYPE *, 'Compare System ''I'' to System ''J''
TYPE *, 'where ''I'' and ''J'' = A, B, C or D'
TYPE *
TYPE *, 'Enter ''I'', ''J''
READ(6,100) SYSTM, SYSREF
IF(SYSTM EQ 'B' AND SYSREF EQ 'A' OR
- SYSTM EQ 'C' AND SYSREF EQ 'A' OR
- SYSTM EQ 'D' AND SYSREF EQ 'A' OR
- SYSTM EQ 'C' AND SYSREF EQ 'D') THEN
GOODSYS = TRUE
TYPE *
TYPE *, 'Comparing System ''',SYSTM,''' to System ''',SYSREF,'''
TYPE *
TYPE *, 'Satisfied with Systems ?'
READ(6,200) ANSRSYS
IF(ANSRSYS EQ 'N') THEN
GOODSYS = FALSE
END IF
ELSE

```

```

TYPE *
TYPE e.'***** System '','',SYSTM.''' *****
TYPE e.'***** cannot be compared *****
TYPE e.'***** to System '','',SYSREF.''' *****
END IF
END DO

```

```

C _____ Format statement
100 FORMAT(A,IX,A)
200 FORMAT(A)

RETURN
END

```

```

C _____ Subroutine INPARAM
C _____ Reads systems' input parameters from files DSA & DSB
C _____ and enter pointer for THETA_PRIME value
SUBROUTINE INPARAM

```

```

C _____ Specification statements
CHARACTER SYSTM, SYSREF
DIMENSION COMPENSATION(40), COMPUT_TIME(40)
DIMENSION FREQUENCY(40), DAMPING(40)

COMMON /SYS/ SYSTM, SYSREF
COMMON /NUMTIM/ NT, NS
COMMON /INPARRAYS/ COMPENSATION, COMPUT_TIME,
FREQUENCY, DAMPING
COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
COMMON /INPINTER/ NUMTHETA, ITC

```

```

C _____ Read number of cycles per solution and data storage
C _____ sampling period
READ(30,e) NT, NS

```

```

C _____ Read system parameters (files DSA & DSB)
READ(10,e) NFREQ, (FREQUENCY(I), I=1,NFREQ)
READ(10,e) NDAMP, (DAMPING(I), I=1,NDAMP)
READ(20,e) NCOMP, (COMPENSATION(I), I=1,NCOMP)
READ(20,e) NTIME, (COMPUT_TIME(I), I=1,NTIME)

```

```

C _____ Enter the pointer for THETA_PRIME value
IF((SYSTM EQ 'C') OR (SYSTM EQ 'D')) OR
(SYSREF EQ 'C') OR (SYSREF EQ 'D')) THEN
TYPE *
TYPE e.'Enter Theta Prime number where '
TYPE 100.'Theta Prime number ',(I, I = 1,NCOMP)
TYPE 200.'Theta Prime value: ',(COMPENSATION(I), I = 1,NCOMP)
READ(6,e) NUMTHETA
END IF

```

```

C _____ Format statements
100 FORMAT(A21.10(I3,4X))
200 FORMAT(A21.10(F5.3,2X))

RETURN
END

```

```

C _____ Subroutine INUNIT
C _____ Determines the input device unit numbers and opens
C _____ input files
SUBROUTINE INUNIT

```

```

C _____ Specification statements
CHARACTER SYSTM, SYSREF

INTEGER SYSUNITX, SYSUNITY

COMMON /SYS/ SYSTM, SYSREF
COMMON /INPINTER/ NUMTHETA, ITC
COMMON /UNIT/ SYSUNITX, SYSUNITY

```

```

C _____ Set required input unit device
IF(SYSTM EQ 'A') THEN
SYSUNITY = 1
ELSE IF(SYSTM EQ 'B') THEN
SYSUNITY = 2
ELSE IF(SYSTM EQ 'C') THEN
SYSUNITY = 3
ELSE IF(SYSTM EQ 'D') THEN
SYSUNITY = 4
END IF

```

```

IF(SYSREF EQ 'A')THEN
  SYSUNITX = 1
ELSE IF(SYSREF EQ 'B')THEN
  SYSUNITX = 2
ELSE IF(SYSREF EQ 'C')THEN
  SYSUNITX = 3
ELSE IF(SYSREF EQ 'D')THEN
  SYSUNITX = 4
END IF

```

```

C _____ Open appropriate input file
IF(SYSTEM EQ 'A' OR SYSREF EQ 'A') THEN
  OPEN(01,FILE='DSRA DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
END IF
IF(SYSTEM EQ 'B' OR SYSREF EQ 'B') THEN
  OPEN(02,FILE='DSRB DAT',STATUS='UNKNOWN',FORM='UNFORMATTED')
END IF
IF(SYSTEM EQ 'C' OR SYSREF EQ 'C') THEN
  IF(NUMTHETA EQ 1) THEN
    OPEN(03,FILE='DSRC1 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 2) THEN
    OPEN(03,FILE='DSRC2 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 3) THEN
    OPEN(03,FILE='DSRC3 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 4) THEN
    OPEN(03,FILE='DSRC4 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 5) THEN
    OPEN(03,FILE='DSRC5 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  END IF
END IF
IF(SYSTEM EQ 'D' OR SYSREF EQ 'D') THEN
  IF(NUMTHETA EQ 1) THEN
    OPEN(04,FILE='DSRD1 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 2) THEN
    OPEN(04,FILE='DSRD2 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 3) THEN
    OPEN(04,FILE='DSRD3 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 4) THEN
    OPEN(04,FILE='DSRD4 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  ELSE IF(NUMTHETA EQ 5) THEN
    OPEN(04,FILE='DSRD5 DAT',STATUS='UNKNOWN',
      FORM='UNFORMATTED')
  END IF
END IF
RETURN
END

```

```

C _____ Subroutine FINDERR
C _____ Computes RMS error for every combinations
C _____ of the input parameters
SUBROUTINE FINDERR

```

```

C _____ Specification statements
CHARACTER SYSTEM, SYSREF

DIMENSION COMPENSATION(40), COMPUT_TIME(40)
DIMENSION FREQUENCY(40), DAMPING(40)
DIMENSION ERRARRAY(40,40)
DIMENSION FNTC(40)

COMMON /SYS/ SYSTEM, SYSREF
COMMON /INPARRAYS/ COMPENSATION, COMPUT_TIME,
  FREQUENCY, DAMPING
COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
COMMON /ERRPARAM/ K1
COMMON /FINTIM/ T1
COMMON /NUMTIM/ NT, NS
COMMON /INPOINTER/ NUMTHETA, ITC
COMMON /ERRDAT/ ERMSN
COMMON /ERRARR/ ERRARRAY
COMMON /FNCAHR/ FNTC, NFNTC

```

```

C _____ Initialize constant KI, the number of squared difference
C _____ data to be taken in COMPUTERR
KI = 300

C _____ Give a value of 1 to the computation time indicating that
C _____ the program will not deal with Tc if comparing solutions
C _____ of Systems A and B
IF(SYSM.EQ.'A'.AND.SYSREF.EQ.'B'.OR
-   SYSTM.EQ.'B'.AND.SYSREF.EQ.'A') THEN
    NTIME = 1
    COMPUT_TIME(1) = 1.0
END IF

C _____ Find and store in array FNFC every possible combination of
C _____ the product Fn with Tc Define number NFNTC of such
C _____ combinations
NFNTC = 1
FNFC(1) = 10000.
DO ITC = 1, NTIME
    DO IFREQ = 1, NFREQ
        FREQTIME = FREQUENCY(IFREQ)*COMPUT_TIME(ITC)
        ICNT = 1
        DO WHILE(FREQTIME - FNFC(ICNT).GT..000001)
            ICNT = ICNT + 1
        END DO
        IF(ABS(FREQTIME - FNFC(ICNT)).GT. 000001) THEN
            DO I = NFNTC, ICNT, -1
                FNFC(I+1) = FNFC(I)
            END DO
            FNFC(ICNT) = FREQTIME
            NFNTC = NFNTC + 1
        END IF
    END DO
END DO
NFNTC = NFNTC - 1

C _____ Inform user for which Theta Prime value the errors are being
C _____ computed; only if Systems C or D are involved
IF(NTIME.NE.1) THEN
    TYPE *
    TYPE 100.'Theta Prime = ',COMPENSATION(NUMTHETA)
END IF

C _____ Compute errors for every values of Tc
DO ITC = 1, NTIME

C _____ Inform user which systems are being compared and with which
C _____ Tc value
IF(NTIME.NE.1) THEN
    TYPE 200.'Comparing System ',SYSM,' to System ',
    SYSREF,' for Tc = ',COMPUT_TIME(ITC)
ELSE
    TYPE 300.'Comparing System ',SYSM,' to System ',
    SYSREF,'
END IF

C _____ Compute errors for every values of Fn
DO IFREQ = 1, NFREQ

C _____ Find pointer IFNTC for which the combination of product
C _____ in array FNFC matches the present product-FREQTIME
FN = FREQUENCY(IFREQ)
FREQTIME = FN*COMPUT_TIME(ITC)
IFNTC = 1
DO WHILE(ABS(FREQTIME - FNFC(IFNTC)).GT..000001)
    IFNTC = IFNTC + 1
END DO

C _____ Compute errors for every values of ZETA
DO IZETA = 1, NDAMP

C _____ Read response data of both systems to be compared
CALL INRESPNS

C _____ Find the minimum value of both final solution times
CALL FINDT1(FN)

C _____ Compute the normalized RMS error between both solutions
CALL COMPUTERR

C _____ Store error
ERRARRAY(IZETA,IFNTC) = ERMSN

END DO
END DO

```

C \_\_\_\_\_ Rewind file DSRA or DSRB  
F \_\_\_\_\_ CALL REWIND

END DO

C \_\_\_\_\_ Format statements

100 FORMAT(' ', A14, F4, 2)  
200 FORMAT(' ', A18, A, A13, A, A11, F5, 3, /)  
300 FORMAT(' ', A18, A, A13, A, /)

RETURN  
END

C \_\_\_\_\_ Subroutine INRESPNS

C \_\_\_\_\_ Reads response data points of both systems being compared  
SUBROUTINE INRESPNS

C \_\_\_\_\_ Specification statements  
INTEGER SYSUNITX, SYSUNITY

DIMENSION RESPNSX(1000), RESTIMX(1000)  
DIMENSION RESPNSY(1000), RESTIMY(1000)  
DIMENSION RESPNSDX(1000), RESPNSDY(1000)

COMMON /UNIT/ SYSUNITX, SYSUNITY  
COMMON /RESPNSDATX/ NPOINTX, RESTIMX, RESPNSX, RESPNSDX  
COMMON /RESPNSDATY/ NPOINTY, RESTIMY, RESPNSY, RESPNSDY

C \_\_\_\_\_ Read one solution of both systems

READ(SYSUNITX) NPOINTX, (RESPNSX(I), I=1,NPOINTX),  
(RESTIMX(I), I=1,NPOINTX),  
(RESPNSDX(I), I=1,NPOINTX)

READ(SYSUNITY) NPOINTY, (RESPNSY(I), I=1,NPOINTY),  
(RESTIMY(I), I=1,NPOINTY),  
(RESPNSDY(I), I=1,NPOINTY)

RETURN  
END

C \_\_\_\_\_ Subroutine FINDT1

C \_\_\_\_\_ Finds a fixed solution-time to study the error between both  
C \_\_\_\_\_ The solution-time T1 is fixed to NT cycle periods of the  
C \_\_\_\_\_ analytical solution  
SUBROUTINE FINDT1(FN)

C \_\_\_\_\_ Specification statements

DIMENSION RESTIMX(1000), RESPNSX(1000)  
DIMENSION RESTIMY(1000), RESPNSY(1000)  
DIMENSION RESPNSDX(1000), RESPNSDY(1000)

COMMON /RESPNSDATX/ NPOINTX, RESTIMX, RESPNSX, RESPNSDX  
COMMON /RESPNSDATY/ NPOINTY, RESTIMY, RESPNSY, RESPNSDY  
COMMON /NNTIM/ NT, NS  
COMMON /FINTIM/ T1

C \_\_\_\_\_ Find the minimum of the last response-time of both solutions  
TMIN = MIN(RESTIMX(NPOINTX), RESTIMY(NPOINTY))

C \_\_\_\_\_ If the minimum final time (TMIN) of both solutions is within  
C \_\_\_\_\_ 90% of NT cycle periods then set T1 to the min of TMIN and NT  
C \_\_\_\_\_ cycle periods. If not, set T1 to -1 indicating that one solution  
C \_\_\_\_\_ was not solved long enough to find the error (i.e. error too large)  
IF (TMIN GE 0.90\*NT/FN) THEN  
T1 = MIN(TMIN, NT/FN)  
ELSE  
T1 = -1  
END IF

C \_\_\_\_\_ Find the pointer for the largest time data value smaller  
C \_\_\_\_\_ than T1 for both solutions

I = 1  
DO WHILE(RESTIMX(I) LT T1)  
I = I + 1  
END DO  
NPOINTX = I

```

I = 1
DO WHILE(RESTIMY(I).LT. T1)
  I = I + 1
END DO
NPOINTY = 1

RETURN
END

```

```

C _____ Subroutine COMPUTERR
C _____ Computes the normalized RMS error between the two
C _____ time-responses X and Y
SUBROUTINE COMPUTERR

C _____ Specification statements
DIMENSION RESTIMX(1000), RESPNSX(1000)
DIMENSION RESTIMY(1000), RESPNSY(1000)
DIMENSION RESPNSDX(1000), RESPNSDY(1000)

COMMON /RESPNSDATX/ NPOINTX, RESTIMX, RESPNSX, RESPNSDX
COMMON /RESPNSDATY/ NPOINTY, RESTIMY, RESPNSY, RESPNSDY
COMMON /ERRPARAM/ K1
COMMON /FINTIM/ T1
COMMON /ERRDAT/ ERMSN

C _____ Set error to a large value (1.0) if T1 equals -1 as set in
C _____ subroutine FINDT1
IF (T1 EQ -1) THEN
  ERMSN=1.0
ELSE

C _____ Initialization of variables
DELTASQR = 0.0
NDELTA = 0
IPTRX = 1
IPTRY = 1

C _____ Initialize square difference computation interval
DELTAT = T1/K1

C _____ Find maximum values of responses X and Y
RESPXM = -1.0E30
RESPYM = -1.0E30
DO I = 1, NPOINTX
  RESPXM = MAX(RESPXM, ABS(RESPNSX(I)))
END DO

DO I = 1, NPOINTY
  RESPYM = MAX(RESPYM, ABS(RESPNSY(I)))
END DO

C _____ Find maximum of both maximums
RESPM = MAX(RESPXM, RESPYM)

C _____ Find response X pointer where time of X is greater than
C _____ or equal to first time-data value of response Y
DO WHILE(RESTIMX(IPTRX) LT RESTIMY(IPTRY))
  IPTRX = IPTRX + 1
END DO

C _____ Initialize present time and present response values for
C _____ response X
TIMX = RESTIMX(IPTRX)
RESPX = RESPNSX(IPTRX)
RESPDX = RESPNSDX(IPTRX)

C _____ Compute RMS error until the final solution time
DO WHILE(TIMX LT T1)

C _____ Find response Y pointer where time of Y is greater than
C _____ present time of response X
DO WHILE(RESTIMY(IPTRY) LE TIMX)
  IPTRY = IPTRY + 1
END DO

C _____ Interpolate to find value of response Y (RESPY) at
C _____ present time of response X (TIMX)
CALL INTERP(RESTIMY, RESPNSY, IPTRY, TIMX, RESPY)

C _____ Compute difference between solutions only if the vertical
C _____ difference is larger than .05X of the maximum amplitude
IF(ABS(RESPY - RESPX) GT 0.0005*RESPM) THEN

```

```

C _____ Count number of observed squared differences between
C _____ both responses
      NDELTA = NDELTA + 1

C _____ Add every squared differences (perpendicular to response X)
      DELTASQR = DELTASQR + (((RESPY - RESPX)/RESPH)
      *COS(ATAN(RESPDX*T1/RESPH)))**2.

      END IF

C _____ Increment present time of response X by a pre-defined
C _____ constant interval
      TIMX = TIMX + DELTAT

C _____ Find new response X pointer where time of X is greater
C _____ than or equal to present time of X
      DO WHILE(RESTIMX(IPTRX) LT TIMX)
        IPTRX = IPTRX + 1
      END DO

C _____ Interpolate to find value of response X (RESPX) at
C _____ new present time of X (TIMX)
      CALL INTERP(RESTIMX,RESPONSX,IPTRX,TIMX,RESPX)

C _____ Interpolate to find value of derivative of X (RESPDX) at
C _____ new present time of X (TIMX)
      CALL INTERP(RESTIMX,RESPONSDX,IPTRX,TIMX,RESPDX)

      END DO

C _____ Compute normalized RMS error dividing the sum of
C _____ every squared differences by the number of observed
C _____ squared differences and taking the square root
      IF(NDELTA EQ 0) THEN
        ERMSN = 0.0
      ELSE
        ERMSN = SQRT(DELTASQR/NDELTA)
      END IF

      END IF

      RETURN
      END

```

```

C _____ Subroutine INTERP
C _____ Interpolate to find response value (RESPZ) at present
C _____ time (TIMX) between response at IPTRZ and response at
C _____ IPTRZ-1
      SUBROUTINE INTERP(RESTIMZ,RESPONSZ,IPTRZ,TIMX,RESPZ)

C _____ Specification statements
      DIMENSION RESTIMZ(1000), RESPONSZ(1000)

C _____ Find slope between response at IPTRZ and response at
C _____ IPTRZ-1
      SLOP = (RESPONSZ(IPTRZ) - RESPONSZ(IPTRZ-1))/
      (RESTIMZ(IPTRZ) - RESTIMZ(IPTRZ-1))

C _____ Find value of response at time TIMX
      RESPZ = SLOP*(TIMX - RESTIMZ(IPTRZ)) + RESPONSZ(IPTRZ)

      RETURN
      END

```

```

C _____ Subroutine REWIND
C _____ Rewinds files DSRA or DSRB
      SUBROUTINE REWIND

C _____ Specification statements
      INTEGER SYSUNITX, SYSUNITY

      COMMON /UNIT/ SYSUNITX, SYSUNITY

C _____ Rewind appropriate file
      IF(SYSUNITX EQ 1 OR SYSUNITY EQ 1) THEN
        REWIND(O1)
      END IF
      IF(SYSUNITY EQ 2 OR SYSUNITX EQ 2) THEN
        REWIND(O2)
      END IF

      RETURN
      END

```

```

C _____ Subroutine OUTDATA
C _____ Produce table and graph of RMS error and graph of
C _____ acceptable error
SUBROUTINE OUTDATA

C _____ Open output data files
OPEN(21, FILE='DSEBA.TBL', STATUS='UNKNOWN')
OPEN(31, FILE='DSECA.TBL', STATUS='UNKNOWN')
OPEN(41, FILE='DSEBA.TBL', STATUS='UNKNOWN')
OPEN(34, FILE='DSECD.TBL', STATUS='UNKNOWN')

C _____ Produce table and graph of RMS error
CALL DISPLAY1

C _____ Close output data files
CLOSE(21)
CLOSE(31)
CLOSE(41)
CLOSE(34)

C _____ Produce graph of acceptable error
CALL DISPLAY2

RETURN
END

C _____ Subroutine DISPLAY1
C _____ Produce formatted tables of RMS error
SUBROUTINE DISPLAY1

C _____ Specification statements
INTEGER SYSUNIT, SYSUNITX, SYSUNITY

CHARACTER SYSTM, SYSREF, DEVICE, MOREDEVIC, LOC

LOGICAL FOUND, FIRSTLINE

DIMENSION COMPENSATION(40), COMPUT_TIME(40),
           FREQUENCY(40), DAMPING(40)
DIMENSION ERRARRAY(40,40), FNFC(40), FNFCW(40)
DIMENSION XARRAY(40), YARRAY(40)
DIMENSION YTABLE(40,40), XTABLE(40,40)
DIMENSION NPPOINT(40)

COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
COMMON /SYS/ SYSTM, SYSREF
COMMON /UNIT/ SYSUNITX, SYSUNITY
COMMON /INPARRAYS/ COMPENSATION, COMPUT_TIME,
                  FREQUENCY, DAMPING
COMMON /INPOINTER/ NUMTHETA, ITC
COMMON /ERRARR/ ERRARRAY
COMMON /FNFCARR/ FNFC, NFNFC
COMMON /FNFCWARR/ FNFCW, NFNFCW

C _____ Read (from DSD) values of FnFc wanted in table; values
C _____ of Fn in case of System B
READ(40,*) NFNFCW, (FNFCW(K), K = 1, NFNFCW)

C _____ Determine output file unit number
SYSUNIT = 10*SYSUNITY + SYSUNITX

C _____ Write on a new page
WRITE(SYSUNIT,100)

C _____ Write top part of the table
CALL INITBL1(SYSUNIT)

C _____ Initialize minimum and maximum of Y axis
YMIN = 1.0E30
YMAX = -1.0E30

C _____ Write RMSERR values in table for every
C _____ value of ZETA
DO IZETA = 1, NDAMP

C _____ Write ZETA value in table
WRITE(SYSUNIT,(200) DAMPING(IZETA)

C _____ Write RMSERR values in table for every
C _____ frequency values
NFNFCF = 0
DO IFNFC = NFNFC, 1, -1
   FOUND = .FALSE.

```

```

C _____ Check if the combination product of Fn and Tc is one
C _____ of the values requested by user in DSD. If so, write
C _____ error value in table
      DO IFNTCW = NFNTCW, 1, -1
        IF(ABS(FNTC(IFNTC) - FNTCW(IFNTCW)).LT. 000001) THEN
          NFNTCF = NFNTCF + 1
          FOUND = TRUE
        END IF
      END DO
      IF(FOUND) THEN

C _____ Choose different format depending on output
C _____ value
      IF(ERRARRAY(IZETA, IFNTC).LT. 0 001) THEN
        WRITE(SYSUNIT, 300) ERRARRAY(IZETA, IFNTC)
      ELSE IF(ERRARRAY(IZETA, IFNTC).LT. 1 ) THEN
        WRITE(SYSUNIT, 400) ERRARRAY(IZETA, IFNTC)
      ELSE
        WRITE(SYSUNIT, 500) ERRARRAY(IZETA, IFNTC)
      END IF

C _____ Store error value and damping in table arrays for
C _____ plotting. Find minimum and maximum of Y axis
      IF(ERRARRAY(IZETA, IFNTC) LE. 1 0) THEN
        NPPOINT(NFNTCF) = NPPOINT(NFNTCF) + 1
        YTABLE(NFNTCF, NPPOINT(NFNTCF)) = ERRARRAY(IZETA, IFNTC)
        XTABLE(NFNTCF, NPPOINT(NFNTCF)) = DAMPING(IZETA)
        YMIN = MIN(YMIN, ERRARRAY(IZETA, IFNTC))
        YMAX = MAX(YMAX, ERRARRAY(IZETA, IFNTC))
      END IF
      END IF

      END DO

C _____ Write a full horizontal line
      WRITE(SYSUNIT, 600)
      WRITE(SYSUNIT, 700)

      END DO

C _____ Write values of THETA PRIME at bottom of table
      IF(NTIME EQ 1) THEN
        WRITE(SYSUNIT, 800) SYSTM, SYSREF
      ELSE
        WRITE(SYSUNIT, 900) SYSTM, SYSREF, NUMTHETA
        WRITE(SYSUNIT, 1000) COMPENSATION(NUMTHETA)
      END IF

C _____ Plot curves while user wants output on any device
      MOREDEVIC = 'Y'
      DO WHILE(MOREDEVIC EQ 'Y')

C _____ Ask user to specify output device
      TYPE *
      TYPE *, 'Enter output device where you'
      TYPE *, 'want graph of RMS error'
      TYPE *, '    Enter S. for VGI Screen'
      TYPE *, '    P. for Line-Printer'
      TYPE *, '    H. for HP Plotter'
      READ(6, 1100) DEVICE

C _____ Initialize output device
      IF(DEVICE EQ 'P') THEN
        CALL OUTPUT('PRINTX', 'JML', 0)
      ELSE IF(DEVICE EQ 'H') THEN
        CALL OUTPUT('HPLOT', 'JML', 0)
      ELSE
        CALL OUTPUT('VGTERM', 'JML', 0)
      END IF

C _____ Initialize minimum and maximum of X axis
      XMIN=DAMPING(1)
      XMAX=DAMPING(NDAMP)

C _____ Initialize plotting
      CALL INITT(30)
      CALL BINITT

C _____ Set location and size of graph depending on output device
      IF(DEVICE EQ 'P') THEN

C _____ Initialize location and size of graph
      CALL SWCHAR(1)
      MINHOR = 200
      MAXHOR = MINHOR + 195
      MINVER = 370
      MAXVER = MINVER + 115

```

```

C _____ Set page location
CALL SLIMX(MINH0R,MAXH0R)
CALL SLIMY(MINVER,MAXVER)

ELSE IF(DEVICE.EQ.'H') THEN

C _____ Initialize location and size of graph
CALL SCHAR(1)
MINH0R = 260
MAXH0R = 310
TYPE =
TYPE = 'Top or Bottom ? (T/B)'
READ(6,1100) LOC
IF(LOC.EQ.'T') THEN
MINVER = 450
MAXVER = 590
ELSE
MINVER = 120
MAXVER = 260
END IF

C _____ Set page location
CALL SLIMX(MINH0R,MAXH0R)
CALL SLIMY(MINVER,MAXVER)

END IF

C _____ Set other details of graph
CALL INITGRPH1

C _____ Plot some lines
FIRSTLINE = TRUE
DO IFNTCF = NFNTCF - 5, NFNTCF - 1

C _____ Write error and damping values into arrays
DO K = 1, NPPOINT(IFNTCF)
YARRAY(K) = YTABLE(IFNTCF,K)
XARRAY(K) = XTABLE(IFNTCF,K)
END DO

C _____ Plot one line
IF (NPPOINT(IFNTCF) NE. 0) THEN
CALL NPTS(NPPOINT(IFNTCF))
IF(FIRSTLINE) THEN
CALL CHECK(XARRAY,YARRAY)
CALL DISPLAY(XARRAY,YARRAY)
FIRSTLINE = FALSE
ELSE
CALL CPLOT(XARRAY,YARRAY)
END IF
END IF

END DO

C _____ End plotting
CALL FINITT(0,0)
CALL TRNSLT(1)

C _____ Ask user if he wants output on any other device
TYPE =
TYPE = 'Any other output device ? (Y/N):'
READ(6,1100) MOREDEVIC

END DO

C _____ Format statements
100 FORMAT('1')
200 FORMAT(1X,10X,' : ',F6.3,' : ',S)
300 FORMAT('++',',',E5.1E1,' : ',S)
400 FORMAT('++',',',F4.3,' : ',S)
500 FORMAT('++',',',F4.2,' : ',S)
600 FORMAT('++')
700 FORMAT('++',10X,' _____',7('_____'))
800 FORMAT('///++',10X,'TABLE ',A1,A1,'///')
900 FORMAT('///++',10X,'TABLE ',A1,A1,1X,11,'///')
1000 FORMAT(1X,10X,'0' = ',F3.1)
1100 FORMAT(A)

RETURN
END

```

```

C _____ Subroutine INITBL1
C _____ Initializes table
SUBROUTINE INITBL1(SYSUNIT)

C _____ Specification statements
INTEGER SYSUNIT

      DIMENSION FNTC(40), FNTCW(40)

      COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP
      COMMON /FNTCARR/ FNTC, NFNTC
      COMMON /FNTCWARR/ FNTCW, NFNTCW

C _____ Write table variables
WRITE(SYSUNIT,100)
IF(NTIME EQ 1) THEN
  WRITE(SYSUNIT,200)
ELSE
  WRITE(SYSUNIT,300)
END IF

C _____ Check if values of FntC requested by user are values
C _____ for which the error was found and write these values
C _____ in table
DO I = NFNTCW, 1, -1
  DO J = NFNTC, 1, -1
    IF(ABS(FNTCW(I) - FNTC(J)) LT 000001) THEN
      IF(NTIME EQ 1) THEN
        WRITE(SYSUNIT,400) 1 /FNTCW(I)
      ELSE
        WRITE(SYSUNIT,500) 1 /FNTCW(I)
      END IF
    END IF
  END DO
END DO
WRITE(SYSUNIT,600)

WRITE(SYSUNIT,700)
WRITE(SYSUNIT,100)

C _____ Format statements
100 FORMAT(' ',10X, ' ',7(' ',))
200 FORMAT(1X,10X, ' ',10(' ',S))
300 FORMAT(1X,10X, ' ',10(' ',S))
400 FORMAT(' ',F6.3, ' ',S)
500 FORMAT(' ',F6.0, ' ',S)
600 FORMAT(' ')
700 FORMAT(1X,10X, 'ZETA', 1,7(6X, ' '))

RETURN
END

```

```

C _____ Subroutine INITGRPH1
C _____ Sets details of graph
SUBROUTINE INITGRPH1

C _____ Set limits of X and Y axes
CALL DLIMX( 001,10 )
CALL DLIMY( 0001, 1 )

C _____ Set type of frame, no grid line
CALL XFRM(2)
CALL YFRM(2)

C _____ Set tic marks length
CALL XLEN(4)
CALL YLEN(4)

C _____ Set density of tic marks
CALL XDEN(3)
CALL YDEN(5)

C _____ Set maximum number of character in tic mark labels
C _____ of Y axis
CALL YWDTH(5)

C _____ Set logarithmic X and Y axes
CALL XTYPE(2)
CALL YTYPE(2)

C _____ Set character size for tic mark labels
CALL PLCHAR(25,40)

RETURN
END

```

```

C_____ Subroutine DISPLAY2
C_____ Produces formatted tables of acceptable RMS error
SUBROUTINE DISPLAY2

C_____ Specification statements
CHARACTER DEVICE, MOREDEVIC, MOREACCEPT

LOGICAL FOUND

DIMENSION COMPENSATION(40), COMPUT_TIME(40),
          FREQUENCY(40), DAMPING(40),
DIMENSION YARRAY(2000), XARRAY(2000)
DIMENSION FNTC(40)
DIMENSION ERRARRAY(40,40)

COMMON /NUMINPUT/ NDCMP, NTIME, NFREQ, NDAMP
COMMON /INPARRAYS/ COMPENSATION, COMPUT_TIME,
          FREQUENCY, DAMPING
COMMON /INPOINTER/ NUNTHETA, ITC
COMMON /ERRARR/ ERRARRAY
COMMON /FNTCARR/ FNTC, NFNTC

MOREACCEPT = 'Y'
DO WHILE(MOREACCEPT EQ 'Y')

C_____ Ask user for acceptable RMSERR value
TYPE *
TYPE *, 'Enter acceptable RMSERR value'
READ(6,*) ACCEPT

C_____ Initialize minimum and maximum of Y axis
YMIN = 1.0E30
YMAX = -1.0E30

C_____ Find FNTC values where RMSERR is acceptable and store
C_____ values of 1/FnTc and damping in arrays for plotting
NPNT = 0
DO IZETA = 1, NDAMP
  DO IFNTC = NFNTC, 1, -1
    YMIN = MIN(YMIN, 1./FNTC(IFNTC))
    YMAX = MAX(YMAX, 1./FNTC(IFNTC))
    IF(ERRARRAY(IZETA, IFNTC) LE ACCEPT) THEN
      NPNT = NPNT + 1
      XARRAY(NPNT) = DAMPING(IZETA)
      YARRAY(NPNT) = 1./FNTC(IFNTC)
    END IF
  END DO
END DO

C_____ Plot the curve while user wants output on any device
MOREDEVIC = 'Y'
DO WHILE(MOREDEVIC EQ 'Y')

C_____ Ask user to specify output device
TYPE *
TYPE *, 'Enter output device where you'
TYPE *, 'want graph of acceptable error'
TYPE *, '    Enter S. for VGT Screen'
TYPE *, '    P. for Line-Printer'
TYPE *, '    H. for HP Plotter'
READ(6,100) DEVICE

C_____ Initialize output device
IF(DEVICE EQ 'P') THEN
  CALL OUTPUT('PRINTX', 'JKL', 0)
ELSE IF(DEVICE EQ 'H') THEN
  CALL OUTPUT('HPLOT', 'JKL', 0)
ELSE
  CALL OUTPUT('VGTTERM', 'JKL', 0)
END IF

C_____ Initialize minimum and maximum of X axis
XMIN=DAMPING(1)
XMAX=DAMPING(NDAMP)

C_____ Initialize plotting
CALL INITT(30)
CALL BINITT

```

```

C _____ Set location and size of graph depending on output
C _____ device
      IF (DEVICE EQ 'P') THEN

C _____ Initialize location and size of graph
      CALL SWCHAR(L)
      MINH0R = 80
      MAXH0R = 400
      MINV0R = 150
      MAXV0R = 400

C _____ Set page location
      CALL SLIMX(MINH0R, MAXH0R)
      CALL SLIMY(MINV0R, MAXV0R)

      ELSE IF (DEVICE EQ 'H') THEN

C _____ Initialize location and size of graph
      CALL SWCHAR(I)
      MINH0R = 120
      MAXH0R = 520
      MINV0R = 160
      MAXV0R = 630

C _____ Set page location
      CALL SLIMX(MINH0R, MAXH0R)
      CALL SLIMY(MINV0R, MAXV0R)

      END IF

C _____ Set other details of graph
      CALL INITGRPH2

C _____ Plot the points on graph
      IF (NPNT NE 0) THEN
        CALL NPIS(NPNT)
        CALL CHECK(XARRAY, YARRAY)
        CALL DISPLAY(XARRAY, YARRAY)
      END IF

C _____ End plotting
      CALL FINIT(0,0)
      CALL TRNSL(I)

C _____ Ask user if he wants output on any other device
      TYPE *
      TYPE *, 'Any other output device ? (Y/N) '
      READ(6,100) MOREDEVIC

      END DO

C _____ Ask user if he wants output for another acceptable
C _____ RMS error value
      TYPE *
      TYPE *, 'Any other acceptable RMS error value ? (Y/N) '
      READ(6,100) MOREACCEPT

      END DO

C _____ Format statement
      100 FORMAT(A)

      RETURN
      END

C _____ Subroutine INITGRPH2
C _____ Sets details of graph
      SUBROUTINE INITGRPH2

C _____ Specification statements
      COMMON /NUMINPUT/ NCOMP, NTIME, NFREQ, NDAMP

C _____ Set limits of X and Y axes depending on which system
C _____ is involved
      CALL DLIMX( 001,10 )
      IF (NTIME EQ 1) THEN
        CALL DLIMY( 01,100 )
      ELSE
        CALL DLIMY( 1,10000 )
      END IF

C _____ Set type of frame, no grid line
      CALL XFRM(2)
      CALL YFRM(2)

```

C \_\_\_\_\_ Set tic marks length  
CALL XLEN(6)  
CALL YLEN(6)

C \_\_\_\_\_ Set density of tic marks  
CALL XDEN(10)  
CALL YDEN(8)

C \_\_\_\_\_ Set maximum number of character in tic mark labels  
C \_\_\_\_\_ of Y axis  
CALL YWIDTH(5)

C \_\_\_\_\_ Set logarithmic X and Y axes  
CALL XTYPE(2)  
CALL YTYPE(2)

C \_\_\_\_\_ Set no solid line (dots only)  
CALL LINE(-4)

C \_\_\_\_\_ Set character size for tic mark labels  
CALL PLCHAR(25,45)

RETURN  
END

APPENDIX K

Program Run Examples

Contents

- Program RESPLT
- Program RESPONS
- Program RMSERR

# Program RESPLT

```
$ LET MOD=INDUSET.LIMIT $1-
$ LET PFDLSS.PRIORITY=28
$ RUN RESPLT
```

Enter System : A, B, C or D  
C

Enter input parameters :  
Damping Ratio: ZETA  
Natural Frequency: F<sub>n</sub>  
Compensation Factor: THETA FRINE  
Computation Time: Tc  
.1 .1 1.00

Satisfied with parameters ? (Y/N):  
ZETA= 0.1000  
F<sub>n</sub> = 0.1000  
THETA FRINE= 1.0000  
Tc = 0.0900  
Y

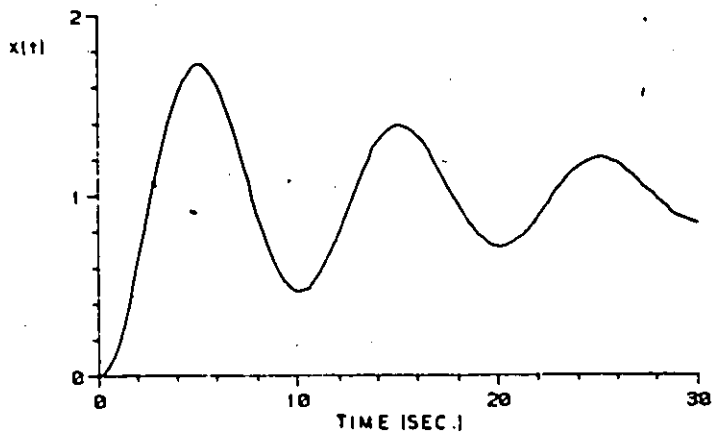
Switch FACER to VAX port and press RETURN.

Bootstrap FACER to establish connection  
(message when connection established)

```
* FACER CONNECTION ESTABLISHED *
* VAX/FACER NOW RUNNING *
```

Solution time = 30.00000 Sec.

Enter output device:  
Enter C for UGT Screen  
F for Line-Printer  
H for HP Plotter



Any other output device ? (Y/N):

N

Output of another curve ? (Y/N):

Y

System = C

Satisfied with system ? (Y/N):

N

Enter System : A, B, C or D

A

Enter input parameters :

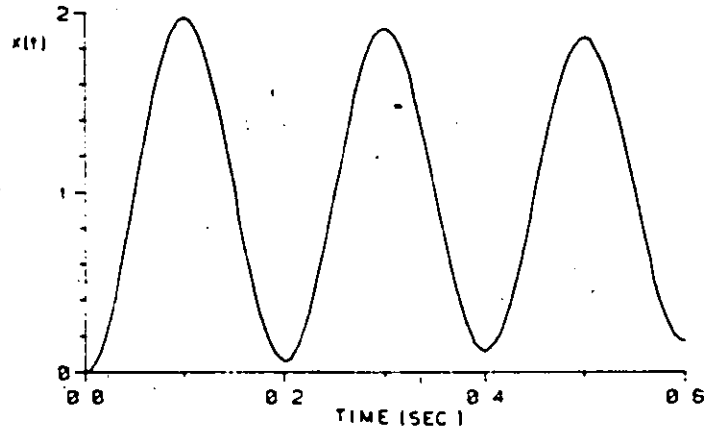
Damping Ratio: ZETA  
Natural Frequency: F<sub>n</sub>  
.01 5

Satisfied with parameters ? (Y/N):

ZETA = 0.010  
F<sub>n</sub> = 5.000

Enter output device:

Enter S<sub>1</sub> for VDI screen  
F<sub>1</sub> for Line-Printer  
H<sub>1</sub> for HP Plotter



And other output device ? (Y/N):

N

Output of another curve ? (Y/N):

N

Enter System : A

Satisfied with system ? (Y/N):

N

Enter System : A, B, C or D

B

\*\*\*\* System 'B' is not implemented \*\*\*\*

Output of another curve ? (Y/N):

N

Enter System : A, B, C or D

Enter input parameters :

Damping Ratio: ZETA  
Natural Frequency: F<sub>n</sub>  
Damping Ratio Factor: INETA  
Exponentiation Time: Tc  
.01 5

Satisfied with parameters ? (Y/N):

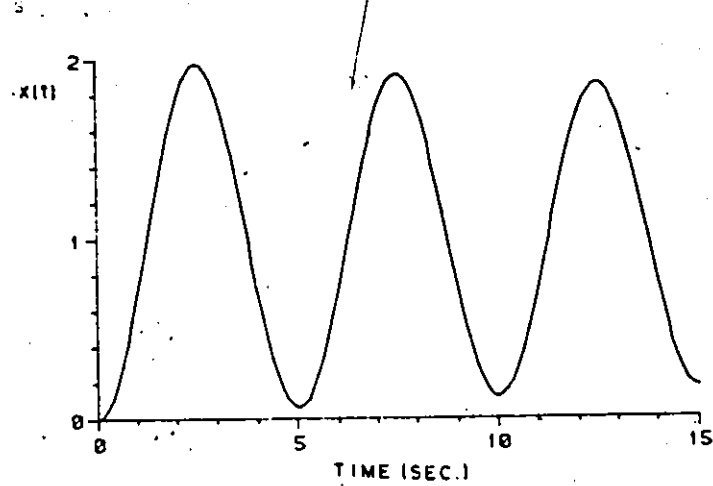
ZETA = 0.0100  
F<sub>n</sub> = 5.0000  
INETA = 0.5000  
Tc = 0.0200

Enter input parameters :  
 Damping Ratio: ZETA  
 Natural Frequency: F<sub>n</sub>  
 Compensation Factor: THETA PRIME  
 Computation Time: T<sub>c</sub>  
 .01 .2 0 .005

Satisfied with parameters ? (Y/N):  
 ZETA= 0.0100  
 F<sub>n</sub> = 0.2000  
 THETA PRIME= 0.0000  
 T<sub>c</sub> = 0.0050

Y  
 Solution time = 15.00000 Sec.

Enter output device:  
 Enter S for VGT Screen  
 F for Line-Printer  
 H for HP Plotter



Any other output device ? (Y/N):  
 N

Output of another curve ? (Y/N):  
 N

System = L

Satisfied with system ? (Y/N):  
 Y

Enter input parameters :  
 Damping Ratio: ZETA  
 Natural Frequency: F<sub>n</sub>  
 Compensation Factor: THETA PRIME

Computation Time: T<sub>c</sub>  
 .02 .2 0 .003

Satisfied with parameters ? (Y/N):  
 ZETA= 0.0200  
 F<sub>n</sub> = 0.2000  
 THETA PRIME= 0.0000  
 T<sub>c</sub> = 0.0030

Y  
 Solution time = 15.00000 Sec.

\*\*\*\*\* TIME CONSTRAINT \*\*\*\*\*

Enter output device:  
 Enter S for VGT Screen  
 F for Line-Printer  
 H for HP Plotter

Any other output device ? (Y/N):

N

Output of another curve ? (Y/N):

Y

System: C

Satisfied with system ? (Y/N):

N

Enter System: A, B, C or D:

B

Enter input parameters:

Damping Ratio: ZETA  
Natural Frequency: F<sub>n</sub>

: 1.00  
: 0.05

Satisfied with parameters ? (Y/N):

ZETA = 1.000  
F<sub>n</sub> = 0.050

Switch FACER to VAX port and press RETURN

Bootstrap FACER to establish connection  
(message when connection established)

\* FACER CONNECTION ESTABLISHED \*

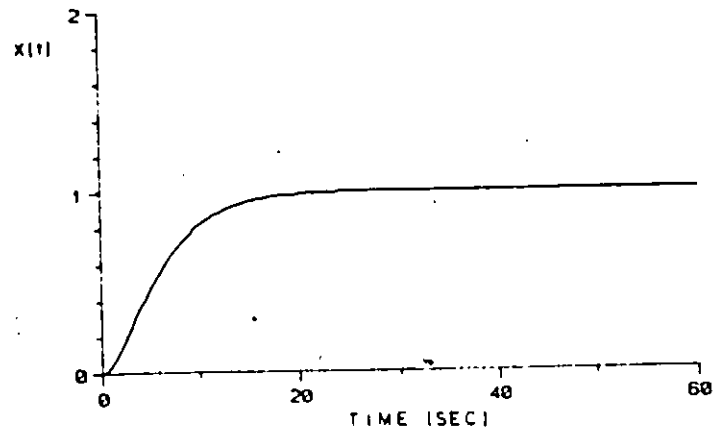
\* VAX/FACER NOW RUNNING \*

Solution time = 00.0000 Sec.

Enter output device:

Enter: S for VGT Screen  
L for Line-Printer  
H for HP Plotter

C



Any other output device ? (Y/N):

N

Output of another curve ? (Y/N):

N

S

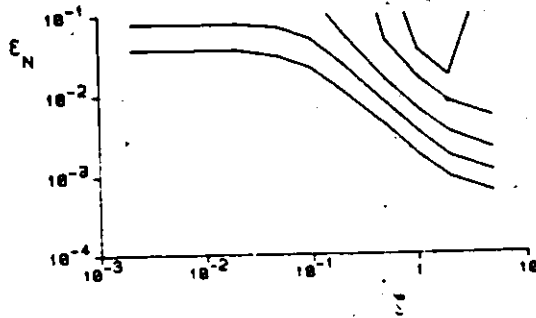
## Program RESPOND

```
1 RUN RESPOND
Enter System : A, B, C OR D
A
System : A
Satisfied with System ?
Y
1 RUN RESPOND
Enter System : A, B, C OR D
B
System : B
Satisfied with System ?
Y
Enter Theta Prime number where:
Theta Prime number: 1 2 3 4 5
Theta Prime value: 0.000 0.500 1.000 1.500 2.000
2
1
```

## Program RMSERR

```
1 RUN RMSERR
Compare System 'I' to System 'J'
where 'I' and 'J' = A, B, C or D
Enter 'I'/'J'
B/A
***** System 'H' *****
***** cannot be compared *****
***** to System 'A' *****
Compare System 'I' to System 'J'
where 'I' and 'J' = A, B, C or D
Enter 'I'/'J'
B/A
Comparing System 'B' to System 'A'
Satisfied with Systems ?
Y
Enter Theta Prime number where:
Theta Prime number: 1 2 3 4 5
Theta Prime value: 0.000 0.500 1.000 1.500 2.000
2
Theta Prime = 0.50
Comparing System 'B' to System 'A' for Ic = 0.010
Comparing System 'B' to System 'A' for Ic = 0.025
Comparing System 'B' to System 'A' for Ic = 0.050
Comparing System 'B' to System 'A' for Ic = 0.100
Comparing System 'B' to System 'A' for Ic = 0.200
```

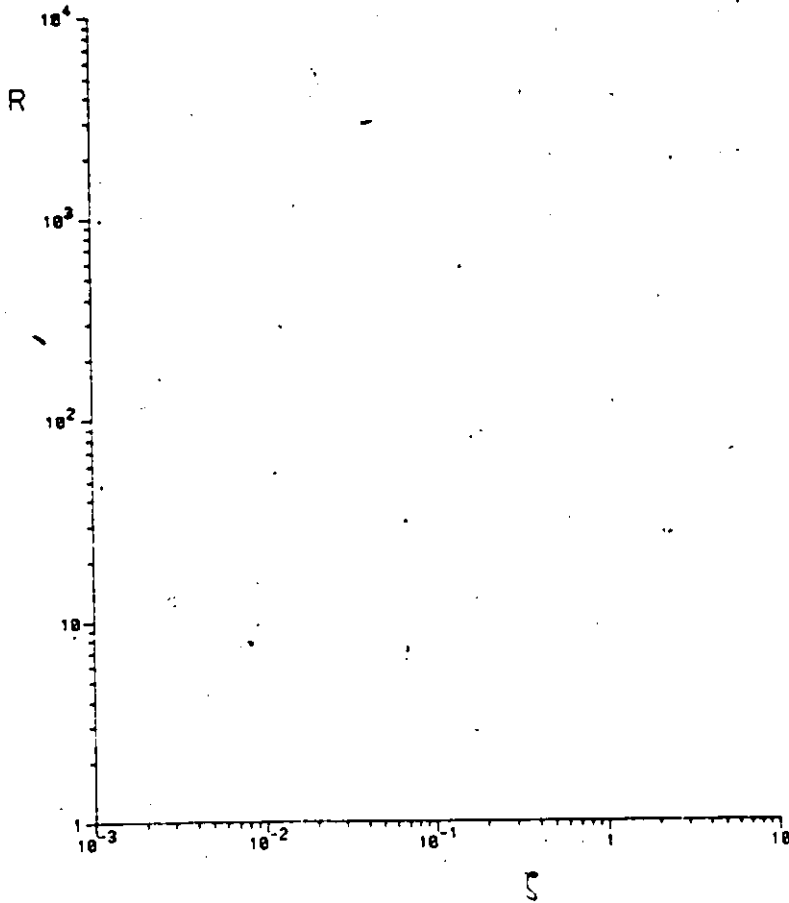
Enter output device where you  
 want graph of RMS error:  
 Enter S. for VGT Screen  
 F. for Line-Printer  
 H. for HP Plotter



Any other output device ? (Y/N):  
 N

Enter acceptable RMS error value:  
 0.001

Enter output device where you  
 want graph of acceptable error:  
 Enter S. for VGT Screen  
 F. for Line-Printer  
 H. for HP Plotter



Any other output device ? (Y/N):

N

Any other acceptable RMS error value ? (Y/N):

Y

Enter acceptable RMS error value

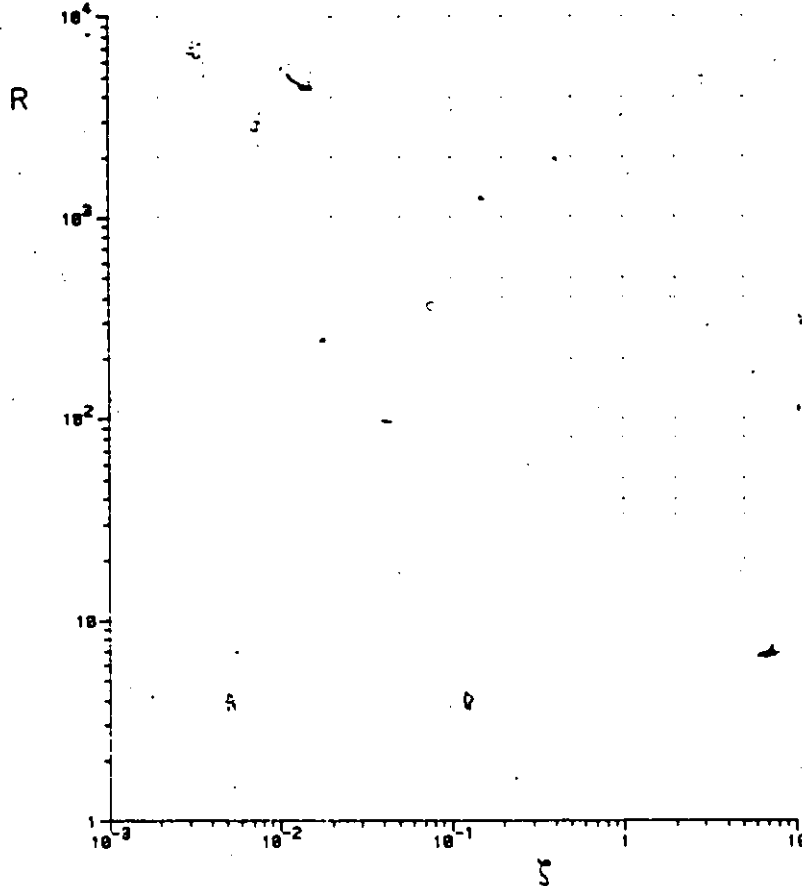
.01

Enter output device where you  
want graph of acceptable error:

Enter S, for VGT Screen

P, for Line-Printer

H, for HP Plotter



Any other output device ? (Y/N):

N

Any other acceptable RMS error value ? (Y/N):

N

S

APPENDIX L

Digital Equivalent Stability Boundaries  
Documentation

Contents

- Mathematical Basis
- Flowchart
- Listings

## Mathematical Basis

The stability contour in the complex plane of system characteristic roots derived by Vichnevetsky<sup>7</sup> is given by

$$\lambda T_c = \frac{(Z-1)Z}{\theta_v Z + (1-\theta_v)} \quad (L1)$$

where

$$\theta_v = 1.5 \cdot \theta' \quad (L2)$$

This may be transformed further to the ( $\zeta$ ,  $R$ ) plane by substituting

$$Z = e^{j\gamma} = \cos \gamma + j \cdot \sin \gamma \quad (L3)$$

on the right hand side of equation (L1), letting  $\gamma$  vary in the interval  $(0, \gamma_L]$ , where  $\gamma_L$  is given by equation (L7), and substituting for the roots of the SOLDE

$$\lambda = \omega_n (-\zeta \pm \sqrt{\zeta^2 - 1}) = \frac{2\pi}{RT_c} (-\zeta \pm \sqrt{\zeta^2 - 1}) \quad (L4)$$

where  $\omega_n = 2\pi F_n$  and  $R = (F_n T_c)^{-1}$ . By these substitutions and algebraic and trigonometric manipulations, equation (L1) may be expressed in the form:

$$\frac{2\pi}{R} (-\zeta \pm \sqrt{\zeta^2 - 1}) = \text{Re}(\theta_v, \gamma) + j \cdot \text{Im}(\theta_v, \gamma) \quad (L5)$$

where

$$\operatorname{Re}(\theta_V, \gamma) = \frac{(2\theta_V - 1) \cos \gamma + (1 - \theta_V) \cos 2\gamma - \theta_V}{\theta_V^2 + 2\theta_V(1 - \theta_V) \cos \gamma + (1 - \theta_V)^2} \quad (\text{L5a})$$

and

$$\operatorname{Im}(\theta_V, \gamma) = \frac{(2\theta_V - 1) \sin \gamma + (1 - \theta_V) \sin 2\gamma}{\theta_V^2 + 2\theta_V(1 - \theta_V) \cos \gamma + (1 - \theta_V)^2} \quad (\text{L5b})$$

The stability boundary (viz. Figure L-1 for a typical example) is given by equations (L5a) and (L5b) for a given value of  $\theta_V$  and  $\gamma \in [0, \gamma_L]$  where  $\gamma_L$  is the value of  $\gamma$  which satisfies

$$\operatorname{Im}(\theta_V, \gamma) \Big|_{\gamma = \gamma_L} = 0 \quad (\text{L6})$$

i. e.,

$$\gamma_L = \begin{cases} \cos^{-1} \left( \frac{1 - 2\theta_V}{2 - 2\theta_V} \right), & 0 \leq \theta_V < .75 \\ \pi & \theta_V \geq .75 \end{cases} \quad (\text{L7})$$

This limiting value of  $\gamma$  was determined by the fact that the roots of the system remain real for  $\zeta \in [1, \infty)$ .

The characteristic roots of the system are given by the left hand side of equation (L5). Typical root loci are shown in Figure L-1. They are complex conjugates when  $\zeta \in [0, 1)$  and real when  $\zeta \in [1, \infty)$ . The root locus in the  $\lambda T_c$  complex plane

intersects the stability boundary as follows:

(1) If  $\zeta \in [0, 1)$ , the intersection is given by equating the real and imaginary parts:

$$\operatorname{Re}(\theta_v, \gamma) = -2\pi\zeta / R \quad (\text{LB})$$

or

$$R = -2\pi\zeta / \operatorname{Re}(\theta_v, \gamma) \quad (\text{LBa})$$

and

$$\operatorname{Im}(\theta_v, \gamma) = \pm 2\pi\sqrt{1 - \zeta^2} / R \quad (\text{L9})$$

Substituting equation (LBa) into (L9) and solving for  $\zeta$  yields:

$$\zeta = \left[ (\operatorname{Im} / \operatorname{Re})^2 + 1 \right]^{-1/2} \quad (\text{L10})$$

The stability boundary in the  $(\zeta, R)$  plane is obtained by substituting values of  $\gamma \in [0, \gamma_L]$  into equations (LBa) and (L10).

(2) If  $\zeta \in [1, \infty)$ , the intersection is given by equating the real parts of (L5) and solving for R to obtain

$$R = -2\pi(\zeta + \sqrt{\zeta^2 - 1}) / \operatorname{Re}(\theta_v, \gamma_L) \quad (\text{L11})$$

where  $\gamma_L$  is given by equation (L7) and  $\text{Re}(\theta_V, \gamma_L)$  is obtained by substituting  $\gamma = \gamma_L$  into equation (L5a).

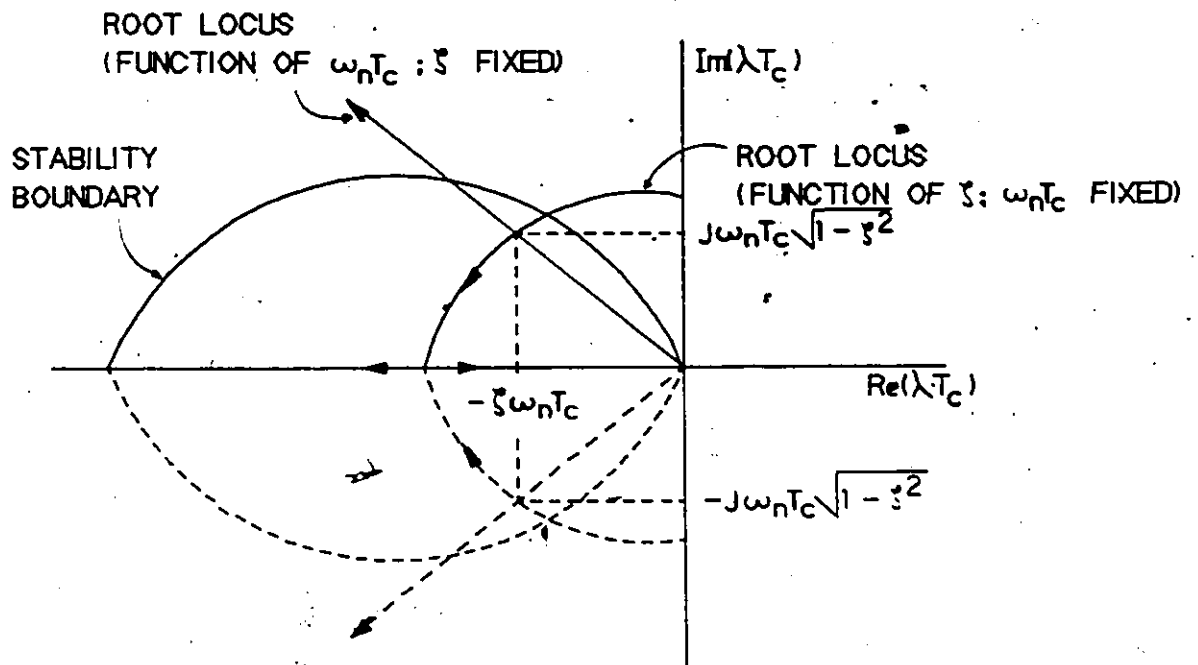


Figure L-1 : Typical stability boundary and root locus in  $\lambda T_c$  complex plane

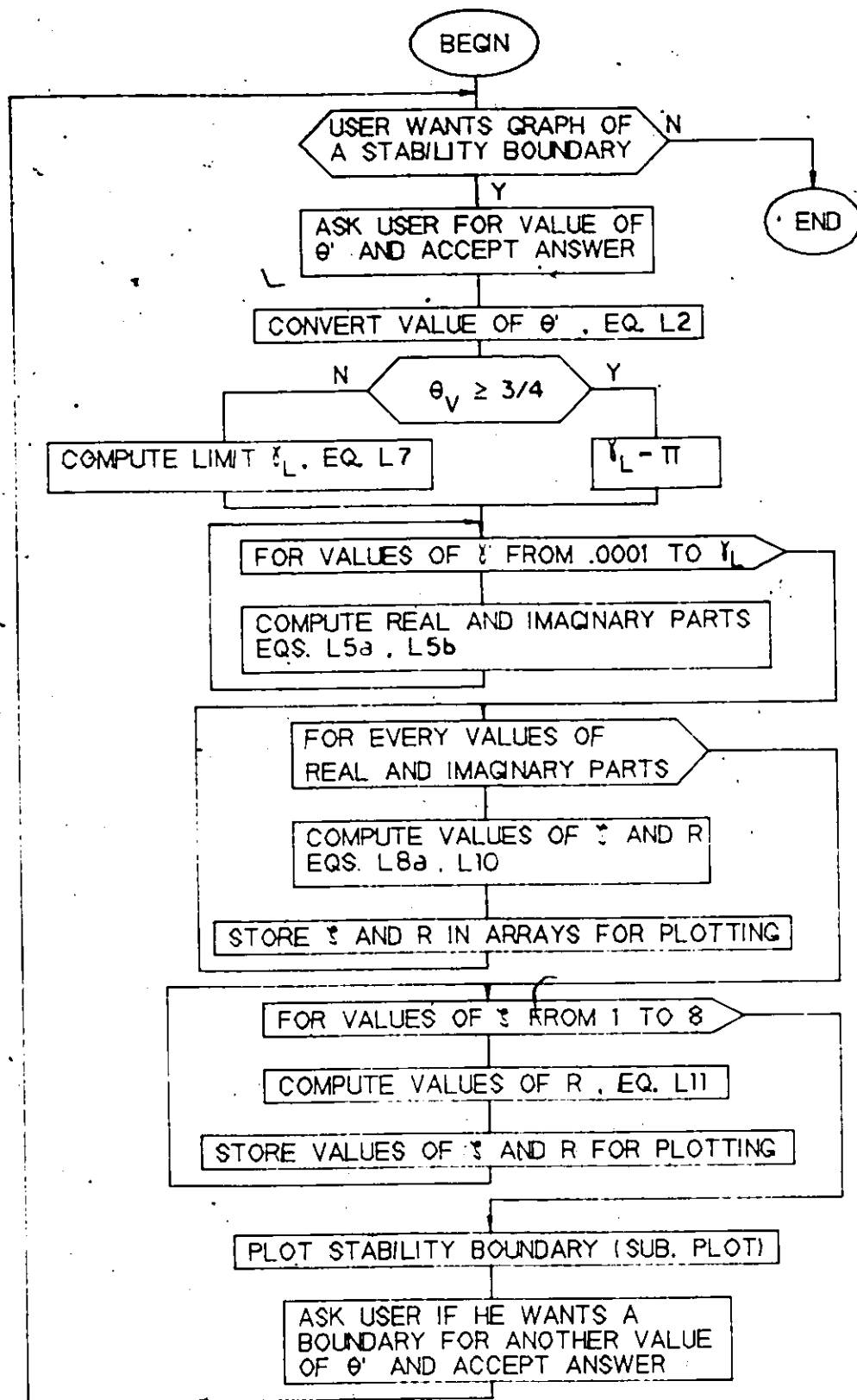


Figure L-2 : Program STABILITY flowchart



```

C _____ Compute and store values of ZETA and R for each values of IMAG and
C _____ REEL computed above .The real part must be negative
I=0
DO J = 1, NPNT
  IF (REEL(J) LT 0) THEN
    ZETA = 1 / (DSORT((IMAG(J)/REEL(J))**2 + 1))
    R = -(2 *PI*ZETA)/REEL(J)
    I=I+1
    XAXIS(I) = ZETA
    YAXIS(I) = R
  END IF
END DO

C _____ Compute and store values of R for values of ZETA=1 to 2
DO ZETA = 1, 2, .05
  I=I+1
  R = -(2 *PI*(ZETA+DSORT(ZETA**2 - 1)))/REEL(NPNT)
  XAXIS(I) = ZETA
  YAXIS(I) = R
END DO

C _____ Compute and store values of R for values of ZETA=2 to 8
DO ZETA = 2, 8, .3
  I=I+1
  R = -(2 *PI*(ZETA+DSORT(ZETA**2 - 1)))/REEL(NPNT)
  XAXIS(I) = ZETA
  YAXIS(I) = R
END DO
NPPOINT = I

C _____ Plot the stability boundary
CALL PLOT

C _____ Ask user if he wants a boundary for another theta prime
C _____ value
TYPE *
TYPE * Another stability boundary ?
READ(6,100) MORECURV
END DO

10 _____ Format statement
FORMAT(A10)
END

```

```

C _____ Subroutine PLOT
C _____ Plots stability boundary
SUBROUTINE PLOT

C _____ Specification statements
CHARACTER ANSRDEVI, DEVICE
LOGICAL MOREDEVIC

DIMENSION RESPONSE(1000), RESTIME(1000)
COMMON /RESPNSDAT/ NPOINT,RESPONSE,RESTIME

C _____ Plot curve while user wants output on any device
MOREDEVIC= TRUE
DO WHILE (MOREDEVIC)

C _____ Ask user for output device
TYPE *
TYPE * Enter output device
TYPE * Enter S. for VGT Screen
TYPE * Enter P. for Line-Printer
TYPE * Enter H. for HP Plotter
READ(6,100) DEVICE

C _____ Initialize output device
IF (DEVICE EQ 'P') THEN
  CALL OUTPUT('PRINTX', 'JKL', 0)
ELSE IF (DEVICE EQ 'H') THEN
  CALL OUTPUT('HPLOT', 'JKL', 0)
ELSE
  CALL OUTPUT('VCTERM', 'JKL', 0)
END IF

```

```

C_____ Initialize plotting
      CALL INITT(30)
      CALL BINITT

C_____ Define limits of X and Y axes
      CALL DLIMX(0.002,8 )
      CALL DLIMY(1.,10000 )

C_____ Set type of axes to logarithmic
      CALL XTYPE(2)
      CALL YTYPE(2)

C_____ Set no grid lines
      CALL XFRM(2)
      CALL YFRM(2)

C_____ Define length of tic marks
      CALL XLEN(6)
      CALL YLEN(6)

C_____ Define density of tic marks
      CALL XDEN(8)
      CALL YDEN(8)

C_____ If output is going on printer or plotter, define
C_____ location on paper and size of graph, and set software
C_____ characters in order to adjust label sizes
      IF(DEVICE EQ 'P') THEN
        CALL SLIMX(100.375)
        CALL SLIMY(50.190)
        CALL SWCHAR(1)
        CALL PLCHAR(30.50)
      ELSE IF(DEVICE EQ 'H') THEN
        CALL SLIMX(120.520)
        CALL SLIMY(160.630)
        CALL SWCHAR(1)
        CALL PLCHAR(25.45)
      END IF

C_____ Set line to solid
      CALL LINE(0)

C_____ Plot curve
      CALL NPTS(NPOINT)
      CALL CHECK(RESTIME,RESPONSE)
      CALL DISPLAY(RESTIME,RESPONSE)

C_____ End plotting
      CALL FINITT(0,0)
      CALL TRNSLT(1)

C_____ Ask user if he wants output on any other device
      TYPE *
      TYPE *, 'Any other output device ? (Y/N) '
      READ(6,100) ANSRDEVI
      IF(ANSRDEVI EQ 'N') THEN
        MOREDEVIC= FALSE
      END IF

      END DO

C_____ Format statement
      100  FORMAT(A)

      RETURN
      END

```