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NUMERICAL INTEGRATION ROUTINES
FOR THE
GEST SIMULATION ENVIRONMENT

by

Michael Ian Barrett

A thesis
presented to the University of Ottawa
in fulfillment of the
thesis requirement for the degree of
Master of Science
in

Systems Science
(Department of Computer Science)
University of Ottawa
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Michael Ian Barrett, Ottawa, Canada, 1988.

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ABSTRACT

The advances of the applications of artificial intelligence in modelling and simulation are currently an important area of research in the field of simulation. A rationale is presented to explain why this paradigm shift from traditional simulation is inevitable. Additionally, current applications of artificial intelligence in simulation environments are discussed along with some promising directions for the future.

A particular advanced simulation environment based on the Gest language which demonstrates an application of artificial intelligence techniques in modelling and simulation is highlighted. The main correspondences between simulation programs written in the Gest language and their procedural equivalents are given. This, along with some test examples showing the structure of the specification program and its procedural equivalent provide good insight for the Gest translator to be built.

The run time library for the Gest environment is developed. It is that part of the environment responsible for actually driving the simulation at run time after the model building process and the necessary translation have been completed. It includes various integration algorithms for tackling some of the non-stiff initial value problems in continuous simulation. The features of a robust simulation run time library are discussed and suggestions as to how this can be ensured in the Gest environment are proposed.

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CHAPTER 1

INTRODUCTION

Simulation is being increasingly accepted as a powerful tool for decision support. Its growth in several independent fields continues to rise with the increasing availability of computers. As a direct consequence, in the last few years, many simulation systems have begun to provide aid to the user in the model building as well as other stages in the simulation process. This aid has become increasingly important since although the users may be experts in their respective fields, their knowledge of the simulation process may be such that software tools providing advanced assistance would be welcomed. As a result, it continues to be the focus of current research to improve the simulation process using artificial intelligence techniques to meet the demands of simulation today.

1.1 AIM AND STRUCTURE OF THESIS

This thesis consists of two parts. The first part presents some of the latest developments in the field of simulation, in particular simulation environments, and how they will shape the future of the simulation process as the synergy between artificial intelligence and simulation becomes more complete. The second part looks at an advanced environment based on the Gest language (Ören 1984b) which is an application of artificial intelligence in modelling and

simulation environments. This part constitutes the major purpose of the study which is two-fold. The first contribution consists of providing pertinent information to aid in the construction of the Gest translator for the environment. This involves giving detailed information on the structures of the programs written in the specification language Gest, their procedural equivalents (expressed in Fortran 77) and the correspondence between the two as well as test examples included in the appendices of the thesis which practically illustrate this. The second contribution is in providing run time software for the execution of continuous simulation models within the Gest environment at the run time stage, once the model translation has been completed. The software is used in driving the test examples for the translator. Finally, the quality assurance of the software is discussed. Part one of the thesis embodies chapters one and two while part two embodies chapters three to seven.

In the latter part of chapter one, we discuss the basic concepts of traditional simulation. In Chapter two, the paradigm shift from traditional simulation to artificial intelligence applications in simulation is discussed. Some of the current possibilities in the field are explained in detail. These include the use of artificial intelligence in modelling and simulation environments as well as quality assurance in modelling and simulation in the artificial intelligence era. The latter discusses new classes of

quality assurance concepts and techniques which are needed— for advanced simulation environments. Finally, possibilities for future research in the field are enumerated.

Chapter three explains an advanced software environment based on the Gest language. Also, detailed explanations of Gest specification programs and their equivalent procedural programs for single and several component models are provided. Chapter four introduces the integration algorithms that will comprise the run-time library and discusses which algorithms are most advantageous for different types of problems of the non-stiff initial value type. In addition, the general purpose algorithms along with the multi-rate integration algorithm are presented in detail. Chapter five expounds the discontinuity problem along with the processing algorithm to deal with systems having such problems. In chapter six, we provide suggestions as to how quality assurance of the run - time library may be maintained within the Gest environment. Furthermore, the concept of guidance by the advanced simulation environment Gest in the selection of an appropriate integration algorithm for the model of interest is introduced. Chapter seven discusses the conclusions and the further studies that would enhance the existing research.

1.2 CONCEPTS OF TRADITIONAL SIMULATION

Simulation is a vastly used powerful decision support tool. The simulation technology has evolved over the years

from building models of systems in the form of diagrams, to more sophisticated physical prototype models to the construction of models in logical rather than physical form with the advent of the computer (Nielsen 1986). Simulation is important in decision support, control, and in aiding human knowledge processes by allowing theories to be tested practically (Birtwistle 1985). Computer simulation based on mathematical models has been used with great success for many years by engineers and scientists for analysis and design. Over the last couple of decades, the advancement and acceptance of simulation as a method of decision analysis is in sharp contrast to the early view by operations research practitioners who considered simulation as a last resort when all else failed (Wagner 1975). This advancement has been as a direct result of development in computer hardware and software making more powerful computers available at decreasing costs as well as recent advances in simulation systems and simulation methodology. This has further resulted in use and growth of quantitative simulation in other areas such as business models and management support activities. Traditionally, the major strength of a simulation model is in providing a prediction as to the consequences of a selected course of action under some experimental conditions usually referred to as a scenario (Reddy and Fox 1986). A typical application where a simulation model may be used by a decision support system is in the evaluation of two alternate courses of action to

improve the productivity of a factory. Simulation can be summed up as being experimentation with dynamic models (Ören 1986a) and the simulation model can be viewed simply as a special type of knowledge. The model is driven under some experimental conditions to generate model behaviour through time.

In the literature, two main types of simulation are discussed. These consist of discrete simulation and continuous simulation. In discrete simulation or simulation with discrete-change models, the changes which occur to the behaviour of the model are discrete and can be represented by step functions. Continuous simulation which is simulation with continuous-change models uses as its behaviour generation technique a numerical algorithm to solve a set of ordinary differential equations. However, it should be noted that a simulation study may involve a system which requires a variety of models. A systematization of the study of different types of simulation reveals a very large number of possibilities. A detailed taxonomy of types of simulation is given by Ören (1984c).

1.2.1 Elements Of A Simulation Study

In traditional simulation, as shown in Fig 1.1 the main elements of a study are the following : 1) Specification of the simulation study 2) Behaviour generation and 3) Model behaviour and its processing (Ören 1984c). Specification of

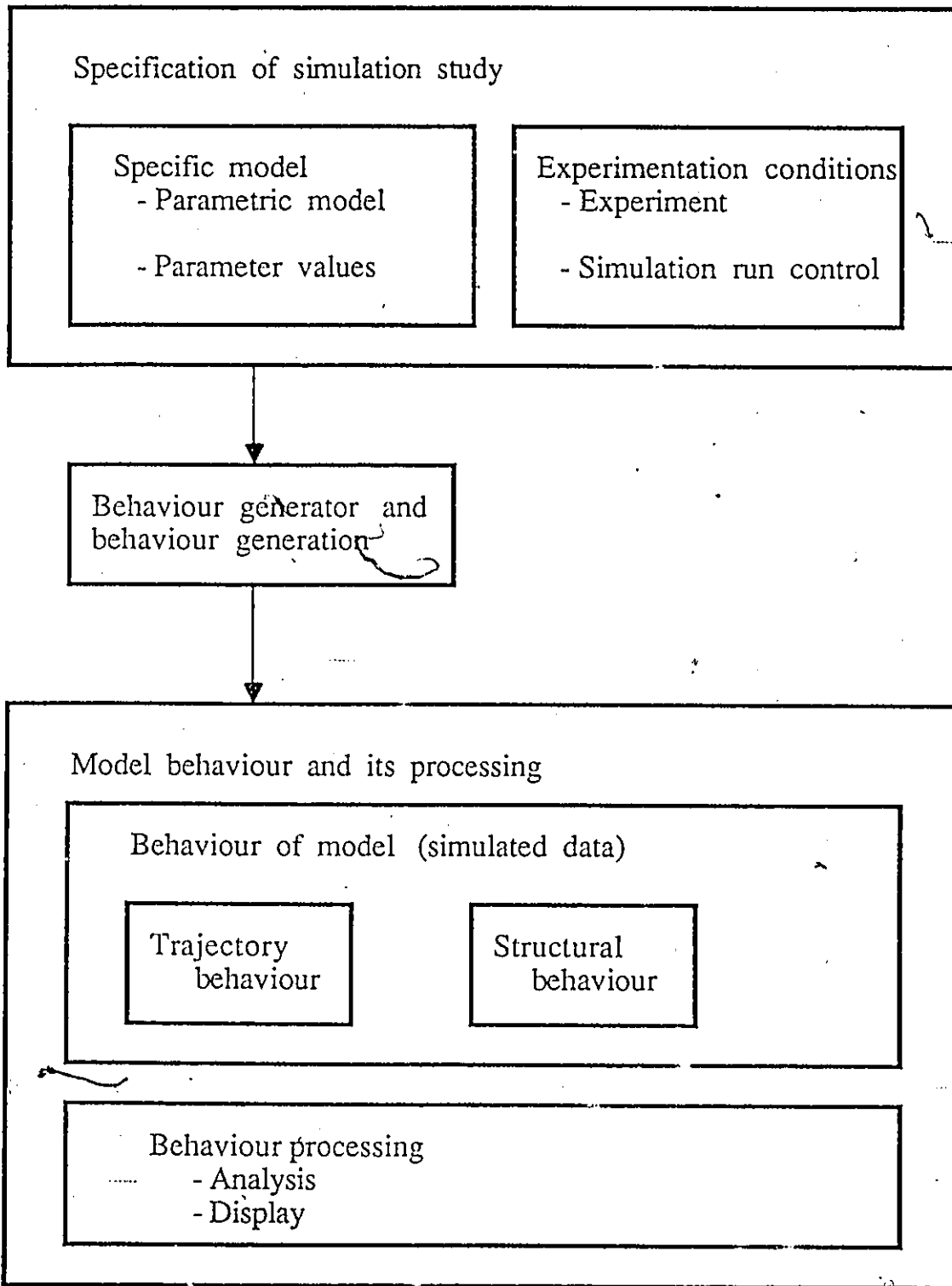


Figure 1.1 Fundamental Elements of a Simulation Study

the study requires knowledge of a parametric model and its associated parameter values as well as experimentation knowledge.

Behaviour generation is usually carried out in a computer by a behaviour generator that drives the model which comprises a parametric model and associated parameter set, under the specified experimental conditions to generate model behaviour. In simulation, model behaviour can be either trajectory behaviour or structural behaviour. In trajectory behaviour, a sequence of values of descriptive variables of interest, indexed with time, are generated. Then, using numerical or statistical techniques, the behaviour can be reduced to a figure of merit. In structural behaviour, the behaviour of a system is generated to depict a time indexed sequence of structural representations of the system. This is done under the control of a fixed or variable set of goals such as in the growth of plants in botany. After the simulation run, behaviour can be processed for analysis, compression and display purposes.

Traditional simulation is iterative. If necessary, the process is repeated for the parametric model, developing another scenario and the new experiment run. There are no design aids for developing the model. The modification of the experimental conditions and the model itself is controlled by the modeler and not incorporated into the system as an automatic computerized feature.

1.2.2 Traditional Simulation Languages

For some time now, traditional simulation languages have consisted of declarative as opposed to procedural types. Typical procedural simulation programs use a third generation language such as Fortran and traditionally have the control and data information components pertaining to the model combined in the model structure. These simulation languages are procedural since the program explicitly specifies the steps which must be performed to reach a solution.

Some continuous system simulation languages used in the former case such as ACSL, make the coding activities considerably easier. However, their execution point of view necessitates conceiving simulation programs in three sections: pre-run activities, run-time activities, and post-run activities as discussed in detail in chapter 3. This view was previously seen mainly due to the limited abilities of computers but has continued for an unnecessarily long time. As a result, traditional simulation still needs a great deal of expertise to translate the needs, goals, and objectives of the user into the appropriate model, using the right data, executed under the correct design of experiment and analyzed appropriately (Shannon et. al. 1985).

As a final remark, the principal characteristics of traditional simulation are emphasised as :

- 1) Knowledge processing of the system is limited only

.. to numerical processing.

2) Model is integrated with specification of experiment and behaviour generation.

CHAPTER 2

ARTIFICIAL INTELLIGENCE IN SIMULATION

2.1 THE PARADIGM SHIFT FROM TRADITIONAL SIMULATION TO
ARTIFICIAL INTELLIGENCE APPLICATIONS IN SIMULATION2.1.1 Introduction To Artificial Intelligence And
Expert Systems

Artificial intelligence deals with the discovery of techniques that will allow us to design and program machines which are able to emulate certain characteristics of human thought such as the ability to learn, solve problems and understand small contexts of human language. Artificial intelligence research which looks at how humans acquire, organize, and use knowledge can be categorized into :-

- 1) Attempting to duplicate or imitate the rational knowledge processing abilities in the same manner humans do. An example includes natural language query systems which allow the user to ask questions of a data base without using special commands.
- 2) Ability to use knowledge and learn so as to duplicate the results of learned skills or expertise without concern for whether it is exactly the process used by the human expert. This is often termed expert systems or knowledge-based systems. These are knowledgeable systems which may increase their knowledge by learning and have advanced knowledge processing characteristics including symbolic knowledge processing.

Expert systems research has grown out of more general concerns in artificial intelligence and is considered by some researchers to be "applied artificial intelligence." An expert system is a computing system capable of representing and reasoning about some knowledge-rich domain, such as internal medicine or geology, with a view to solving problems and giving advice (Jackson 1985). Feigenbaum, one of the pioneers in research and development of expert systems, has defined an expert system as:

" .. an intelligent computer program that uses knowledge and inference procedures to solve problems that are difficult enough to require significant human expertise for their solution. Knowledge necessary to perform at such a level, plus the inference procedures used, can be thought of as a model of the expertise of the best practitioners of the field."

(Harmon, P., King, D. 1985)

2.1.2 Rationale For And Description Of The Paradigm Shift

Changes of paradigm always seem to take an unnecessarily long period of time primarily due to dogmatic thinking in most cases. However, there is a need to see simulation in a new light and it is inevitable that artificial intelligence will have a tremendous impact on simulation as we know it today (Ören 1984c). This need arises out of the fact that simulation is being utilized more and more in a variety of

fields and it is clear that traditional systems could benefit from further enhancements. The original requirements of such systems can be further enhanced via model processing abilities as well as experiment control and evaluation of simulation results. A variety of tools and techniques from the artificial intelligence field for working with knowledge models have only recently been applied to traditional simulation.

Artificial intelligence and simulation are based on models to generate new knowledge. In the case of a rule-based system, inference is used to generate knowledge. In the case of simulation, knowledge is generated by driving the model under experimental conditions. In particular, there is a methodological similarity between simulation models and expert systems (Shannon et. al. 1985, Lehmann 1987). These include :

- 1) Expert systems and simulation both represent in a modular form knowledge and expertise about a system and its behaviour in specific domains. The knowledge representation involves the use of events and processes in discrete event simulation and frames, rules, etc. in expert systems.
- 2) The control flow in expert systems and simulation both depend on logical decisions in contrast to numerical values calculated in other programs. The control or inference mechanism for an event driven

simulation can be described as a next-event time scheduling similar to inference mechanisms such as forward or backward chaining in expert systems.

- 3) There are similarities in the description and processing of uncertainty in a model as well as in an expert system. In stochastic simulation, this uncertain knowledge is expressed by probabilities and in an expert system application by means like certainty factors, fuzzy logic etc.

As a result techniques and results from artificial intelligence and particularly expert systems appear to offer a new and exciting technology for simulation application.

The paradigm shift in simulation is towards the use of artificial intelligence techniques in simulation. Knowledge-based simulation is the name adopted to describe this synergy. It deals specifically with knowledge-based techniques for model building and processing such as execution and analysis. This area of research in artificial intelligence concerned with building of tools and expert aids, has had a significant effect on the modelling and simulation field. The main benefits achieved using an artificial intelligence based simulation tool include :

- 1) Aids in improving the process of transcribing the real world problem into the simulation thus shortening the development time of the model.

- 2) Structural changes can be carried out a lot quicker with faster synthesis and/or modification of simulation by the user.
- 3) Reduces the time required by users to work with the system since there is no need to learn a simulation language and develop modelling skills.
- 4) Improves the average user's quality of interpreting simulation runs and case studies.

Systems utilizing such tools would be responsible for the following developments to name a few :

- 1) A simulation query system which the user can use to determine the behaviour of some model or models in a model base, maybe with respect to a particular problem.
- 2) The creation of models for a specific problem in a well understood domain via a modelling environment.
- 3) Use a behaviour processing system to provide for analysis and display.

2.2. CURRENT APPLICATIONS OF ARTIFICIAL INTELLIGENCE IN SIMULATION ENVIRONMENTS

In the past few years due to the increasing abilities of computers on symbolic processing and the general maturing of the simulation field, the focus of simulation languages and

packages has changed and is being replaced by a more comprehensive concept, namely simulation environments (Ören 1986b). The creation of such environments is one of the possibilities for artificial intelligence to have an impact on the simulation field. These environments should be created to take advantage of current computer capabilities for data base management and graphics to name a few. The simulation environment is the term used to denote a comprehensive computer-aided design and simulation system. Furthermore, Henricksen (1983) defines an integrated simulation environment as "a collection of software tools for designing, writing, and validating models; writing and verifying simulation programs; preparing model input data; analyzing model output data; and designing and carrying out experiments with models." This is essentially the goal of artificial intelligence based expert simulation systems, in addition to embedding as much expertise into the simulation software as possible.

There is a clear need for simulation environments which provide an integrated and comprehensive set of tools for all areas of simulation (Langer and Schmidt 1987). Within a simulation system, three main kinds of environments are desirable: 1) Simulation modelling environment 2) Model processing environment 3) Environment for analysis of simulation results. These environments are discussed in detail in the following sections.

2.2.1 Simulation Modelling Environments

The simulation modelling environment is concerned with the ~~model building stage~~ of the simulation process. The environment assists the user in the model building process by providing a variety of software tools. Advanced user/system interfaces are commonly provided to simplify the user's task of specifying the model. Additionally, during the model creation, an advisory system guides the user with explanation thus ensuring model completeness and certification.

A major concern of current software developers is the interface between the user and the computer. Artificial intelligence researchers are among those developing user friendly interfaces to improve this communication. Advanced user/system interfaces enable the user to focus on the problem definition and analysis of results. It helps to form an advanced user/system interface for a simulation model for use by an inexperienced simulationist. The simulationist is able to develop and modify the model without requiring previous knowledge about the simulation language or programming environment. Such interfaces are significant contributions to the field providing better user control of his/her model and thus increased efficiency in the modelling process (Khoshnevis and Austin 1986).

As proposed by Ören (1986b), in an interactive environment, the user would have a display unit on which

several concurrent, overlapping or non-overlapping windows may be seen. The windows may consist of: 1) Design and simulation windows to display the design and trajectories of descriptive variables. 2) Active icons that can be selected for model design. 3) Dialog diary to display system messages and user invoked tasks and operations. 4) Instruction window to specify to the system a particular operation which has to be operated on a given object related with a task. Recent simulation modelling environments provide similar advanced user/system interfaces.

The knowledge base simulation system developed by Reddy and Fox (1986) uses a window-based schema editor, which offers a fairly general facility to create or alter schemata. The model is a collection of schema representation language schemata that represents physical and abstract system entities. Model creation is simply the creation of schemata that represent the model's entities, including specifications for their event behaviour and interconnections with other schemata. One window displays the schema being edited, while the other window accepts commands to manipulate that schema.

In the intelligent simulation model generator (Guariso et. al. 1987), the interface is incorporated into the LISP environment and input and output are mainly performed via menus, forms representing the frames and graphics. The slots of the frames provided are filled by the user, the editing

being performed by extensive use of windows. An example is the use of the graphic editing window in creating compound models or models with several component models.

The Simplex II Simulation System (Langer and Schmidt 1987) is easy to use due to its menu-driven user guidance. For each complex system feature a menu is provided, which includes the necessary commands to perform all possible functions of this feature. These commands manipulate individual model components (create, copy, modify etc.) and also manage the various model banks. In the Gest environment which is explained in detail, in chapter 3, the system aids in the generation of the Gest source program using a model template generator which generates appropriate templates or frames whose slots are to be filled by the user.

Finally, it should be realized that it is technologically feasible to build natural language interfaces for domain specific applications. Additionally, a natural language representation of continuous systems is feasible since they have only a few types of variations in the transition logic (Khoshnevis and Austin 1986). It should be noted, however that while natural language interfaces are feasible solutions to human interface problems one must assess and determine when such an interface is feasible. Rich (1984) outlines seven key factors that should be considered in such a choice.

A truly successful understanding system incorporates knowledge about language, grammar, semantics and the specific domain of the problem. A natural language interface for model building is appropriate because of the variety and complexity of the inputs for problems formulation.

An advisory system is an expert system that uses a knowledge base and inference system to provide the user with relevant expert advice on fault finding as the consultation proceeds. It is a decision support tool that guides the user in correcting the fault. Simulation knowledge must be separated from domain knowledge. As would be expected, then, two different types of advisory systems are perceived in simulation, namely those with expertise in simulation and those with expertise in an application domain. Two main types of advisory systems are proposed. These consist of: 1) expert systems knowledgeable in the simulation methodology and 2) expert systems knowledgeable in the domain knowledge.

Another important feature of the advisory system is that they should possess explanation facilities. These facilities generate explanations so as to try to address or substantiate the accountability of guidance given by advisory systems. They do this by systematically relating to the chains of reasoning employed by rule-based systems. This is done by backtracking through the processes of inference used in generating the advice and presenting the

user with the knowledge used at each stage. One of the main compelling reasons for the requirements that advisory systems should be able to explain their reasoning and justify their conclusions in a manner that is intelligible to users is (Jackson 1985): 1) The users of automatic advisory systems need to be convinced that the reasoning behind a conclusion is substantially correct, and that the solution proposed is appropriate to their particular case. Finally, the advisory system has certification functions which are responsible for certifying the model.

The knowledge-based simulation system (Reddy and Fox 1986) contains a language and an interpreter so as to specify model consistency and completeness rules. Additionally, the logic programming techniques are incorporated in the Schema Representation Language. In this way, the knowledge-based simulation system evaluates the model using the interpreter's trace facility to aid in finding and explaining errors such as missing schemata and schemata with inconsistent slot values. The advisory system in the intelligent model generator (Guariso et. al. 1987) performs consistency checks and informs the user, forcing him to correct the errors found or to quit his current action.

The Simplex II Simulation System performs only syntactic checks on models to ensure they are syntactically correct. The advisor for modelling present in the Gest environment is

called Magest . Magest uses its available knowledge to assist the user in the model specification and performs several syntactic as well as semantic checks to ensure the model's certification. These checks consist primarily of checks for completeness, correctness, and compatibility. The available knowledge consists of: 1) problem independent knowledge concerning the morphology of Gest programs 2) incremental knowledge obtained from and about user specified Gest programs. The details of the rules and facts used by Magest to perform semantic checks can be seen in the recent article by Ören and Sheng (1988).

The use of the advisory systems and advanced user/system interfaces outlined above makes the modelling simulation environment within the simulation system a useful tool in aiding the user in the model building process.

2.2.2 Experimentation Specification And Model Processing Environments

The experimentation specification and model processing environments may be responsible for a variety of functions such as specification of experiments, simulation execution, and data collection. The experimentation environment would consist primarily of an experimentation advisor, an experimentation base, and its manager (Ören 1986b). The advisor may have several functions including:

- 1). Specification of experimentation including

specification of variables to be observed and monitored. The specification of the variables to be observed includes behaviour compression types (e.g. statistical), behaviour display period (beginning, end) and frequency (communication interval). An example of the specification of variables to be monitored involves having audio/visual warnings when a critical variable reaches a threshold value.

- 2) In the case of multiple runs, experimental conditions can be modified based on specification of generic experimental conditions. In the simplest case, the system can directly link to a model different experimental conditions specified by the user. It may have the ability to conduct a series of experiments without human intervention. Individual experiments should be improvements on past experiments. The improvements are automatically achieved by rule bases detailing the diagnosis and correction heuristics (Reddy and Fox 1986). The rules must allow for reasoning between several model scenarios. The Simplex II Simulation System (Langer and Schmidt 1987) contains an experimentation environment. This environment provides a menu experiment which allows various experiments to be performed on the model.

Symbolic model processing is possible during the

execution of the simulation. At the end of each simulation run, a rule can be activated from a rule base that will suggest changes to the model for the next run. After running many of these goal-directed experiments, we hope to get scenarios that come close to satisfying the simulation goal (Reddy and Fox 1986). A limit on the number of experiments prevents the system from getting lost while determining a desirable scenario.

Data collection is concerned with recording the changes in the value of a parameter. This is usually done either by constantly monitoring the parameter or by sampling the parameter (Reddy 1987). The parameter to be monitored usually has attached to it instruments for measuring current values to be displayed. In the knowledge-based simulation system, monitoring is done by attaching demons to slots and the process of data collection is similar to measuring instruments. Usually, only data relevant to a particular goal is gathered and analyzed and the user is required to manually instrument each schema. The menu item called Monitor in the the Simplex II Simulation System is available for the user to select which model variables are to be recorded during the experiment for subsequent analysis and display, the menu present being subsequently used to graphically output the results.

2.2.3 Environment For Analysis of Simulation Results

This environment is primarily concerned with analysis of the simulation results. This is a recent feature in simulation systems. Within the knowledge-based simulation system, scenarios can be rated to measure the goodness or badness of simulation results. This is important so that the analyst can fine tune the input parameters to the model in order to bring the values of output variables within a desired range. The Simplex^{II} Simulation System has available a menu item called Analyze which contains methods for the mathematical analysis of data which has been recorded by the monitor.

It is clear that current applications of artificial intelligence in simulation environments have made a positive impact on the aid given to the user throughout the simulation process. Current systems tend to place more emphasis on the modelling simulation environment with less emphasis on the other environments described above especially the environment for analysis of results. This trend is changing and future systems can be expected to have a variety of tools available in the three main environments.

2.3 DIRECTIONS FOR FUTURE RESEARCH

The latest developments in the area of simulation

strongly indicate that AI based simulation systems will be the trend in the near future. Many areas such as manufacturing are adopting this trend and the first steps and attempts in this direction have been taken (Shannon et. al. 1985).

Although a plethora of ideas could be suggested, Oren (1987b) Shannon et. al. (1985) and Elzas (1986b) have proposed that major developments in artificial intelligence based simulation environments can be expected to be seen in:

- 1) Improved dialogue facilities with modelling and simulation systems especially those possessing model bases via advanced intelligent interfaces. These interfaces can be improved using AI techniques such as the use of natural language programming for problem specification.
- 2) Future model bases which should provide access to models and submodels developed earlier in similar applications. They could be stored using a specification formalism in a number of domain specific model bases (Kettenis 1986). The model base would consist of a number of clearly written, well documented models.
- 3) Expert systems for modelling and simulation consultation. These systems would be very useful in providing advice as to which model in a model base is best suited for a particular application.

- 4) Model search and inferencing from assemblies of model components in model bases for a particular domain.
- 5) Intelligent simulation model generators to perform automated simulation program generation from structured model and experimental frame specification.
- 6) Advanced methodological concepts involving the possibility of generating experimental condition and interpretation of results within simulation environments.
- 7) Advanced tools to cope with the complexity of systems. This would involve design of other knowledge-based tools such as KEE (Fikes and Kehler 1985).
- 8) Expanding the knowledge available in current knowledge based environments to include domain specific knowledge on different application areas.
- 9) New knowledge representation structures in artificial intelligence environments for modelling and simulation support systems.
- 10) Input data management systems capable of storing, manipulating and retrieving data for specific

simulation experiments. It would require the ability to distinguish which data is needed for the different experiments.

- 11) An experiment supervisor which would make decisions based on the output of simulation runs e.g. sample sizes, number of runs needed etc.

In the last couple of years, the field of artificial intelligence in simulation has grown tremendously and continues to mature. Several books already exist on the topic: Birtwistle (1985) Elzas, Ören and Zeigler (1986), Holmes (1985), Kerchoffs, Vansteenkiste, and Zeigler (1986), Luker and Adelsberger (1986), Luker and Birtwistle (1987), Widman, Loparo, and Helman (1987) whilst others are now in preparation such as Elzas, Ören, and Zeigler (1988 + In Preparation). It is quite clear that some of the developments discussed above will become a reality in the near future thus realizing yet more advanced simulation environments than those available today.

CHAPTER 3

GEST AND ITS ENVIRONMENT

3.1 SOFTWARE ENVIRONMENT FOR GEST

3.1.1 The Gest Language

Gest, which stands for General System Theory Implementor, is based on the axiomatic system theory of Wymore (1967) and departs radically from other simulation languages in that the specifications of the model and the experiment are totally separated. It is the first model and simulation specification language. As a result, it is declarative in nature acting as documentation easily comprehensible by users.

In the Gest language, a program has several distinct parts (Oren 1984b):

- 1) Mathematical Model
- 2) Parameter Set
- 3) Experimentation(s) and
- 4) Output Module(s)

The model consists of a parametric model and associated set(s) of parameter values. The experimentation is the specification of experimental conditions which have to be applied to the model. The output module is the specification of the output program to be used to display the results of the simulation study. The definition of a Gest program expressed in Backus-Naur form (BNF) is as

follows:

Program -

```

    "Program" Program Identifier
    Parametric Model Specification
    [{Parameter Set}]
    {Experiment}
    {Run Specification}
    {Output Module Specification}
    "End Program" Program Identifier

```

In the BNF representation, non-terminals are enclosed within " ". { } indicate repetition, [] indicate options, [{ }] indicate repetition of optional elements.

3.1.2 Elements of Gest Environment

The world view of Gest makes it a good basis for a comprehensive modelling and simulation environment. This environment is a major project currently being implemented at the University of Ottawa. It will provide assistance to users in the development of models in several application areas. As depicted in Figure. 3.1, the elements of the Gest environment consist of the following main components:

- 1) Gest executive
- 2) Magest system
- 3) Gest Translator

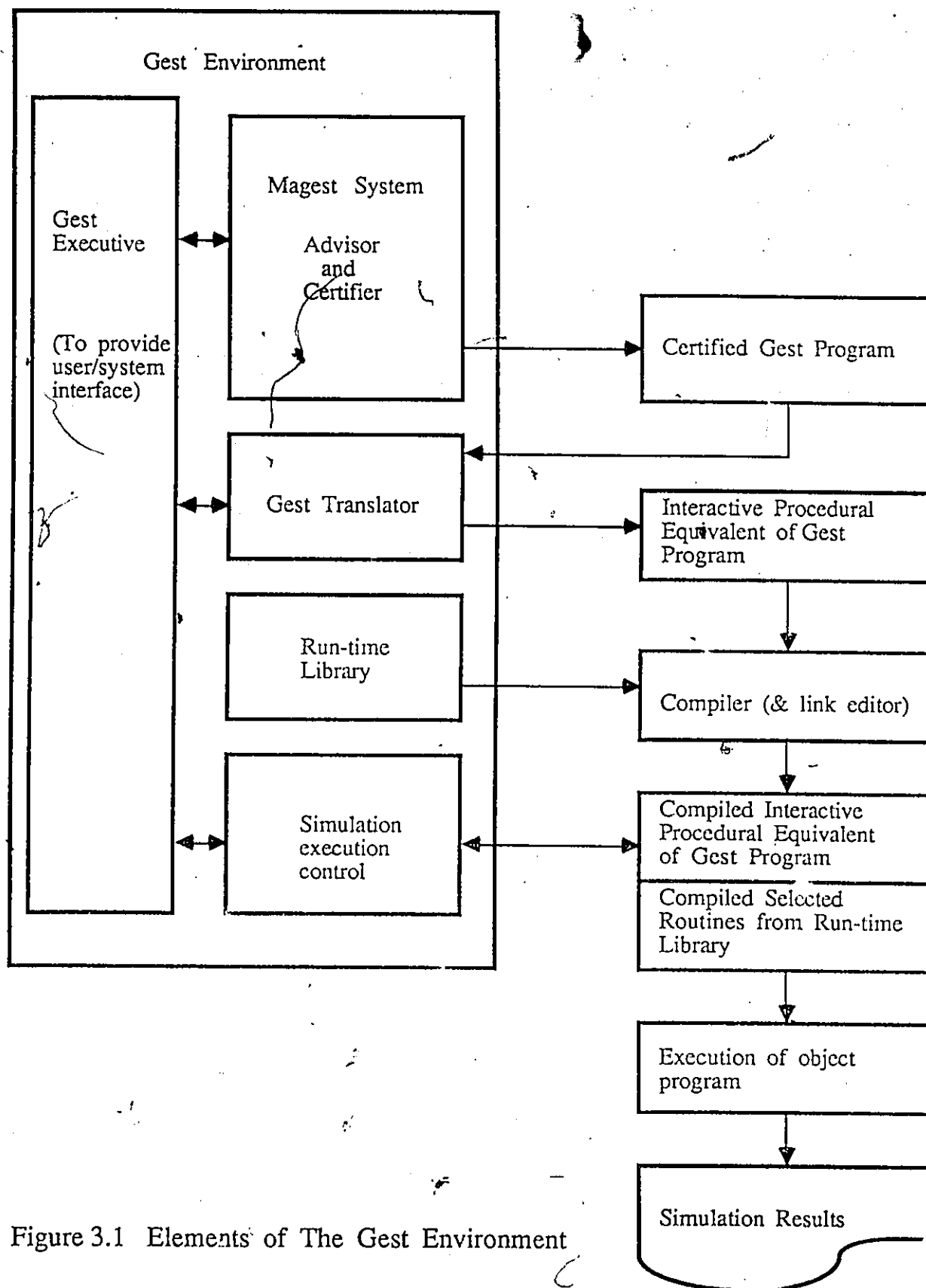


Figure 3.1 Elements of The Gest Environment

- 4) Gest Run-Time Library
- 5) Simulation execution control

The Gest executive is the user/system interface that assists the user at each stage of the simulation process. The executive is linked to the Magest system which provides assistance in the model building process. Additionally, it is connected to the simulation execution control, so that the user may be interactively involved in the execution of the simulation runs. Magest which stands for modelling advisor and certifier for Gest programs is a knowledge-based modelling and simulation system. It provides a user/oriented specification and certification environment for Gest. It has basically two modes of operation, the guidance mode and the certification mode. It also has access to a template file from which it can select templates and then tailor them dynamically.

In its template generating mode, Magest provides a dynamic template of the Gest source program or frame-like structure whose slots are to be filled by the user. As an example, for every component model, a template of static and dynamic structures are generated. The user then fills in the relevant model information in the appropriate slots. This is illustrated in Section 3.2.1. In this way, Magest guides the user in the specification of a model, parameter set, and experimentation.

During the generation of the Gest source program in the above manner, the certifier and advisor program uses its available knowledge to assist the user in the specification of his model and also performs several syntactic as well as semantic checks. These checks consist primarily of checks for completeness, correctness and compatibility of the specification.

The Magest system provides computer assistance by ensuring consistency and completeness of the specifications. The assistance provided by the system to the user while specifying his Gest program, also involves knowledge-based help on parameters to be specified as well as details on the experimentation specification pertaining to each component model such as initialization of all state variables.

Finally, once a Gest program passes these checks made by Magest, Magest then certifies the program making it ready for translation by the Gest Translator into an interactive procedural program.

The Translator will translate the declarative Gest program into an interactive procedural program. This program is then compiled by the procedural language compiler to allow for future execution.

The Translator recognizes three distinct levels of activities namely:

- 1) Pre-Run Activities

2) Run-Time Activities

3) Post-Run Activities

The pre-run activities involve the declaration of variables, initialization of state variables, parameters, input values, and run-control variables.

The run-time activities are concerned with experimentation with the model. These activities involve the determination of model inputs, outputs and the calls to the relevant integration algorithm in the Gest run-time library for integration. In the case of a model with several component models not utilizing the multi-rate integration algorithm, the translator lumps the differential equations of each component model into a derivative subroutine consisting of a single collection of differential equations. This derivative subroutine is used by the integration algorithm to integrate the model. In the case where the multi-rate algorithm is used, the large model which has widely varying characteristics is partitioned into two component systems having similar characteristics. They additionally have independent error control and utilize the best suited algorithm for each component model. The Gest translator in this case translates the specification ensuring two derivative subroutines containing the differential equations describing the two component models exists.

The post-run activities involve display of model results in tabular as well as graphical forms.

For all the activities described above, the necessary information required by the translator to determine these activities is taken from the pertinent modules of the Gest specification. This correspondence is explained in detail in Section 3.2.1.3.

The Gest run-time library consists of a variety of integration algorithms to deal with the different situations that arise in continuous simulation. The user expresses his choice of integration algorithm dependent on his model's needs in the experimentation section of his Gest Program. The Magest system ensures that the chosen algorithm is indeed available in the run-time library and may give advice to the user on the suitability of the chosen algorithm to the model at hand.

Then, during the execution phase, after the relevant inputs and outputs have been determined, the next states are computed by utilizing the relevant integration algorithm within the Gest run-time library via a call statement along with the subroutine DERIV containing the necessary functions and information to carry out the computational steps. The details of the proposed Gest run-time library are given in Chapters 4, 5, and 6.

Finally, the simulation execution control allows the user

to be interactively involved with the procedural equivalent of the Gest program. This may include the different specifications of the simulation runs to be executed for the different scenarios desired by the user.

3.1.3. The Disspla Software

Within the IBM environment, the Disspla software is the graphics package utilized by the Gest environment in providing post-run graphics of the simulation results at the end of the simulation. This 'high-level' plotting language which requires a minimum number of CALLS to produce graphs is used to facilitate data plotting in the Gest environment. It is machine independent as well as graphics device independent, enabling the user to take full advantage of the characteristics of a variety of output devices.

Once the translated procedural simulation program is run, the program is linked to Disspla to give post-run plots of the results of the simulation model. The graphics subroutine in the procedural program which utilizes the library Fortran subroutines available in Disspla, first determines and rounds the maximum and minimum values of the elements of the arrays of the variables of interest. These variables of interest are the outputs of the simulation for which the trajectory plot is required. Once these values are determined, scale factors are automatically generated in the subroutine by simple calculations. These factors along

with the maximum and minimum values are then used as arguments for the Disspla subroutines to generate the desired trajectory plots. For each model, the only significant changes to the graphics subroutine would involve labelling of axes, and title names. Full details of the Disspla software can be seen in the Disspla user's guide (ISSC 1982). In each of the test examples for the translator provided in this thesis, a graphics subroutine utilizes Disspla routines for carrying out the desired data plots.

3.1.4. The Xmenu/e Software

The XMENU/E software is used to provide interactive ability in the procedural equivalent of the Gest program. The XMENU/E system is a collection of programs that allow interactive creation and manipulation of display data and menus. XMENU/E allows the user to create and use full screen menus quickly and easily under his application program. Menus are useful tools for presenting users with a formatted list of options and input areas. XMENU/E provides the following basic facilities : 1) The XMENU program which allows the user to interactively create and modify his/her menus. 2) XMENUSUB, a collection of subroutines which can be called to use menus from programs written in high level procedural languages such as Fortran and Pascal.

As a result, this software can be utilized as a tool for interactive procedural programs. For a particular model, the

menu consisting of model parameters, initial values, experimentation variables, and relevant user information is created. Menu creation is performed on a blank input screen using PF keys to assign fields. The menu can be viewed as comprising of a number of fields with particular characteristics called 'attributes'. The fixed information on the menu have the following attributes : 1) PROT - The user is not allowed to enter data into that field from the terminal. 2) SKIP - This attribute facilitates easy access to the slots that need to be filled by the user. 3) DIM - The intensity of the field is given a normal display. 4) NMDT - This represents a no modification tag since these fields will not be modified at any time.

The slots which need to be filled by the user have the following set of attributes : 1) NUMERIC - This is an unprotected field that allows the user to enter only numeric data from the terminal. This is an obvious advantage for our purposes of simulation ensuring model integrity. It should be noted, however, that this attribute is only operational from some terminals such as the IBM 3179G terminals in the current version of the software. 2) NOSKIP - This attribute ensures that the user enters the appropriate input data. 3) BRIGHT - This attribute highlights the input, giving a bright intensity. 4) MDT - This Modified Data Tag ensures that data in each input field will be returned to the program as user input. At each simulation run, the current values are used in the simulation.

The XMENU/E software is first linked to the user's disk. The interactive procedural program is run, and with the aid of the appropriate subroutine from the XMENUSUB, the appropriate menu is presented to the user. The user is requested to fill in the slots according to the model, after which, he returns control to the program by selecting an appropriate PF key (in the current implementation PF 10 or PF 12) as specified on the menu. With the aid of subroutines from the XMENUSUB, the program is able to use the values from the menu to run the simulation. Another subroutine prints the values used for that particular simulation run into a file which is available to the user. This process is repeated for each simulation run which the user desires to carry out. The XMENU/E procedures are utilized in most of the test examples in this thesis to provide the desired interactive abilities of the procedural equivalents of the Gest programs.

3.2 STRUCTURE OF GEST AND EQUIVALENT PROCEDURAL PROGRAMS

In this section, detailed structures of the two main types of Gest programs for continuous simulation and their equivalent in a procedural language are provided. These involve specifications of continuous change models which are a subset of the possibilities available in the Gest language. In particular, the two main types are a Gest program with a single continuous component model and the

Gest program with several component models. For Gest programs with a single continuous component model, the ability to specify an updateable continuous change model is discussed. In the case of the Gest program with several component models, the ability to specify the Gest program using the multi-rate integration is also discussed. The structures show how programs are developed to facilitate the simulation of a user's model, whether it is a purely continuous model, a piece-wise continuous model, or a large dynamic system. Also, the correspondence between the Gest programs and their procedural counterparts are provided along with the computational steps needed in the simulation of the different types of models discussed. This information along with the Gest examples provided in the appendices of this thesis will aid in the construction of the Gest translator for the environment.

3.2.1 Gest Program : One Component Model

3.2.1.1 Gest Program

As shown in Figures 3.2(a) and (b), the Gest specification of a single component model consists of :

- 1) A parametric continuous component model
- 2) At least one parameter set

```

-----
| Program (Name)
|-----
| Continuous Model (Name)
|-----
|   Static Structure
|-----
|     Inputs (including Random if any)
|     States
|     Outputs
|     Auxiliary Variables
|     Constants
|     Parameters
|     Tabular Functions
|-----
|   End Static Structure
|-----
|   Dynamic Structure
|-----
|     Derivatives           : State equations for computing
|                           : values of state variables
|-----
|     Output Function       : Function for computing output
|     (optional)
|-----
|     Update (optional)     : Model update made when a particular
|                           : condition is satisfied
|-----
|   End Dynamic Structure
|-----
| End Continuous Model (Name)
|-----

```

Figure 3.2(a) Gest Specification of a Parametric Component Model

Parameter Set
Assignment of Parameter Values
Assignment of Tabular Function values
End Parameter Set
Experiment
External Input Function
End External Input Function
Time Initialization
Initialization of states
Integration utilizing some particular algorithm
Interpolation used (if any)
Assign user tolerance
Assign frequency of communication
Collect and save inputs and outputs
Specify end time of simulation
End Experiment
Run
Specify the triplet : (Model, Parameter Set, Experiment)
Post-Run Requirements (optional)
End Run
Output Module
Print output heading
List values of saved variables
Plot values of saved variables
End Output Module
End Program (Name)

Figure 3.2(b) Gest Specification of Parameter Set, Experimentation and Output Module for a Component Model.

3) At least one experimentation specification

which consists of :

- an experiment
- a run
- an optional post-run specification

4). An Output Module

The continuous component model consists of two sections:

1) static structure section and the dynamic structure section. The static structure is descriptive, and contains all the model descriptive elements such as inputs, states etc. as shown along with their types and ranges of values where applicable. The dynamic structure contains information needed for behaviour generation. This includes 1) a derivative block which contains the derivatives of state variables along with any computations necessary for auxiliary variables. 2) An optional output block containing output function(s). In cases where an output variable is not identical to a state variable, or an auxiliary variable, it must be computed from an output function. 3) An optional update block. This block provides a model-oriented specification of any discontinuities that may exist in the model. This includes update of state variables or parameters and the conditions which trigger them.

The parameter set contains the values of all model parameters and tabular functions if any. The experiment block consists of the values of all experimentation

variables, states and inputs. In addition, the type of algorithm to be used in the simulation is specified by the user in this block along with the Interpolation used if any. The Run specification specifies the triplet (model, parameter set, and experiment) to be used in the simulation. This essentially defines the scenario used with the model. In a typical simulation study, the modeler may need to test his model under a number of different scenarios. Thus, a number of parameter sets and experiment blocks may exist for any particular model, and the model may be specified to be run with different combinations of parameter sets and experiments. Finally, the Output Module specifies the format of display of the saved variables of interest along with an appropriate heading.

3.2.1.2. Interactive Procedural Program

The interactive procedural program equivalent to a Gest program (for the single component model) has three main sections, the details of which are shown in Figure. 3.3. The first section deals with pre-run activities where all model variables and experimentation variables are initialized. These values are initialized from the information available in the Gest parameter set and experimentation module. If more than one simulation run is required, the specification

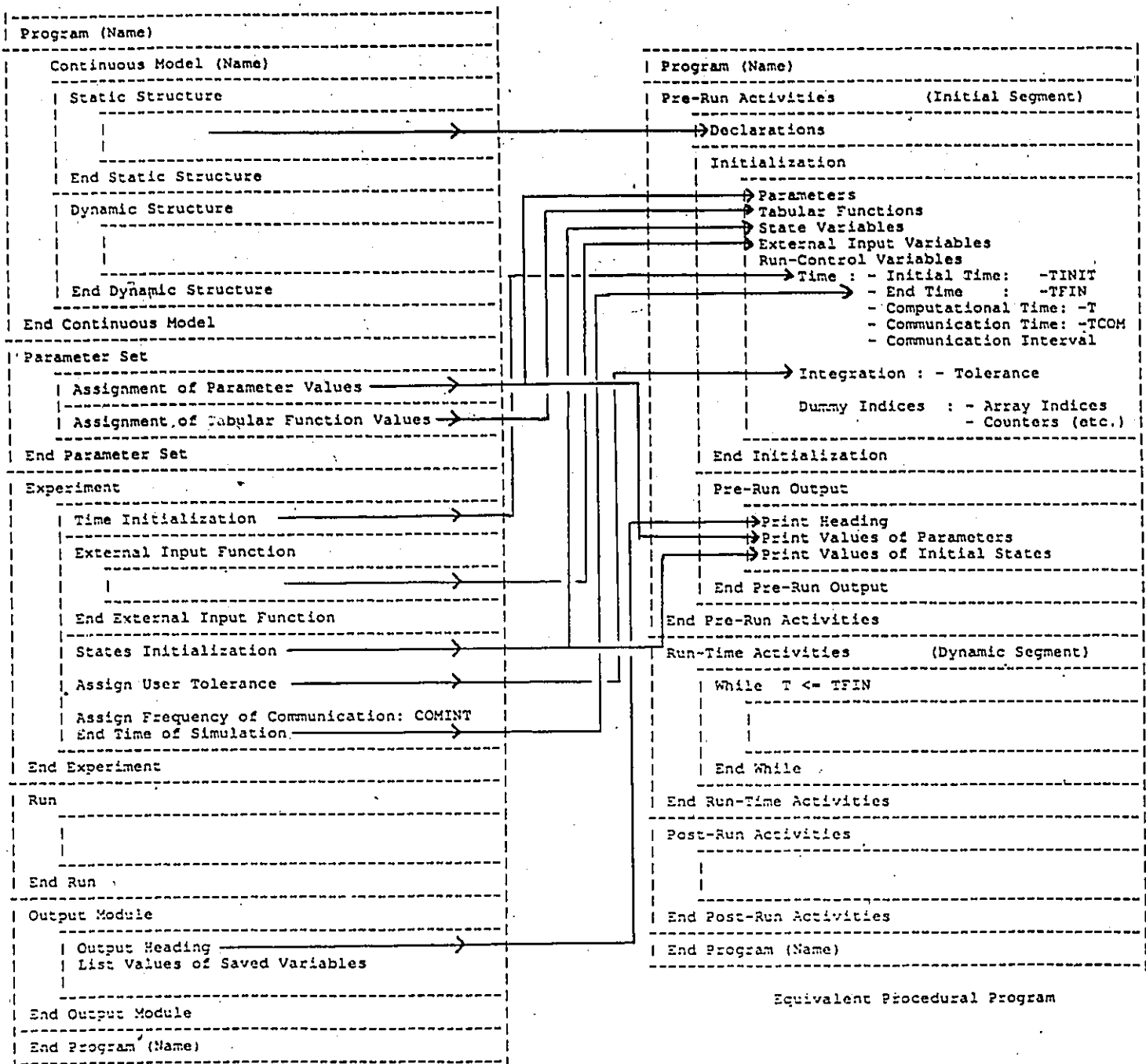
Program (Name)	(For Single Continuous Component Model)
Pre-Run Activities	(Initial Segment)
Declarations	
Initialization (using XMENU)	
Parameters Tabular Functions State Variables External Input Variables Run-Control Variables Time : - Initial Time: -TINIT - End Time : -TFIN - Computational Time: -T - Communication Time: -TCOM - Communication Interval: -COMINT Integration : - Tolerance Dummy Indices : - Array Indices - Counters (etc.)	
End Initialization	
Pre-Run Output	
Print Heading Print Values of Parameters Print Values of Initial States	
End Pre-Run Output	
End Pre-Run Activities	
Run-Time Activities	(Dynamic Segment)
While T <= TFIN	
While T <= TCOM	
If there is a time for a model update	
Then Perform model update	
End If	
Compute external input(s) Compute model output(s) Compute next state(s)	
If a state value for a model update is detected	
Then Locate the discontinuity point	
Perform model update	
Recompute next state(s)	
End If	
Store next state(s) Terminate simulation if condition given as a function of state variable is satisfied Time update : $T = T + h$	
End While	
Collect and save model output(s) at communication time Update TCOM: $TCOM = TCOM + COMINT$	
End While	
Collect and save model output(s) at TFIN	
End Run-Time Activities	
Post-Run Activities	
Post-Run Computations (if any)	
Display Output(s) -In Tabular Form -In Graphical Form	
End Post-Run Activities	
End Program (Name)	

Figure 3.3 Interactive Procedural Program For A Component Model

is interactively carried out using the XMENU/E package. The menu is simply invoked and the necessary modifications made to the variables. After the reinitialization is performed, the simulation is run once more. This process is repeated for all the simulation runs. Also, as part of the pre-run activities, any pre-run computations or assignments of inputs and/or outputs are carried out. The second section contains all the activities that must be carried out during the run-time of the simulation. The run - time computations are expounded in Section 3.2.1.3. The last section involves the post-run activities that need to be carried out. These include any computations to be carried out after the run as well as how the output is to be displayed after the simulation is finished. The output is listed in tabular form and with the aid of the DISSPLA software displayed in graphical form.

3.2.1.3 Correspondence Between Gest and Procedural Program

For each set of activities, i.e. the pre-run, run-time and post-run activities the corresponding parts of the Gest program are shown. The correspondence for the pre-run activities are shown in Figure. 3.4. In a nutshell, information included in the static structure, parameter set, and experimentation section form the components of the pre-run activities. It is from these sections of the Gest program that the initial values of the model parameters,



Gest Specification

Figure 3.4 Correspondence Between Gest Specification and Equivalent Procedural Program For Pre-Run Activities

initial state values, external input variables, tabular functions, and run - control variables such as time and integration variables are determined. Preliminary information such as the heading in the output module of the Gest specification, additionally, provides the pre-run output in the procedural equivalent. Once the pre-run activities are completed, the run-time activities can proceed.

Figure 3.5 shows the correspondence for the run-time activities. The dynamic structure along with the triplet specification in the Run section provide the information required to perform the run-time activities of the procedural equivalent. Once the triplet (Model, Parameter Set, and Experiment) has been specified, the simulation run along with its activities can proceed. The run-time activities start with the computational time equal to the initial simulation time, and the integration algorithm is utilized to integrate over a communication interval or until a termination condition is met.

For each communication interval, a check is done for a possible discontinuity at a specific time. If one exists model update is performed. Any external inputs to the model are computed from the external input function along with an interpolation method if, necessary. Model outputs are computed from the appropriate output function. The next states can be computed using the integration algorithm

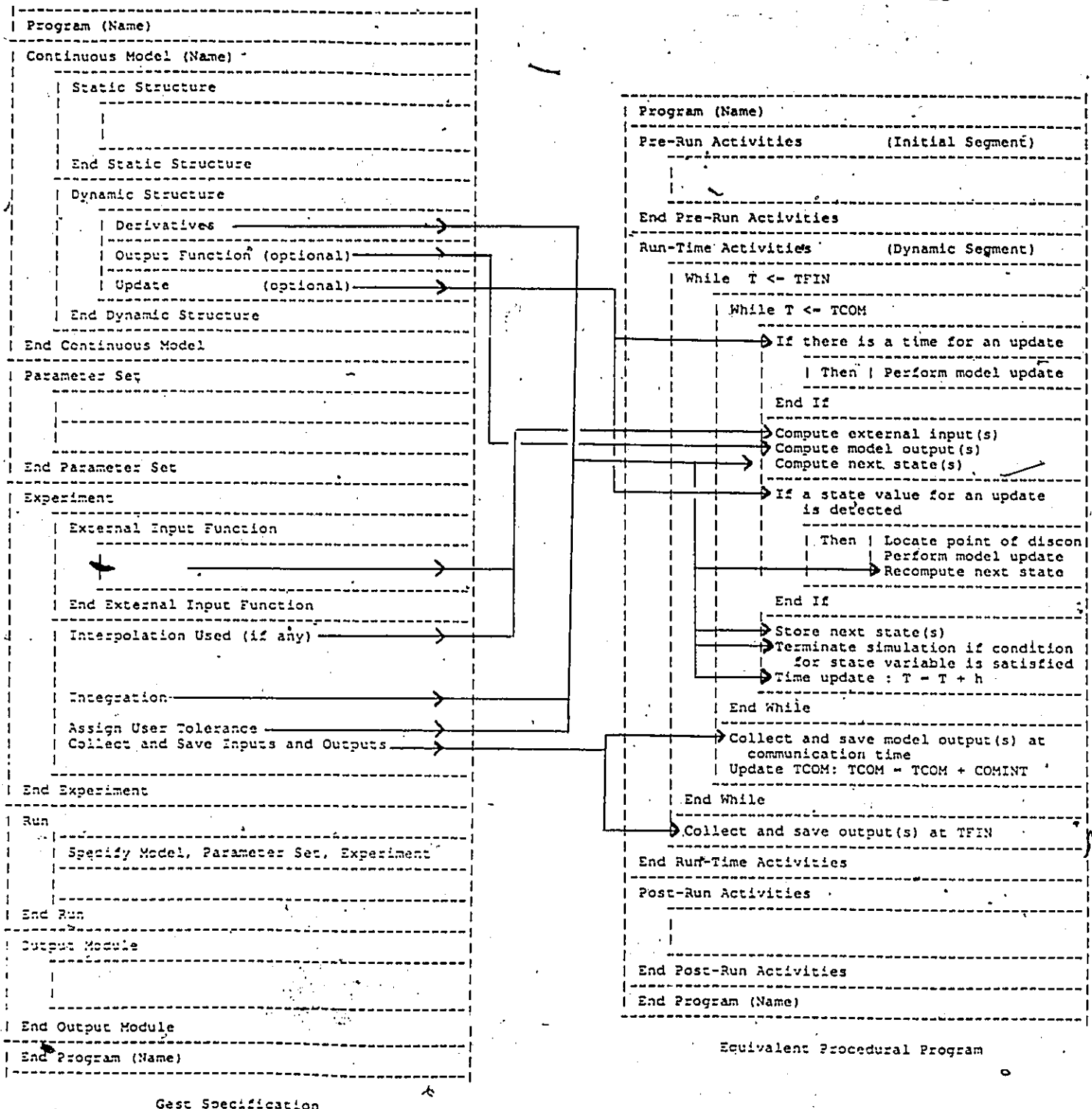
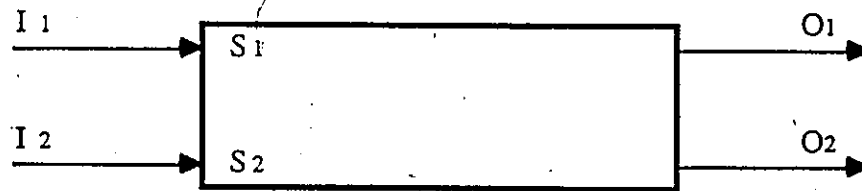


Figure 3.5 Correspondence Between Gest Specification and Equivalent Procedural Program For Run-Time Activities

chosen with the specified user tolerance, along with the initial state variable values and the derivatives that describe the model. At this point, a check is done to detect whether a discontinuity due to some state value exists. If it does, then the discontinuity point is located, the model update performed, and the next states recomputed. The next states are then stored, the termination condition for the simulation checked and finally the integration time updated. At the end of each communication time (TCOM), the model outputs are collected and saved for future display. Finally, the next communication time is computed using the information specified for the frequency of communication (COMINT). The process is repeated until the present computational time is greater than the specified end time of the simulation. Figs. 3.6(a) and (b) further clarify the computational steps that must be carried out during the run time of a single component model.

Finally, as shown in Figure 3.7, the Output module and the optional post-run requirements in the Run section provide all the information for the post-run activities of the procedural simulation program. These include carrying out all the post-run computations and displaying the output in tabular as well as graphical forms. The latter uses the Disspla package for this purpose.



f : Transition function

g : Output function

$$S(T_N + H) = f(S(T_N), I[T_N, T_N + H])$$

$$O(T_N) = g(S(T_N))$$

Initial Time : T_0

$$T_1 = T_0 + H$$

End Time $T_2 = T_1 + H$

S : State Vector (S_1, S_2)

I : Input Vector (I_1, I_2)

O : Output Vecctor (O_1, O_2)

At Time T_0 :

- Initialize State Variables
 - $S_1(T_0)$: given
 - $S_2(T_0)$: given
- Compute Initial Inputs
 - $I_1(T_0)$ and $I_2(T_0)$
- Compute Outputs
 - $O_1(T_0) = g_1(I(T_0), S(T_0))$
 - $O_2(T_0) = g_2(I(T_0), S(T_0))$
- * - Compute Inputs $I_1(T_0, T_1)$ and $I_2(T_0, T_1)$
- Compute Next States
 - $S_1(T_1) = f_1(S(T_0), I[T_0, T_1])$
 - $S_2(T_1) = f_2(S(T_0), I[T_0, T_1])$
- Update Time
 - $T_1 = T_0 + H$

At Time T_1 :

- Compute Outputs
 - $O_1(T_1) = g_1(I(T_1), S(T_1))$
 - $O_2(T_1) = g_2(I(T_1), S(T_1))$
- * - Compute Inputs $I_1(T_1, T_2)$ and $I_2(T_1, T_2)$
- Compute Next States
 - $S_1(T_2) = f_1(S(T_1), I[T_1, T_2])$
 - $S_2(T_2) = f_2(S(T_1), I[T_1, T_2])$
- Update Time
 - $T_2 = T_1 + H$

At Time T_2 :

- $S_1(T_2)$ = given from last step
- $S_2(T_2)$ = given from last step
- Compute Outputs
 - $O_1(T_2) = g_1(I(T_2), S(T_2))$
 - $O_2(T_2) = g_2(I(T_2), S(T_2))$
- * (computed only at points needed for integration)

Figure 3.6(a) Computation of States and Outputs for a Single Component Model in the Interval $[T_0, T_2]$

Time	State			External Inputs		Outputs		Comments
	Action	S_1	S_2	I_1	I_2	O_1	O_2	
$T = T_0$	1) Given	$S_1(T_0)$	$S_2(T_0)$					Initialize State Variables
	2) Compute Outputs					$O_1(T_0)$	$O_2(T_0)$	Evaluate all Output Functions
	3) Given or Evaluate			$I_1[T_0, T_1]$	$I_2[T_0, T_1]$			Get values of External Inputs
	4) Compute Next States	$S_1(T_1)$	$S_2(T_1)$					Compute using integration algorithm, derivative section of model and initial states
	5) Update Time							$T_1 = T_0 + H$
$T = T_1$	1) Given	$S_1(T_1)$	$S_2(T_1)$					All states are available from previous step
	2) Compute Outputs					$O_1(T_1)$	$O_2(T_1)$	Evaluate all Output Functions
	3) Given or Evaluate			$I_1[T_1, T_2]$	$I_2[T_1, T_2]$			Given or Computed from Input Function or Interpolated from Tabular Functions
	4) Compute Next States	$S_1(T_2)$	$S_2(T_2)$					Compute using integration algorithm, previous states and derivative section of model
	5) Update Time							$T_2 = T_1 + H$, Integration finished
$T = T_2$	1) Given	$S_1(T_2)$	$S_2(T_2)$					All states are available from previous step
	2) Compute Outputs					$O_1(T_2)$	$O_2(T_2)$	Evaluate all output functions

Figure 3.6(b) Computational Steps Required During Run Time of Single Component Model in Interval $[T_0, T_2]$

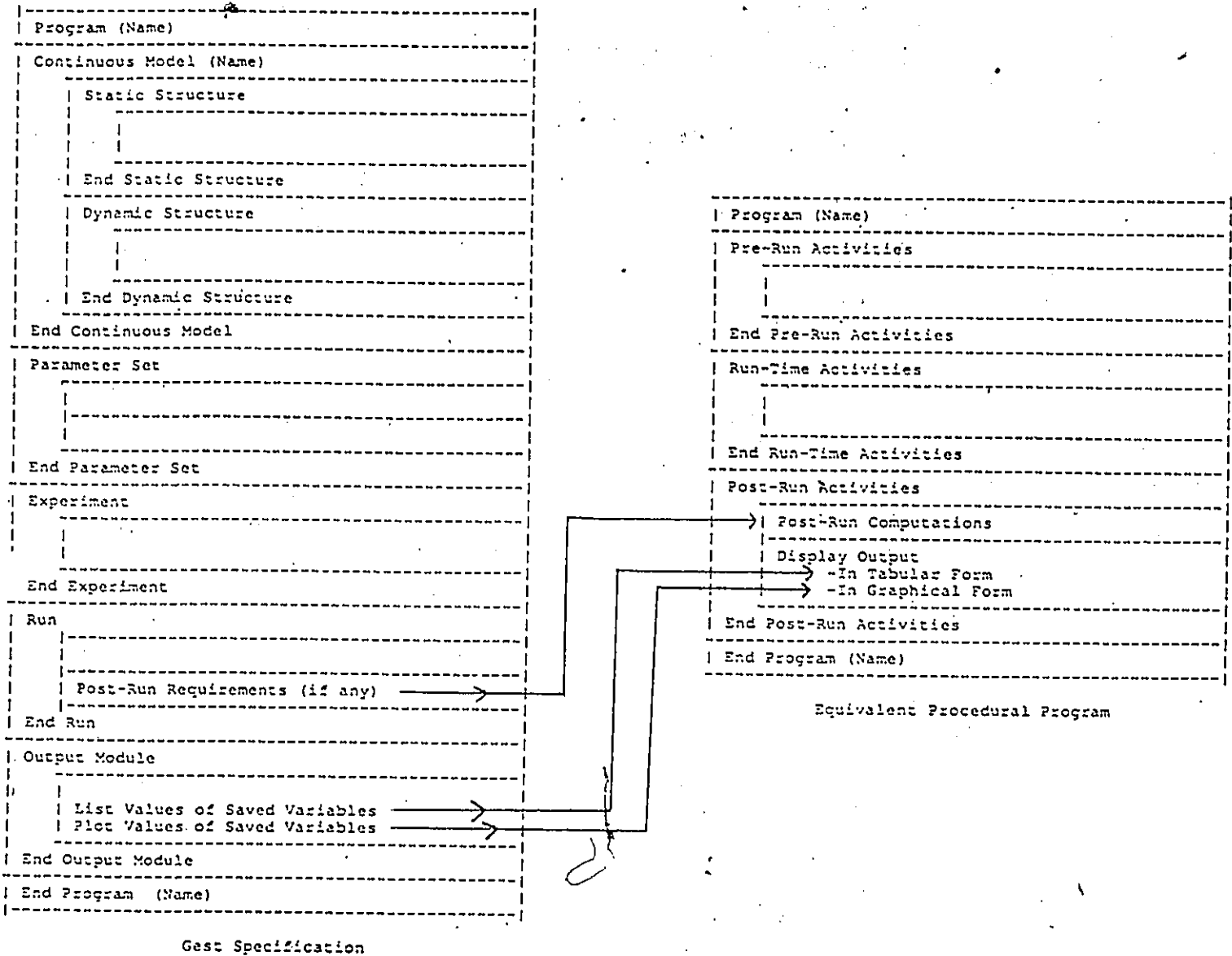


Fig 3.7 Correspondence Between Gest Specification And Equivalent Procedural Program For Post-Run Activities

3.2.2 Gest Program: Several Component Models

3.2.2.1 Coupled Model

In the case of a coupled model which is a Gest program with several component models, each component model is specified separately. Then the coupling or input/output relationships of the component models are specified. In Gest, the coupling of component models consists of : 1) external coupling where the equivalent external and internal inputs and outputs are specified. 2) Internal coupling where the input/output relationships between the component models are specified.

The example model Z given in Figure.3.8 consists of two component models M and N. As can be seen, both external and internal coupling exist for model Z and can be specified as follows : 1) External Coupling : The external input is given by IN and is specified as Z.IN. It corresponds to the internal input B of component model M. Hence, as shown, the coupling information is given by:

Z.IN --> M.B

Similarly, the internal output H of component model N corresponds to the output OUT of the model Z. As a result, the coupling information is given by :

Z.OUT <-- N.H

2) Internal coupling: For every input of each component model one distinguishes external inputs and internal inputs.

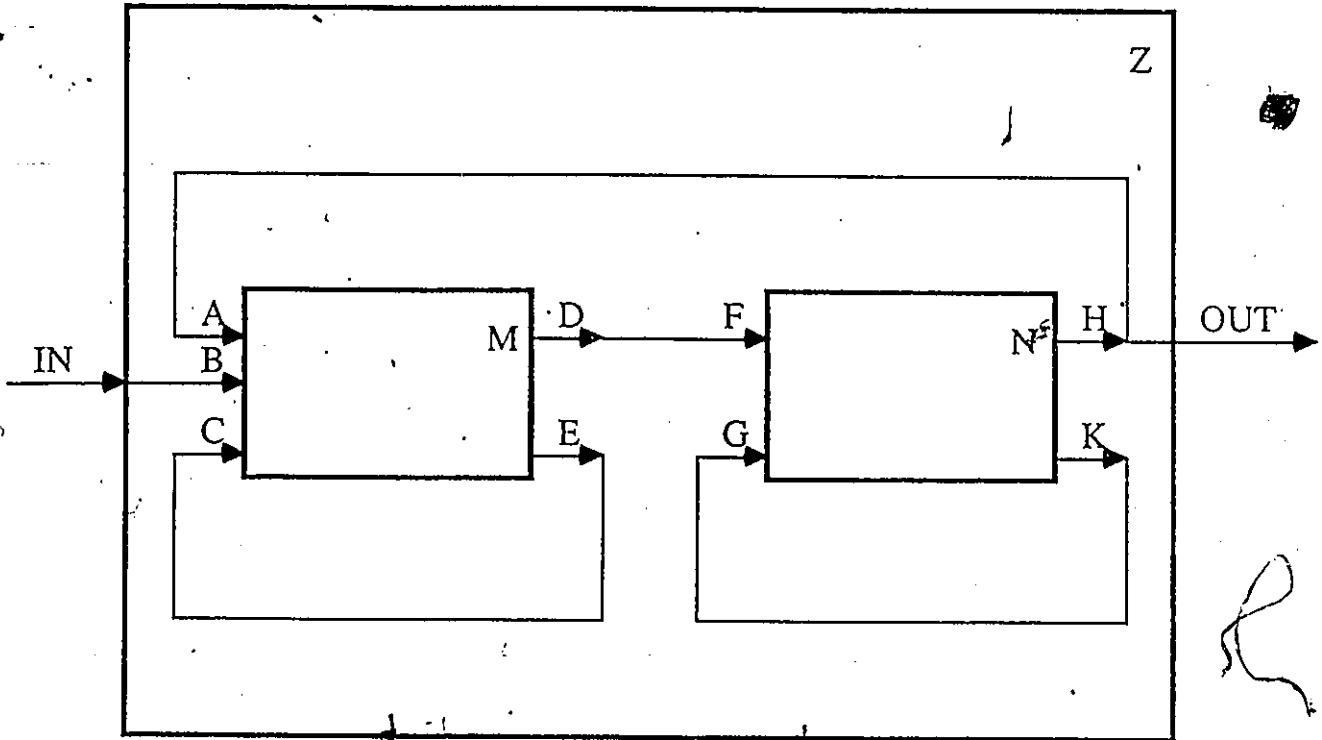


Figure 3.8 Pictorial Representation of Coupled Model Z With Component Models M and N

An external input of a component model is connected to an external input of the coupled model. All other inputs are internal inputs. Afterwards, for every internal input, one specifies from which output variable of which component model the values are provided. The internal coupling information that exists between the component systems M and N of model Z is given by :

M.A <-- N.H

M.C <-- M.E

N.F <-- M.D

N.G <-- N.K

It should be noted that the left hand side of the specification would be automatically generated by the Magest system of the Gest environment and the user would be asked to complete the specification.

To be able to specify a coupled model, one has to finish specification of each component model. Finally, for the parameter set and experimentation section, further modularization is required. The parameter set of the coupled model would consist of the specification of the parameters and tabular functions for each component model in a modular fashion. The experiment would consist of modular and separate specifications of the input functions and initial states for each component model. The specification of the Gest program consisting of several component models is shown in Figure 3.9.

```

-----
| Program (Name)                               ( For Coupled Model)
-----
| Coupled Model (Name)
|-----
|   Externals
|   | Inputs -list of external inputs
|   | Outputs -list of external outputs
|   |-----
|   | End Externals
|   |-----
|   | Component Models -list of component models
|   |-----
|   | Macro Models - list of macro models
|   |-----
|   | External Coupling
|   |   Inputs -list of equivalent external and internal inputs
|   |   Outputs -list of equivalent external and internal outputs
|   |   |-----
|   |   | End External Coupling
|   |   |-----
|   |   | Internal Coupling
|   |   |   For every component model
|   |   |   |-----
|   |   |   |   For every input variable
|   |   |   |   | (not appearing in the external coupling)
|   |   |   |   |-----
|   |   |   |   | Specify from which output variable of which
|   |   |   |   |   component model the values are provided
|   |   |   |   |-----
|   |   |   |   | Loop
|   |   |   |   |-----
|   |   |   |   | Loop
|   |   |   |   |-----
|   |   |   | End Internal Coupling
|   |   |   |-----
|   | End Coupled Model (Name)
|   |-----
|   | Parameter Set
|   |   For every component model specify
|   |   |-----
|   |   |   Parameter
|   |   |   Tabular Functions
|   |   |-----
|   |   Loop
|   |   |-----
|   | End Parameter Set
|   |-----
|   | Experiment
|   |   For every component model specify
|   |   |-----
|   |   |   Input Functions
|   |   |   Initial States
|   |   |-----
|   |   | Loop
|   |   |-----
|   |   | Associated Time and Integration Knowledge for Simulation
|   |   |-----
|   | End Experiment
|   |-----
|   | Run
|   |   Specify the Triplet          (Model, Parameter Set, Experiment)
|   |   Post-Run Requirements      (Optional)
|   |   |-----
|   | End Run
|   |-----
|   | Output Module
|   |   Print Output Heading
|   |   List and Plot Variables of Interest
|   |   |-----
|   | End Output Module
|   |-----
| End Program (Name)
|-----

```

Figure 3.9 Gest Specification For A Coupled Model With Several Component Models

3.2.2.2 Multi-Rate Gest Program

The multi-rate Gest program specifies the model with several component models in such a way as to facilitate the use of the multi-rate integration algorithm. This algorithm is discussed in detail in Chapter 4. Essentially, a system having widely different dynamic characteristics is partitioned into two component systems having similar characteristics. These component systems are integrated using the best suited algorithms with independent error control. Hence, the main differences from a coupled Gest program are : 1) Two component models comprising of the Fast Continuous Model and Slow Continuous Model must be specified with the appropriate coupling as in the Gest Program for the coupled model. 2) In the experimentation section, for each component model an integration algorithm along with its allowed error is specified. The details of the specification are shown in Figure 3.10.

3.2.2.3 Interactive Procedural Program

The primary distinction between the procedural program for a single component model and a coupled model with several component models is in the computation steps required within the run time activities as shown in Figure 3.11 and further elaborated in Figs. 3.12 (a) and (b) proceed in a similar manner to that of the single component model using the initial states, and the derivative

```

PROGRAM (NAME)      ( For Coupled Model Using Multi-Rate Algorithm)
Multi-Rate Model (Name)
  Externals
    Inputs -list of external inputs
    Outputs -list of external outputs
  End Externals
  Component Models
    Slow Continuous Model (Name)
    Fast Continuous Model (Name)
  End Component Models
  Macro Models - list of macro models
  External Coupling
    Inputs -list of equivalent external and internal inputs
    Outputs -list of equivalent external and internal outputs
  End External Coupling
  Internal Coupling
    For every component model
      For every input variable
        (not appearing in the external coupling)
        Specify from which output variable of which
        component model the values are provided
      Loop
    Loop
  End Internal Coupling
End Multi-Rate Model (Name)
Parameter Set
  For every component model (i.e. Fast model, Slow model) specify
    Parameter
    Tabular Functions
  Loop
End Parameter Set
Experiment
  For every component model (i.e. Fast model, Slow model) specify
    Integration Algorithm to be used
    User tolerance
    Input Functions
    Initial States
  Loop
  Specify Associated Time Knowledge for Simulation
End Experiment
Run
  Specify the Triplet      (Model, Parameter Set, Experiment)
  Post-Run Requirements   (Optional)
End Run
Output Module
  Print Output Heading
  List and Plot Variables of Interest
End Output Module
End Program (Name)

```

Figure 3.10 Specification For Multi-Rate Gest Program With
Two Component Models

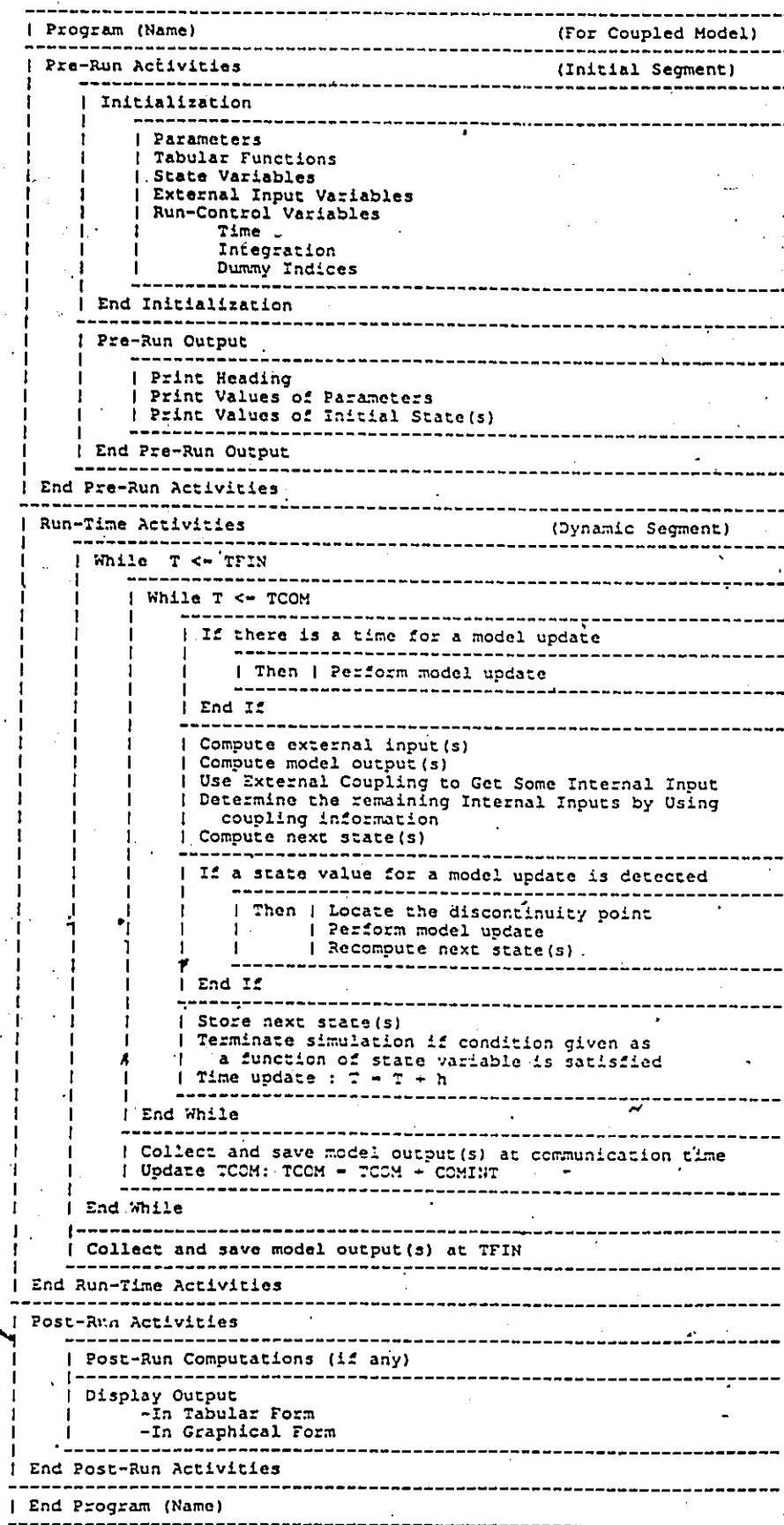
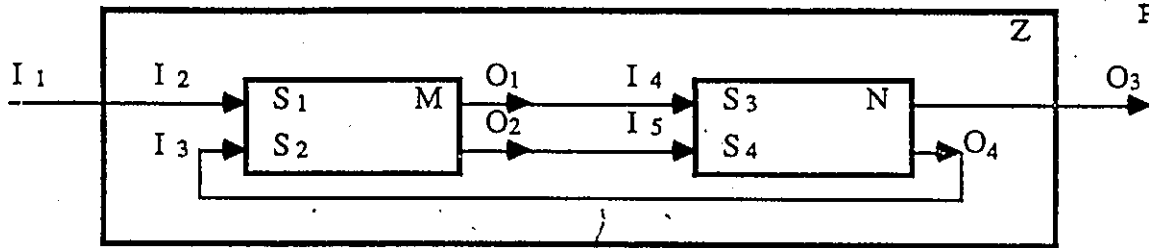


Figure 3.11 Equivalent Procedural Program For A Coupled Model With Several Component Models



f : Transition function

g : Output function

S_M : Model M State Vector (S_1, S_2)

I_M : Model M Input Vector (I_2, I_3)

O_M : Model M Output Vector (O_1, O_2)

$S(T_N + H) = f(S(T_N), I[T_N, T_N + H])$

$O(T_N) = g(S(T_N))$

Initial Time: T_0

$T_1 = T_0 + H$

End Time: $T_2 = T_1 + H$

S_N : Model N State Vector (S_3, S_4)

I_N : Model N Input Vector (I_4, I_5)

O_N : Model N Output Vector (O_3, O_4)

At Time T_0 :

1 Initialize State Variables

$S_M(T_0)$: given

$S_N(T_0)$: given

- Compute Outputs

$O_M(T_0) = g_1(S_M(T_0))$

$O_N(T_0) = g_2(S_N(T_0))$

* - Compute Inputs $I_M[T_0, T_1]$ and $I_N[T_0, T_1]$

- Compute Next States

$S_M(T_1) = f_1(S_M(T_0), I_M[T_0, T_1])$

$S_N(T_1) = f_2(S_N(T_0), I_N[T_0, T_1])$

- Update Time

$T_1 = T_0 + H$

At Time T_1 :

- Compute Outputs

$O_M(T_1) = g_1(S_M(T_1))$

$O_N(T_1) = g_2(S_N(T_1))$

* - Compute Inputs $I_M[T_1, T_2]$ and $I_N[T_1, T_2]$

- Compute Next States

$S_M(T_2) = f_1(S_M(T_1), I_M[T_1, T_2])$

$S_N(T_2) = f_2(S_N(T_1), I_N[T_1, T_2])$

- Update Time

$T_2 = T_1 + H$

At Time T_2 :

$S_M(T_2)$ = given from last step

$S_N(T_2)$ = given from last step

- Compute Outputs

$O_M(T_2) = g_1(S_M(T_2))$

$O_N(T_2) = g_2(S_N(T_2))$

* (computed only at points needed for integration)

Figure 3.12(a) Computation of States and Outputs of a Coupled Model Z With Component Models M and N in the Interval $[T_0, T_2]$.

Time	Action	Model M - States		External Input	Model M Inputs			Model M Outputs		Model N Inputs			Model N Outputs		
		S _M	S _N		I ₁	I ₂	I ₃	O ₁	O ₂	I ₄	I ₅	O ₄	O ₃		
T = T ₀	1) Given	S _M (T ₀)	S _N (T ₀)											Initialize State Variables In All Component Models	
	2) Compute Outputs						O ₁ (T ₀)	O ₂ (T ₀)			O ₄ (T ₀)	O ₃ (T ₀)	For all component models, evaluate output functions to get output variables		
	3) Given or Evaluate			I ₁ (T ₀ , T ₁)										All external input for all component models given or evaluated from input functions	
	4) Determine Inputs			I ₂ (T ₀)=I ₁ (T ₀)										Evaluate all external couplings	
	5) Determine remaining internal inputs													Evaluate all internal couplings	
	6) Compute Next states	S _M (T ₁)	S _N (T ₁)				I ₃ (T ₀)=O ₄ (T ₀)							Compute using integration algorithm, initial states, and state derivatives	
	7) Update Time													T = T ₀ + H = T ₁	
T = T ₁	1) Given	S _M (T ₁)	S _N (T ₁)											All states available from the previous step	
	2) Compute Outputs													All external inputs for all component models given or evaluated from input functions	
	3) Given or Evaluate			I ₁ (T ₁ , T ₂)			O ₁ (T ₁)	O ₂ (T ₁)			O ₄ (T ₁)	O ₃ (T ₁)	For all component models, evaluate output functions to get output variables		
	4) Determine Inputs			I ₂ (T ₁)=I ₁ (T ₁)										Evaluate all external couplings	
	5) Determine remaining internal inputs													Evaluate all internal couplings	
	6) Compute next states	S _M (T ₂)	S _N (T ₂)				I ₃ (T ₁)=O ₄ (T ₁)							Compute using integration, algorithm, initial states, and state derivatives.	
	7) Update Time													T = T ₁ + H = T ₂	
T = T ₂	1) Given	S _M (T ₂)	S _N (T ₂)											All states available from the previous step	
	2) Compute Outputs						O ₁ (T ₂)	O ₂ (T ₂)			O ₄ (T ₂)	O ₃ (T ₂)	For all component models, evaluate output functions to get output variables		

Figure 3.12(b) Computational Steps Required During Run Time of Coupled Model In Interval $[T_0, T_2]$

subroutine which is a single collection of the differential equations of the component models. However, at the end of each integration step, internal coupling between the component systems and external coupling may be necessary as opposed to the single component model where this does not occur. As a result, once the external input is computed, the coupling information is used to get the associated internal input. The output(s) of the model may also need to be determined from the output(s) of some component model(s) via the external coupling information. In addition, values of any remaining internal inputs are determined from the internal coupling information.

The same steps are carried out for the Multi-rate Gest program. However, the Multi-rate algorithm integrates the coupled model by integrating two derivative subroutines for the Slow and Fast continuous component models independently.

CHAPTER 4

GEST RUN-TIME LIBRARY - SECTION 1

4.1 INTRODUCTION

The run-time library for the simulation specification language Gest, consists of a variety of integration algorithms in the form of structured Fortran subprograms designed to generate the numerical solution of continuous models which can be described as non-stiff initial value problems.

The variety of algorithms to be included in such a run-time library is a very important decision since not all codes are equally effective in their handling and up to date, no single integration algorithm has been found to handle all kinds of problems equally well. As a result, users must be careful which algorithm they apply to particular situations. In the last decade, considerable research by Hull et. al. (1972), Hull (1980), and Shampine et. al. (1980) has been done to compare certain aspects of existing methods in order to identify those methods which would be good candidates for inclusion in such a library. In addition, apart from the numerous algorithms available, there are also as pointed out by Gear (1981) a number of major problem areas which require specialized algorithms. Thus, it has been decided that initially the run-time library should consist of algorithms to deal specifically

with a few problem areas with a view of expansion in the future. As stated previously, the set of problems chosen belong to the non-stiff initial value type. In particular, they consist of problems having known discontinuities, multi-rate methods, and general purpose methods.

The discontinuity handling algorithm is designed to deal with piece-wise continuous systems which have known time event discontinuities, state event discontinuities, or a combination of both. The multi-rate integration algorithm is included for use in the integration of large dynamic systems having widely different dynamic characteristics that can be efficiently partitioned into two component systems with similar characteristics. In addition, the coupling that exists between the component systems should involve few interconnections. Finally, some of the more popular general purpose algorithms are included to be used in the integration of systems which can be described by a fixed set of differential equations with state variables and first state derivatives both being continuous over the whole run. These include the fixed step Runge Kutta method, the variable step Runge-Kutta Fehlberg method and the variable step Adams Predictor Corrector Method. Each of these methods may be advantageous depending on such factors as the complexity of the model, the user's accuracy requirements, and the frequency of output stipulated. This is discussed at greater length in Chapter 6.

As described by Shampine et. al. (1980) the more popular methods for the solution of a non-stiff initial value problem are the Runge Kutta, Adams and extrapolation methods. Depending on the structure of the particular problem, one of these is usually more advantageous. Shampine et. al. (1980) concluded that extrapolation codes require a lot of storage and a high overhead. In addition, they are quite inefficient in dealing with problems exhibiting mild stiffness or requiring frequent output. It is recommended that they be exchanged with a variable order Runge Kutta in a library. However, the advantages of the latter are usually in coping with a wide range of tolerances and in the extreme instances handling a discontinuity in a derivative. The latter case is easily handled using the discontinuity handling algorithm described above. To deal with the range of tolerances, we have included a high order variable step Runge-Kutta Fehlberg method for stringent tolerances demanded by the user and a low order fixed step Runge-Kutta method for less stringent ones (Hull, T.E. et. al. 1972). Hence, in our library, the variable order Runge-Kutta method proposed by Shampine (1980) has been replaced by high and low order Runge-Kutta methods and an efficient discontinuity handling algorithm. As discussed by Shampine et.al. (1980), the Runge Kutta codes could not possibly replace the Adams especially for situations where function evaluations are relatively expensive. To this end, the variable step Adams Predictor Corrector method has been

included in the library.

In each of the sections 4.2 and 4.3, the general purpose algorithms and the multi-rate algorithm are discussed in detail. As explained in Chapter 3, the modeler specifies in the Experiment section of his Gest program the type of integration algorithm to be used to drive the particular model in question. Once the Gest program has been translated into an equivalent procedural program, the integration algorithm requested by the user is used to carry out the run-time activities of the model. Hence, one may perceive the integration algorithm to be embedded within the procedural simulation program.

4.2 GENERAL PURPOSE INTEGRATION ALGORITHMS

4.2.1 Fourth-Order Runge-Kutta

4.2.1.1 Description of Algorithm

The Fourth Order Runge-Kutta algorithm is one of a family of Runge Kutta formulas which are powerful numerical techniques for solving ordinary differential equations. These numerical techniques can be applied with varying degrees of success and effectiveness to virtually any differential equation which is in sharp contrast to the problem of trying to find an analytical solution to a differential equation (Hornbeck 1975). The Fourth Order Runge-Kutta Method is to be used in generating the solution of initial value problems and utilizes a fixed step size procedure.

If we consider the initial value problem :

$$Y' = F(T, Y(t))$$

with $Y(0) = Y_0$ (given) over the interval (T_0, T_f)

where Y' represents a set of n first order differential equations.

As illustrated in Figure 4.1, the objective of the Runge-Kutta technique is to advance the solution in steps such as $T_{j+1} = T_j + H$ over some interval $[T_0, T_f]$ which is clearly an extrapolation principle (Hornbeck 1975). In using formulas of the Runge-Kutta type to solve such problems, the

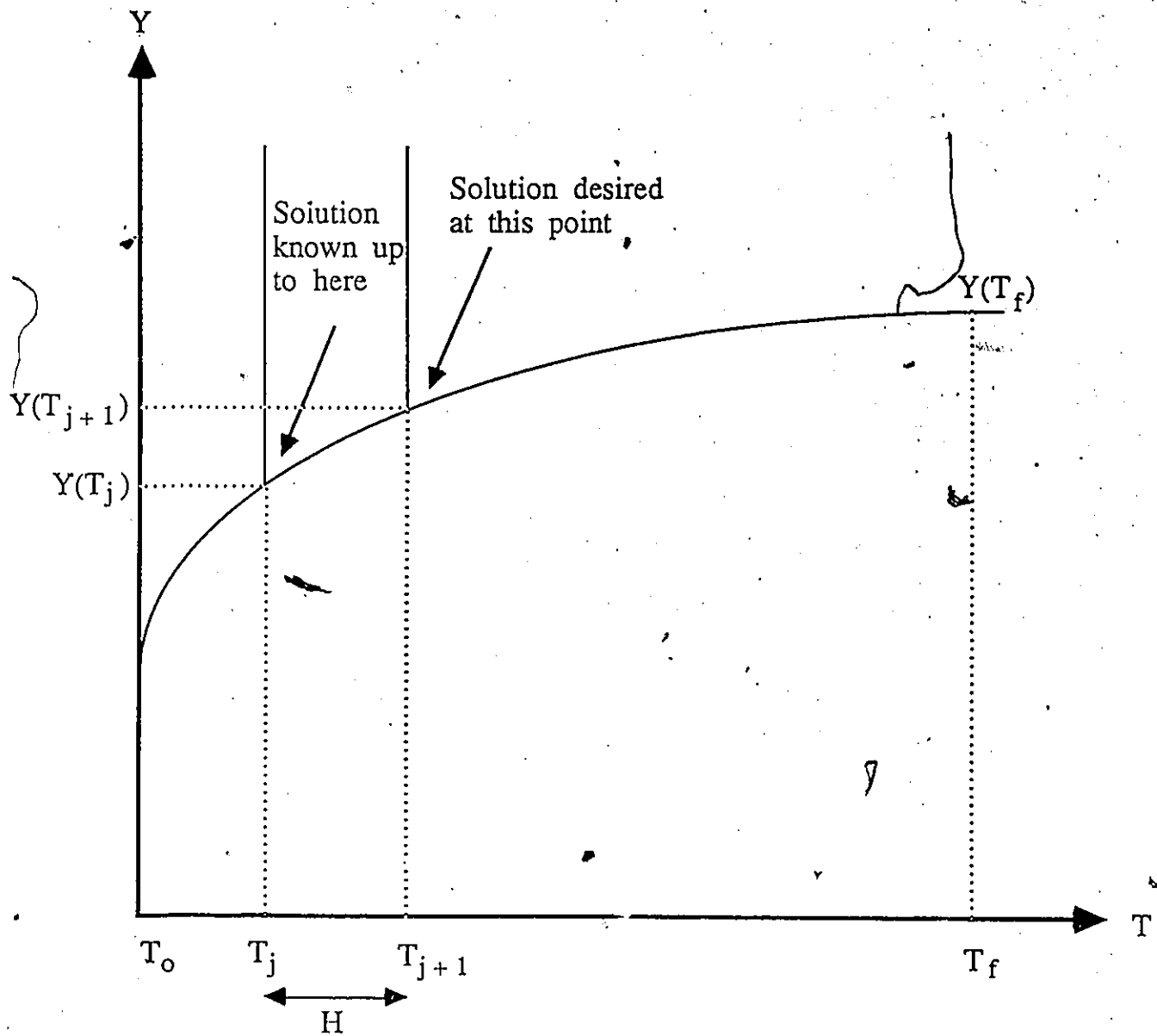


Figure 4.1 Solution Procedures for Runge-Kutta Methods

desired solution Y_{j+1} is obtained in terms of Y_j , $F(T_j, Y_j)$ and $F(T, Y)$ evaluated for various estimated values of Y between T_j and $T_j + H$. The method is a self-starting one requiring no previous values for Y or $F(T, Y)$. Hence in the initial value problem above, at the first step, $T_j = 0$ and $Y_j = Y(0) = Y_0$, the method can be used to find $Y_{j+1} = Y(0 + H) = Y(H)$ and any other successive values of Y .

As applied to the initial value problem stated above, the formulas used by the fourth order Runge Kutta Method for the step from Y_j to Y_{j+1} are :

$$S1 = F(T_j, Y_j)$$

$$S2 = F(T_j + (H/2), Y_j + (S1 * H/2))$$

$$S3 = F(T_j + (H/2), Y_j + (S2 * H/2))$$

$$S4 = F(T_j + H, Y_j + (S3 * H))$$

$$Y_{j+1} = Y_j + (H/6) * (S1 + 2*S2 + 2*S3 + S4)$$

Graphically, as shown in Figure 4.2, one can consider $S1, \dots, S4$ as slopes and the values of $Y_j + (S1 * H/2)$, $Y_j + (S2 * H/2)$ as approximations to Y_j at $T_{j+1/2}$ and $Y_j + (S3 * H)$ as an approximation to Y at T_{j+1} .

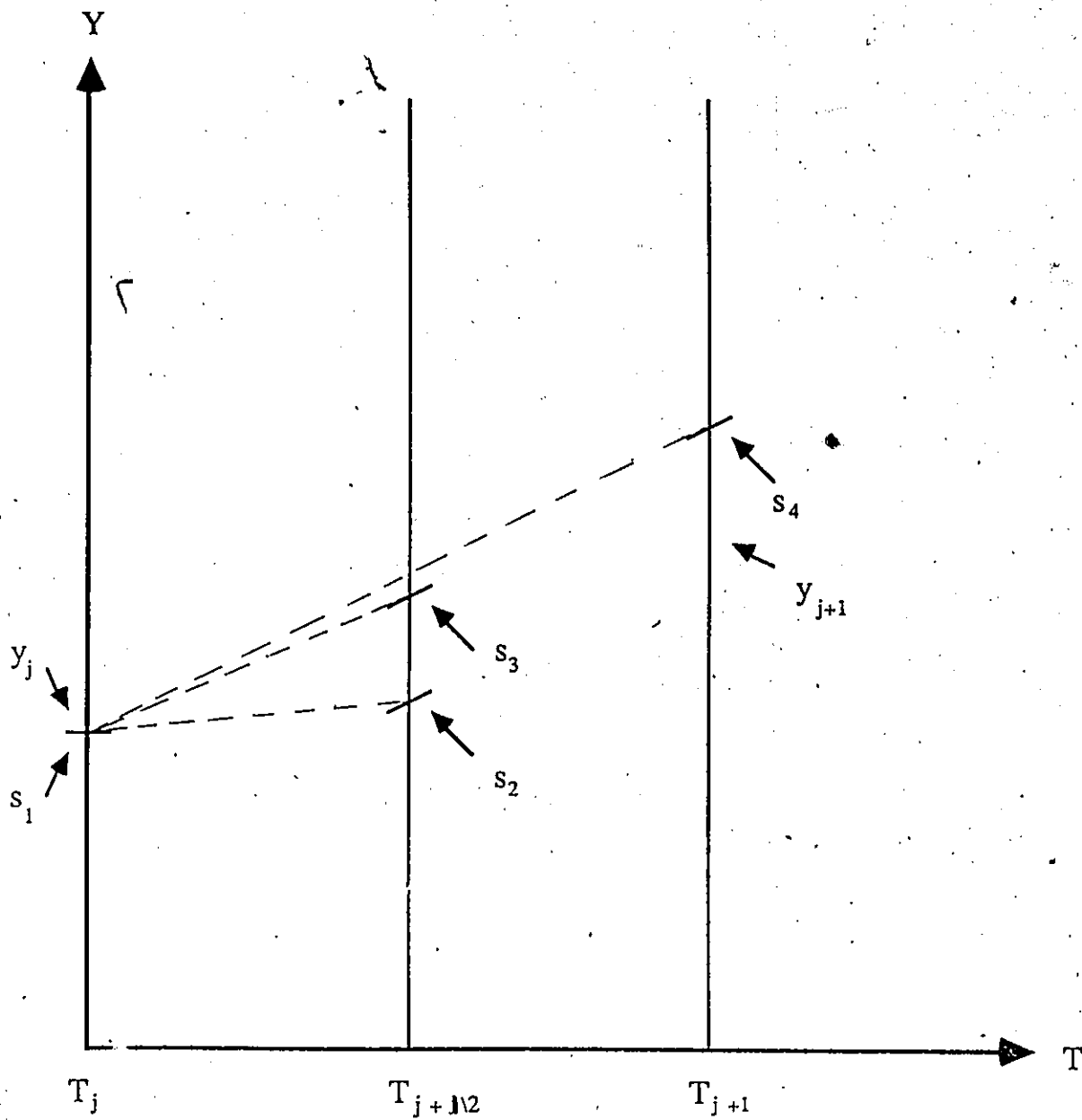


Figure 4.2 Graphical Representation of One Step of the Fourth Order Runge-Kutta Method

4.2.1.2 Structured Algorithm

Figures 4.3(a) and (b) show the details of the Fourth Order Runge-Kutta algorithm used in the run-time library.

List of variables for Fourth Order Runge-Kutta Algorithm

T	- Computational Time
TINIT	- Initial Time of Simulation
TFIN	- End Time of Simulation
TCOM	- Communication Time
COMINT	- Communication interval
H	- Current step size
HINIT	- Initial step size
HMIN	- Minimum allowable step size
HBOUND	- Upper bound on initial step size
Y	- Vector of state variables
N	- Dimension of vector
TOL	- User tolerance
FDER	- Maximum value of derivative functions at initial point
NFLAG	-
	- 0 TCOM has not been detected
	- 1 TCOM has been detected

Figure 4.3(a) List of variables used in RK4 Algorithm

```

Subroutine Fourth Order Runge-Kutta

Initialization

Set T = TINIT
Set NFLAG = 0 (TCOM has not been detected)
Compute initial step size : HINIT
HINIT = min(HBOUND, ((abs(0.5*TOL/FDER)) ** 0.5)/4)
Compute initial Communication Time:
TCOM = T + COMINT
Set H = HINIT

While (T < TFIN)
    While (T < TCOM)
        If (((TCOM - T) <= (HINIT + HMIN) AND (NFLAG = 0)))
            Then | H = (TCOM - T)/2
                | Set NFLAG = 1 (Communication time detected)
        End If
        Compute next states for each state variable
        Update Time:
        T = T + H
    End While

    Call OUTPUT (Y,N,T)
    Compute next TCOM:
    TCOM = T + COMINT

    If ((TCOM >= TFIN)
        Then | TCOM = TFIN
    End If

    Set NFLAG = 0
    Set H = HINIT

End While

CALL OUTPUT(Y,N,T)

EndSubroutine Fourth Order Runge-Kutta

```

Figure 4.3.(b) Details of The RK4 Algorithm

4.2.1.3 Program Structure

Figure 4.4 shows the pictorial view of a program using the Fourth Order Runge-Kutta method to drive the simulation of a single component model.

Main Program



The structure of the main program has three main blocks, namely pre-run activities run-time and post-run activities as discussed in Chapter 3. In the pre-run activities, a CALL is made to subroutine INIT. This subroutine invokes the XMENU and the user initializes all the state variables, parameters, and experimentation variables contained on the full screen menu. After this, any necessary pre-run computations are carried out as well as the pre-run output.

The run time activities of the main program involve a CALL to the RK4 algorithm. This integrates the system over the length of the simulation. Control is returned to the main program after the run is complete, at which point results are displayed tabular form and a CALL is made to the subroutine GRAPH in order to plot the results.

Subroutine INIT

This subroutine is linked to the MAIN program and utilizes the XMENU software within the IBM environment to allow the user to interactively initialize the appropriate model parameters, initial values, and other experimentation variables.

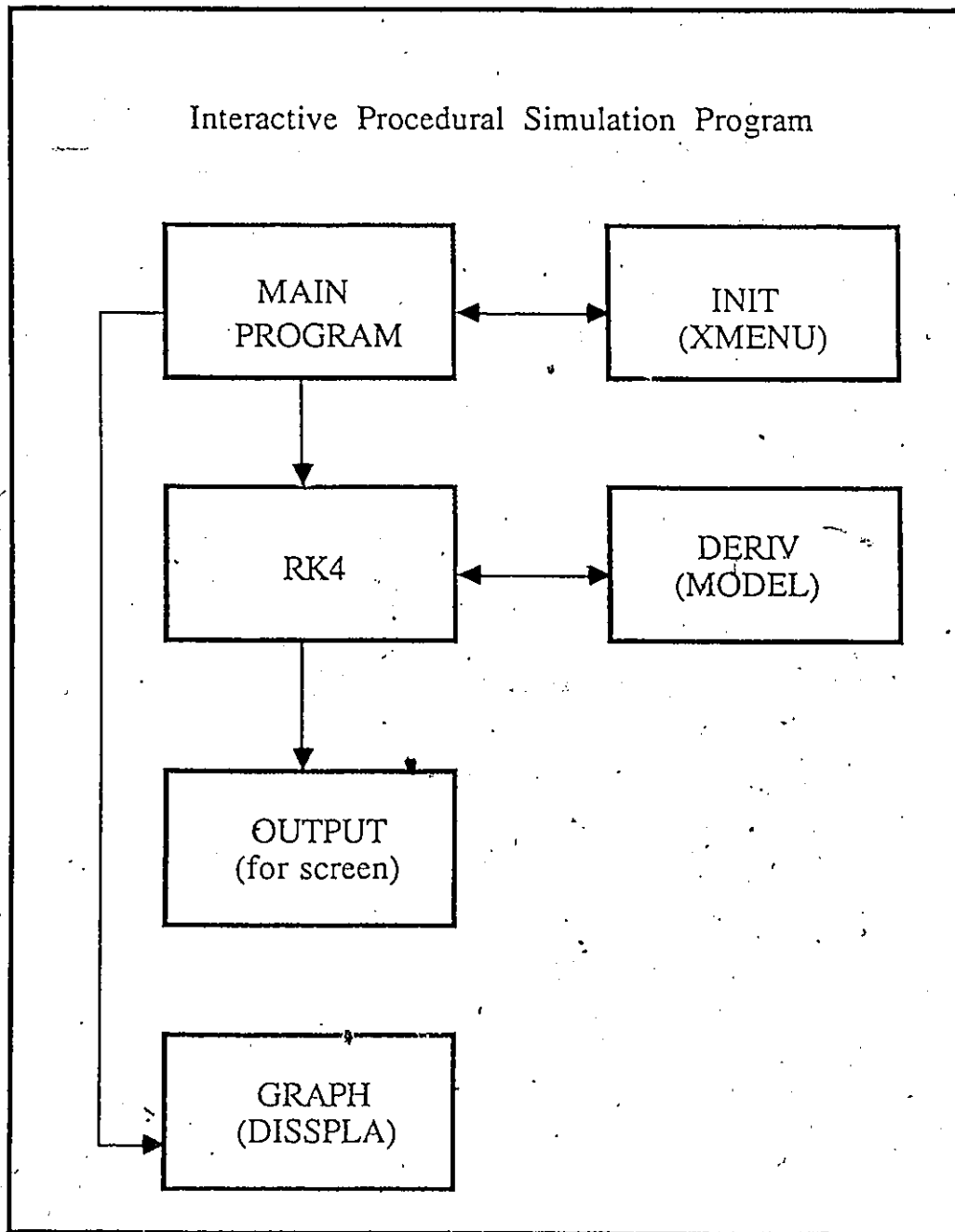


Figure 4.4 Modules of Interactive Procedural Simulation Program using the RK4 Algorithm

Subroutine RK4

This subroutine implements the fourth order Runge-Kutta integration method for integrating systems having frequent output points but not requiring a high level of accuracy. It makes calls at each stage of the integration to the DERIV subroutine. Additionally, at every communication time, a call is made to the OUTPUT subroutine.

Subroutine DERIV

This is a model dependent routine and contains the necessary functions and information to carry out the computational steps. These consist of the output function(s), the external input(s) if any exist, the internal and external coupling information, and the derivatives of the state variables that describe the model in the order shown in Figure 4.5. For a coupled model with several component models, the output functions that may exist for each component model are simply lumped together. In a similar way, as shown, the derivative functions that describe each component model are lumped together.

Subroutine OUTPUT

The values of the outputs at the communication intervals are stored and an interactive tabular display is shown to

DERIV Subroutine

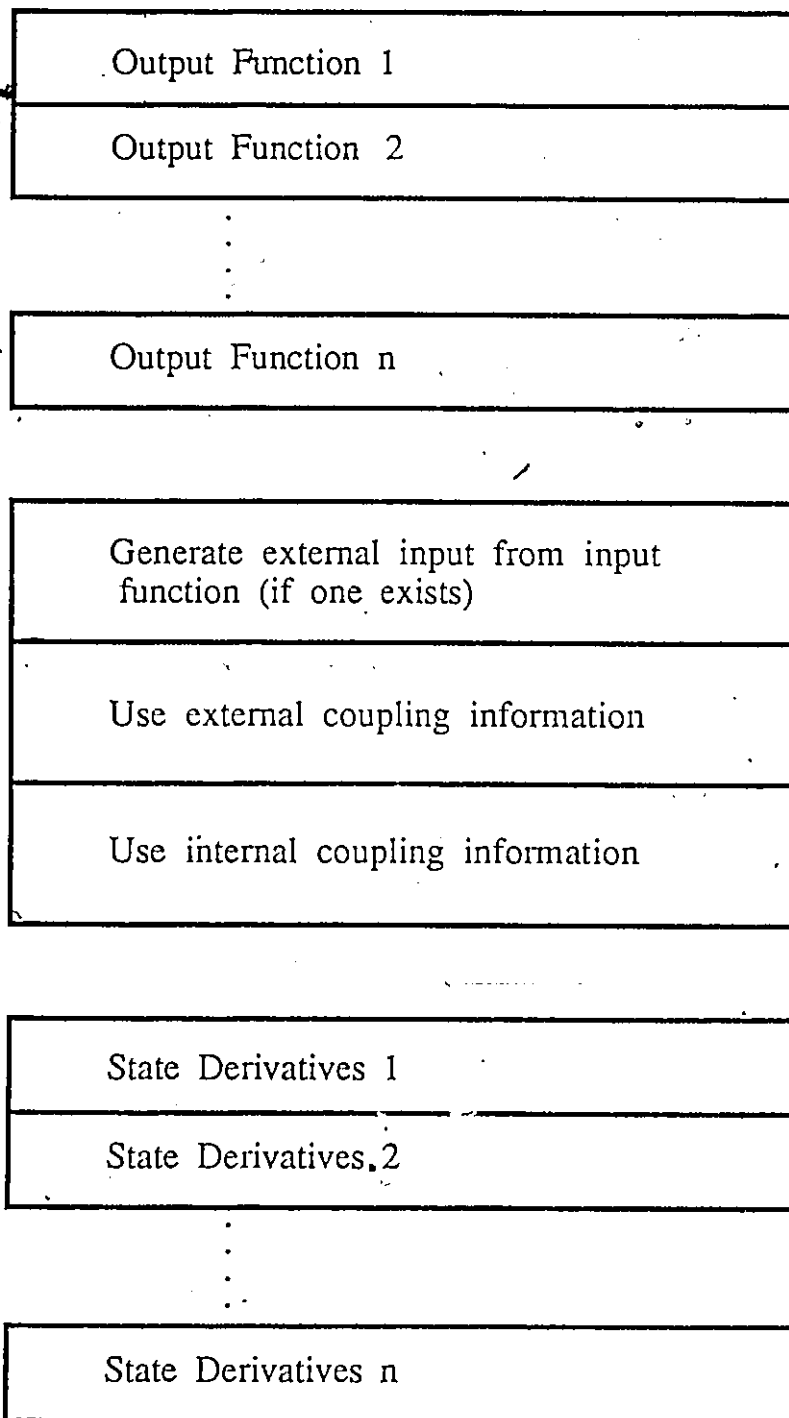


Figure 4.5 Details of DERIV Subroutine

the user during the simulation run.

Subroutine GRAPH

This subroutine linked to the MAIN program utilizes the Disspla software within the IBM environment to provide post-run hard copy graphic displays of the desired model outputs with time.

The fixed step RK4 algorithm is imbedded within the Diabetes Mellitus model example given in Appendix A and in the Forest Biomass model example given in Appendix F.

4.2.2 FIFTH-ORDER RUNGE-KUTTA FEHLBERG

4.2.2.1 Description of Algorithm

This method is a fifth order variable step algorithm and is another in the family of the Runge Kuttas. The algorithm involves computing six function evaluations, but then an estimate of the local truncation error is made available which is used as a basis to decide on the integration step size.

The basis is to compute two Runge-Kutta estimates for the new value of Y_{j+1} but of different orders of error. Hence, instead of comparing estimates of Y_{j+1} for H and $H/2$ as is necessary for the fixed step Runge-Kutta, one compares the estimates of Y_{j+1} using fourth and fifth order Runge-Kutta formulas and comparing the results. The formula for the step

Y_j to Y_{j+1} is given as follows (Gerald and Wheatley 1984 P.310) where Y is the vector of state variables and $F(T,Y)$ is the value of the derivative function at time T .

Compute:

$$K1 = H * F(T, Y(T))$$

$$K2 = H * F(T + H/4, Y(T) + K1/4)$$

$$K3 = H * F(T + 3*H/8, Y(T) + (3/32)*K1 + (9/32)*K2)$$

$$K4 = H * F(T + 12*H/13, Y(T) + (1932/2197)*K1 \\ - (7200/2197)*K2 + (7296/2197)*K3)$$

$$K5 = H * F(T + H, Y(T) + (439/216)*K1 - 8*K2 \\ + (3680/513)*K3 - (845/4104)*K4)$$

$$K6 = H * F(T + H/2, Y(T) - (8/27)*K1 + 2*K2 \\ - (3544/2565)*K3 + (1859/4104)*K4 - (11/40)*K5)$$

$$ERR = ABS(K1/360 - (128/4275)*K3 - (2197/75240)*K4 + \\ K5/50 + (2/55)*K6)/H$$

State at $T+H$:

$$Y(T+H) = Y(T) + ((25/216)*K1 + (1408/2565)*K3 + (2197/4104) * \\ K4 - K5/5)$$

Figure 4.6 illustrates the major parts of a variable step size integration algorithm.

```

Initialize integration step size and states
While (T <= TFIN)
    Compute state derivatives for each state variable
    Compute local truncation error estimates
    Determine the maximum local truncation error: ERRMAX
    If (ERRMAX < TOL)
        Then | Compute next states
              | Update Time:  $T = T + H$ 
              | Update value of H
        Else | Compute reduced value of H (reject previous step)
    End If
End While

```

Figure 4.6 Major Parts of a Variable Step Size Algorithm

4.2.2.2 STRUCTURED ALGORITHM

Figures 4.7(a), (b), and 4.8 show the details of the fifth order Runge-Kutta algorithm used in the run-time library.

List of variables for fifth order Runge-Kutta Fehlberg Algorithm

T	- Computational Time
TFIN	- End Time of Simulation
TINIT	- Initial Time of Simulation
TCOM	- Communication Time
COMINT	- Communication interval
H	- Current step size
HINIT	- Initial step size
HPREV	- Previous step size
HMIN	- Minimum allowable step size
HBOUND	- Maximum allowable step size
ERR(N)	- Vector of local error estimates for all state variables
ERRMAX	- Maximum local error estimate
Y	- Vector of state variables
N	- Dimension of vector
TOL	- Integration error tolerance
NORD	- Order of method
FDER	- Maximum value of derivative functions at initial point
NFLAG	-
	- 0 TCOM has not been detected
	- 1 TCOM has been detected

Figure 4.7(a) List of Variables Used in RK Fehlberg Algorithm

```

Subroutine Runge-Kutta Fehlberg
Set NFLAG = 0          (TCOM has not been detected)
Compute initial step size : HINIT
  HINIT = min(HBOUND, ((abs(0.5*TOL/FDER)) ** 0.5)/4)
Compute initial Communication Time:
  T = T + COMINT
Set H = HINIT

While (T < TFIN)
  While (T < TCOM)
    If (((TCOM - T) <= (HINIT + HMIN) AND (NFLAG.EQ.0))
      Then | H = (TCOM - T)/2
      | Set NFLAG = 1      (Communication time detected)
    End If

    Compute state derivatives (k1...k6) for each state variable
    Compute local error estimates for each state variable
    Determine the maximum local error estimate : ERRMAX

    If (ERRMAX <= TOL)
      Then | Update Time : T = T + H
      | Compute new states at T
    End If

    If (NFLAG = 0)
      Then | Perform Step Size Control (See Fig. 4.9)
    End If

  End While

  Call OUTPUT (Y,N,T)
  Compute next TCOM:
  TCOM = TCOM + COMINT

  If (TCOM >= TFIN)
    Then | TCOM = TFIN
  End If

  Set NFLAG = 0

End While

CALL OUTPUT(Y,N,T)

EndSubroutine Runge-Kutta Fehlberg

```

Figure 4.7.(b) Details of Fifth Order Runge Kutta Fehlberg Algorithm

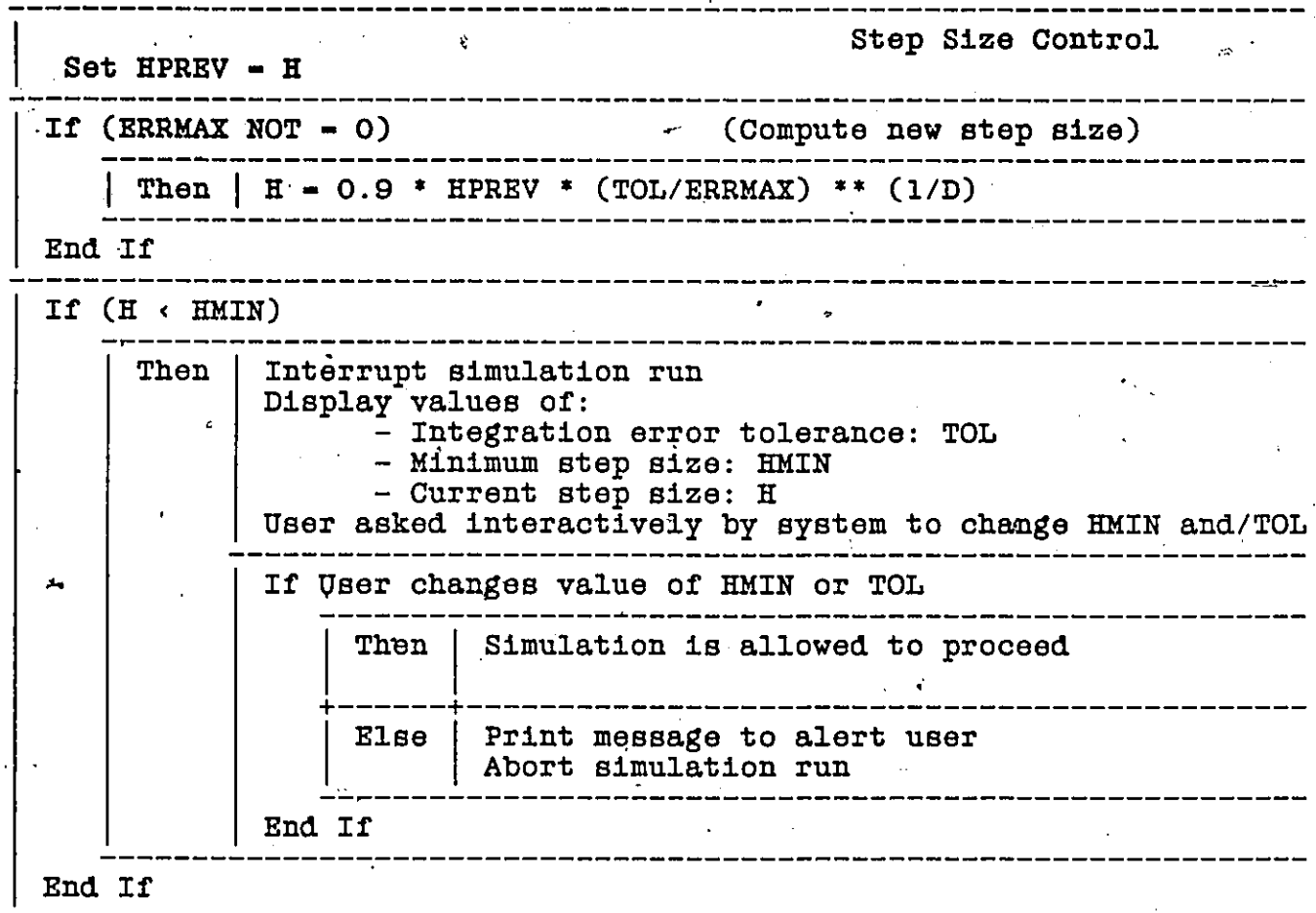


Figure 4.8 Step Size Control for Variable Step Algorithm.

4.2.2.3 Program Structure

The program structure for the program using the Runge-Kutta Fehlberg algorithm to drive the simulation of a model is identical to that of a program using the Fourth Order Runge-Kutta algorithm. As a result, no other details are given except to note that the fifth order Runge-Kutta Fehlberg method is used to integrate the system instead of the fourth order Runge-Kutta method.

The variable step Runge Kutta Fehlberg method is used in the Electronic Oscillator model in Appendix B.

4.2.3 FOURTH-ORDER ADAMS PREDICTOR-CORRECTOR METHOD

4.2.3.1 Description of Algorithm

This method belongs to the class of methods having formulas of the multi-step type. These formulas as depicted in Figure 4.9 require previous information for $T < T_j$. In general, such formulas may require the value of Y_j and values of $F(T, Y)$ at T_j , T_{j-1} , T_{j-2} and T_{j-3} to compute a solution for Y_{j+1} and are hence not self starting. This class of methods for the numerical solution of ordinary differential equations can be represented by the following formula:

$$Y_{j+1} = \sum_{i=1}^k (A_i * Y_{j+1-i}) + H * \sum_{i=0}^k (B_i * F_{j+1-i})$$

Special Cases

- (i) If $k=1$, then single step method.
- (ii) If $k \geq 1$, then multi-step method used requiring past values to generate Y_{j+1} .
- (iii) If $B_0 = 0$, then the method is termed an open method.
- (iv) If B_0 is not equal to 0, then the method is termed a closed one.

This actual algorithm is a combination of open and closed

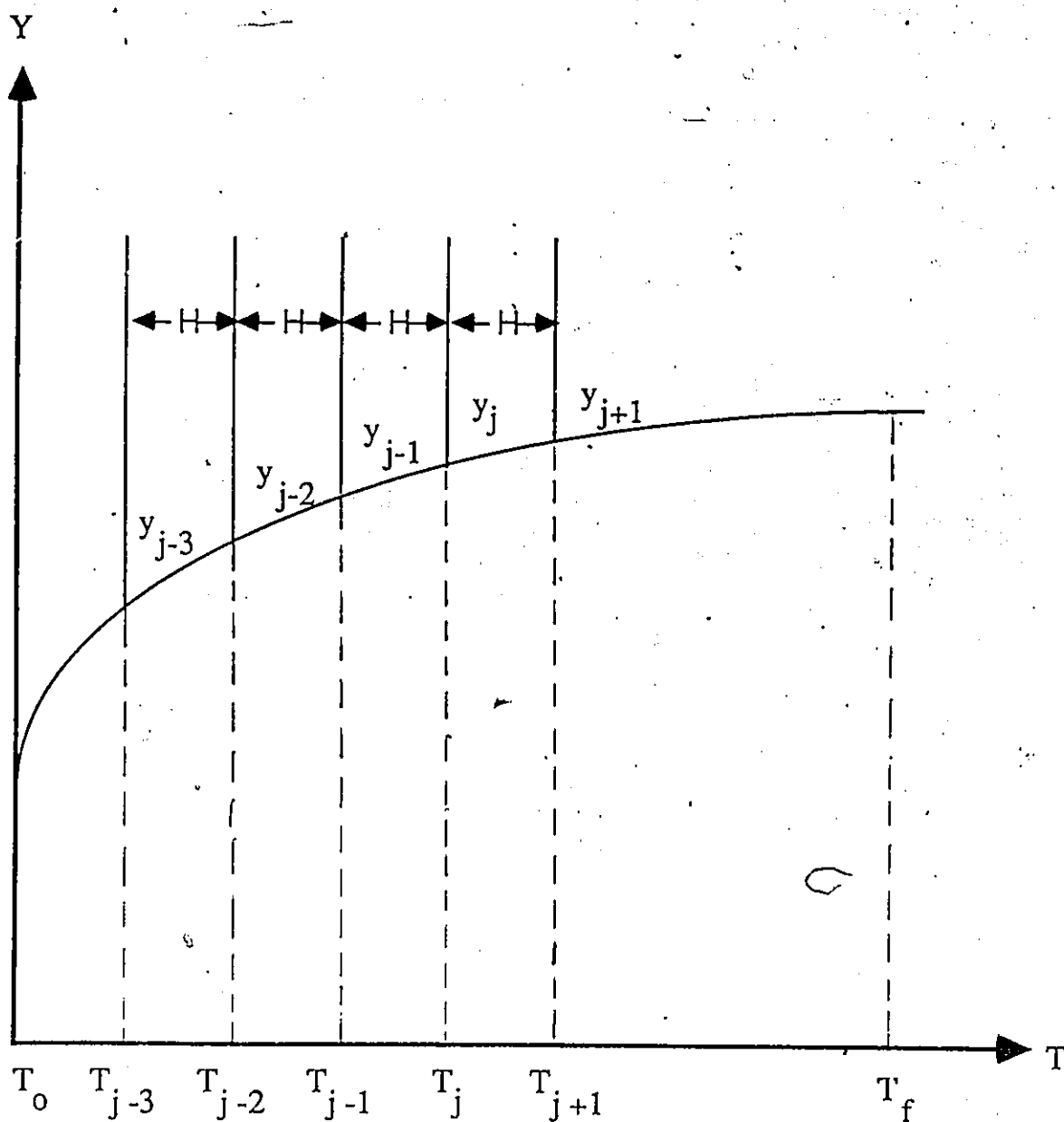


Figure 4.9 Solution Procedures for Multistep type Formulas Requiring Information for $T < T_j$

formulas seeking to utilize the advantages of both types of formulas to make a more efficient algorithm. The open formula used is the predictor method and is called the Adams-Bashforth method given by (Hornbeck 1975):

$$Y_{j+1} = Y_j + ((H/24) * (55*F_j - 59*F_{j-1} + 37*F_{j-2} - 9*F_{j-3}))$$

The closed formula used is the corrector method and is called the Adams-Moulton method given by (Hornbeck 1975):

$$Y_{j+1} = Y_j + ((H/24) * (9*F_{j+1} - 19*F_j - 5*F_{j-1} + F_{j-2}))$$

The algorithm's procedure involves firstly using a fourth order Runge-Kutta formula to obtain the values of Y and F for the first three step sizes beyond the initial condition. The open formula described by the Adams Bashforth is used to predict or estimate Y_{j+1} (p) the value of Y at the next step since the closed formula although accurate requires iterative procedure. Then using this predicted value of Y_{j+1} (p) as a first estimate, the closed formula described by the Adams Moulton can be iterated until the desired degree of convergence is obtained. A similar procedure for step size control as that of the Runge-Kutta Fehlberg is used. However, in this case, since the multi-step method requires equal step sizes for the starting values, any change in step size necessitates recalculating new starting values at that point using the Fourth Order Runge-Kutta algorithm. As a result, this algorithm is inefficient when

frequent output points are requested by the user. In addition, the tolerance specified by the user is used to calculate the initial step size as shown in the Runge-Kutta, Fehlberg Algorithm.

Finally, the algorithm has embedded in its structure a stiffness indicator. As pointed out by Hull (1980), a desirable feature of a non-stiff method, is to provide a warning of any stiffness that might be experienced. In general terms, a problem exhibits stiffness if its solution components are slowly varying but solutions with very rapidly changing components are possible. These problems are physically important and as a result we have decided to follow the advice of Hull and include a rough measuring criterion for indicating where stiffness is likely to occur. The test is merely to monitor the number of steps required by the models to complete the integration using a low order method since stiffness is usually detected by such a method (Shampine and Gordon 1975 pp.143-145). If the actual number of steps required by the model to complete the integration exceeds the computed value, then the user is alerted as to the possibility of stiffness occurring in the model.

The limitations of the test must be realized. It is quite obvious that false returns can occur. It may be the case that the model actually requires low orders and a lot of work. The test would then return a false statement of stiffness. Thus, the test should not be seen as being

perfect but to identify situations which warrant further investigations as to the validity of the stiffness suspicions given by the test. The value of the number of steps used in the testing procedure is dependent on the interval and the starting step size.

Number of steps: $NSTEPS = (TFIN - TINIT) / (HINIT * 10)$

4.2.3.2. Structured Algorithm

Figures. 4.10 and 4.11 show the details of the Fourth Order Adams algorithm used in the run-time library.

List of variables for Fourth- Order Adams Algorithm

T	- Computational Time
TINIT	- Initial time of Simulation
TFIN	- End Time of Simulation
TCOM	- Communication Time
COMINT	- Communication interval
H	- Current step size
HINIT	- Initial step size
HMIN	- Minimum allowable step size
HBOUND	- Upper bound on initial step size
N	- Dimension of vector
Y	- Vector of state variables
Yp	- Predicted values of state variables
Yc	- Corrected values of state variables
Fn-1..Fn-3	- Values of three previous state derivatives
ERR(N)	- Vector of local error estimates for all state variables
ERRMAX	- Maximum local error estimate
TOL	- Integration error tolerance
NFLAG	-
	- 0 TCOM has not been detected
	- 1 TCOM has been detected
NSTEPS	- Number of steps for stiffness check
NCHECK	- Actual number of steps taken during simulation

Figure 4.10 List of Variables Used in Fourth-Order Adams Method

Subroutine Adams Predictor-Corrector Method

Compute initial step size HINIT

$$HINIT = \min(HBOUND, ((\text{abs}(0.5 \cdot TOL / FDER)) ** 0.5) / 4)$$

Determine number of steps for stiffness check:

$$NSTEPS = 10 * (TFIN - TINIT) / HINIT$$

Set NCHECK = 0

Compute starting values using RK4 method

While (T < TFIN)

While (T < TCOM)

If ((TCOM - T) <= (H + HMIN)) AND (NFLAG = 0)

Then H = (TCOM - T) / 2

Set NFLAG = 1 (Communication time detected)

End If

Predict new states at next step using Adams-Basforth :

$$Yp = Y + (H/24) * (55 * (Fn) - 59 * (Fn-1) + 37 * (Fn-2) - 9 * (Fn-3))$$

Compute corrected values of states using Adams-Moulton :

$$Yc = Y + (H/24) * (9 * (Fn+1) + 19 * (Fn) - 5 * (Fn-1) + (Fn-2))$$

Compute local error estimate of all state variables :

$$E = |Yc - Yp| / (10 * H)$$

Determine the maximum local error estimate: ERRMAX

If (ERRMAX > TOL)

Then

Reduce Step Size

Perform step size control (as in Figure 4.9)

Reject computed state values

Recompute starting values using RK4

NCHECK = NCHECK + 3

Else

Update time: T = T + H

Store values of new states

NCHECK = NCHECK + 1

End If

If ((ERRMAX <= (0.1 * TOL))

Then

Augment Step Size

Perform step size control (as in Figure 4.9)

If ((T + (3 * H)) <= TCOM)

Then

Recompute starting values using

RK4

NCHECK = NCHECK + 3

Else

H = HPREV

End If

End If

If (NCHECK > NSTEPS)

(Perform stiffness check)

Then Alert user that model stiffness is suspected

End If

End While

Call OUTPUT(Y,N,T)

Compute next TCOM :

TCOM = TCOM + COMINT

If ((TCOM >= TFIN) .AND. (T NOT = TFIN))

Then TCOM = TFIN

End If

Set NFLAG = 0

End While

Call OUTPUT(Y,N,T)

End Subroutine Adams Predictor-Corrector Method

Figure 4.11. Details of The Adams Predictor Corrector Method

4.2.3.3 Program Structure

Figure 4.12 shows the pictorial view of a program using the Adams Predictor Corrector Method to drive the simulation of a model.

Main Program

This is very similar to the main program for the Runge-Kutta Method. However, it makes CALLS to the Adams subroutine to carry out the run-time activities for the model.

Subroutine INIT

This subroutine is linked to the MAIN program and utilizes the XMENU software within the IBM environment to allow the user to interactively initialize the appropriate model parameters, initial values, and other experimentation variables.

Subroutine ADAMS

This subroutine contains the integration algorithm for the Adams Predictor Corrector Method. It is called from the main program to carry out the run-time activities. In carrying out the integration, it makes subsequent CALLS to the Runge-Kutta starter subroutine as necessary, and to the ADCOMP subroutine.

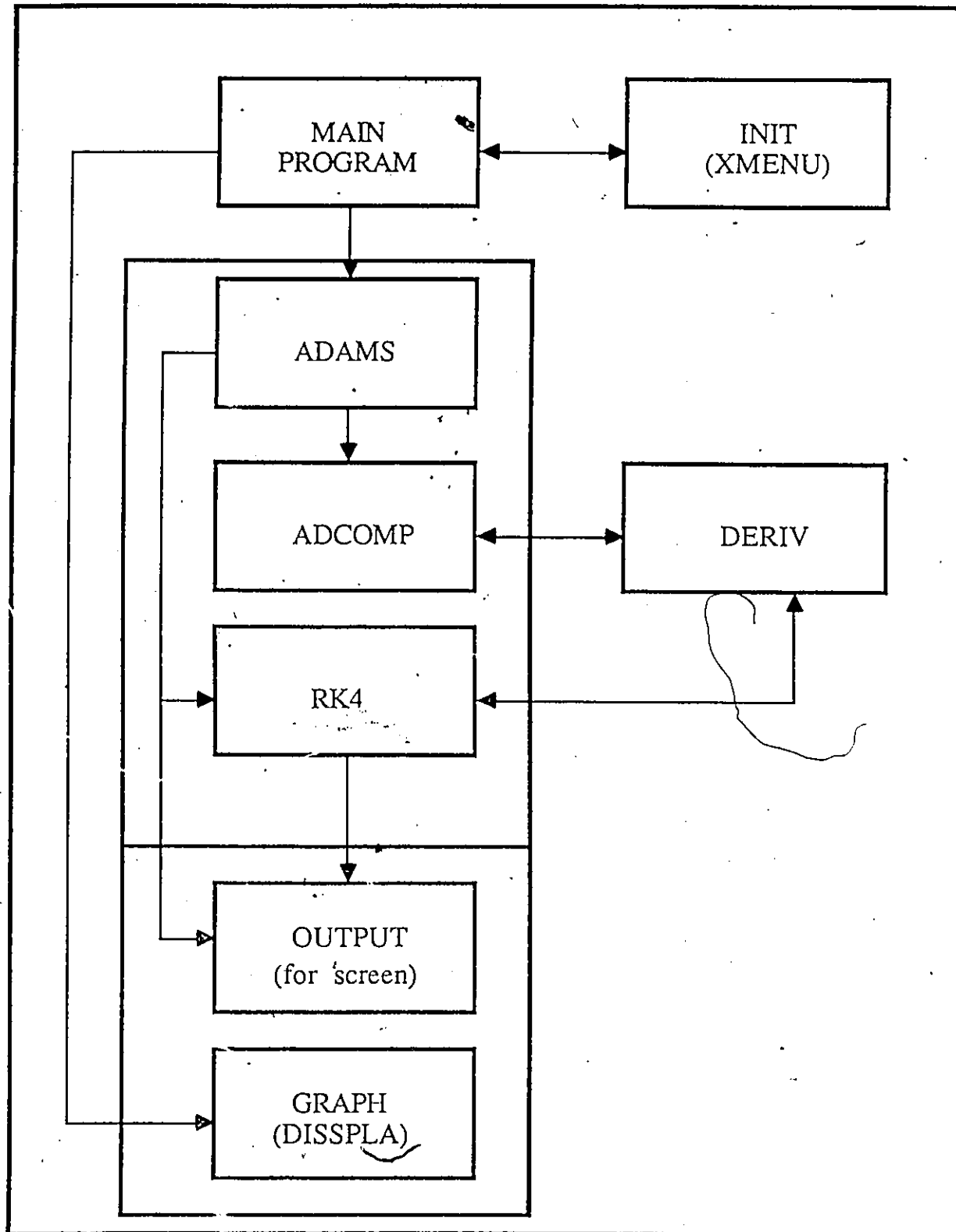


Figure 4.12 Modules of an Interactive Procedural Program using Adams Method

Subroutine RK4

This subroutine uses the Runge-Kutta algorithm as a starter to determine the three previous function evaluations needed by the Adams Method. It is invoked at the beginning of the simulation from the subroutine Adams and at each step size change. It makes CALLS at each stage of the integration to the DERIV subroutine to determine the values of the derivatives of the states.

Subroutine DERIV

This is a model dependent routine containing the necessary functions and information to carry out the computational steps as explained in section 4.2.1.3. It is used by the starter RK 4 subroutine and the subroutine ADCOMP.

Subroutine ADCOMP

This subroutine performs the calculations of the predictor and corrector formulas for the Adams Method. It utilizes the subroutine DERIV in carrying out its calculations.

Subroutine OUTPUT

The values of the outputs at each communication time are stored and an interactive tabular display is shown to the user during the simulation run. This subroutine is called

from the subroutine ADAMS.

Subroutine GRAPH

This subroutine linked to the MAIN program utilizes the Disspla software within the IBM environment to provide post-run hard copy graphic displays of the desired model outputs with time.

The variable step Fourth Order Adams method is imbedded within the Rudder Control model in Appendix C.

4.3. MULTI-RATE INTEGRATION ALGORITHM

4.3.1. Introduction

This particular type of integration algorithm has been included in the library to deal specifically with the simulation of large dynamic systems which involve relatively few interconnections. This essentially means that relatively few of the outputs (usually state variables in the absence of an output function) of some component system are inputs to some component system (Birta 1980). In practice, large dynamic systems, such as those in many chemical and petroleum processes, require frequent experimentation with the initial value problem that describes the process. As a result, what the integration does is to reduce the CPU time required by the process especially in cases where a system having widely different

characteristics can be partitioned into two or more component systems with similar characteristics. This is done without sacrificing the overall accuracy of the solution (Palusinski 1985).

The conventional approach to solving a large system consisting of component systems is simply to group together all the equations describing the component systems into one subroutine and then solve them as a single collection of differential equations. However, using this approach in a system comprising of two component systems having varied frequency components would involve significant computational inefficiency. This would arise, since the integration would proceed at a rate totally dependent on the most severe conditions experienced amongst the component systems. This occurs when the maximum local error estimate of the state variables provided by the integration formula exceeds the user's specified tolerance. As a result, some component systems which could have been integrated using a larger step size are unable to do so.

Birta (1980) has considered this problem along with a particular implementation of a quasi-parallel method. In addition, he suggests and formulates possible measures for evaluating the computational advantages of such a method. Finally, he provides results of numerical experiments that provide insight into the question of trade-offs between accuracy and computational gain.

The quasi-parallel method allows the solution to each component system to move forward independently in time. It does this by using an interpolation/extrapolation scheme based on a cubic polynomial to compute the interconnection variables when they are required by the integration of a particular component system. The coefficients of the polynomial are determined from data at two previously computed time points on the trajectory of the interconnecting variable. In addition, a strategy is used to sequence the advancement of the various component systems forward in time so as to minimize extrapolation errors involved in handling the interconnecting variables.

The conclusion of the study using the quasi-parallel method was that its effectiveness was limited to the case where not more than three interconnecting variables were involved. The method's accuracy was also found to be dependent on the order of the integration method and the order of the interpolation being the same. This is again a limiting factor since the computational requirement of the interpolation procedure increases significantly with the order. Even for a third order method whose accuracy is not very high, the cubic polynomial interpolation already has significant computational requirements. Hence, the use of such a method as a potentially efficient way of handling the simulation of large dynamic systems may be hard to justify especially if high order integration methods are to be employed.

Brosilow (1985) suggests a modular integration technique. This allows computational speed through the parallel processing of individual component systems and allows the best integration methods to be used for each component system. Independent error control used in the individual dynamic simulators ensures that the proper step size is taken in each component system. Hence the efficiency of the overall simulation is not adversely influenced by the step size in any single component system. Several coordination algorithms including a new Newton type algorithm are suggested to deal with the interconnection problem and to keep the various component systems in time synchronization. These coordination algorithms have essentially three phases after initialization:

- 1) Estimation of error,
- 2) Adjustment of time horizon or interconnection variables, and
- 3) Computation of interconnection variables for the next time horizon.

The conclusion of such a method is that modular integration methods are robust and efficient particularly supported by the theoretical analysis of the stability and convergence properties of the methods as presented by Brosilow (1985). As indicated previously, the software for such an algorithm, is developed on parallel processors.

4.3.2. DESCRIPTION OF THE ALGORITHM

The algorithm implemented does not involve parallel processing and hence is based on the method by Palusinski (1985) for the integration of two time scale systems. The large dynamic system is characterized by the following initial value problem:

$$Z' = p(Z, T); Z = Z(0)$$

$T \in [0, T_f]$ where vector Z is composed of rapidly varying components X , as well as slowly varying components Y over the interval T where $\dim Z = \dim X + \dim Y$. It is assumed that the single large dynamic system can be partitioned into two individual component systems which are not independent of one another, one a so called fast component system and the other a slow component system with specified initial conditions as follows:-

$$\begin{aligned} X' &= F(X, T, Y) && - \text{fast component system} \\ Y' &= G(Y, T, X) && - \text{slow component system} \\ X_0 &= X(0) \\ Y_0 &= Y(0) \end{aligned}$$

In general, coupling exists between the component systems such that the outputs of one component system may be inputs to another. In integrating the resulting two time scale systems, two routines are utilized. The Slow Routine is used to integrate the slow component system while the Fast Routine is used in the fast component system integration.

Each component system is integrated independently using different step sizes and independent error control. The explicit Runge Kutta Merson algorithm is used in the integration of both the Slow and Fast Routines. The formula used by the Runge-Kutta Merson algorithm for the step Y_j to Y_{j+1} is :

$$K1 = H * F(T, Y),$$

$$K2 = H * F(T + H/3, Y + K1/3),$$

$$K3 = H * F(T + H/3, Y + K1/6 + K2/6),$$

$$K4 = H * F(T + H/2, Y + K1/8 + (3/8)*K3),$$

$$K5 = H * F(T + H, Y + K1/2 - (3/2)*K3 + 2*K4);$$

$$Y_{j+1} = Y_j + (K1 + 4*K4 + K5)/6$$

$$E = H * \text{abs}(K1/3 - (3/2)*K3 + (4/3)*K4 - K5/6)$$

The underlying idea in the multi-rate integration approach is to carry out the following steps. The Slow Routine firstly computes the values of the slow state variables at each step size of the integration. It does this by utilizing imbedded Runge-Kutta schemes to compute each $K1...K5$ at each stage as depicted by the above formula.

The imbedded formulas for computing intermediate approximations using explicit Runge Kutta schemes are (Palusinski 1985, P. 273):

- 1) First-Order formula for computing the approximation of the solution Y at $T = T_j + H/3$ also called Euler formula is:

$$Y_{j+1/3} = Y_j + H * K1/3 ;$$

$$K1 = F(Y_j, T_j, X_j)$$

- 2) Second-Order formula for computing the approximation of Y at the same time also called improved Euler formula defined as:

$$Y_{j+1/3} = Y_j + H * (K1 + K2)/6 ;$$

$$K1 = F(Y_j, T_j, X_j)$$

$$K2 = F(Y_j + H * K1/3, T_j + H/3, X_{j+1/3})$$

- 3) Third-Order formula for computing the approximation of Y at $T + H/2$ is obtained from the third order formula (Lambert 1973) by taking half of the step and has the form:

$$Y_{j+1/2} = Y_j + H * (K1 + 3*K3)/8$$

$$K1 = F(Y_j, T_j, X_j)$$

$$K2 = F(Y_j + H * K1/3, T_j + H/3, X_{j+1/3})$$

$$K3 = F(Y_j + H*(K1 + K2)/6, T_j + H/3, X_{j+1/3})$$

Additionally, the Fast Routine integration uses the conventional Runge Kutta Merson Method to compute the values of the fast system variables over time horizons which are multiples of the Slow Routine step size during each step size of the Slow Routine, in particular at $H/3$, $H/2$ and H . Depending on the coupling resulting from the system partition, interpolation/extrapolation techniques are used to determine values of interconnecting Slow Routine state variables Y necessary for the Fast Routine integration at

each step size of the integration. The following interpolation/extrapolation scheme is used in the integration algorithm at the different stages of each integration step:

Linear Interpolation:

$$1) Y(T) = Y_j + (T - T_j) ;$$

$$T_j \leftarrow T \leftarrow T_j + H/3$$

$$2) Y(T) = Y_j + H/3 + (T - T_j + H/3) * (-K1/4 - K2 + (9/4) * K3) ;$$

$$T_j + H/3 \leftarrow T \leftarrow T_j + H/2$$

Extrapolation using Euler Method:

$$Y(T) = Y_j + H/2 + (T - T_j + H/2) * K4 ;$$

$$T_j + H/2 \leftarrow T \leftarrow T_j + H$$

4.3.3 Structured Algorithm

Figures 4.13(a),(b), and 4.14 show the details of the multi-rate integration algorithm used in the run-time library.

List of variables for Multi-Rate Integration Algorithm

$\dagger$	- Computational Time
TINIT	- Initial Time of Simulation
TFIN	- End Time of Simulation
TCOM	- Communication Time
THOR	- Next Horizon Time
COMINT	- Communication interval
H	- Current step size
HINIT	- Initial step size
HSMIN	- Minimum allowable step size for slow system
HFMIN	- Minimum allowable step size for fast system
HBOUND	- Upper bound on initial step size
Y	- Vector of slow system state variables
X	- Vector of fast system state variables
N	- Dimension of slow system state vector
M	- Dimension of fast system state vector
ERR(N)	- Vector of local error estimates for all slow system state variables
ERRMAX	- Maximum local error estimate of slow system state variables
ERF(M)	- Vector of local error estimates for all fast system state variables
ERFMAX	- Maximum local error estimate of fast system state variables
TOLERS	- Slow system error tolerance
TOLERF	- Fast system error tolerance
FDER	- Maximum value of derivative functions at initial time
NFLAG	-
	- 0 TCOM has not been detected
	- 1 TCOM has been detected

Figure 4.13(a) List of Variables Used in the Multi-Rate Algorithm

```

Subroutine Multi-Rate Algorithm
-----
Slow Routine- Modified RK Merson
-----
Set NFLAG = 0 (TCOM has not been detected)
Compute initial step size
  HINIT = min(HBOUND, ((abs(0.5*TOL/FDER)) ** 0.5)/4)
Compute initial TCOM
-----
While (T < TFIN)
  While (T < TCOM)
    If (((TCOM - T) <= (HINIT + HMIN)) AND (NFLAG = 0))
      Then H = (TCOM - T)/2
      NFLAG = 1 (Communication time detected)
    End If
    Compute K1: Y - Slow system variables
                at T
                K1 = DERIVS(Y, T, X) X - Fast system variables
                at T
    Use Imbedded Euler Method to predict
      Y at T + H/3 :
      Y + H/3(p) = Y + (H/3)*K1
    CALL Fast Routine to determine X + H/3
    Compute K2:
      K2 = DERIVS(Y + H/3(p), T + H/3, X + H/3)
    Use Imbedded Improved Euler Method to
      correct Y at T + H/3:
      Y + H/3 = Y + (H/6)*(K1+K2)
    Compute K3:
      K3 = DERIVS(Y - H/3, T + H/3, X + H/3)
    Use Imbedded third order RK formula to estimate
      Y at T + H/2:
      Y + H/2 = Y + (H/8)*(K1+3*K3)
    CALL Fast Routine to determine X + H/2
    Compute K4:
      K4 = DERIVS(Y - H/8*(K1+3*K3), T+H/2, X + H/2)
    CALL Fast Routine to determine X + H
    Compute K5:
      K5 = DERIVS(Y - H/2)*K1 + 3*(H/2)*K3 + 2*H*K4,
            T + H, X + H)
    Compute local error estimates of states : ERR(N)
    Determine maximum local error estimate : ERRMAX
    If (ERRMAX <= TOLERRS)
      Then Update Time: T = T + H
      Compute new Y at T
    End If
    If ((NFLAG = 0)
      Then Perform step size control (as in Figure 4.13)
    End If
  End While
  CALL OUTPUT(Y, N, T)
  Compute next TCOM : TCOM = TCOM - COMINT
  If ((TCOM >= TFIN)
    Then TCOM = TFIN
  End If
  Set NFLAG = 0
End While
CALL OUTPUT(Y, N, T)
End Subroutine Multi-Rate Algorithm

```

Figure 4.13.(b) Details of Slow Routine of Multi-Rate Algorithm

```

Subroutine Fast Routine                                     (RK-Merson Method)
Compute initial step size
  HINIT = min(HBOUND, ((abs(0.5*TOL/FDER)) ** 0.5)/4)
While (T <= THOR)
  If (THOR - T < H/3)
    Then | Linearly interpolate for values of input variables
          | from the slow system between [T, T + H/3]
    ElseIf (THOR - T < H/2)
      Then | Linearly interpolate for values of input
            | variables from the slow system between
            | [T, T + H/2]
    ElseIf (THOR - T < H)
      Then | Extrapolate utilizing Euler's Method for
            | values of input variables from the slow system
            | between [T + H/2, T + H]
    EndIf
  Compute state derivatives K1..K5 for each state variable
  Compute local error estimates of all state variables: ERF(M)
  Determine the maximum local error estimate : ERFMAX
  If (ERFMAX <= TOLERF)
    Then | Update Time: T = T + H
          | Compute new states at T
    End If
  Perform step size control                               (as in Figure 4.8)
End While
End Subroutine Fast Routine

```

Figure 4.14 Details of Fast Routine of Multi-Rate Algorithm

4.3.4 Program Structure

Figure 4.15 shows the pictorial view of a program using the multi-rate integration method to drive the simulation of a model.

Main Program

This is very similar to the main program for the Runge-Kutta Method. However, it calls to the subroutine SRATE to carry out the run-time activities for the model.

Subroutine INIT

This subroutine is linked to the MAIN program and utilizes the XMENU software within the IBM environment to allow the user to interactively initialize the appropriate model parameters, initial values, and other experimentation variables.

Subroutine SRATE

This subroutine uses the variable step Runge Kutta Merson method to integrate the slow routine during the simulation. However, the values of the state variables at the different stages of each step size are computed using imbedded formulas for computing intermediate approximations using explicit Runge-Kutta schemes. These formulas use the subroutine DERIVS in their computations.

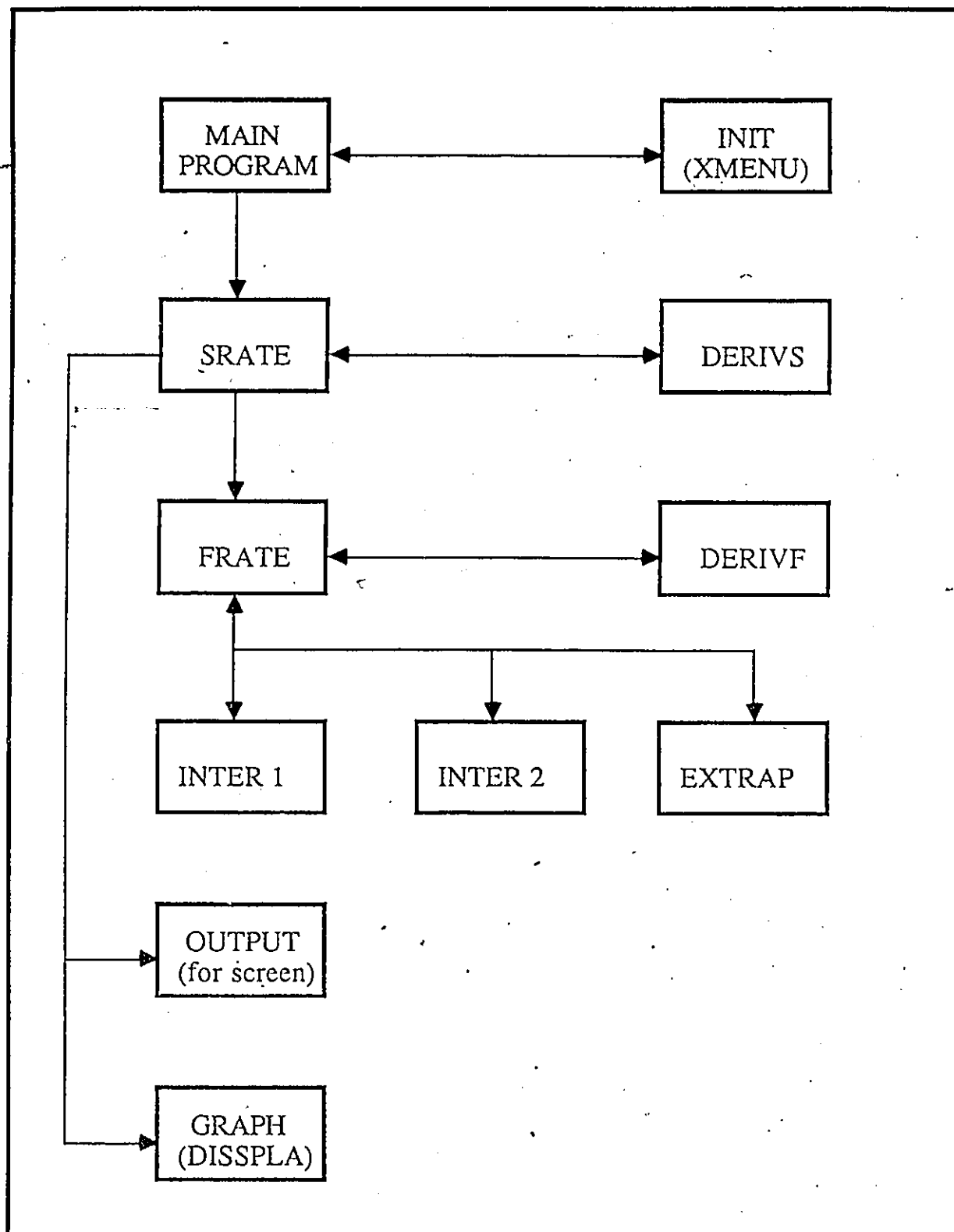


Figure 4.15 Modules of an Interactive Procedural Simulation Program using Multi-Rate Algorithm

Subroutine FRATE

Called by the subroutine SRATE, it uses the normal variable step Runge-Kutta Merson to integrate the fast routine during the simulation using the subroutine DERIVF in its computations.

Subroutine INTER1

This subroutine determines the value of the slow system interconnection variables by linear interpolation during the fast routine integration between T_j and $T_j + H/3$

Subroutine INTER2

This subroutine determines the value of the slow system interconnection variables by linear interpolation during the Slave Routine integration between $T_j + H/3$ and $T_j + H/2$

Subroutine EXTRAP

This subroutine determines the value of the slow system interconnection variables by extrapolation using Euler's Method during the fast routine integration between $T_j + H/3$ and $T_j + H/2$

Subroutine DERIVS

This is a model dependent subroutine and contains the necessary functions and information to carry out the computational steps needed for the integration of the slow

routine:

Subroutine DERIVF

This is a model dependent subroutine and contains the necessary functions and information to carry out the computational steps needed for the integration of the Fast Routine.

Subroutine OUTPUT

The values of the outputs at each communication time are stored and an interactive tabular display is shown to the user during the simulation run. This subroutine is called from the subroutine SRATE.

Subroutine GRAPH

This subroutine linked to the MAIN program utilizes the Disspla software within the IBM environment to provide post-run hard copy graphic displays of the desired model outputs with time.

The multi-rate integration algorithm is imbedded within the Electronic Oscillator Model in Appendix G.

CHAPTER 5

GEST RUN-TIME LIBRARY - SECTION 2

5.1 THE DISCONTINUITY PROBLEM

It is quite common to encounter discontinuities in the simulation of continuous systems and it is one of the main problem areas in the solving of ordinary differential equations. In general, the continuous simulation model will be comprised of the set of ordinary differential equations having the form

$$Y' = F(T, Y(T))$$

where Y represents the state vector $(Y_1, \dots, Y_n)$ and each F represents the corresponding system derivative function.

The types of discontinuities associated with such systems can be classified as derivative discontinuities and jump discontinuities (Ören 1987d). Derivative discontinuities correspond to a model update as shown in Figure 5.1. This update may involve a model change which can take place by replacing the function which specifies the derivative of a state variable or by merely updating the value of one or more parameters which appear in the derivative function. Jump derivatives refer to the reinitialization of a state variable and correspond to a sudden change of a state variable as shown in Figure 5.2. Finally, it should be further realized that both jump and derivative discontinuities can take place simultaneously as shown in

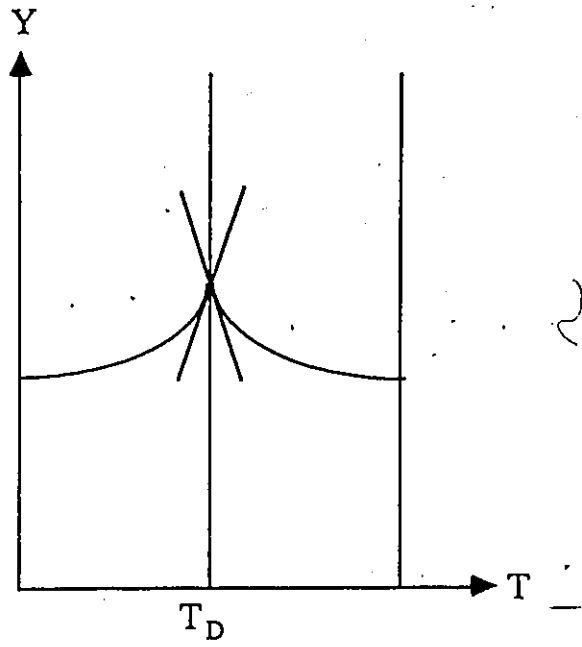


Figure 5.1 Derivative Discontinuity

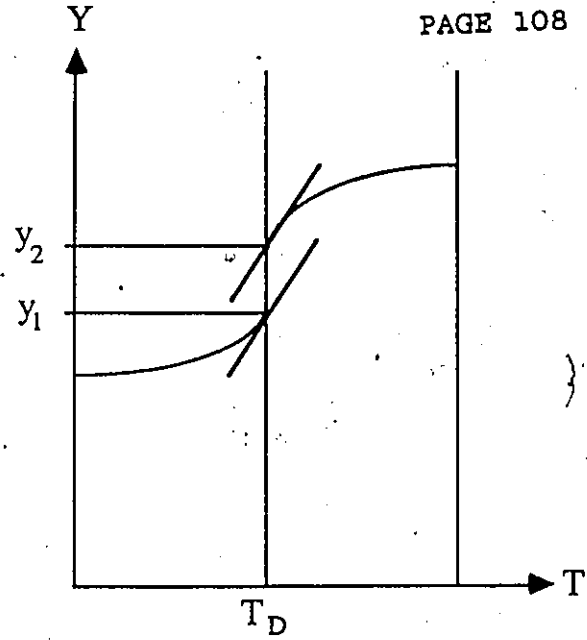


Figure 5.2 Jump Discontinuity

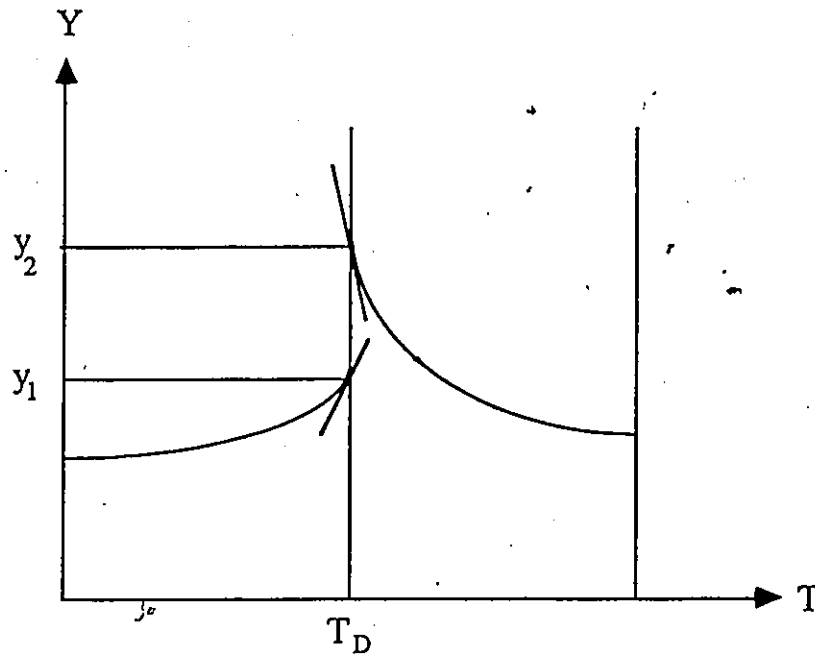


Figure 5.3 Jump and Derivative Discontinuity

Figure 5.3.

In the literature (Cellier 1979), from the implementation point of view, two types of discontinuity processing are discussed. These consist of 1) time events and 2) state events. If the discontinuity time is known a priori, one can schedule a time event at that point. In the processing of a time event, the step size simply has to be reduced to the scheduled event time. When the integration has reached the event time, depending on the nature of the discontinuity i.e. derivative or jump discontinuity, the model update or state variable reinitialization can be performed. In the case of state events, time is not known a priori, and they are triggered once some pre-specified state condition is met. An example of such a condition could be when a state variable reaches some threshold value.

In the processing of state event discontinuities, the conditions which determine the changes in the model can be expressed as a set of discontinuity functions or as more commonly referred to in the literature switching functions $S_1(T, Y(T))$, $i = 1 \dots m$ such that an actual model change occurs when one of the

$$S_1(T, Y(T)) = 0$$

Thus it can be clearly seen that the discontinuity processing problem for state events reduces to firstly detecting the zeros of the discontinuity functions using an appropriate detection scheme. Upon detection, the unknown

event times must be accurately located using an iteration procedure inherent in the procedure. Once located, the step size will be adjusted so that the integration proceeds right up to the point of discontinuity. At that point, the appropriate model updates and/or reinitialization of state variables as determined by the discontinuity function(s) are triggered.

5.2 REVIEW OF PREVIOUS WORKS

A number of methods have been developed to deal with this problem especially since it was clear that standard ordinary differential equation solvers were both inadequate and inefficient. The early solvers dealt with the discontinuities by estimating the local truncation error. Based on the error, the integration would either continue or the step size would be halved and the integration step repeated. This causes excessive creeping around the discontinuities (Ellison 1981)

The most common methods involve the use of switching functions, although few such as Gear and Osterby (1984) look at processing discontinuities in situations where external indicators such as pre-defined switching functions, are not available. In this method, the magnitude and order of the discontinuity is estimated based on examining the local truncation error and its estimate. The method involves a predictor-corrector integration process. However, in our discussion, we concentrate on the methods where switching functions are known.

Carver's method (Carver 1978) for detecting and processing discontinuities represents them as switching functions, as mentioned earlier, which are triggered when particular conditions are fulfilled. The switching functions are differentiated by the user and attached to the

system of equations as an auxiliary set. Also, scaled derivatives up to the order of the integration q are stored so that the prediction of Y at time $T + H$ is given by a set of equations. From these equations, an accurate estimate of the discontinuities eliminates the creeping mentioned above. The detection of the crossover points where the switching function passes through zero results in determining an H_1 such that the set of equations mentioned earlier is zero in the neighbourhood of $S(T)$. This reduces to the problem of solving a q th order polynomial for $S(H_1)$. However, a simpler criterion involving the product of the switching functions and their derivative at the interval points is usually adequate.

Cellier (1979) introduces a distinction for continuous systems possessing discontinuities and those that do not. The following definitions clarify this distinction:

" Combined systems are systems described, either during the whole period under investigation or during a part of it, by a fixed or variable set of differential equations where, at least one state variable or one state derivative is not continuous over a simulation run. " >

(Cellier 1979, P. 17)

" Continuous systems are systems described by a fixed set of differential equations with state variables and first state derivatives both being continuous over the whole simulation run. "

(Cellier 1979, P. 17)

Cellier considers the two types of discontinuities discussed earlier and conveys the fact that continuous simulation has to be performed either up to the next scheduled event time or until a state condition is met which triggers execution of a state event, whichever comes first. His detection criterion involves realizing the integration step where a discontinuity function changes its sign for the first time. Within this step, it is clear that a state event has taken place. In the location of the discontinuity, he suggests that although any good iteration procedure can solve the problem, an iteration procedure with a quadratic or cubic convergence ratio should be used so that the iteration procedure could converge as soon as possible for efficiency. In addition, for software robustness requirements, the procedure should have an infinite convergence range. For these above reasons, he proposes a combination of the inverse Hermite Interpolation (fast convergence) with Regula-Falsi (unlimited convergence range) methods.

Ellison (1981) uses a similar approach to the problem by classifying types of discontinuities as time and state events. His method claims that time events can be immediately located, while the state events require one inverse interpolation. With this breakdown of events the

inefficiency produced by other procedures (e.g. Carver 1978) for systems which involve time events only or mixed time and state events is eliminated.

In the integration of the system where time and state events both occur separately, we will know the time of the 'time' event but cannot advance the step until it has been concluded that no state event occurs before this. If a particular condition for the state event has been met, the time of occurrence dictates the new integration step. The location of this time is determined as accurately as the tolerance designated by the user. The method is an adaption of the Shampine method and uses a fairly simple threshold detection criterion for detecting the discontinuity. Additionally, it utilizes the inverse third order Hermite interpretation procedure requiring values of y and y' at t_j and t_{j+1} for location of the discontinuity.

Birta et.al. (1985) utilize a robust procedure for dealing with the problem. The procedure assumes the presence of state events only. It considerably improves on the detection criterion suggested by Carver and others. The criterion is based on a cubic polynomial model requiring values of the switch functions and their derivatives at the interval boundaries. The only real limitation occurring if three stationary points exist in the interval. The location problem is dealt within a two stage procedure. In the first stage, the regula falsi is first carried out for all

switching functions identified as having a cross over in the interval. The evaluation of S_i at points in the interval as required by the process is done using estimated x values obtained from a fifth-order Hermite Interpretation. The second stage uses the Newton Raphson method to refine the results produced by the first stage.

5.3 PROPOSED INTEGRATION ALGORITHM

The method chosen for use in the run-time library is a modified version of the adaptive order algorithm developed by Ören and Ma (1986). Essentially, it incorporates the breakdown of events as illustrated by Cellier and Ellison and discussed earlier with the adaptive order algorithm. The detection criterion of the algorithm utilizes the values of the discontinuity functions at the boundaries of each interval whilst the location of the discontinuity is found by using an inverse aitken interpolation method with variable order. The algorithm is further enhanced by its ability to deal with systems which involve time events only, state events only, or mixed time and state events. The following advantages provide a good base as to why this algorithm was chosen for use in the run-time library:

- 1) The fact that the code does not require the derivatives of the switching functions makes the code simpler and less of a burden to the modeler.
- 2) The procedure utilizes inverse interpolation, the

robustness of which depends on the existence of the inverse function. From a mathematical viewpoint, (Ma and Liu 1986) one need only check the monotonicity of the switch function over the particular integration interval to guarantee this existence. The fact that the software requirements could be considered on a strict mathematical base further enhances the choice of the method as the discontinuity processing algorithm in the library.

- 3) The order of the interpolation being variable and dependent on the tolerance specified by the user is a very useful component since unnecessary computations will not be carried out. This is so since as the order increases, the number of components of the aitken's table increases.
- 4) The performance of the algorithm is very good since the convergence rate increases as the order of the interpolation increases.
- 5) The main benefit of using an inverse interpolation should be realized. A unique solution exists for the time at which the interpolation polynomial is zero. In addition, the process will be quicker than if the direct polynomial method is used which may have several solutions to choose the correct one from.

- 6) The efficiency achieved by the algorithm being able to handle systems involving time events only, state events only, or mixed state and time events is clearly advantageous over other methods.
- 7) The iterative process of the aitken's method makes it a very useful method to implement on the computer.

The main disadvantage of the algorithm exists in its detection scheme. The detection criterion involving the product of the values of the switch functions at the interval boundaries may not always be totally reliable, for example, in cases where an even number of cross-overs occur in the same step interval as Figure 5.4 illustrates. In such cases, the algorithm has no chance to detect the crossovers. Such discontinuities are labelled short-living discontinuity functions (Cellier 1979). However, as Gear and Osterby (1984) point out, the detection of a discontinuity should involve a very low cost set of tests since they have to be activated, as in our case, at each step of the integration routine. Additionally, to circumvent this problem the size of the integration step has been restricted to a value HMAX. In keeping the step size relatively small, the probability of missing a discontinuity will be smaller.

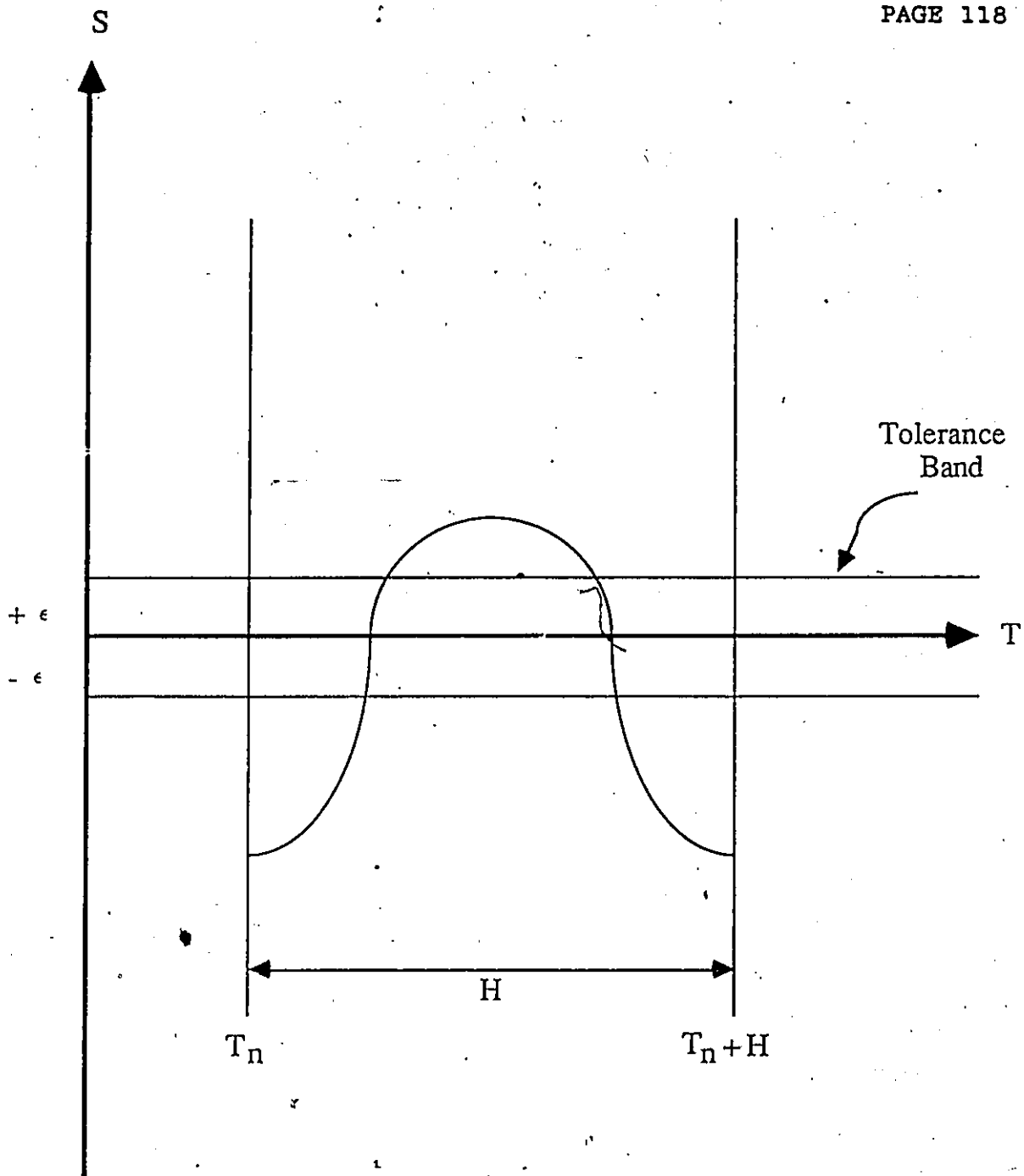


Figure 5.4 Even Number (2) of Cross overs in a Step Size

5.3.1 Details of Algorithm

As discussed previously, the algorithm effectively deals with systems having both derivative and jump discontinuities expressed as time and state conditions. Thus, for the sake of clarity, we discuss how the algorithm deals with systems having each of the different types of events.

5.3.1.1 Time Events

In the situation where the system exhibits time events only, the algorithm is somewhat simplified. The number of time events and their exact locations are easily predetermined by the user, who then inputs them to the algorithm. The time values are input in the form of a vector in ascending order of their occurrence. The normal routine using the variable step Runge-Kutta Merson is used to drive the simulation until it is evident that in the next integration step the time of the event will have been surpassed.

At this point, the step size of the integration is adjusted and the Modified Runge-Kutta Merson method is utilized to step right up to the discontinuity point. The model is then updated as specified by the time event. This information is given in a user-supplied subroutine called MODUPD. The process is repeated for the next time event if one exists or if not, the normal Runge-Kutta Merson

integration routine drives the simulation to the end time TFIN. The integration subroutines are discussed later in this section. The step size control is identical to the one used in the Runge- Kutta Fehlberg Method.

5.3.1.2 State Events

In the case where state event discontinuities only are known to exist, the values of the discontinuity functions are calculated at the end of each integration step. A cross over is detected once the product of the previous and present values of a discontinuity function is found to be negative as shown in Figure-5.5.

At this point, the algorithm starts its search to determine the precise location of the crossover within the user's tolerance. This reduces to determining the time of the zero of the corresponding discontinuity function $S(T, Y(T)) = 0$. Using the inverse interpolation method, we simply change the two axes which are 'value of discontinuity function' and 'time' as illustrated by Figures 5.6 and 5.7. Mathematically, the inverse function could be written as $T = T(S)$. At this point, the time T can be approximated by an n degree polynomial, T being available at n corresponding points of S . Thus, using the known values of n points and the Aitken's interpolation formula we can derive T which is corresponding to $S = 0$.

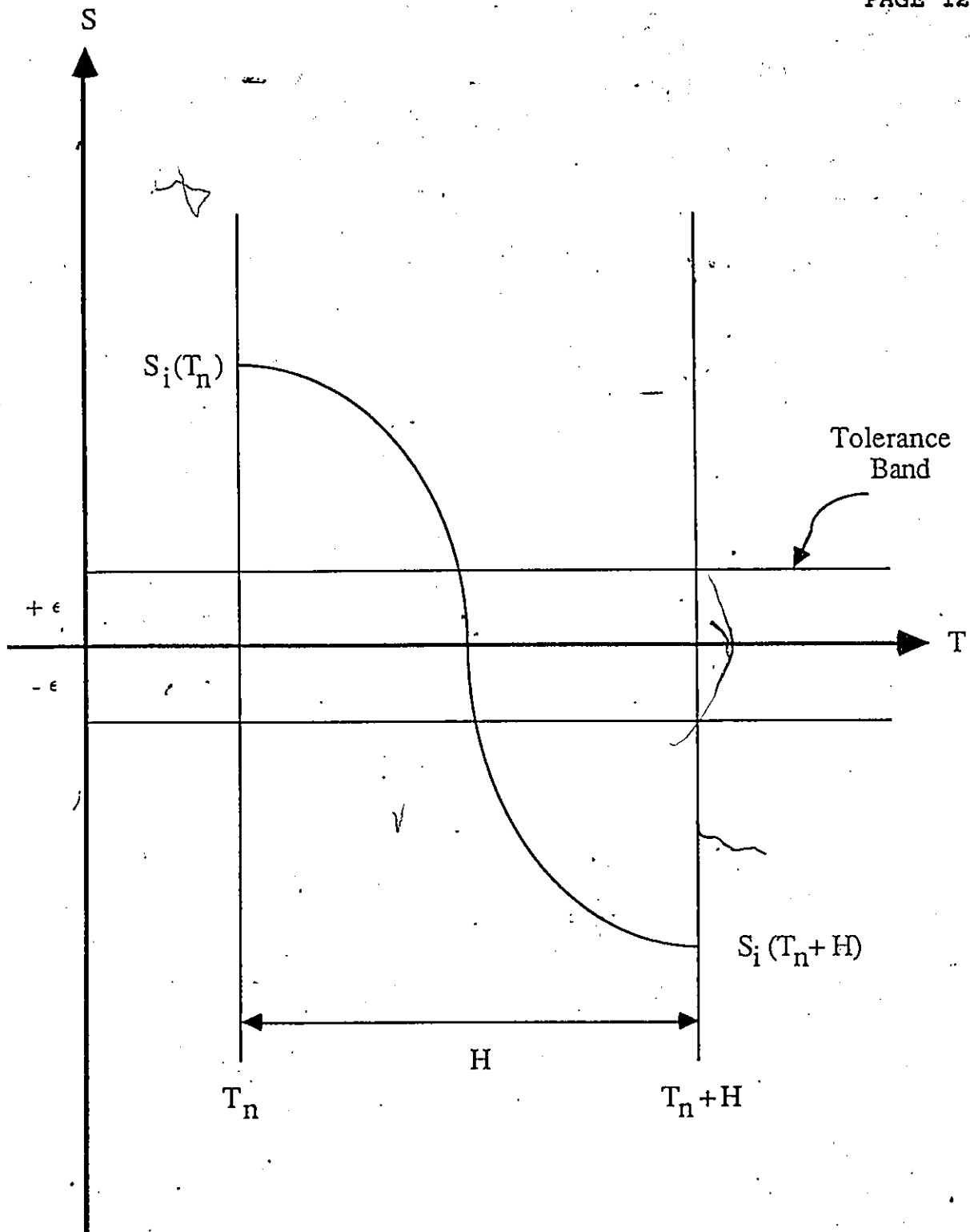


Figure 5.5 Cross-Over Detected in this Step Size

T	T_1	$T_2 \dots$	T_n
$S(T, Y(T))$	$S(T_1)$	$S(T_2) \dots$	$S(T_n)$

Figure 5.6 Initial Interpolation Table

$S(T)$	$S(T_1)$	$S(T_2) \dots$	$S(T_n)$
$T = T(S)$	T_1	T_2	T_n

Figure 5.7 Interpolation Table With Axes Changed

The adaptive algorithm will start with linear interpolation using the previous and current values of the discontinuity function. The first approximation of the time $T(2,2)$ can be calculated from the linear interpolation formula:

$$T(2,2) = \frac{1}{F(2)-F(1)} * \begin{vmatrix} T(1,1) & F(1)-\bar{F} \\ T(2,1) & F(2)-\bar{F} \end{vmatrix}$$

where $F(1)$ and $F(2)$ are values of the discontinuity functions at the boundaries of the last step and $\bar{F}$ is the value of the discontinuity functions we require equal to zero.

Aitken interpolation table now becomes:

$F(1)$	$T(1,1)$	
$F(2)$	$T(2,1)$	$T(2,2)$

The integration step is repeated using the step size $H = (T(2,2) - T(1,1))$ and the new corresponding value of the discontinuity function $F(3)$ is calculated. If the absolute value of $F(3)$ lies within the band of tolerance, the interpolation procedure is stopped. If not, the order of interpolation is increased so that quadratic interpolation can be effected by linear interpolation over two independent linear interpolation polynomials to determine $T(3,3)$. The table, ready for quadratic interpolation will have three points:-

$F(1)$	$T(1,1)$	
$F(2)$	$T(2,1)$	$T(2,2)$

F(3) T(3,1)

where $T(3,1)=T(2,2)$. We calculate $T(3,2)$ in a similar way to $T(2,2)$ and then compute $T(3,3)$ by :-

$$T(3,3) = \frac{1}{F(3)-F(2)} * \left| \begin{array}{cc} T(2,2) & F(2)-\bar{F} \\ T(3,2) & F(3)-\bar{F} \end{array} \right|$$

The process is repeated again, determining the new corresponding value of the discontinuity function $F(4)$ and checking to see if it lies within the tolerance. If not, one could effect cubic interpolation by linear interpolation over two independent quadratic interpolation polynomials. This interpolative process is continued until the tolerance is met.

In the implementation of the algorithm, the iterative inverse Aitkens's interpolation formula is summed up by

$$\begin{array}{l} \text{FOR } K=2 \text{ to } N \\ \text{FOR } I=K \text{ to } N \\ T(I,K) = \frac{1}{F(I)-F(K-1)} * \left| \begin{array}{cc} T(K-1,K-1), (F(K-1)-\text{DELTA}) \\ T(I,K-1), (F(I)-\text{DELTA}) \end{array} \right| \end{array}$$

where DELTA = -0.5 * sign f(d(N)*TOL),
 D(N) = nth value of the stored derivative
 functions of the last step
 TOL = the user tolerance

The DELTA ensures that the S lies within the specified tolerance boundaries totally on the 'opposite' side of the axis, so that at the computed t, S will have changed sign.

Robust checks are carried out for each successive iteration of the interpolation procedure from the start. The validity of the interpolation table generated is checked. Any useless points are discarded and the table generated once more. As an example, using the table above, $T(2,2)$ would be discarded if it was found to be greater than $T(2,1)$ or less than $T(1,1)$. Additionally, at each iteration, the Aitken interpolation table is rearranged according to the ascending order of the discontinuity functions. The algorithm also has a subroutine which handles multi-discontinuities and does a non-monotony check. When several discontinuities occur during an integration step, the routine considers the one which crosses the axis first. This check is repeated for each iterative cycle.

5.3.1.3 Time And State Events

In the final case, the system may have both time and state events. The number and times of the time events will be known exactly, being predetermined by the user. We will try to advance each time event but must first conclude that no state events occur before each one of them. If one or more state events are detected, we must locate their times once again using the inverse Aitken interpolation method as described previously. At each state event, the model is updated as stipulated by the event. Similarly, once a time event is reached, the model must also be updated.

Initially, as long as it has been confirmed that a time event will not occur in the next step, the normal Runge-Kutta Merson method is used to drive the simulation, the discontinuity algorithm, checking at each step for signs of a state event discontinuity. If a state event is detected, the point is located and the modified Runge-Kutta Merson method used to drive the system up to that point. The model update by the state event is carried out, and then the same routine used to continue the integration of the system to the point of the time event discontinuity. Once a time event has been identified to be present in the next step, the modified Runge-Kutta method is used to integrate the system up to the point of discontinuity, as long as a state event is not detected. Model update as required by the time event is then carried out. This process is repeated for each time event interval, and then finally up to the end of the simulation.

5.3.2 Structured Algorithm

Figures 5.8 - 5.11 show the details of the discontinuity algorithm used in the run-time library. Figure 5.8 gives the list of variables while Figure 5.9 shows the global structure of the algorithm. Figure 5.10 shows the details for processing systems where time events only exist. Figure 5.11 shows the details for cases where state events or mixed time and state events occur.

List of variables for Discontinuity Processing Algorithm

T	- Computational Time
TINIT	- Initial time of Simulation
TFIN	- End Time of Simulation
TCOM	- Communication Time
THOR	- Next Horizon Time
TE	- Vector of times at which time events occur
COMINT	- Communication interval
H	- Current step size
HINIT	- Initial step size
HMIN	- Minimum allowable step size
HMAX	- Maximum allowable step size
HBOUND	- Upper bound on initial step size
N	- Dimension of vector
Y	- Vector of state variables
BRR(N)	- Vector of local error estimates for all state variables
ERRMAX	- Maximum local error estimate
TOL	- Integration error tolerance
FDER	- Maximum value of derivative functions at initial time
NTEALL	- Flag showing model has time events only
NUM	- Flag counter
NUMTE	- The number of time events existing in the model
NTIMEV	- Flag showing Time Event taking place
NTIMUP	- Flag showing time update took place

Figure 5.8 List of variables used in the Discontinuity Processing Method

```

Discontinuity Processing Algorithm
Compute initial step size : HINIT
HINIT = min(HBOUND, ((abs(0.5*TOL/FDER)) ** 0.5)/4)
Set H = HINIT
Set NTIMEV = 0
Compute communication time TCOM:
TCOM = T + COMINT

While (T < TFIN)
    Determine next time horizon THOR
    If ((NUM <= NUMTE) AND (NTIMUP = 1))
        Then
            If (TE(NUM) < TCOM)
                Then
                    THOR = TE(NUM)
                    NTIMUP = 0
                Else
                    THOR = TCOM
                    NTIMUP = 0
                End If
            End If
        End If
    If ((NUM > NUMTE) AND (NTIMUP = 1))
        Then
            If (TFIN > TCOM)
                Then
                    THOR = TCOM
                    NTIMUP = 0
                Else
                    THOR = TFIN
                    NTIMUP = 0
                End If
            End If
        End If
    While ((T + H) < THOR)
        Time horizon reached in next step
        If (TEALL = 1)
            Check if all events are time events
            Then
                Integrate system for time events only
                (See Figure 5.9)
            Else
                Integrate system for state events and/or time
                and state events (See Figure 5.10)
            End If
        End If
    End While
    Modified Runge Kutta Merson
    HDIS = THOR - T
    H = HDIS
    Compute state values at THOR
    Update Time : T = T + H
    Set NTIMEV = 1
    If (THOR = TE(NUM))
        Then
            NTIMEV = 1
        End If
    End If
End While
Call OUTPUT(Y,N,T)
End Discontinuity Processing Algorithm

```

Figure 5.9: Global Structure of Discontinuity Processing Algorithm

Processing of Time Events only		
If (NTIMEV = 1)		Time Event Reached
Then	CALL MODUPD	Update model as specified by time event
End If		
Normal Runge Kutta Merson Method		
Compute state derivatives K1..K5 for each state variable		
Compute local error estimates for each state variable : ERR(I)		
Determine the maximum local error estimate: ERRMAX		
If (ERRMAX <= TOL)		
Then	Update Time : $T = T + H$ Store values of new states	
End If		
Perform step size control (as for Runge Kutta Fehlberg)		
End Time Events only Processing		

Figure 5.10 Processing of Time Events only

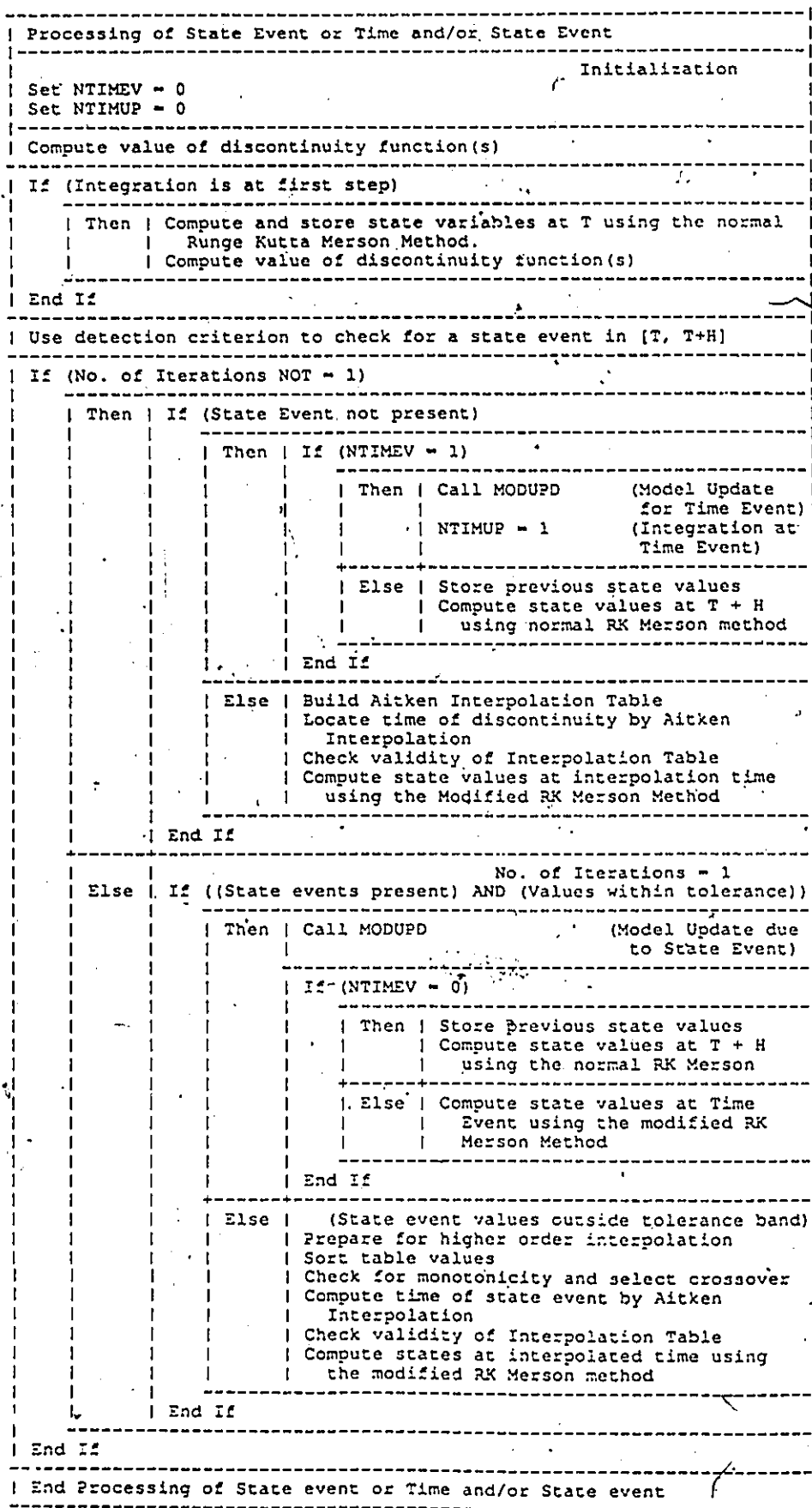


Fig. 5.11: Processing of State events or Time and/or State events

5.3.3 Program Structure

Figure 5.12 shows the pictorial view of a program using the discontinuity processing method to drive the simulation of a model. For systems known to have time event discontinuities only, subroutines DISFUN, AITKEN, SORT, and SELECT are not utilized.

MAIN Program

This is very similar to the main program for the Runge-Kutta Method. However, it makes calls to the subroutine DISCON to carry out the run-time activities for the model.

Subroutine INIT

This subroutine is linked to the MAIN program and utilizes the XMENU software within the IBM environment to allow the user to interactively initialize the appropriate model parameters, initial values, and other experimentation variables.

Subroutine DISCON

This subroutine is linked directly to the MAIN program and contains the body of the discontinuity processing algorithm. It makes calls to other subroutines which are involved in the integration of the model.

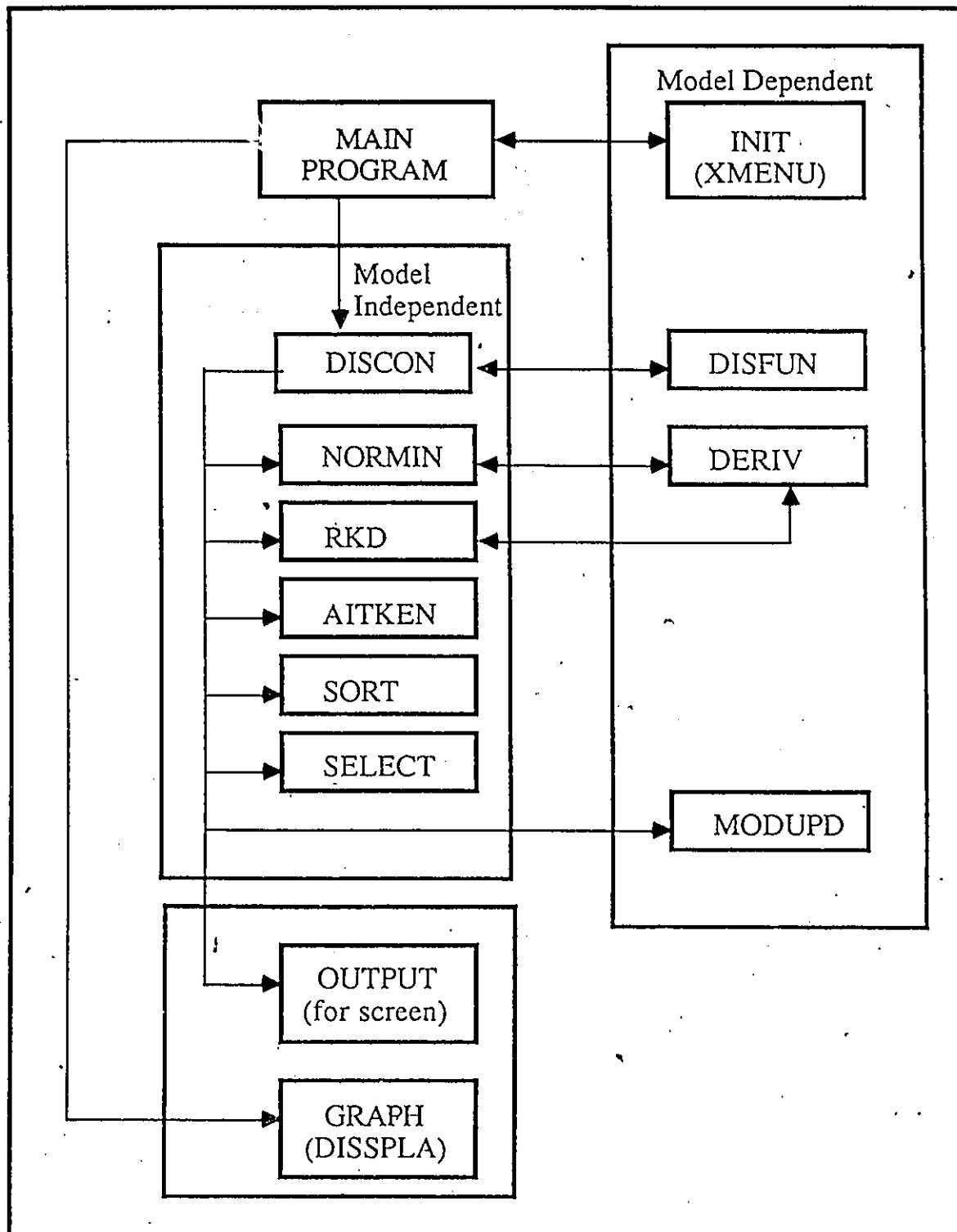


Figure 5.12 Modules of an Interactive Procedural Program using the Discontinuity Processing Algorithm

Subroutine RKD

This subroutine utilizes the variable step RK-Merson method to drive the simulation right up to the discontinuity point which has been detected in the last step. As soon as a discontinuity is detected the normal routine is stopped and the step is repeated with a new step size $H_{DIS} - THOR - T$ computed by the algorithm dealing with the discontinuity. This step size, assuming the estimated error does not go beyond the specified tolerance, allows us to step right up to the discontinuity point computed by the algorithm and pass it. If the error does go beyond the specified tolerance, the integration will be repeated over a multiple of subintervals, using a fraction of the step size, as is necessary, until the last step ends up exactly on the discontinuity point located by the algorithm.

Subroutine NORMIN

This subroutine utilizes the variable step RK-Merson method to drive the simulation at each step where a discontinuity has not been detected. Integration using the normal Runge-Kutta Merson algorithm continues throughout the simulation until an event discontinuity (time or state) occurs or the end of the simulation does, whichever comes first. In the former case, the normal routine is disabled and the modified routine takes over as explained above. As soon as the point of discontinuity is reached and the model updated, control is returned to the normal routine.

7

1

Subroutine MODUPD

This subroutine contains the model update information. This consists of the update of state variables or parameters and the conditions which should trigger them. It is a model independent subroutine.

Subroutine AITKEN

This subroutine is responsible for generating the interpolation table in the quest for determining the time of the state event discontinuity. The validity of the interpolation table generated is also checked and any useless points are discarded and the table generated once more.

Subroutine SORT

This subroutine is model independent. It is responsible for rearranging the interpolation table in ascending order of the discontinuity functions after each iterative interpolation.

Subroutine DISFUN

This subroutine is model dependent and contains the discontinuity functions that exist in the model. The zeros of these functions indicate when a model update should occur as a result of a state event.

Subroutine SELECT

This subroutine selects the useful points which will increase the convergence rate and discards those points which should produce absurd interpolation results . It also performs a monotonic check.

Subroutine OUTPUT

The values of the outputs at each communication time are stored and an interactive tabular display is shown to the user during the simulation run. This subroutine is called from the subroutine DISCON.

Subroutine GRAPH

This subroutine linked to the MAIN program utilizes the Disspla software within the IBM environment to provide post-run hard copy graphic displays of the desired model outputs with time.

CHAPTER 6

GEST RUN-TIME LIBRARY - SECTION 3

6.1 QUALITY ASSURANCE IN MODELLING AND SIMULATION IN
THE ARTIFICIAL INTELLIGENCE ERA

6.1.1 Introduction

The validation of models and verification of simulation programs are extremely important factors especially in large scale simulation studies. Additionally, the topic requires attention in light of the fact that huge amounts of money are being spent annually in developing, using and maintaining computer models worldwide. It is widely accepted that modelling and simulation may add other sources of error to the large number of errors that may exist in basic computerization. As a result, quality assurance along with reliability of models used and associated software is of primordial importance. As defined by Ören (1986c): "Quality Assurance of an element of a simulation study is an assessment of its characteristics to certify its acceptability or to recommend ways and means for its improvement or to recommend its rejection".

Quality assurance for traditional modelling and simulation has been well elaborated in the literature over the years and is only briefly discussed here. Ören (1987a) gives a global taxonomy of studies and references that deal with the topic. The main focus, however, in this section is to discuss the currently advanced quality assurance

concepts.

The main problems that are investigated to ensure the quality assurance in traditional modelling and simulation include :

- 1) Applicability of validity and verification of experimental conditions.
- 2) Computational validity
- 3) Experiment and Model Compatibility
- 4) Formal checks for model integrity, consistency, completeness and comprehensibility
- 5) Software quality assurance of the Run Time Library

In addition, due to the increasing applications of simulation studies, the development of an assessment methodology is essential. The quality assessment studies fall under two main categories (Ören 1984a). They are : 1) Descriptive assessment which consists of syntactic assessment, morphological assessment, and semantic assessment. 2) Normative assessment consisting of pragmatic assessment and ethical assessment.

6.1.2 ADVANCED QUALITY ASSURANCE CONCEPTS IN MODELLING AND SIMULATION

With the advent of advanced knowledge processing paradigms such as knowledge based systems or the like in

complex systems, a new class of quality assurance techniques are required. The need for such techniques are to :

- 1) Avoid additional sources of errors to already complex systems.
- 2) Take advantage of artificial intelligence techniques to eliminate some types of errors.

As a result, three additional areas of advanced quality assurance techniques have been formulated by Ören (1987a):

- 1) Quality assurance in cognizant modelling and simulation
- 2) Cognizant quality assurance in modelling and simulation
- 3) Cognizant quality assurance in cognizant modelling and simulation

Cognizant simulation or artificial intelligence based simulation is the term given to a simulation where the modelling environment and/or simulation system have cognitive abilities. Cognizant simulation systems may allow goal directed modification of a model's structure during a simulation study while cognizant simulation environments can be used to specify models, parameters, etc., as well as to monitor the simulation process. It is clear that such a system requires special needs for quality assurance. Traditional concepts that must be extended to such systems include adequacy, completeness, consistency and integrity of

both static and dynamic knowledge bases which may include model and rule bases which are critical components of current expert and knowledge based systems.

For static knowledge bases, techniques need to be developed and implemented to ensure knowledge base adequacy, completeness and consistency. Dynamic knowledge bases may exist in an advanced simulation environment such as those that need updating as a result of machine learning to provide knowledge rich environments for specifications and executions of simulations. In such a case, one needs to additionally ensure knowledge base integrity. Each time a need for an update occurs, correctness and consistency of the knowledge base needs to be assured via relevant syntactic and semantic checks. This should help to ensure that catastrophes do not occur when knowledge processing takes place. A similar need occurs in rule-based simulation systems. In such systems, the rule base must be carefully monitored since logical programming can quite easily give way to erroneous answers. This can occur as the inference engine can function and generate answers even in the absence of a rule or if another rule is added to the original rule-base. As a result, automated consistency checks of the rule-base are critical after every change of rules.

There are two main ways in which cognizant quality assurance can be utilized in modelling and simulation (Ören 1986c). In the first case, one can use cognizant techniques

such as rule based programming to enhance quality assurance operations by building a rule base for such operations.

Secondly, one can assure quality by using cognizant techniques to guide the user in the specification phase of the simulation in order to eliminate some types of error such as morphological and semantic ones (Ören 1987a). This "on line" approach allows immediate remedial action at each stage, say, of a specification rather than to check the existence of cases which need to be improved as quality assured. This feature is present in Magest (Aytac and Ören 1986) which is an advisory system for simulation modelling that carries out a variety of semantic checks to assure completeness and compatibility of specifications. The system additionally, provides in its advisory mode, user friendly explanation and can also suggest alternatives to correct them.

The third area pertaining to cognizant quality assurance in cognizant modelling and simulation is in its early stages of development. Concepts and techniques need to be generated to deal with this problem. Typical techniques should include the use of a dynamically enhanceable knowledge base containing knowledge or knowledge processing knowledge relevant to quality assurance operations for quality assurance of cognizant simulation or simulative environments (Ören 1987a).

6.2 QUALITY ASSURANCE OF THE RUN TIME LIBRARY IN THE GEST ENVIRONMENT

The quality assurance of the run-time library is an important subset of the quality assurance required in traditional modelling and simulation. This is easily conceivable if one realizes the role of the run-time library in the continuous simulation process. The library is the engine which is responsible for driving the simulation to determine its resulting behaviour. The aim of this section is to highlight the quality assurance considerations present in the run-time library. Also, potential ways in which the Gest environment can be utilized in the future to enhance the quality assurance is discussed in this section and in section 6.3. This can be seen as an important subset of cognizant quality assurance in modelling and simulation.

As discussed in chapter 3, the information about the specific model to be simulated and the conditions under which the results are to be obtained are specified by the user in the Gest language with the aid of the Magest system. After translation of the specification by the Gest translator, the program is executed using the Gest run-time library. The latter is developed with careful consideration for the attribute of 'robustness' as specified by Cellier (1979). In doing so, the user is relieved as much as possible of those aspects that deal with the execution of his model such as the integration step size and other associated parameters. The user is not required to provide

any information he does not have at his disposal but instead is allowed to concentrate on those factors involving the specification of his model in Gest . As a result, in the implementation of the run-time library, the user when specifying a discontinuous model, is given the option of specifying a maximum step size. As mentioned earlier in Chapter 5, this is important in reducing the probability of the detection criterion missing a discontinuity. For the other algorithms in the run-time library, there is no need to specify a maximum step size, HMAX. This would unnecessarily restrict the rate of integration which should be controlled by the tolerance or accuracy of the integration required by the user. However, in each algorithm of the run-time library, the option of specifying a minimum step size is given. This is important so as to prevent the possibility of a run-time error occurring due to overflow exception. This can occur if the algorithms are used in the integration of stiff or oscillating models where the step size control mechanism can force the step size to be reduced to a very small value for the user tolerance specified. On the other hand, the value of HMIN should not be relatively large, since this would cause the integration to be interrupted unnecessarily. Once the values are specified, the Magest system could do appropriate simple checks to determine their acceptability. These checks involve determining whether the given values are valid ones. The accuracy and stability of the methods is dependent on their

values being positive and less than one. Additionally, the value of HMAX for the discontinuity processing algorithm must be greater than the value specified for HMIN. The users are alerted if the specified values are invalid, at which point Magest would suggest an appropriate optimal range and request the user to make the appropriate changes.

If the user does not specify any values then the algorithm automatically assigns the above mentioned values for these variables.

The user is not allowed to specify the initial step size for the integration in all of the algorithms of the run-time library except the Fourth-Order Runge-Kutta method where it is allowed as an option. This feature is a significantly important one which some available codes neglect and the user is requested to guess some initial step size. This is an unsatisfactory procedure to which users should not be subjected. Instead of specifying the step size, the step size controlled integration algorithms require the user to provide a tolerance for the accuracy of the results desired. In all the algorithms in the run-time library, the algorithms are automatically assigned an initial step size based on the formula derived by Shampine and Gordon (1975). It is given by:

$$HINIT = \min(HBOUND, ((\text{abs}(0.5 * \text{TOL}/FDER)) ** 0.5)/4)$$

where

HBOUND is the upper bound on the initial step size

TOL is the user specified tolerance

FDER is the maximum value of the derivative
functions at the initial point

A value for HBOUND should be specified by the user. This value which indicates the general scale of the problem is important so as to prevent any difficulty due to a state derivative being zero in the computation of the initial step size HINIT. As mentioned earlier, some flexibility has been allowed for specifying an initial step size. In some cases, the user may have a good reason for specifying an initial step size for his/her simulation run. In these cases, the user should use the Fourth-Order Runge-Kutta method which has this option available. However, before proceeding with this step size the algorithm checks to see whether the value of HBOUND has been exceeded. If so, the user is warned that this is the case, and is given the option to use the value specified for the initial step size or to use the value of HBOUND.

As mentioned above, the value of TOL is important in controlling the rate or step size of the integration. Magest could also carry out checks on the value of TOL supplied by the user to ensure its validity. It must necessarily be a positive number and should be very small less than one.

The run-time library also has internal mechanisms to control the integration process and also to indicate when

the algorithm is unable to proceed properly. These include:

1) Ensuring that the integration proceeds efficiently. This requires that the integration advance as close to optimal as possible at each step. This is pertinent to all algorithms in the library excluding the Fourth Order Runge-Kutta. In some available codes, this aspect is not considered seriously. The step size update procedure is carried out quite arbitrarily. The following step size control scheme proposed by Birta (1980) ensures an efficient update close to optimality.

$$H = 0.9 * H_{PREV} * ((TOL/E)) ** 1/D$$

Then,

$$H_{NEW} = \begin{cases} H & 1/D < H/H_{PREV} < D \\ H_{PREV}/D & H < H_{PREV} / D \\ D * H_{PREV} & H > D * H_{PREV} \end{cases}$$

E represents $\text{MAX}_j (E_j)$

E_j represents local truncation error estimate

TOL represents the specified user tolerance

D represents the order of the method

2) In the discontinuity processing algorithm, at the end of each integration step size, a check is made to ascertain whether the new step size produced by the algorithm is

larger than the value of HMAX. If it is, the value of the new step size is replaced by the value of HMAX, thus ensuring that the algorithm does not ever proceed with a step size greater than HMAX as desired.

3) For all the algorithms in the run-time library, the user is alerted and the integration suspended if the new step size produced by the algorithm is smaller than HMIN. The system has dialogue with the user to try to rectify the situation by requesting the user to either specify a smaller HMIN or a less stringent TOL if practically feasible so that the integration step may proceed past this point. If it is not practically feasible, then the simulation is aborted and the user requested to investigate the model closely.

4) A check is done to ensure that an output point is not required at a step size less than or equal to HMIN after the next integration step is taken. If such a case exists, the new step size is replaced by the value $(TCOM - T)/2$ where TCOM is the communication time where output is required, and T is the present computational time. This will avoid unnecessary suspension of the integration and possible abortion since the step size H would be less than or equal to HMIN. The integration is repeated with this step size until TCOM is reached. Once the output point is reached, the step size update is carried out according to the step size control scheme described above in all algorithms except the Fixed Step Runge-Kutta method where the initial step size is

again employed. The above features present in the run-time library are responsible for ensuring its 'robustness'.

6.3 FUTURE POSSIBILITIES FOR INTEGRATION ALGORITHM SELECTION WITHIN THE GEST ENVIRONMENT

In the run-time library, a range of integration algorithms are offered for the user to choose from in carrying out the simulation of his continuous model. Unfortunately, even in recently developed languages the user is not aided in determining the optimal choice of algorithm from amongst those available in the run-time library for simulating his specific model. This non-trivial problem is further complicated by the fact that in the majority of cases, the users though knowledgeable about the problem domain area may not be in a position to make such a decision. The end result of such a situation is usually a poor choice, the user specifying some algorithm he may be familiar with or merely using the default option that may be available in the run-time library.

For the Gest environment, this limitation can be somewhat overcome. It is proposed that Magest perform checks on the model provided by the user to determine whether his specified algorithm is indeed a suitable and optimal choice. If Magest is not in agreement, it advises the user as to which algorithm, is the most appropriate one to be chosen from the Gest run-time library and the reasons for its

conclusions. This task requires considerable research and experimentation to develop and validate appropriate rules for giving advice on the choice of a particular integration algorithm for a specific model. The aim of this section is to provide insight and information as to what factors should be considered and utilized in the formulation of such rules. A well developed set of rules would be a valuable asset of such an environment and would further enhance its abilities as a computer aided modelling tool.

In the current run-time library, the user is able to choose from five integration algorithms. These consist of :

- 1) Fixed Step Runge-Kutta
- 2) Variable Step Runge-Kutta
- Fehlberg
- 3) Adams Predictor Corrector Method
- 4) Discontinuity Processing Algorithm
- and 5) Multi-Rate Integration Algorithm.

The first three algorithms are termed general purpose algorithms, while the discontinuity processing algorithm and Multi-Rate algorithm are specialized algorithms.

The rules that could be utilized by Magest in advising that the discontinuity algorithm be selected in the simulation of a particular system is quite straightforward.

1)

IF the model has a 'model update' section

THEN the discontinuity processing algorithm
should be used.

2)

IF there is an "if then else" structure in
the derivative section

THEN the discontinuity processing algorithm
should be used.

The rules that could be used by Magest in advising the multi-rate integration algorithm be selected is not as straightforward. Firstly, it must be determined under which conditions the algorithm can be advantageously utilized. For coupled models with several component models the advantage of using the algorithm should be dependent on the number of interconnections that exist in the internal coupling section of the specification. Although, Palusinski (1985) does not make direct reference to it for his algorithm, the results of his experiments indicate as would be expected that the CPU time savings decreases with the number of interconnection variables. This is understandable in light of the fact that although considerable CPU time is achieved by partitioning the original system into two component systems with similar characteristics, the amount of interpolation required in integrating the resulting structure increases with the number of interconnection variables. It is clear that at some number of interconnection variables, the amount of interpolation

required does not warrant the use of the multi-rate method. As explained previously, Birta (1980) conducted numerical experiments to investigate this problem for his algorithm and concluded that a maximum of three interconnection variables should be allowed for his method to be feasible. From the numerical experiments given by Palusinski (1985) this number seems like a suitable rough benchmark for his algorithm. Needless to say, as mentioned earlier, detailed experimentation should be carried out to provide a much more accurate benchmark. It has previously been cited that the method is usually advantageous for large dynamic systems. Another question arises as to how one defines large. Additionally, the algorithm is particularly favorable when the dimension of the slow system is significantly greater than the fast system. Experimentation is required to develop rules based on the above information which Magest can then use in providing the user with advice on the applicability of the Multi-Rate integration algorithm.

In general, two situations may occur. Firstly, the user has been able to partition the system beforehand and has used the Gest definition for a system employing the use of multi-rate integration, that is, slow and fast component models have been specified etc. In this case, Magest would carry out the appropriate checks based on the rules developed. If the conditions of the checks do hold then Magest ensures that the multi-rate integration algorithm is used. If one or more of the conditions is violated, then

Magest advises the user that the multi-rate algorithm must be used because of the structure of the model specification, but that no advantage in terms of CPU savings may be achieved by using the algorithm. At this point, the user may use the algorithm and run the simulation or respecify the simulation and use an appropriate general purpose algorithm with aid from Magest once more.

The other possibility involves a system being specified with as a coupled model as opposed to a multi-rate model which satisfies the conditions of the checks made by Magest for the applicability of multi-rate integration. For such a system, Magest indicates that the multi-rate integration algorithm could be potentially advantageous if a suitable partition for establishing a slow and fast system could be determined by the user. Magest does not allow the multi-rate algorithm to be used until the system has been properly partitioned and respecified for use by the multi-rate integration. At this point, the user has the option of merely using a general purpose algorithm with the aid of Magest, or determining a suitable partitioning and then respecifying his model so that the multi-rate integration can be used. The partitioning problem up till now has been left entirely up to the responsibility of the user. The user must examine the qualitative features of the process in order to determine a suitable partition (Palusinski 1985). In chapter 7, an expert monitor is proposed to aid the user in the partitioning problem.

Once an appropriate partitioning is found (if possible), then the user re-specifies the model in the appropriate form including a fast and slow system etc. Magest then ensures multi-rate integration is used for the simulation. This procedure is hardly worthwhile for a simulation that is to be carried out only once. However, in practice this is usually not the case. Large dynamic processes require frequent experimentation with the initial value problem that describes the process, and from this point of view the procedure could very well prove effective.

The choice of a particular general purpose algorithm involves consideration of a few factors while examining the system. It is clear from previous discussions, the conditions under which one of the general purpose algorithms is considered for selection. 1) An update section is not present in the dynamic structure of the specification nor does an 'if then else' structure occur in the derivative section. 2) The model specified as a multi-rate model satisfies the conditions under which the multi-rate integration algorithm is potentially advantageous. 3) The system is specified as a coupled model even though the use of the multi-rate algorithm could have potential advantages. However, for some reason, such as a suitable partition not able to be defined, the user desires not to use the multi-rate integration and Magest allows the flexibility of using a general purpose algorithm which it gives advice on.

Once it has been ascertained by Magest that a general purpose algorithm is to be used in the integration, three main factors should be considered and investigated to develop appropriate rules to be used by Magest in advising on the best choice of general purpose algorithm to be employed. These consist of : 1) the accuracy requirements of the model 2) the frequency of output required by the model and 3) the expense of the function evaluations in the model.

As Cellier (1979) points out, the CPU cost to execute a specific model can be graphed versus the required relative accuracy as shown in Figure 6.1. The rules for accuracy could be based on the rule of thumb cited by Cellier and may have the form

IF the tolerance specified by the user

$\geq 10^{(-4)}$

THEN the Fixed Step Runge Kutta

algorithm is favoured

IF the tolerance specified by the user

$< 10^{(-4)}$

THEN the Adams method or the Runge Kutta

Fehlberg algorithm is favoured.

For the frequency of output criteria, Cellier (1979)

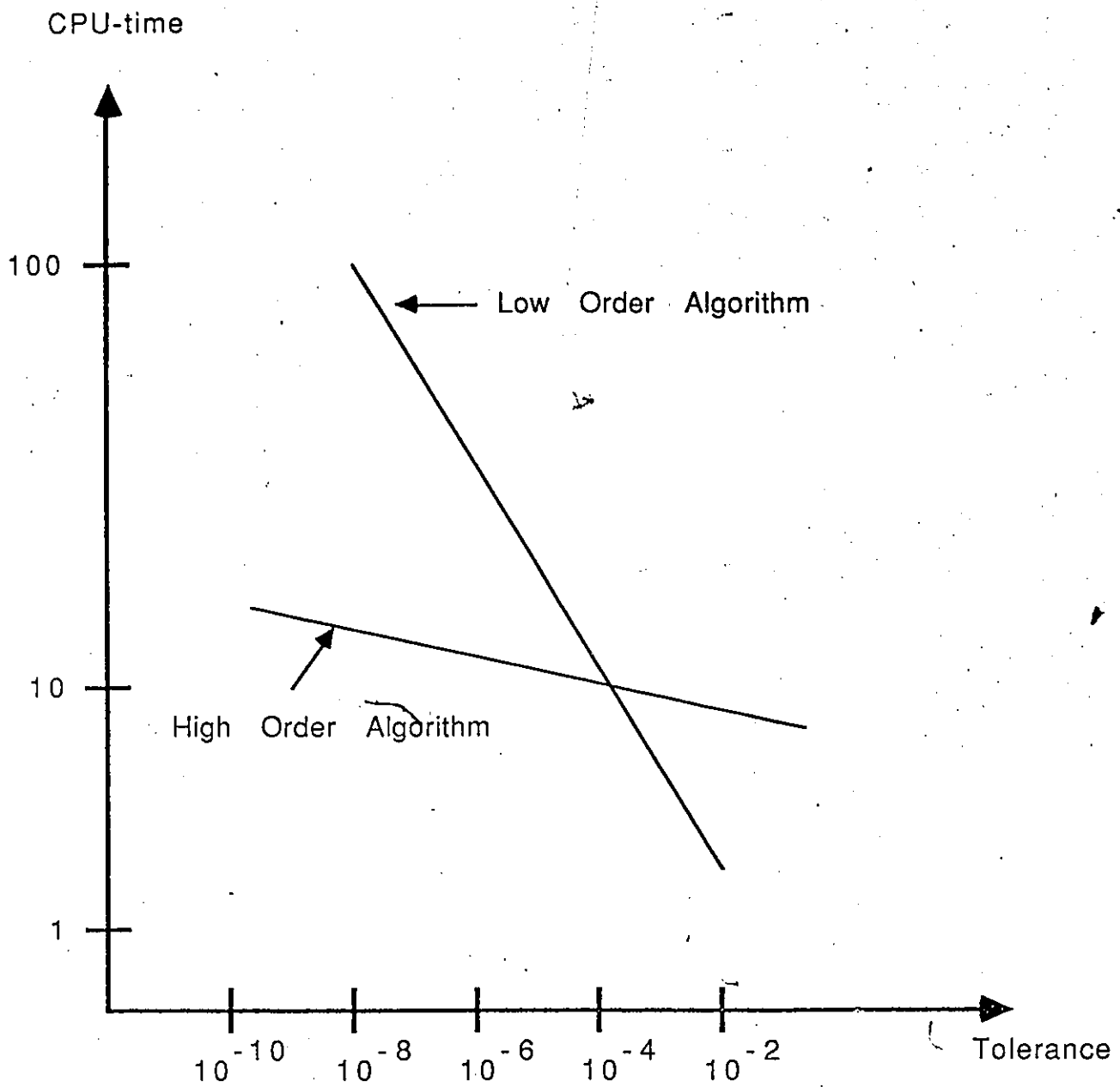


Figure 6.1 CPU-time versus Tolerance Requirements for Low and High Order Algorithms

shows the accumulated CPU-cost graphed versus the simulation clock for one step and multi-step integration as shown in Figure 6.2. The graph illustrates the fact that one step methods are more economic initially because of their self starting mechanism. However, the multi-step algorithm becomes more economic over a longer period of time provided the problem is a purely continuous one. Finally, the low order single step algorithm favours continuous problems where frequent output is required as opposed to their higher order equivalents. Frequency of output could be easily determined by Magest, from the communication interval specified and the values for the start and end times of the simulation as specified by the user. The number of output points is given simply by $(TFIN - TINIT)/COMINT$. In summarizing, factors should be considered in developing rules for this criteria would be :

IF a high frequency of output is computed from the
appropriate information in the specification

THEN the Fixed step Runge Kutta algorithm
is favoured.

IF a low frequency of output is computed from the
appropriate information in the specification

THEN the Runge Kutta Fehlberg or the Adams Predictor
algorithm is favoured.

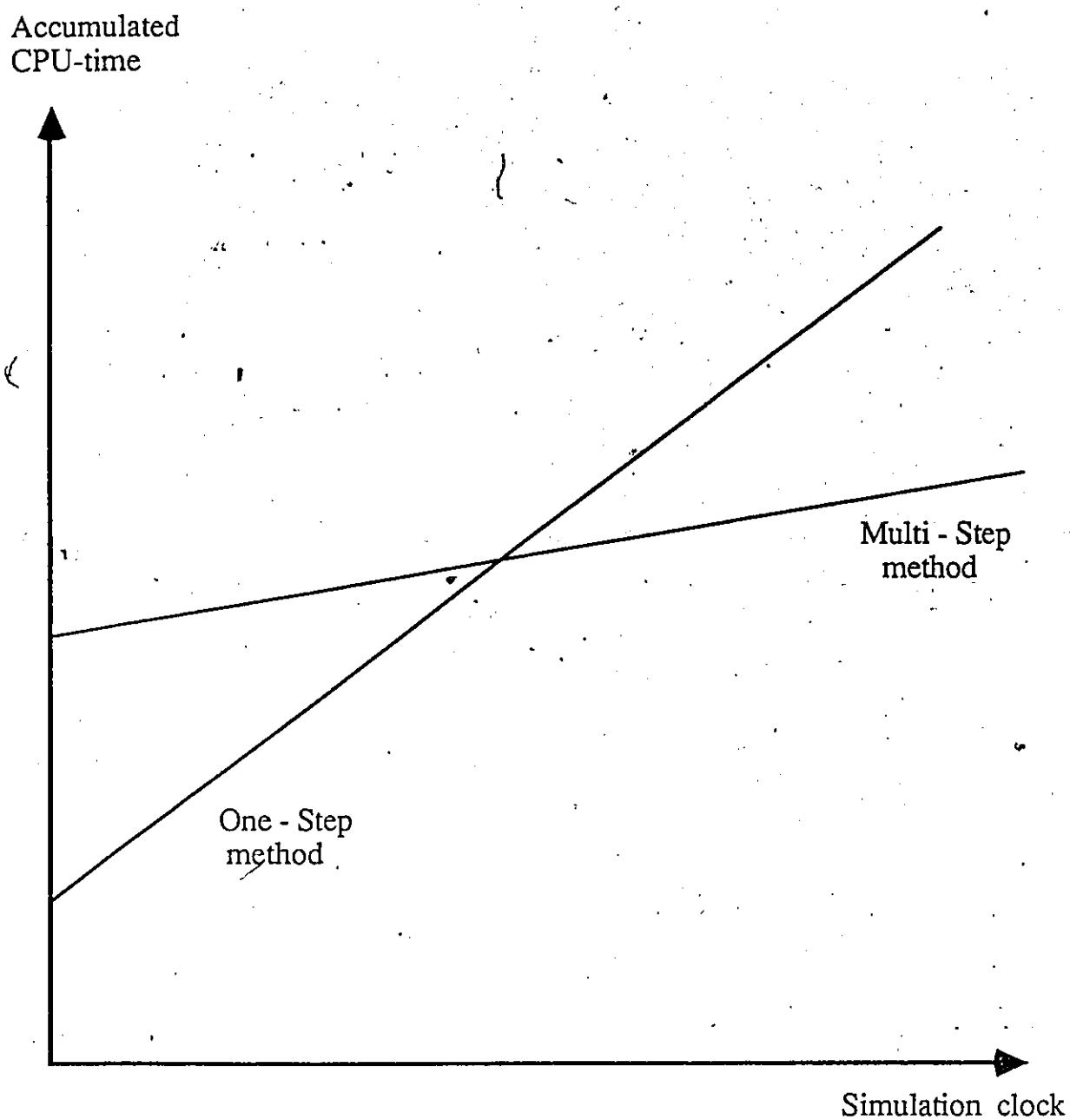


Figure 6.2 Accumulated CPU-time Versus Simulation Clock for One-Step and Multi-Step Integration

The final criteria concerning the expense of function evaluations is investigated by Magest determining a relative complexity factor from the equations describing the model. A suitable benchmark is required for this non-trivial problem to distinguish a high complexity model from a low complexity one. A high complexity model favours the use of the Adams predictor corrector algorithm while a low complexity model favours one of the one step Runge Kutta methods. The following factors should be used in developing rules for this criteria to be used by Magest in recommending a general purpose algorithm for a particular model.

IF the model has been ascertained to have a high complexity factor

THEN the Adams Predictor Corrector Method is favoured.

IF the model has been ascertained to have a low complexity factor

THEN either the Fixed Step Runge Kutta or the Runge Kutta Fehlberg algorithm is favoured.

Figure 6.3 summarizes the conditions under which each of the general purpose algorithms is favoured based on the factors described above. As should be evident, a number of possible combinations of factors may exist for a particular model. However, the number of rules could be significantly

	Accuracy		Model Complexity		Output Frequency	
	Low $<10^{-4}$	High $\geq 10^{-4}$	Low	High	Low /	High
Fixed Step Size Runge-Kutta Method	✓		✓			✓
Variable Step Size Runge-Kutta Fehlberg Method		✓	✓		✓	
Adams Predictor Corrector Method		✓		✓	✓	

Figure 6.3 Factors Affecting Selection of General Purpose Algorithms

reduced as follows. Firstly, because of the problems associated with restarting the Adams method, Magest should only consider this algorithm when the user specifies a long communication interval. Secondly, the accuracy requested by the user via the specified value for TOL should be deemed the most important criteria. This is a viable assumption in light of the fact that, with the increasing power of computers, the other factors are becoming less and less important.

These considerations not only drastically reduce the number of rules needed but improves the ability of Magest to select the appropriate general purpose algorithm despite the combinations of factors that may have to be considered for any particular model.

As a result, the following factors can be summarized which could be used in the development of rules for Magest in selecting an appropriate general purpose algorithm for a particular model.

- 1) The Adams Predictor Corrector Method would be advantageous in all cases where the model has a high complexity factor and a high tolerance is specified by the user.

- 2) The Runge-Kutta Fehlberg Method would be advantageous in all cases where the model has a low complexity factor and a high tolerance is specified by the user.

In all other cases, the Fourth Order Runge-Kutta Method would be recommended for use.

In a nutshell, each of the algorithms in the run-time library may be advantageous for a particular model. The Magest system should be able to provide advice concerning the selection of the integration algorithm for a model. Further research and detailed experimentation utilizing the knowledge above should result in the development of a set of rules that Magest can use to this end.

CHAPTER 7

CONCLUSIONS AND FURTHER STUDY

In this thesis, several issues concerning the applications of Artificial Intelligence in Simulation are discussed. The main theme, however, deals with advanced simulation environments, in particular the one based on 'Gest' as discussed in Chapter Three. The correspondence shown between the structures of the Gest specification programs and their equivalent procedural programs along with the test examples demonstrate how the translator for the Gest environment is to function thus providing aid in its construction. The run-time library for the Gest environment has been developed to handle non-stiff initial value problems and the algorithms are used to drive the test examples in the thesis.

A number of areas for further study are possible apart from those mentioned as future directions for artificial intelligence applications in simulation environments in section four of Chapter two. As indicated previously in the thesis, one should use the algorithm that is most advantageous for a certain class of problems. As a result, it is highly recommended that the run time library be expanded to include other algorithms for handling the different problem areas in continuous simulation as outlined by Gear (1981). In particular, an algorithm for handling stiff systems, preferably Gear's algorithm (Gear 1971)

should be included.

It is recommended that a set of rules to be used by Magest in advising the user as to the integration algorithm to be selected from the run-time library for a particular model be well developed using section 6.2 of chapter 6 as a base and then implemented. As stressed in section 6.2, this will require further research and a series of experimentations to determine the relative importance of these suggestions. The successful implementation of this set of rules would further enhance the computer aided modelling abilities of the Gest environment.

As mentioned in Chapter 6, the development and implementation of the intelligent monitor during simulation run time could be a useful aid to the user in dealing with the partitioning problem for use of multi-rate integration. The user would first shorten the length of the simulation time so that the simulation is run for a sufficient period of time that the model is behaving in 'steady state'. This usually occurs a fair length of time after the initial transient time has elapsed and is estimated from the dynamics of the process. Additionally, a variable step method is chosen to drive the simulation. During the simulation, the monitor would collect statistics giving the weight each state had in controlling the step size. This, it would determine by studying the local error estimates of the state variables at each step. The use of the monitor in this

way could aid in the partitioning process. If certain state variables have large error estimates responsible for slowing the rate at which the system integration proceeds, then these can be identified as being potential fast system variables. It is necessary to incorporate into the final decision of the partitioning any a priori knowledge of the qualitative features of the system. Preliminary studies done using the electronic oscillator model confirmed the usefulness of the monitor in aiding the user to determine an appropriate partitioning. Additionally, assuming the run-time library has been expanded as outlined above, this 'intelligent' monitor could be further enhanced by incorporating into the system functions of stiffness detection, order selection and abnormal phenomena processing as discussed by Xiong and Song (1986). Appropriate rules for these situations would be collected and put into a knowledge base. The knowledge base would have a learning mode as discussed by Xiong and Song and the inference strategy would be a sequential one.

The present post-run graphics ability of the run-time library could be improved to include interactive abilities so that the trajectory of the simulation can be monitored during each stage of the simulation.

Further studies into the choice of interpolation algorithm for subsystem interfacing could be extremely useful. Palusinski (1985) mentions this as being very

important in the design of a multi-rate integration algorithm for partitioned system simulation. This is also a major consideration and handicap in the use of the quasi-parallel method proposed by Birta as discussed in Chapter four. If this handicap could be overcome, the proposed algorithm by Birta (1980) could be most advantageous if the large dynamic system consisted of component systems with known general characteristics such as discontinuous and stiff component systems for example. With the expanded version of the run-time library, the use of the best integration algorithms for each component system can be employed so that each component system moves forward in time independently. In this case, then, it is clear that such a method would have distinct advantages over the traditional method of dealing with a system having several component systems with known general characteristics. Gear's algorithm (Gear 1971) would be utilized in the integration of the stiff component system while the discontinuity algorithm would be utilized for the discontinuous component system.

Alternatively, the implementation of the algorithm proposed by Brosilow (1985) would be most advantageous for a system having component systems with known general characteristics since it would allow the parallel processing of the individual component systems using the best integration algorithms for each component system. However, this method would require software that runs on parallel processors.

APPENDICES. EXAMPLES FOR GEST TRANSLATOR

Appendix A. THE DIABETES MELLITUS MODEL: NORMAL PERSON

A.1 Problem Definition

This example utilizes the Differential Model of Diabetes Mellitus (Davies 1976) to simulate the blood sugar and insulin levels of a normal person over a typical day. The model for the normal person consists of two differential equations describing the state derivatives of the model, the food source input, and the associated parameter set. The state variables consist of the sugar level and insulin level in the blood. The Fourth Order Runge-Kutta method is used as the method of integration. Figure A.1 shows the pictorial representation of this component model. The results are identical to those given in the article by Davies.

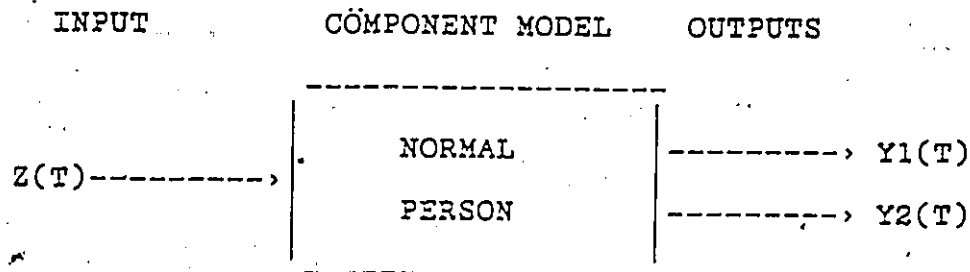


Figure A.1 System Representation For Normal Person

A.2 Gest Specification of The Diabetes Mellitus Model: Normal Person

Program StudyOfNormalPerson

ContinuousModel NormalPerson

StaticStructure

Inputs

Z	(* Food Input	*)
---	---------------	----

States

Y1,	(* Blood Sugar Level	*)
-----	----------------------	----

Y2	(* Blood Insulin Level	*)
----	------------------------	----

Outputs

Y1,	(* Blood Sugar Level	*)
-----	----------------------	----

Y2	(* Blood Insulin Level	*)
----	------------------------	----

AuxiliaryVariables

H	(* Step Function	*)
---	------------------	----

Constants YI1, YI2

YI1 = 100	(* Initial Sugar Level	*)
-----------	------------------------	----

YI2 = 0	(* Initial Insulin Level	*)
---------	--------------------------	----

EndConstants

Parameters

A1,	(* Sensitivity of sugar level gradient to insulin	*)
-----	--	----

A2,	(* Sensitivity of sugar level gradient to low blood sugar levels	*)
-----	--	----

A3,	(* Sensitivity of sugar level gradient to the input	*)
-----	--	----

B1,	(* Sensitivity of insulin level gradient to high blood sugar levels	*)
-----	---	----

B2,	(* Sensitivity of insulin level gradient to insulin levels	*)
-----	---	----

QFOOD[3],	(* Quantity of food at three meal times	*)
-----------	--	----

TFOOD[3],	(* Meal times	*)
-----------	---------------	----

KFOOD[3]	(* Delay parameter	*)
----------	--------------------	----

EndStaticStructure

DynamicStructure

Derivatives

If ((Y1 - YI1) < 0.0)

Then H = 0

Else H = 1

EndIf

Y1' = -A1*Y1*Y2 + A2*(YI1-Y1)*(1-H) + A3*Z

Y2' = B1*(Y1-YI1)*H - B2*Y2

EndDerivatives

EndDynamicStructure

EndModel NormalPerson

Parameter Set 1

Parameters

A1 = 0.05

A2 = 1.0

A3 = 4.0

B1 = 0.5

B2 = 2.0

QFOOD[1] = 50

QFOOD[2] = 100

QFOOD[3] = 100

```

KFOOD[1] = 4.0
KFOOD[2] = 4.0
KFOOD[3] = 4.0
TFOOD[1] = 8
TFOOD[2] = 13
TFOOD[3] = 20

```

```

EndParameters
EndParameter Set 1

```

Parameter Set 2

Parameters

```

A1      = 0.05
A2      = 1.0
A3      = 4.0
B1      = 0.5
B2      = 2.0
QFOOD[1] = 50
QFOOD[2] = 100
QFOOD[3] = 100
KFOOD[1] = 6.0
KFOOD[2] = 6.0
KFOOD[3] = 6.0
TFOOD[1] = 8
TFOOD[2] = 13
TFOOD[3] = 20

```

```

EndParameters
EndParameterSet 2

```

Experiment 1

```
TimeUnitIs Hour
```

```
StartTime = 0
```

```
IntegrateBy Fourth-Order Runge Kutta.
```

```
RelError = 0.001
```

```
Communicate at every 0.5 Hour
```

```
SimulateUntil Time = 24
```

```
InitialStates
```

```
YI1 = 100.0
```

```
YI2 = 0.0
```

```
EndInitialStates
```

```
SaveOutputs Y1,Y2
```

```
Input Function Z
```

```
At Times TFOOD(I)
```

```
IF (T.GE.TFOOD(I))
```

```
THEN Z = QFOOD(I)*EXP(-KFOOD(I)*(T-TFOOD(I)))
```

```
ELSE Z = 0
```

```
ENDIF
```

```
EndInput Function Z
```

```
EndExperiment 1
```

Run 1

```
ToObserve NormalPerson
```

```
WithParameterSet 1
```

```
InExperiment 1
```

```
WithPostRun
```

```
OutputModule 1 On Printer
```

```
EndPostRun
```

```
EndRun 1
```

Run 2

```
ToObserve NormalPerson
```

```
WithParameterSet 2
```

```
InExperiment 1
```

```
WithPostRun
```

OutputModule 1 On Printer
EndPostRun
EndRun 2

OutputModule 1
New Page
Heading ForFirstPage 1 Line
'Study of NormalPerson'
List Parameters And InitialConditons
PlotandList Y1,Y2
EndOutputModule 1

EndProgram StudyOfNormalPerson

C A.3 Equivalent Fortran Program With Results For
C Diabetes Mellitus Model: Normal Person

DIA00020
DIA00030
DIA00040
DIA00050
DIA00060
DIA00070
DIA00080
DIA00090
DIA00100
DIA00110
DIA00120
DIA00130
DIA00140
DIA00150
DIA00160
DIA00170
DIA00180
DIA00190
DIA00200
DIA00210
DIA00220
DIA00230
DIA00240
DIA00250
DIA00260
DIA00270
DIA00280
DIA00290
DIA00300
DIA00310
DIA00320
DIA00330
DIA00340
DIA00350
DIA00360
DIA00370
DIA00380
DIA00390
DIA00400
DIA00410
DIA00420
DIA00430
DIA00440
DIA00450
DIA00460
DIA00470
DIA00480
DIA00490
DIA00500
DIA00510
DIA00520
DIA00530
DIA00540
DIA00550
DIA00560
DIA00570
DIA00580
DIA00590
DIA00600
DIA00610
DIA00620
DIA00630
DIA00640

Variable List

C
C
C Input : N --Dimension of the Vector of State Variables
C
C Y(1)-Y(N) --Initial Values of State Variables
C
C TINIT --Initial Time of Simulation
C
C TCOM --Communication Time
C
C T --Computational Time
C
C TFIN --End Time of Simulation
C
C COMINT --Communication Interval
C
C HBOUND --Upper Bound on Initial Step Size
C
C HMIN --Minimum step size integration is
C allowed to proceed at
C
C HINIT --Starting Integration Step Size
C
C H --Current Integration Step Size
C
C TOL --Tolerance or Accuracy specified by user
C
C Output : TIME --Vector of times of Output Values
C
C YVAL --Vector of Values of Y1 at Output Points
C
C YVAL3 --Vector of Values of Y2 at Output Points
C Program Variables :
C Y(N) --State Variables Vector
C
C DY(N) --Derivative Vector of State Variables
C
C DY1(15)-DY4(15) --Working Vectors in Integration Routine
C capable of integrating systems with up
C to 15 state variables.
C
C F1(15)-F3(15) --Working Vectors in Integration Routine
C capable of integrating systems with up
C to 15 state variables.
C
C NFLAG --Flag Which Signals Collection of Output
C Variables.
C
C HPOS --Intermediate variable used in computing HINIT
C
C NPL --Counter used for Graphics Routine.
C
C FDER --Maximum value of derivative functions at
C initial time
C

PROGRAM MAIN

C This is a test program utilizing the Fourth Order
 C Runge-Kutta Integration Algorithm to drive the
 C Simulation of A Component Model DiabetesMellitus.

IMPLICIT REAL (A-H,O-Z)
 DIMENSION Y(5)
 REAL*4 YVAL1(300),YVAL2(300),TIME1(300)
 EXTERNAL DERIV
 COMMON/DIFF/YVAL(342),YVAL3(342),TIME(342),NPL
 COMMON/PAR/YI(2),TFOOD(3),KFOOD(3),QFOOD(3),A1,A2,A3,B1,B2,Z
 COMMON/SAME/PU(24)
 CHARACTER*1 CHOICE

PRINT*,'Welcome To The Diabetes Mellitus Simulator'
 PRINT*,'
 PRINT*,'Would You Like To Perform a Simulation ? (Y/N) '
 READ*, CHOICE
 IF (CHOICE .EQ. 'Y') THEN
 200 CALL INIT

Initialization from Menu

Initialize Parameters

199 A1 = PU(1)
 A2 = PU(2)
 A3 = PU(3)
 B1 = PU(4)
 B2 = PU(5)
 QFOOD(1) = PU(6)
 QFOOD(2) = PU(7)
 QFOOD(3) = PU(8)
 TFOOD(1) = PU(9)
 TFOOD(2) = PU(10)
 TFOOD(3) = PU(11)
 KFOOD(1) = PU(12)
 KFOOD(2) = PU(13)
 KFOOD(3) = PU(14)

Initialize State Variables

N = .2
 Y(1) = PU(16)
 Y(2) = PU(17)
 YI(1) = Y(1)
 YI(2) = Y(2)

Initialize External Input
 Variable

Z = PU(15)

Initialize Run Control Variables

TINIT = PU(18)
 TFIN = PU(19)
 COMINT = PU(20)
 HMIN = PU(21)

DIA00650
 DIA00660
 DIA00670
 DIA00680
 DIA00690
 DIA00700
 DIA00710
 DIA00720
 DIA00730
 DIA00740
 DIA00750
 DIA00760
 DIA00770
 DIA00780
 DIA00790
 DIA00800
 DIA00810
 DIA00820
 DIA00830
 DIA00840
 DIA00850
 DIA00860
 DIA00870
 DIA00880
 DIA00890
 DIA00900
 DIA00910
 DIA00920
 DIA00930
 DIA00940
 DIA00950
 DIA00960
 DIA00970
 DIA00980
 DIA00990
 DIA01000
 DIA01010
 DIA01020
 DIA01030
 DIA01040
 DIA01050
 DIA01060
 DIA01070
 DIA01080
 DIA01090
 DIA01100
 DIA01110
 DIA01120
 DIA01130
 DIA01140
 DIA01150
 DIA01160
 DIA01170
 DIA01180
 DIA01190
 DIA01200
 DIA01210
 DIA01220

C	HBOUND	= PU(22)		DIA01230
C			Tolerance Specified by user for	DIA01240
C			computation of initial step size	DIA01250
	TOL	= PU(23)		DIA01260
	HINIT	= PU(24)		DIA01270
				DIA01280
	T	= TINIT		DIA01290
				DIA01300
				DIA01310
				DIA01320
				DIA01330
	NPL	= 1		DIA01340
C			Pre-Run Output :	DIA01350
C			Set Up Output Format and	DIA01360
C			Output Initial Values.	DIA01370
C				DIA01380
	WRITE(8,17)			DIA01390
	17 FORMAT(1X,'Method:',1X,'Fixed Step Fourth-Order Runge-Kutta'/19X/			DIA01400
	+5X,'Study Of Normal Person'/19X/			DIA01410
	+1X,'Problem: Component Model DiabetesMellitus'/19X/4X,'Time',7X,			DIA01420
	+ 'Value of Blood Sugar',4X,'Value of Blood Insulin')			DIA01430
	PRINT*,			DIA01440
	WRITE(8,21) T,Y(1),Y(2)			DIA01450
	21 FORMAT(1X,F8.3,5X,F8.3,5X,F8.3)			DIA01460
	PRINT*,			DIA01470
	TIME(NPL) = T			DIA01480
	YVAL(NPL) = Y(1)			DIA01490
	YVAL3(NPL) = Y(2)			DIA01500
C			Run-Time Activities :	DIA01510
C			Integrate by Fourth-Order	DIA01520
C			Runge-Kutta Method.	DIA01530
C				DIA01540
	CALL RK4(T,Y,N,TFIN,H,HINIT,HBOUND,HMIN,TOL,COMINT,DERIV)			DIA01550
C			Post-Run Output:	DIA01560
C			Tabulate Values of State	DIA01570
C			Variables and Time at	DIA01580
C			Output Points.	DIA01590
C				DIA01600
	DO 99 I = 2,NPL			DIA01610
	WRITE(8,87)TIME(I),YVAL(I),YVAL3(I)			DIA01620
	87 FORMAT(1X,F8.3,5X,F8.3,5X,F8.3)			DIA01630
	PRINT*,			DIA01640
	99 CONTINUE			DIA01650
C			Plot Values of State	DIA01660
C			Variables with Time	DIA01670
	CALL ANYDEV			DIA01680
	CALL GRAPH(YVAL,TIME,NPL)			DIA01690
	CALL GRAPH1(YVAL3,TIME,NPL)			DIA01700
	PRINT*, 'Do you wish to carry out another simulation (Y/N) ?'			DIA01710
	READ*,CHOICE			DIA01720
	IF (CHOICE.EQ.'Y') THEN			DIA01730
	CALL INIT			DIA01740
	GOTO 199			DIA01750
	ENDIF			DIA01760
	ENDIF			DIA01770
	STOP			DIA01780
	END			DIA01790
				DIA01800
				DIA01810

```

SUBROUTINE DERIV(T,Y,DY,N)
IMPLICIT REAL(A-H,O-Z)
DIMENSION Y(N),DY(N)
COMMON/PAR/YI(2),TFOOD(3),KFOOD(3),QFOOD(3),A1,A2,A3,B1,B2,Z

```

```

C      This is the derivative evaluation
C      subroutine where the user specifies
C      the system derivatives that describe
C      his model. As an example, the model
C      Diabetes Mellitus is used.

```

```

IF ( (Y(1) - YI(1) .LT. 0.0) ) THEN
  H = 0.0
ELSE
  H = 1.0
ENDIF
IF ( T.LT.TFOOD(1) ) THEN
  Z = 0.0
ELSE IF ( (T.GE.TFOOD(1)) .AND. (T.LE.TFOOD(2)) ) THEN
  Z = QFOOD(1) * EXP((-KFOOD(1)) * (T - TFOOD(1)))
ELSE IF ( (T.GE.TFOOD(2)) .AND. (T.LE.TFOOD(3)) ) THEN
  Z = QFOOD(2) * EXP((-KFOOD(2)) * (T - TFOOD(2)))
ELSE IF (T.GE.TFOOD(3)) THEN
  Z = QFOOD(3) * EXP((-KFOOD(3)) * (T - TFOOD(3)))
ENDIF
DY(1) = (-A1 * Y(1) * Y(2)) + A2 * (YI(1) - Y(1)) * (1-H)
+      + A3 * Z
DY(2) = B1 * (Y(1) - YI(1)) * H - (B2 * Y(2))
RETURN
END

```

```

SUBROUTINE GRAPH(YVAL,TIME,NPL)

```

```

C      This Subroutine Provides A
C      Graphical Display Of The
C      Component Model. Value Of
C      Y Is Plotted Against Time.

```

```

IMPLICIT REAL*4(A-H,O-Z)
DIMENSION YVAL(NPL),TIME(NPL)
VALMAX = YVAL(NPL)
VALMIN = YVAL(1)
DO 13 I = 1,NPL
  IF (YVAL(I).GT.VALMAX) THEN
    VALMAX = YVAL(I)
  ELSE IF (YVAL(I).LT.VALMIN) THEN
    VALMIN = YVAL(I)
  ENDIF
13 CONTINUE
MAXVAL = VALMAX + 1
MINVAL = VALMIN - 1
SPAC1 = (TIME(NPL) - TIME(1))/10.0
SPAC2 = (MAXVAL - MINVAL)/10.0
CALL HWROT('MOVIE')
CALL SWISSM
CALL PAGE(8.5,11.0)
CALL AREA2D(6.0,8.0)

```

DIA02900
 DIA02910
 DIA02920
 DIA02930
 DIA02940
 DIA02950
 DIA02960
 DIA02970
 DIA02980
 DIA02990
 DIA03000
 DIA03010
 DIA03020
 DIA03030
 DIA03040
 DIA03050
 DIA03060
 DIA03070
 DIA03080
 DIA03090
 DIA03100
 DIA03110
 DIA03120
 DIA03130
 DIA03140
 DIA03150
 DIA03160
 DIA03170
 DIA03180
 DIA03190
 DIA03200
 DIA03210
 DIA03220
 DIA03230
 DIA03240
 DIA03250
 DIA03260
 DIA03270
 DIA03280
 DIA03290
 DIA03300
 DIA03310
 DIA03320
 DIA03330
 DIA03340
 DIA03350
 DIA03360
 DIA03370
 DIA03380
 DIA03390
 DIA03400
 DIA03410
 DIA03420
 DIA03430
 DIA03440
 DIA03450
 DIA03460
 DIA03470
 DIA03480

```

CALL HEADIN('COMPONENT MODEL DIABETES MELLITUS$',100,1.5,2)
CALL HEADIN('STUDY OF NORMAL PERSONS$',100,-1.15,2)
CALL XNAME('TIME (HOURS)$',100)
CALL YNAME('BLOOD SUGAR (PPM)$',100)
CALL GRAF (TIME(1),SPAC1,TIME(NPL),MINVAL,SPAC2,MAXVAL)
C DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C RATIONAL SPLINE INTERPOLATION
C CALL RASPLN (1.5)
C CALL THKCRV (.015)
C CALL THKRND (0.)
CALL CURVE (TIME,YVAL,NPL,0)
CALL ENDPL(0)
RETURN
END

SUBROUTINE GRAPH1(YVAL3,TIME,NPL)
C This Subroutine Provides A
C Graphical Display Of The
C Component Model. Value Of
C Y Is Plotted Against Time.

IMPLICIT REAL*4 (A-H,O-Z)
DIMENSION YVAL3(NPL),TIME(NPL)
VALMAX = YVAL3(NPL)
VALMIN = YVAL3(1)
DO 13 I = 1,NPL
  IF (YVAL3(I).GT.VALMAX) THEN
    VALMAX = YVAL3(I)
  ELSE IF (YVAL3(I).LT.VALMIN) THEN
    VALMIN = YVAL3(I)
  ENDIF
13 CONTINUE
MAXVAL = VALMAX + 1
MINVAL = VALMIN - 1
SPAC1 = (TIME(NPL) - TIME(1))/10.0
SPAC2 = (MAXVAL - MINVAL)/10.0
CALL HWROT('MOVIE')
CALL SWISSM
CALL PAGE(8.5,11.0)
CALL AREA2D(6.0,8.0)
CALL HEADIN('COMPONENT MODEL DIABETES MELLITUS$',100,1.5,2)
CALL HEADIN('STUDY OF NORMAL PERSONS$',100,-1.15,2)
CALL XNAME('TIME (HOURS)$',100)
CALL YNAME('BLOOD INSULIN (PPM)$',100)
CALL GRAF (TIME(1),SPAC1,TIME(NPL),MINVAL,SPAC2,MAXVAL)
C DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C RATIONAL SPLINE INTERPOLATION
C CALL RASPLN (1.5)
C CALL THKCRV (.015)
C CALL THKRND (0.)
CALL CURVE (TIME,YVAL3,NPL,0)
CALL ENDPL(0)
RETURN
END

SUBROUTINE OUTPUT(Y,N,T)
C This Subroutine stores values of Output Variables
C at communication times. Additionally, it provides
C an interactive tabular display of the results.

```

DIA03490
DIA03500
DIA03510
DIA03520
DIA03530
DIA03540
DIA03550
DIA03560
DIA03570
DIA03580
DIA03590
DIA03600
DIA03610
DIA03620
DIA03630
DIA03640
DIA03650
DIA03660
DIA03670
DIA03680
DIA03690
DIA03700
DIA03710
DIA03720
DIA03730
DIA03740
DIA03750
DIA03760
DIA03770
DIA03780
DIA03790
DIA03800
DIA03810
DIA03820
DIA03830
DIA03840
DIA03850
DIA03860
DIA03870
DIA03880
DIA03890
DIA03900
DIA03910
DIA03920
DIA03930
DIA03940
DIA03950
DIA03960
DIA03970
DIA03980
DIA03990
DIA04000
DIA04010
DIA04020
DIA04030
DIA04040
DIA04050
DIA04060
DIA04070

```

IMPLICIT REAL (A-H,O-Z)
DIMENSION Y(N)
COMMON/DIFF/YVAL(342),YVAL3(342),TIME(342),NPL

```

```

WRITE(6,23) T,Y(1),Y(2)
23 FORMAT(1X,F8.3,5X,F8.3,5X,F8.3)
NPL = NPL + 1
TIME(NPL) = T
YVAL(NPL) = Y(1)
YVAL3(NPL) = Y(2)
RETURN
END

```

SUBROUTINE INIT

```

INTEGER NUM,RC,RLEN
REAL RES1
C CHARACTER*8 KEY,MENUN
CHARACTER*8 FLDN(24)
CHARACTER*4 CC
COMMON/SAME/PU(24)

```

C Xmenu used for Parameters and Initial Conditions

```

FLDN(1) = 'A1'
FLDN(2) = 'A2'
FLDN(3) = 'A3'
FLDN(4) = 'B1'
FLDN(5) = 'B2'
FLDN(6) = 'QFOOD1'
FLDN(7) = 'QFOOD2'
FLDN(8) = 'QFOOD3'
FLDN(9) = 'TFOOD1'
FLDN(10) = 'TFOOD2'
FLDN(11) = 'TFOOD3'
FLDN(12) = 'KFOOD1'
FLDN(13) = 'KFOOD2'
FLDN(14) = 'KFOOD3'
FLDN(15) = 'Z'
FLDN(16) = 'Y1'
FLDN(17) = 'Y2'
FLDN(18) = 'TINIT'
FLDN(19) = 'TFIN'
FLDN(20) = 'COMINT'
FLDN(21) = 'HMIN'
FLDN(22) = 'HBOUND'
FLDN(23) = 'TOL'
FLDN(24) = 'HINIT'

```

```

MENUN = 'DIABETES'
CALL MCLSCR(NUM,RC)
CALL MLOAD(NUM,RC,MENUN)
CALL MPFMAP(NUM,RC,1)
CALL MALARM(NUM,RC,1)
CALL MPRINT(NUM,RC,2,PROUT)
CALL MDSPRD(NUM,RC,KEY)
C CALL MEXIT(NUM,RC)

```

DIA04080
DIA04090
DIA04100
DIA04110
DIA04120
DIA04130
DIA04140
DIA04150
DIA04160
DIA04170
DIA04180
DIA04190
DIA04200
DIA04210
DIA04220
DIA04230
DIA04240
DIA04250
DIA04260
DIA04270
DIA04280
DIA04290
DIA04300
DIA04310
DIA04320
DIA04330
DIA04340
DIA04350
DIA04360
DIA04370
DIA04380
DIA04390
DIA04400
DIA04410
DIA04420
DIA04430
DIA04440
DIA04450
DIA04460
DIA04470
DIA04480
DIA04490
DIA04500
DIA04510
DIA04520
DIA04530
DIA04540
DIA04550
DIA04560
DIA04570
DIA04580
DIA04590
DIA04600
DIA04610
DIA04620
DIA04630
DIA04640
DIA04650
DIA04660

```
IF (KEY .EQ. 'PF10') GOTO 25
IF (KEY .EQ. 'PF12') STOP
25 DO 23 I = 1,17
   CALL MSCR2D(NUM,RC,FLDN(I),CC,4,RLEN)
   CALL MCVTCF(PU(I),RC,CC,4,1)
23 CONTINUE
DO 29 I = 18,24
   CALL MSCR2D(NUM,RC,FLDN(I),CC,7,RLEN)
   CALL MCVTCF(PU(I),RC,CC,7,1)
29 CONTINUE
RETURN
END
```

DIA04670
DIA04680
DIA04690
DIA04700
DIA04710
DIA04720
DIA04730
DIA04740
DIA04750
DIA04760
DIA04770
DIA04780

```

1 .....1.....2.....3.....4.....5.....6.....7.....8+
2      INITIALIZATION
3
4      KINDLY INITIALIZE VARIABLES
5
6      Model Parameters      Experimentation Variables
7      & External Input (Z)
8
9      A1 = 0.05      A2 = 1.00      A3 = 4.00      Initial State Control Variables
10     B1 = 0.50      B2 = 2.00      QF1 = 50.0      HINIT = 0.00
11     QF2 = 100.      QF3 = 100.      TF1 = 8.00      Y1(0) = 100.  TINIT = 0.01
12     TF2 = 13.0      TF3 = 20.0      KF1 = 4.00      Y2(0) = 0.00  TFIN = 24.0
13     KF2 = 4.00      KF3 = 4.00      Z = 0.00      COMINT = 0.50
14                                     TOL = 0.00010
15                                     HBOUND = 0.1000
16                                     HMIN = 0.00001
17
18     Press: PF10 - to start simulation  PF12 - to quit
19
20 .....1.....2.....3.....4.....5.....6.....7.....8+

```

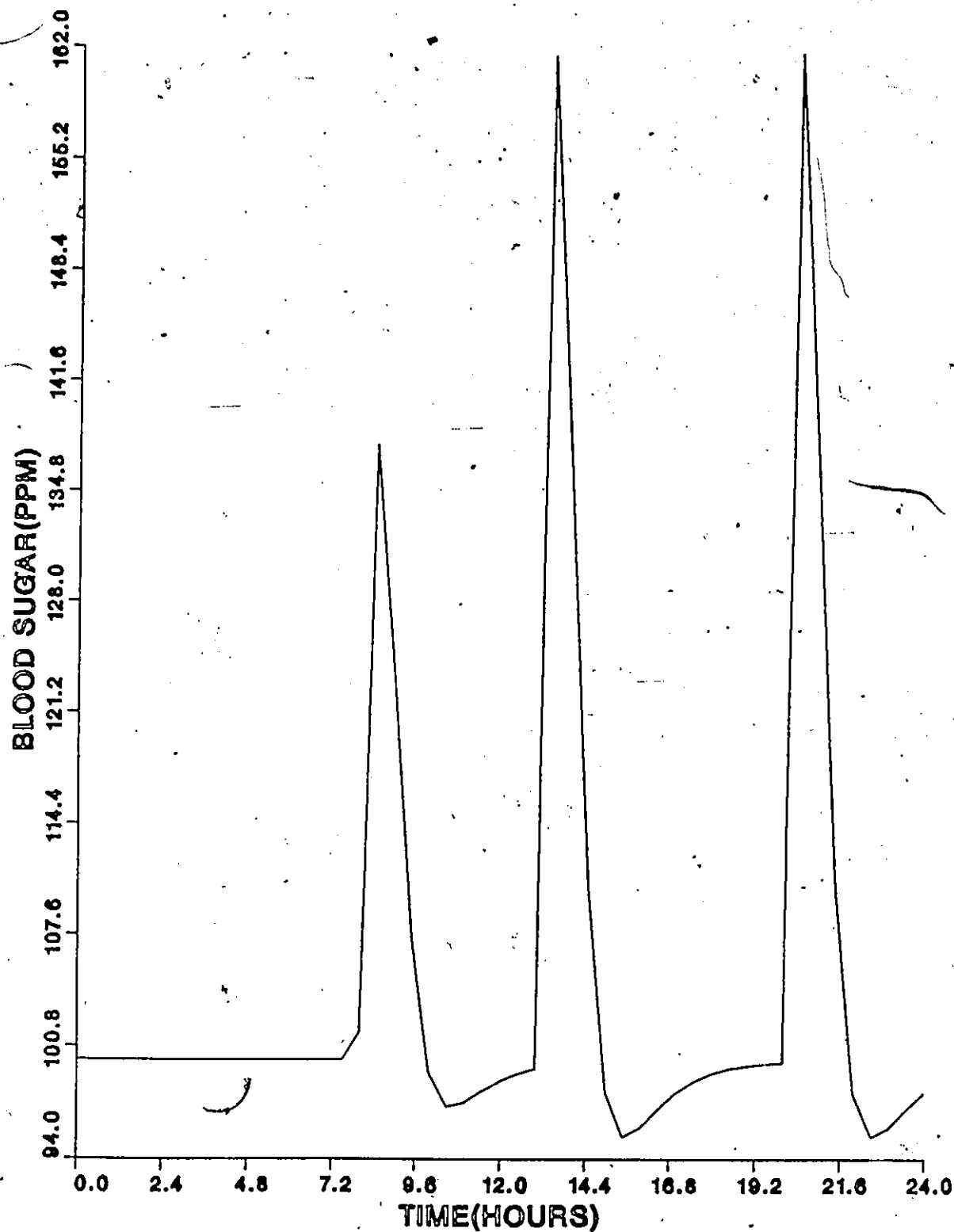
Menu For The Diabetes Mellitus Model: Normal Person

Method: Fixed Step Fourth-Order Runge-Kutta

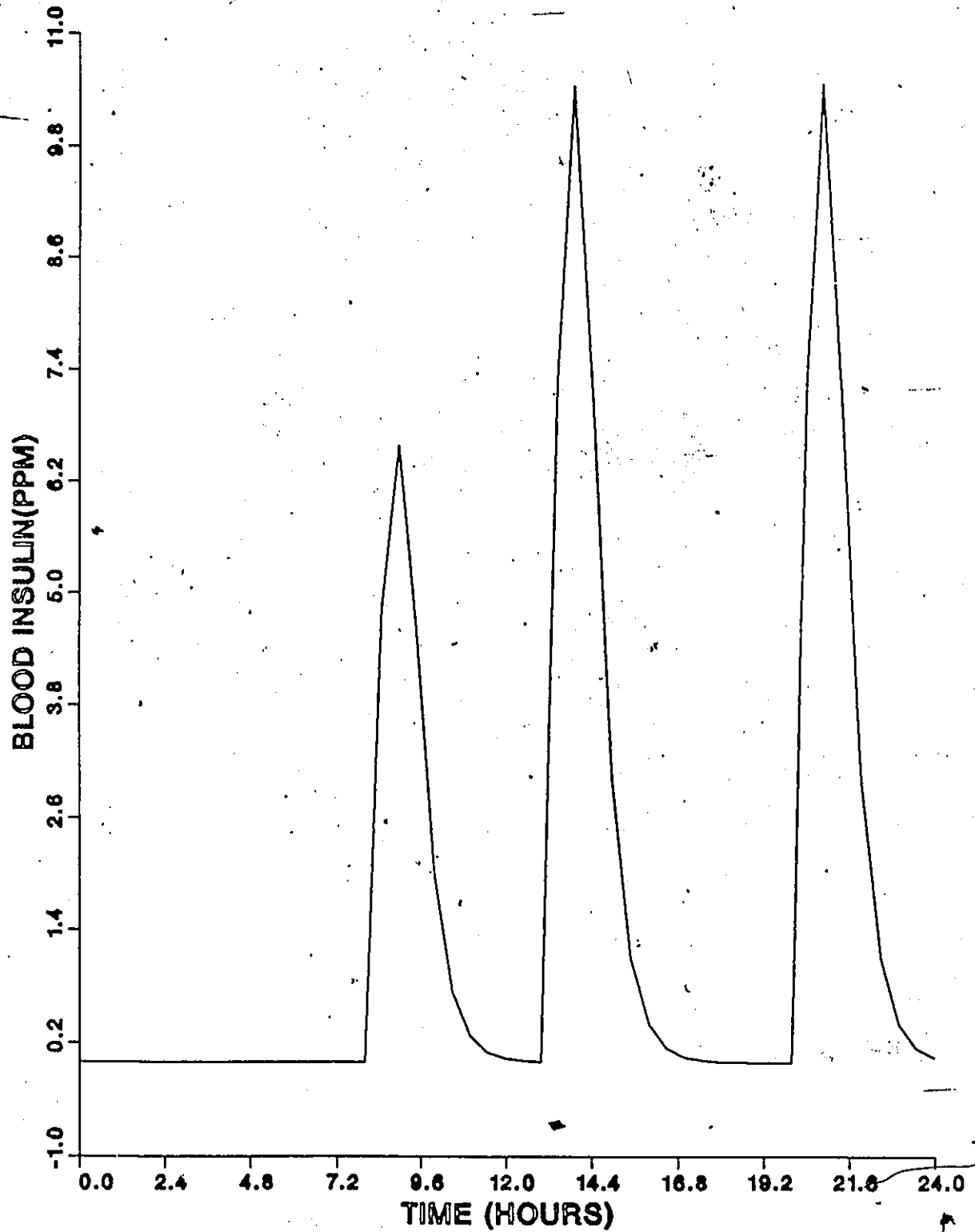
Problem: Component Model Diabetes Mellitus
Study of Normal Person

Time	Blood Sugar	Blood Insulin
0.000	100.000	0.000
0.500	100.000	0.000
1.000	100.000	0.000
1.500	100.000	0.000
2.000	100.000	0.000
2.500	100.000	0.000
3.000	100.000	0.000
3.500	100.000	0.000
4.000	100.000	0.000
4.500	100.000	0.000
5.000	100.000	0.000
5.500	100.000	0.000
6.000	100.000	0.000
6.500	100.000	0.000
7.000	100.000	0.000
7.500	100.000	0.000
8.000	101.867	0.000
8.500	137.675	4.838
9.000	123.274	6.588
9.500	107.539	4.565
10.000	99.275	2.030
10.500	97.199	0.747
11.000	97.436	0.275
11.500	98.125	0.101
12.000	98.744	0.037
12.500	99.194	0.014
13.000	99.495	0.005
13.500	161.532	7.227
14.000	136.847	10.455
14.500	110.583	7.076
15.000	98.069	3.025
15.500	95.374	1.113
16.000	95.928	0.410
16.500	97.060	0.151
17.000	98.041	0.055
17.500	98.747	0.020
18.000	99.216	0.008
18.500	99.515	0.003
19.000	99.703	0.001
19.500	99.819	0.000
20.000	99.889	0.000
20.500	161.794	7.269
21.000	136.907	10.492
21.500	110.560	7.090
22.000	98.038	3.027
22.500	95.353	1.114
23.000	95.915	0.410
23.500	97.051	0.151
24.000	98.036	0.055

COMPONENT MODEL DIABETES MELLITUS STUDY OF NORMAL PERSON



COMPONENT MODEL DIABETES MELLITUS STUDY OF NORMAL PERSON



Appendix B. THE ELECTRONIC OSCILLATOR MODEL

B.1 Problem Definition

This test example is of the electronic oscillator model as described by Palusinski (1985). It consists of six main blocks namely:

- An Oscillator
- A Squaring Operation
- A Sixth-Order Lumped-Parameter Model
Of Thermistor Inertia and Non-Linearity
- A Summing Element
- A Square Root Operation
- The Inertia Of Feedback

The oscillator is modelled by the Van der Pol differential equation and the non-linearities are represented by elementary functions of one variable. The resulting single component model is integrated using the Fifth-Order Runge-Kutta Fehlberg over an interval of 20 seconds and the parameter set suggested by Palusinski (1985, p.269). The initial states were assigned the values as specified in the Gest specification of the model in Section B.2.

B.2 Gest Specification of The Electronic Oscillator Model

Program StudyOfElectronicOscillator .

ContinuousModel ElectronicOscillator
StaticStructure .

States

Y1,

Y2,

X1,

X2,

X3,

X4,

X5,

X6,

V,

S

Outputs

X3,

S

Parameters

R1,

(* Resistance in kOhms

*)

R2,

(* Resistance in kOhms

*)

R3,

(* Resistance in kOhms

*)

R4,

(* Resistance in kOhms

*)

R5,

(* Resistance in kOhms

*)

R6,

(* Resistance in kOhms

*)

C1,

(* Capacitance in microFarads

*)

C2,

(* Capacitance in microFarads

*)

C3,

(* Capacitance in microFarads

*)

C4,

(* Capacitance in microFarads

*)

C5,

(* Capacitance in microFarads

*)

C6

(* Capacitance in microFarads

*)

EndStaticStructure

DynamicStructure

Derivatives

 $X1' = 2*Y1*Y2/R1 + (X2-X1)/R1*C1$ $X2' = X1/R2*C1 - (1/R2*C1 + 1/R2*C2)*X2 + X3/R1*C1$ $X3' = X2/R3*C2 - (1/R3*C2 + 1/R3*C3)*X3 + X4/R3*C3$ $X4' = X3/R4*C3 - (1/R4*C3 + 1/R4*C4)*X4 + X5/R4*C4$ $X5' = X4/R5*C4 - (1/R5*C4 + 1/R5*C5)*X5 + X6/R5*C5$ $X6' = X5/R6*C5 - (1/R6*C5 + 1/R6*C6)*X6$ $Y1' = Y2$ $Y2' = -64*Y1 + 7.5*(2 + S. - Y1**2.0) * Y2$ $V' = X6/C6$ $S' = 0.02*Abs(36 - 5.29 * Sqrt(Abs(V))) ** 1.2 *$ $Sign(Abs(36 - 5.29 * Sqrt(Abs(V))) - 0.02*S)$

EndDerivatives

EndDynamicStructure

EndModel ElectronicOscillator

Parameter Set 1

Parameters

R1 = 8.0

R2 = 8.0

R3 = 8.0

R4 = 8.0

R5 = 8.0

R6 = 8.0

C1 = 6.25

C2 = 4.25

C3 = 1.25

C4 = 1.25

```
C5 = 1.25
C6 = 1.25
EndParameters
EndParameter Set 1

Experiment 1
  TimeUnitIs Second
  StartTime = 0.0
  IntegrateBy Runge-Kutta Fehlberg
  Tol = 0.5
  Communicate at every 0.2 Second
  SimulateUntil Time = 20.0
  InitialStates
    X1 = 80.0
    X2 = 85.0
    X3 = 40.0
    X4 = 45.0
    X5 = 50.0
    X6 = 55.0
    Y1 = 60.0
    Y2 = 70.0
    V = 60.0
    S = 65.0
  EndInitialStates
  SaveOutputs X3,S
  EndContinuousModelElectronicOscillator
EndExperiment 1

Run 1
  ToObserve ElectronicOscillator
  WithParameterSet 1
  InExperiment 1
  WithPostRun
    OutputModule 1 On Printer
  EndPostRun
EndRun 1

OutputModule 1
  New Page
  Heading ForFirstPage 1 Line
  'Study of ElectronicOscillator'
  List Parameters And InitialConditions
  PlotandList X3,S
EndOutputModule 1

Program StudyOfElectronicOscillator
```

C B.3 Equivalent Fortran Program With Results For
C Electronic Oscillator Model

Variable List			
C			FEL00010
C			FEL00020
C			FEL00030
C			FEL00040
C			FEL00050
C			FEL00060
C			FEL00070
C	Input : N	--Dimension of the Vector of State Variables	FEL00080
C			FEL00090
C	Y(1)-Y(N)	--Initial Values of State Variables	FEL00100
C			FEL00110
C	TCOM	--Communication Time	FEL00120
C			FEL00130
C	T	--Computational Time	FEL00140
C			FEL00150
C	TFIN	--End Time of Simulation	FEL00160
C			FEL00170
C			FEL00180
C	HBOUND	--Upper Bound on Initial Step Size	FEL00190
C			FEL00200
C	HMIN	--Minimum step size integration is allowed to proceed at	FEL00210
C			FEL00220
C	HINIT	--Starting Integration Step Size	FEL00230
C			FEL00240
C	H	--Integration Step Size	FEL00250
C			FEL00260
C	TOL	--Tolerance or Accuracy specified by user	FEL00270
C			FEL00280
C	COMINT	--Interval at which output of simulation is required	FEL00290
C			FEL00300
C			FEL00310
C			FEL00320
C	ORD	--ORDER OF THE INTEGRATION METHOD	FEL00330
C			FEL00340
C			FEL00350
C	Output : TIME	--Vector of times of Output Values	FEL00360
C			FEL00370
C	YVAL	--Vector of values of Y at Output Points	FEL00380
C			FEL00390
C	Program Variables :		FEL00400
C	Y(N)	--State Variables Vector	FEL00410
C			FEL00420
C	DY(N)	--Derivative Vector of State Variables	FEL00430
C			FEL00440
C	DY1(15)-DY4(15)	--Working Vectors in Integration Routine capable of integrating systems with up to 15 state variables.	FEL00450
C			FEL00460
C			FEL00470
C			FEL00480
C	F1(15)-F3(15)	--Working Vectors in Integration Routine capable of integrating systems with up to 15 state variables.	FEL00490
C			FEL00500
C			FEL00510
C			FEL00520
C	NFLAG	--Flag Which Signals Collection of Output Variables.	FEL00530
C			FEL00540
C			FEL00550
C	HPOS	--Intermediate variable used in computing HINIT	FEL00560
C			FEL00570
C	NPL	--Counter used for Graphics Routine.	FEL00580
C			FEL00590

ERR(N) --Values of Local Error Estimates of State
 --Variables

ERRMAX --Maximum value of Local Error Estimates

This Test Program Demonstrates the use of the Variable
Step Runge-Kutta Fehlberg Integration Algorithm in the
Simulation of a Coupled Model.

PROGRAM MAIN

IMPLICIT REAL*4 (A-H,O-Z)

DIMENSION Y(10),DY(10),ERR(10)

COMMON/DIFF/YVAL(400),TIME(400),YVAL3(400),NPL

COMMON/PARS/C1,C2,C3,C4,C5,C6,R1,R2,R3,R4,R5,R6

COMMON/XMEN/PU(28)

CHARACTER*1 CHOICE

EXTERNAL DERIV

PRINT*,'Welcome to the Electronic Oscillator Model'

PRINT*,' '

PRINT*,'Would You Like To Perform a Simulation ? (Y/N) '

READ*, CHOICE

IF (CHOICE .EQ. 'Y') THEN

CALL INIT

Initialization from Menu

Initialize Parameters

199 R1 = PU(1)
R2 = PU(2)
R3 = PU(3)
R4 = PU(4)
R5 = PU(5)
R6 = PU(6)
C1 = PU(7)
C2 = PU(8)
C3 = PU(9)
C4 = PU(10)
C5 = PU(11)
C6 = PU(12)

Initialize State Variables

N = 10
Y(1) = PU(13)
Y(2) = PU(14)
Y(3) = PU(15)
Y(4) = PU(16)
Y(5) = PU(17)
Y(6) = PU(22)
Y(7) = PU(18)
Y(8) = PU(19)
Y(9) = PU(20)
Y(10) = PU(21)

Initialize Run Control
Variables

FEL00600
FEL00610
FEL00620
FEL00630
FEL00640
FEL00650
FEL00660
FEL00670
FEL00680
FEL00690
FEL00700
FEL00710
FEL00720
FEL00730
FEL00740
FEL00750
FEL00760
FEL00770
FEL00780
FEL00790
FEL00800
FEL00810
FEL00820
FEL00830
FEL00840
FEL00850
FEL00860
FEL00870
FEL00880
FEL00890
FEL00900
FEL00910
FEL00920
FEL00930
FEL00940
FEL00950
FEL00960
FEL00970
FEL00980
FEL00990
FEL01000
FEL01010
FEL01020
FEL01030
FEL01040
FEL01050
FEL01060
FEL01070
FEL01080
FEL01090
FEL01100
FEL01110
FEL01120
FEL01130
FEL01140
FEL01150
FEL01160
FEL01170
FEL01180

```

T      = PU(23)
TFIN   = PU(24)
COMINT = PU(25)
HBOUND = PU(27)
HMIN   = PU(28)
TOL    = PU(26)
ORD    = 5

```

```
NPL = 1
```

Pre-Run Output :

```

Set Up Output Format and Out
put Initial Values of T and

```

```

WRITE(8,17)
17 FORMAT(1X,'Method:',10X,'Variable Step Runge-Kutta Fehlberg'/10X/
+ 1X,'Problem:',10X,'Coupled Model Electronic Oscillator'/10X/1X,
+ 'Time',10X,'Value of X3',10X,'Value of S')
PRINT*,' '
WRITE(8,21) T,Y(1),Y(6)
21 FORMAT(1X,F8.3,15X,F8.3,15X,F8.3)
TIME(1) = T
YVAL(1) = Y(1)
YVAL3(1) = Y(6)
CALL RKFEL(T,Y,N,TFIN,H,ORD,HBOUND,HMIN,COMINT,DERIV,TOL)

```

Post-Run Output:

```

Tabulate Values of State
Variables and Time at
Output Points

```

```

DO 99 I = 2,NPL
WRITE(8,87) TIME(I),YVAL(I),YVAL3(I)
87 FORMAT(1X,F7.2,15X,F8.3,15X,F8.3)
PRINT*,' '
99 CONTINUE

```

```

Plot Values of State
Variables with Time

```

```

CALL ANYDEV
CALL GRAPH(YVAL,TIME,NPL)
CALL GRAPH1(YVAL3,TIME,NPL)
PRINT*,'Do you wish to carry out another simulation (Y/N) ?'
READ*,CHOICE
IF (CHOICE.EQ.'Y') THEN
CALL INIT
GOTO 199
ENDIF
ENDIF
STOP
END

```

```
SUBROUTINE GRAPH(YVAL,TIME,NPL)
```

```

This Subroutine Provides A Graphical Display Of The
Component Model. Value Of S is Plotted Against Time.

```

```

DIMENSION YVAL (NPL),TIME (NPL)
MINT = TIME(1)
MAXT = TIME(NPL)
VALMAX = YVAL (NPL)
VALMIN = YVAL (1)
DO 14 I = 1,NPL

```

```

FEL01190
FEL01200
FEL01210
FEL01220
FEL01230
FEL01240
FEL01250
FEL01260
FEL01270
FEL01280
FEL01290
FEL01300
FEL01310
FEL01320
FEL01330
FEL01340
FEL01350
FEL01360
FEL01370
FEL01380
FEL01390
FEL01400
FEL01410
FEL01420
FEL01430
FEL01440
FEL01450
FEL01460
FEL01470
FEL01480
FEL01490
FEL01500
FEL01510
FEL01520
FEL01530
FEL01540
FEL01550
FEL01560
FEL01570
FEL01580
FEL01590
FEL01600
FEL01610
FEL01620
FEL01630
FEL01640
FEL01650
FEL03160
FEL03170
FEL03180
FEL03190
FEL03200
FEL03210
FEL03220
FEL03230
FEL03240
FEL03250
FEL03260
FEL03270

```

```

      IF (YVAL (I).GT.VALMAX) THEN
        VALMAX = YVAL (I)
      ELSE IF (YVAL (I).LT.VALMIN) THEN
        VALMIN = YVAL (I)
      END IF
14  CONTINUE
    MAXVAL = VALMAX + 1
    MINVAL = VALMIN - 1
    SPAC1 = (MAXT - MINT)/10.0
    SPAC2 = (MAXVAL - MINVAL)/10.0
    CALL HWROT('MOVIE')
    CALL PAGE(8.5,11.0)
    CALL AREA2D(6.0,8.0)
    CALL SWISSM
    CALL HEADIN('ELECTRONIC OSCILLATOR MODEL$',100,1.5,2)
    CALL HEADIN('PLOT OF S WITH TIMES$',100,-1.15,2)
    CALL XNAME('TIME(SECS)$',100)
    CALL YNAME('VALUE OF S$',100)
    CALL GRAF(MINT,SPAC1,MAXT,MINVAL,SPAC2,MAXVAL)
C   Draw Curve with Rounded and Thickened Line and
C   Rational Spline Interpolation
    CALL RASPLN (1.5)
    CALL THKCRV (.015)
    CALL THKRND (0.)
    CALL CURVE(TIME ,YVAL ,NPL,1)
    CALL ENDPL(0)
    RETURN
    END

```

_____ SUEROUTINE GRAPH1(YVAL3,TIME1,NPL)

C This Subroutine Provides A Graphical Display Of The
C Component Model. Value Of S is Plotted Against Time.

```

    DIMENSION YVAL3(NPL),TIME1(NPL)
    MINT = TIME1(1)
    MAXT = TIME1(NPL)
    VALMAX = YVAL3(NPL)
    VALMIN = YVAL3(1)
    DO 14 I = 1,NPL
      IF (YVAL3(I).GT.VALMAX) THEN
        VALMAX = YVAL3(I)
      ELSE IF (YVAL3(I).LT.VALMIN) THEN
        VALMIN = YVAL3(I)
      END IF
14  CONTINUE
    MAXVAL = VALMAX + 1
    MINVAL = VALMIN - 1
    SPAC1 = (MAXT - MINT)/10.0
    SPAC2 = (MAXVAL - MINVAL)/10.0
    CALL HWROT('MOVIE')
    CALL PAGE(8.5,11.0)
    CALL AREA2D(6.0,8.0)
    CALL SWISSM
    CALL HEADIN('STUDY OF ELECTRONIC OSCILLATOR MODEL$',100,1.5,2)
    CALL HEADIN('PLOT OF X3 WITH TIMES$',100,-1.15,2)
    CALL XNAME('TIME(SECS)$',100)
    CALL YNAME('VALUE OF X3$',100)
    CALL GRAF(MINT,SPAC1,MAXT,MINVAL,SPAC2,MAXVAL)

```

C DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
 C RATIONAL SPLINE INTERPOLATION

CALL RASPLN (1.5)
 CALL THKCRV (.015)
 CALL THKRND (0.)
 CALL CURVE (TIME1, YVAL3, NPL, 1)
 CALL ENDPL (0)
 RETURN
 END

SUBROUTINE OUTPUT(Y,N,T)

C This Subroutine stores values of Output Variables
 C at communication times. Additionally, it provides
 C an interactive tabular display of the results.

IMPLICIT REAL*4 (A-H,O-Z)
 DIMENSION Y(N)
 COMMON/DIFF/YVAL(400), TIME(400), YVAL3(400), NPL

WRITE(6,23) T,Y(1),Y(6)
 23 FORMAT(1X,F5.2,3X,F6.3,3X,F9.3)
 NPL = NPL + 1
 TIME(NPL) = T
 YVAL(NPL) = Y(1)
 YVAL3(NPL) = Y(6)
 RETURN
 END

SUBROUTINE DERIV(T,Y,DY,N)
 IMPLICIT REAL*4 (A-H,O-Z)
 DIMENSION Y(N), DY(N)
 COMMON/PARS/C1,C2,C3,C4,C5,C6,R1,R2,R3,R4,R5,R6

C Subroutine consists of Slow System
 C Derivatives which are specified by
 C the user for his particular model.

DY(1) = Y(10)/(R3*C2) - (1/(R3*C2) + 1/(R3*C3))*Y(1) +
 + Y(2)/(R3*C3)
 DY(2) = Y(1)/(R4*C3) - (1/(R4*C3) + 1.0/(R4*C4))*Y(2) + Y(3)/(R4*C4)
 DY(3) = Y(2)/(R5*C4) - (1/(R5*C4) + 1/(R5*C5))*Y(3) + Y(4)/(R5*C5)
 DY(4) = Y(3)/(R6*C5) - (1.0/(R6*C5) + 1.0/(R6*C6))*Y(4)
 DY(5) = Y(4)/C6
 DY(6) = 0.02 * ABS(36.0 - 5.29*SQRT(ABS(Y(5))))**1.2*
 + SIGN(1.0,ABS(36.0-5.29*SQRT(ABS(Y(5))))) - 0.02*Y(6)
 DY(7) = Y(8)
 DY(8) = -64.0*Y(7) + 7.5*(2.0+Y(6)-(Y(7)*Y(7)))*Y(8)
 DY(9) = 2.0*Y(7)*Y(8)/R1 + (Y(10)-Y(9))/(R1*C1)
 DY(10) = Y(9)/(R2*C1) - Y(10)*(1.0/(R2*C1) + 1.0/(R2*C2)) + Y(1)/(R1*C1)

FEL03870
 FEL03880
 FEL03890
 FEL03900
 FEL03910
 FEL03920
 FEL03930
 FEL03940
 FEL03950
 FEL03960
 FEL03970
 FEL03980
 FEL03990
 FEL04000
 FEL04010
 FEL04020
 FEL04030
 FEL04040
 FEL04050
 FEL04060
 FEL04070
 FEL04080
 FEL04090
 FEL04100
 FEL04110
 FEL04120
 FEL04130
 FEL04140
 FEL04150
 FEL04160
 FEL04170
 FEL04180
 FEL04190
 FEL04200
 FEL04210
 FEL04220
 FEL04230
 FEL04240
 FEL04250
 FEL04260
 FEL04270
 FEL04280
 FEL04290
 FEL04300
 FEL04310
 FEL04320
 FEL04330
 FEL04340
 FEL04350
 FEL04360
 FEL04370
 FEL04380
 FEL04390
 FEL04400
 FEL04410
 FEL04420
 FEL04430
 FEL04440
 FEL04450

RETURN
END

SUBROUTINE INIT

INTEGER NUM, RC, RLEN
CHARACTER*8 KEY, MENUN
CHARACTER*8 FLDN(28)
CHARACTER*4 CC
COMMON/XMEN/PU(28)

C Xmenu used for Parameters and Initial Conditions

FLDN(1) = 'R1'
FLDN(2) = 'R2'
FLDN(3) = 'R3'
FLDN(4) = 'R4'
FLDN(5) = 'R5'
FLDN(6) = 'R6'
FLDN(7) = 'C1'
FLDN(8) = 'C2'
FLDN(9) = 'C3'
FLDN(10) = 'C4'
FLDN(11) = 'C5'
FLDN(12) = 'C6'
FLDN(13) = 'X3'
FLDN(14) = 'X4'
FLDN(15) = 'X5'
FLDN(16) = 'X6'
FLDN(17) = 'V'
FLDN(18) = 'Y1'
FLDN(19) = 'Y2'
FLDN(20) = 'X1'
FLDN(21) = 'X2'
FLDN(22) = 'S'
FLDN(23) = 'TINIT'
FLDN(24) = 'TFIN'
FLDN(25) = 'COMINT'
FLDN(26) = 'TOL'
FLDN(27) = 'HBOUND'
FLDN(28) = 'HMIN'

MENUN = 'OSSIE'

CALL MCLSCR(NUM, RC)

CALL MLOAD(NUM, RC, MENUN)

CALL MPFMAP(NUM, RC, 1)

CALL MALARM(NUM, RC, 1)

CALL MPRINT(NUM, RC, 2, PROUT)

CALL MDSPRD(NUM, RC, KEY)

C CALL MEXIT(NUM, RC)

IF (KEY .EQ. 'PF10') GOTO 25

IF (KEY .EQ. 'PF12') STOP

25 DO 23 I = 1, 22

CALL MSCR2D(NUM, RC, FLDN(I), CC, 4, RLEN)

CALL MCVTCF(PU(I), RC, CC, 4, 2)

23 CONTINUE

FEL04460
FEL04470
FEL04480
FEL04490
FEL04500
FEL04510
FEL04520
FEL04530
FEL04540
FEL04550
FEL04560
FEL04570
FEL04580
FEL04590
FEL04600
FEL04610
FEL04620
FEL04630
FEL04640
FEL04650
FEL04660
FEL04670
FEL04680
FEL04690
FEL04700
FEL04710
FEL04720
FEL04730
FEL04740
FEL04750
FEL04760
FEL04770
FEL04780
FEL04790
FEL04800
FEL04810
FEL04820
FEL04830
FEL04840
FEL04850
FEL04860
FEL04870
FEL04880
FEL04890
FEL04900
FEL04910
FEL04920
FEL04930
FEL04940
FEL04950
FEL04960
FEL04970
FEL04980
FEL04990
FEL05000
FEL05010
FEL05020
FEL05030
FEL05040

29 DO 33 I = 23,28
 CALL MSCR2D(NUM,RC,FLDN(I),CC,7,RLEN)
 CALL MCVTCF(PU(I),RC,CC,7,2)
 33 CONTINUE
 RETURN
 END

FEL05050
 FEL05060
 FEL05070
 FEL05080
 FEL05090
 FEL05100
 FEL05110
 FEL05120

```

sk 10
+....+....1....+....2....+....3....+....4....+....5....+....6....+....7....+....8+
1
2      INITIALIZATION
3
4      KINDLY INITIALIZE VARIABLES
5
6      Model Parameters          Experimentation Variables
7
8          Initial States      Control Variables
9
10     C1 = 6.25 mF  R1 = 8.00 kOhms X3(0) = 40.0 Y1(0) = 20.0 TINIT = 0.00
11
12     C2 = 4.25 mF  R2 = 8.00 kOhms X4(0) = 45.0 Y2(0) = 70.0 TFIN = 20.0
13
14     C3 = 1.25 mF  R3 = 8.00 kOhms X5(0) = 50.0 X1(0) = 80.0 COMINT = 0.20
15
16     C4 = 1.25 mF  R4 = 8.00 kOhms X6(0) = 55.0 X2(0) = 85.0 TOL = 0.50000
17
18     C5 = 1.25 mF  R5 = 8.00 kOhms V(0) = 60.0 S(0) = 65.0 HBOUND = 0.10
19
20     C6 = 1.25 mF  R6 = 8.00 kOhms
21
22          Press: PF10 - to start simulation  PF12 - to quit
23
24 +....+....1....+....2....+....3....+....4....+....5....+....6....+....7....+....8+

```

Menu For Electronic Oscillator Model
Using Runge-Kutta Fehlberg Algorithm

Method: Variable Step Runge-Kutta Fehlberg
Problem: Coupled Model Electronic Oscillator

Time	Value of X3	Value of S
0.00	40.000	65.000
0.20	40.358	64.777
0.40	40.705	64.574
0.60	41.041	64.392
0.80	41.368	64.229
1.00	41.682	64.086
1.20	41.989	63.960
1.40	42.286	63.852
1.60	42.573	63.761
1.80	42.852	63.686
2.00	43.124	63.627
2.20	43.387	63.583
2.40	43.641	63.553
2.60	43.888	63.538
2.80	44.129	63.537
3.00	44.360	63.548
3.20	44.585	63.573
3.40	44.804	63.609
3.60	45.015	63.658
3.80	45.220	63.718
4.00	45.419	63.790
4.20	45.611	63.873
4.40	45.797	63.967
4.60	45.976	64.070
4.80	46.151	64.184
5.00	46.319	64.308
5.20	46.481	64.441
5.40	46.638	64.584
5.60	46.790	64.735
5.80	46.936	64.896
6.00	47.077	65.065
6.20	47.214	65.243
6.40	47.344	65.428
6.60	47.470	65.622
6.80	47.592	65.823
7.00	47.708	66.033
7.20	47.820	66.248
7.40	47.927	66.472
7.60	48.030	66.704
7.80	48.128	66.941
8.00	48.222	67.184
8.20	48.312	67.436
8.40	48.398	67.694
8.60	48.480	67.958
8.80	48.557	68.227
9.00	48.630	68.503
9.20	48.700	68.787
9.40	48.766	69.074

9.60	48.828	69.366
9.80	48.887	69.668
10.00	48.942	69.970
10.20	48.993	70.280
10.40*	49.041	70.595
10.60	49.088	70.917
10.80	49.127	71.242
11.00	49.165	71.573
11.20	49.199	71.906
11.40	49.231	72.250
11.60	49.259	72.592
11.81	49.284	72.949
12.01	49.306	73.303
12.20	49.324	73.651
12.40	49.340	74.012
12.60	49.353	74.378
12.80	49.364	74.748
13.00	49.373	75.122
13.20	49.380	75.501
13.40	49.384	75.882
13.60	49.387	76.267
13.80	49.387	76.657
14.00	49.385	77.052
14.20	49.382	77.447
14.40	49.376	77.847
14.60	49.368	78.252
14.80	49.358	78.661
15.00	49.346	79.069
15.20	49.333	79.484
15.40	49.317	79.901
15.60	49.300	80.323
15.80	49.280	80.748
16.00	49.260	81.172
16.20	49.237	81.603
16.40	49.212	82.040
16.60	49.186	82.476
16.80	49.158	82.916
17.00	49.128	83.358
17.20	49.097	83.802
17.40	49.064	84.249
17.60	49.030	84.700
17.80	48.994	85.155
18.00	48.956	85.611
18.20	48.917	86.076
18.40	48.877	86.527
18.60	48.835	86.991
18.80	48.790	87.460
19.00	48.745	87.928
19.20	48.699	88.399
19.40	48.653	88.873
19.60	48.605	89.349
19.80	48.557	89.828
20.00	48.535	90.122

Appendix C. THE RUDDER CONTROL MODEL

C.1 Problem Definition

This test example uses the Adams Predictor Corrector Method to carry out the integration. The example is adapted from the article by Elzas (1979). As can be seen from the results, the control responds quickly and the trajectories follow closely within the first one-tenth of a second. The full specification of the model is shown in Section C.2.

C.2 Gest Specification of The Rudder Control Model

```
Program StudyOfRudderControl
```

```
ContinuousModel RudderControl
```

```
StaticStructure
```

```
States Y1, Y2
```

```
RangeOf Y1 = ( >= -10.0, <=10.0 )
```

```
RangeOf Y2 = ( >= -20.0, <=20.0 )
```

```
Outputs Y1,Y2
```

```
Parameters A
```

```
EndStaticStructure
```

```
DynamicStructure
```

```
Derivatives
```

```
Y1' = Y2
```

```
Y2' = A*( 1.0 - Y1**2 - Y2**2 )*( Y2 - Y1 )
```

```
EndDerivatives
```

```
EndDynamicStructure
```

```
EndModel RudderControl
```

```
ParameterSet 1
```

```
Model RudderControl
```

```
Parameter
```

```
A = 5.0
```

```
EndParameter
```

```
EndModel RudderControl
```

```
EndParameterSet 1
```

```
Experiment 1
```

```
TimeUnitIs Second
```

```
StartTime = 0.0
```

```
IntegrateBy AdamsPredictorCorrector
```

```
RelError = 0.00001
```

```
Communicate at every 0.10 Second
```

```
SimulateUntil Time = 1.0
```

```
Model RudderControl
```

```
InitialStates
```

```
Y1 = 2.0
```

```
Y2 = -2.0
```

```
EndInitialStates
```

```
SaveOutputs Y1, Y2
```

```
EndModel RudderControl
```

```
EndExperiment 1
```

```
Run 1
```

```
ToObserve RudderControl
```

```
WithParameterSet 1
```

```
InExperiment 1
```

```
WithPostRun
```

```
OutputModule 1 On Printer
```

```
EndPostRun
```

```
EndRun 1
```

```
OutputModule 1
```

```
New Page
```

```
Heading ForFirstPage 1 Line
```

```
Study of RudderControl
```

List Parameters And InitialConditions
PlotandList Y1,Y2 .
EndOutputModule 1

EndProgram StudyOfRudderControl

C	C.3	Equivalent Procedural Program With Results	ADA00020
C		For Rudder Control Model	ADA00030
			ADA00040
			ADA00050
C		Variable List	ADA00060
C			ADA00070
C	Input	: N --Dimension of the Vector of State Variables	ADA00080
C			ADA00090
C		Y(K,1)-Y(K,N)--Initial Values of State Variables	ADA00100
C			ADA00110
C		T --Computational Time	ADA00120
C			ADA00130
C		TINIT --Initial Time	ADA00140
C			ADA00150
C		TFIN --End Time of Simulation	ADA00160
C			ADA00170
C		TCOM --Communication Time	ADA00180
C			ADA00190
C		COMINT --Communication Interval	ADA00200
C			ADA00210
C			ADA00220
C			ADA00230
C		H --Integration Step Size	ADA00240
C			ADA00250
C		HINIT --Starting Integration Step Size	ADA00260
C			ADA00270
C		HBOUND --Upper Bound On Initial Step Size	ADA00280
C			ADA00290
C		HMIN --Minimum step size integration is allowed to proceed at	ADA00300
C			ADA00310
C			ADA00320
C		TOL --Tolerance or Accuracy specified by user	ADA00330
C			ADA00340
C		NORD --Order of the Integration Method	ADA00350
C			ADA00360
C	COUPTUT	:T. --Vector of times of Output Values	ADA00370
C			ADA00380
C		Y(K,1)-Y(K,N) --Vector of Values of Y at Output Points	ADA00390
C			ADA00400
C	CPROGRAM	VARIABLES :	ADA00410
C		-Y(K,N) --State Variables Vector	ADA00420
C			ADA00430
C		DY(N) --Derivative Vector of State Variables	ADA00440
C			ADA00450
C		VP(N) --Vector of Predictor Variables	ADA00460
C			ADA00470
C		VC(N) --Vector of Corrector Variables	ADA00480
C			ADA00490
C		ERR(N) --Vector of Local Error Estimates	ADA00500
C			ADA00510
C		ERRMAX --Variable containing Maximum Error	ADA00520
C			ADA00530
C		DY1(N)-DY4(N) --Working Vectors in R-K Starter Routine	ADA00540
C			ADA00550
C		P1(N)-P3(N) --Working Vectors in R-K Starter Routine	ADA00560
C			ADA00570
C		T1-T3 --Variables storing three time values generated by the R-K Starter	ADA00580
C			ADA00590

C			ADA00600
C	Y1-Y3	--Variables storing three values of State Variables generated by the R-K Starter.	ADA00610
C			ADA00620
C			ADA00630
C	HPOS	--Intermediate variable used in determining HINIT	ADA00640
C			ADA00650
C	NPL	--Counter used for Graphics Routine	ADA00660
C			ADA00670
C	NSTEPS	--Number Of Steps For Stiffness Check	ADA00680
C			ADA00690
C	NCHECK	--Actual Number Of Steps Taken During Simulation	ADA00700
C			ADA00710
C	NFLAG	--Signals A Communication Time	ADA00720
C			ADA00730
C			ADA00740
C	PROGRAM MAIN		ADA00750
C	This test program illustrates		ADA00760
C	the utilization of the Fourth-		ADA00770
C	Order Variable Adams Method		ADA00780
C	in the simulation of a single		ADA00790
C	Component Model		ADA00800
C			ADA00810
C		VARIABLE DECLARATION	ADA00820
	IMPLICIT REAL*4 (A-H,O-Z)		ADA00830
	DIMENSION T(6000),Y(6000,5)		ADA00840
	COMMON/DIFF/ YVAL1(300),YVAL2(300),TIME(300),NPL		ADA00850
	COMMON/PAR/A		ADA00860
	COMMON/SAME/PU(9)		ADA00870
	EXTERNAL DERIV		ADA00880
	CHARACTER*1 CHOICE		ADA00890
			ADA00900
	PRINT*,'Welcome To The Rudder Control Simulator'		ADA00910
	PRINT*,' '		ADA00920
	PRINT*,'Would You Like To Perform a Simulation ? (Y/N) '		ADA00930
	READ*, CHOICE		ADA00940
	IF (CHOICE .EQ. 'Y') THEN		ADA00950
200	CALL INIT		ADA00960
			ADA00970
C		Initialization from Menu	ADA00980
C		Initialize Parameter	ADA00990
199	A = PU(1)		ADA01000
			ADA01010
C		Initialize State Variables	ADA01020
	N = 2		ADA01030
	Y(1,1) = PU(2)		ADA01040
	Y(1,2) = PU(3)		ADA01050
	IF ((Y(1,1).LT.-10.0).OR. (Y(1,1).GT.10.0)) THEN		ADA01060
	PRINT*,' Sorry,This Model Requires Y to be greater than or		ADA01070
	+equal to -10 and less than or equal to 10. Kindly		ADA01080
	+Enter "Y" and Reinitialize Y '		ADA01090
	READ*, CHOICE		ADA01100
	IF (CHOICE .EQ. 'Y') GOTO 200		ADA01110
	ENDIF		ADA01120
	IF ((Y(1,2).LT.-20.0).OR. (Y(1,2).GT.20.0)) THEN		ADA01130
	PRINT*,' Sorry,This Model Requires Y1 to be greater than or		ADA01140
	+equal to -20 and less than or equal to 20. Kindly		ADA01150
	+Enter "Y" and Reinitialize Y1 '		ADA01160
	READ*, CHOICE		ADA01170
	IF (CHOICE .EQ. 'Y') GOTO 200		ADA01180

ENDIF		ADA01190
C	Initialize Run Control Variables	ADA01200
	T(1) = PU(4)	ADA01210
	TFIN = PU(5)	ADA01220
	COMINT= PU(6)	ADA01230
	HBOUND= PU(7)	ADA01240
	HMIN = PU(8)	ADA01250
C	Tolerance Specified by user for	ADA01260
C	computation of initial step size	ADA01270
C		ADA01280
	TOL = PU(9)	ADA01290
		ADA01300
		ADA01310
		ADA01320
		ADA01330
	NPL = 1	ADA01340
	ORD = 4	ADA01350
C	Pre-Run Output :	ADA01360
C	Set up Output Format and	ADA01370
C	Output Initial Values of	ADA01380
C	T(1) and Y(1,1)	ADA01390
	WRITE(8,17)	ADA01400
	17 FORMAT(1X,'Method:',19X,'Variable Step Adams'/1X,'Time',17X,	ADA01410
	+ 'VALUE OF Y1',7X,'VALUE OF Y2')	ADA01420
	PRINT*,'	ADA01430
	WRITE(8,21) T(1),Y(1,1),Y(1,2)	ADA01440
	21 FORMAT(1X,F5.2,5X,F8.3,5X,F8.3)	ADA01450
	PRINT*,'	ADA01460
	TIME(NPL) = T(1)	ADA01470
	YVAL1(NPL)= Y(1,1)	ADA01480
	YVAL2(NPL)= Y(1,2)	ADA01490
C	Run-Time Activities	ADA01500
C	Integrate by Fourth-Order	ADA01510
C	Adams Predictor Method	ADA01520
		ADA01530
		ADA01540
	CALL ADAMS(T,Y,N,TFIN,H,ORD,HBOUND,HMIN,DERIV,COMINT,TOL,K)	ADA01550
C		ADA01560
C	Post-Run Output:	ADA01570
C	Tabulate Values of State	ADA01580
C	Variables and Time at	ADA01590
C	Output Points:	ADA01600
C		ADA01610
	DO 99 I = 2,NPL	ADA01620
	WRITE(8,87)TIME(I),YVAL1(I),YVAL2(I)	ADA01630
	87 FORMAT(1X,F5.2,5X,F8.3,5X,F8.3)	ADA01640
	PRINT*,'	ADA01650
	99 CONTINUE	ADA01660
		ADA01670
C	Plot Values of State	ADA01680
C	Variables with Time	ADA01690
	CALL ANYDEV	ADA01700
	CALL GRAPH(YVAL1,YVAL2,TIME,NPL)	ADA01710
	PRINT*, 'Do you wish to carry out another simulation (Y/N) ?'	ADA01720
	READ*,CHOICE	ADA01730
	IF (CHOICE.EQ.'Y') THEN	ADA01740
	CALL INIT	ADA01750
	GOTO 199	ADA01760
	ENDIF	ADA01770

ENDIF
STOP
END

SUBROUTINE DERIV(T,Y,DY,N,K)
IMPLICIT REAL*4(A-H,O-Z)
DIMENSION Y(6000,5),DY(6000,5),T(6000)
COMMON/PAR/A

C This is the derivative evaluation
C subroutine where the user specifies
C the system derivatives that describe
C his model. As an example, the model
C Rudder Control is used.

DY(K,1) = Y(K,2)
DY(K,2) = A*(1.0-(Y(K,1)*Y(K,1))-(Y(K,2)*Y(K,2))) *
+ (Y(K,2) - Y(K,1))

C WRITE (6,23) DY(K,1),DY(K,2),Y(K,1),Y(K,2),K,T(K-1)
C 23 FORMAT(1X,F9.4,1X,F9.4,1X,F9.4,1X,F9.4,1X,I3,1X,F9.4)

RETURN
END

SUBROUTINE GRAPH(YVAL1,YVAL2,TIME1,NPL)

C This Subroutine Provides A
C Graphical Display Of The
C Component Model. Value Of
C Y Is Plotted Against Time.

IMPLICIT REAL*4(A-H,O-Z)
DIMENSION YVAL1(NPL),YVAL2(NPL),TIME1(NPL)
VALMAX = YVAL2(NPL)
VALMIN = YVAL2(1)
DO 13 I = 1,NPL
IF (YVAL2(I).GT.VALMAX) THEN
VALMAX = YVAL2(I)
ELSE IF (YVAL2(I).LT.VALMIN) THEN
VALMIN = YVAL2(I)
ENDIF

13 CONTINUE

MAXVAL = VALMAX + 1
MINVAL = VALMIN - 1
SPAC1 = (TIME1(NPL) - TIME1(1))/10.0
SPAC2 = (MAXVAL - MINVAL)/10.0
CALL HWROT('MOVIE')
CALL SWISSM
CALL PAGE(8.5,11.0)
CALL AREA2D(6.0,8.0)
CALL HEADIN('Study Of Rudder Control Model\$',100,1.5,3)
CALL HEADIN('Adams Predictor Corrector Method\$',100,1.25,3)
CALL HEADIN('Fourth-Order\$',100,-1.15,3)
CALL XNAME('Time(seconds)\$',100)
CALL YNAME('Values Of Y\$',100)

ADA01780
ADA01790
ADA01800
ADA01810
ADA04330
ADA04340
ADA04350
ADA04360
ADA04370
ADA04380
ADA04390
ADA04400
ADA04410
ADA04420
ADA04430
ADA04440
ADA04450
ADA04460
ADA04470
ADA04480
ADA04490
ADA04500
ADA04510
ADA04520
ADA04530
ADA04540
ADA04550
ADA04560
ADA04920
ADA04930
ADA04940
ADA04950
ADA04960
ADA04970
ADA04980
ADA04990
ADA05000
ADA05010
ADA05020
ADA05030
ADA05040
ADA05050
ADA05060
ADA05070
ADA05080
ADA05090
ADA05100
ADA05110
ADA05120
ADA05130
ADA05140
ADA05150
ADA05160
ADA05170
ADA05180
ADA05190
ADA05200
ADA05210
ADA05220

```

      CALL GRAF (TIME1(1), SPAC1, TIME1(NPL), MINVAL, SPAC2, MAXVAL)
C  DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C  RATIONAL SPLINE INTERPOLATION
C  CALL RASPLN (1.5)
      CALL THKCRV (.015)
      CALL THKRND (0.)
      CALL CURVE (TIME1, YVAL1, NPL, 1)
      CALL CURVE (TIME1, YVAL2, NPL, 1)
      CALL ENDPL (0)
      RETURN
      END

      SUBROUTINE OUTPUT (Y, N, TNOW, K)
C  This Subroutine stores values of Output Variables
C  at communication times. Additionally, it provides
C  an interactive tabular display of the results.

      IMPLICIT REAL*4 (A-H, O-Z)
      DIMENSION Y (6000, N)
      COMMON/DIFF/YVAL1 (300), YVAL2 (300), TIME (300), NPL

      WRITE (8, 23) TNOW, Y (K-1, 1), Y (K-1, 2)
23  FORMAT (1X, F8.3, 5X, F8.3, 5X, F8.3)
      NPL = NPL + 1
      TIME (NPL) = TNOW
      YVAL1 (NPL) = Y (K-1, 1)
      YVAL2 (NPL) = Y (K-1, 2)
      RETURN
      END

      SUBROUTINE INIT

      INTEGER NUM, RC, RLEN
C  REAL RES1
      CHARACTER*8 KEY, MENUN
      CHARACTER*8 FLDN (9)
      CHARACTER*4 CC
      COMMON/SAME/PU (9)

C  Xmenu used for Parameters and Initial Conditions

      FLDN (1) = 'A'
      FLDN (2) = 'Y'
      FLDN (3) = 'Y1'
      FLDN (4) = 'TINIT'
      FLDN (5) = 'TFIN'
      FLDN (6) = 'COMINT'
      FLDN (7) = 'HBOUND'
      FLDN (8) = 'HMIN'
      FLDN (9) = 'TOL'

      MENUN = 'RUDDER'
      CALL MCLSCR (NUM, RC)
      CALL MLOAD (NUM, RC, MENUN)
      CALL MPFMAP (NUM, RC, 1)
      CALL MALARM (NUM, RC, 1)
      CALL MPRINT (NUM, RC, 2, PROUT)
      CALL MDSPRD (NUM, RC, KEY)

```

C	CALL MEXIT(NUM,RC)	ADA05820
	IF (KEY .EQ. 'PF10') GOTO 25	ADA05830
	IF (KEY .EQ. 'PF12') STOP	ADA05840
25	DO 23 I = 1,9	ADA05850
	CALL MSCR2D(NUM,RC,FLDN(I),CC,7,RLEN)	ADA05860
	CALL MCVTCF(PU(I),RC,CC,7,2)	ADA05870
23	CONTINUE	ADA05880
	RETURN	ADA05890
	END	ADA05900
		ADA05910
		ADA05920
		ADA05930
		ADA05940
		ADA05950
		ADA05960
		ADA05970
		ADA05980

```

1 .....1.....2.....3.....4.....5.....6.....7.....8+
2      INITIALIZATION
3
4      KINDLY INITIALIZE VARIABLES
5
6      Model Parameter      Experimentation Variables
7
8      Initial States      Control Variables
9
10
11
12      A = 5.00      ,      Y(0) = 2.000      TINIT = 0.00
13
14      ,Y1(0) = -2.00      TFIN = 1.00
15
16      COMINT = 0.100
17
18      TOL = 0.00001
19
20      HBOUND= 0.010
21
22      HMIN = 0.00001
23
24      Press: PF10 - to start simulation      PF12 - to quit
25
26      Menu For Rudder Control Model

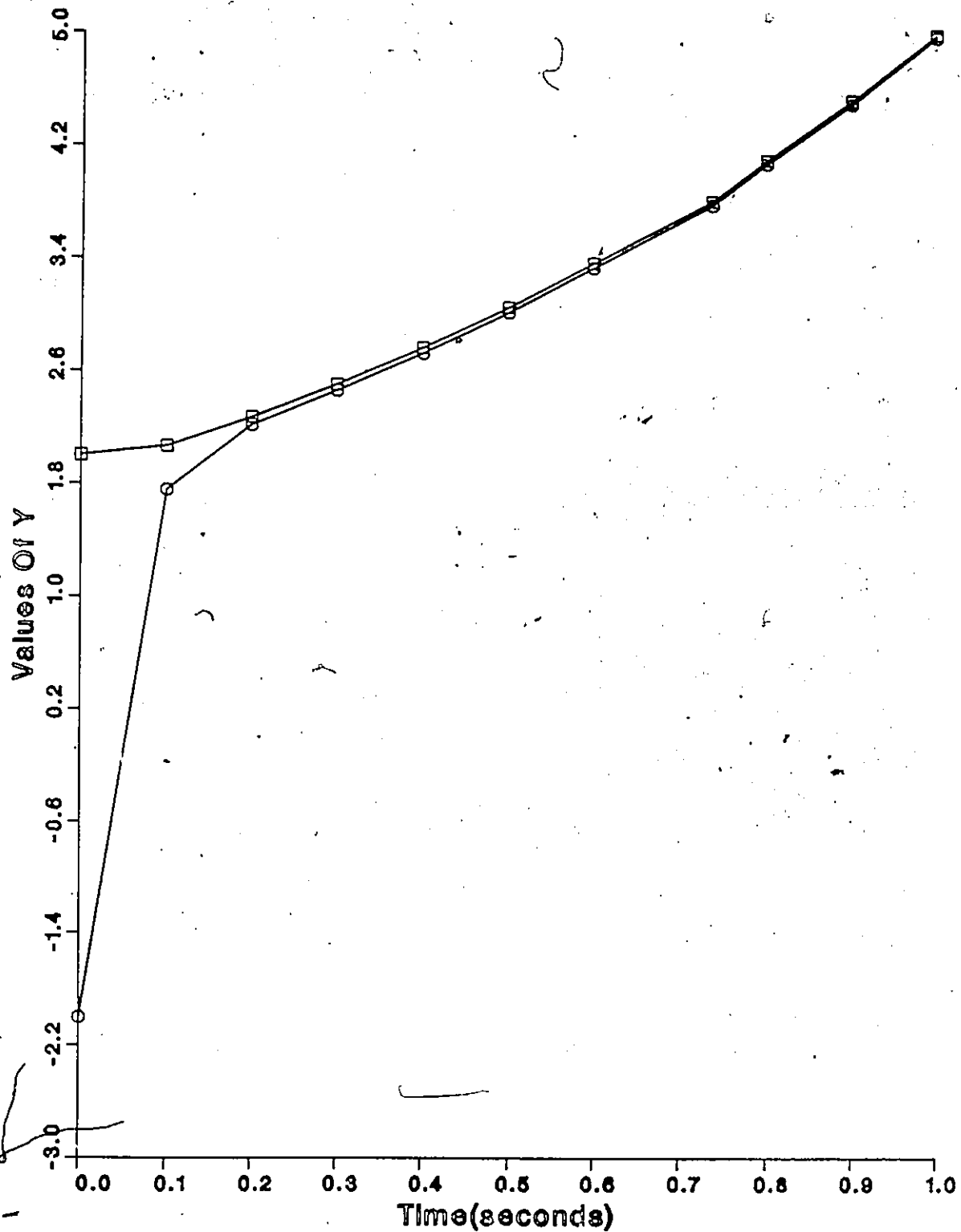
```

Problem: Study Of The Rudder Control Model

Method: Adams Predictor Corrector Method

Time	VALUE OF Y1	VALUE OF Y2
0.00	2.000	-2.000
0.10	2.067	1.758
0.20	2.271	2.215
0.30	2.504	2.460
0.40	2.765	2.725
0.50	3.050	3.015
0.60	3.364	3.332
0.70	3.809	3.781
0.80	4.103	4.077
0.90	4.531	4.509
1.00	5.006	4.985

Study Of Rudder Control Model
Adams Predictor Corrector Method
Fourth-Order



Appendix. D THE BOUNCING BALL MODEL

D.1 Problem Definition

This model is used to demonstrate the use of the discontinuity processing algorithm in the processing of state events. The trajectory of the height of the ball with time is observed. The ball, being initially at rest is dropped from a height of 10m. The model consists of a simple set of differential equations. To prevent the hazardous detection of an erroneous cross-over which could occur in this model, the height of the ball is set to zero in the MODUPD subroutine once the ball hits the ground (i.e. the state event has been detected and located). If this is not supplied, erroneous results would occur. These erroneous results caused by the false detection of a crossover are as a result of the slope of the switching function changing but the sign of the function remaining the same. The algorithm may allow the ball to go underground for a short distance instead of bouncing. This is due to the inverse aiken interpolation terminating as soon as the tolerance is met. The algorithm integrates the system to a small distance underground and the model update at this point allows the ball to start its upward climb. However, in the next integration step, the algorithm detects a change in sign once more and hence an erroneous 'cross-over'. The 'new' point of discontinuity is located and the update involving

the change in sign of the velocity once again activated. The ball would thus start its downward descent and this process is continually repeated giving rise to an incorrect trajectory whereby the ball oscillates within a small range about the origin.

D.2 Gtest Specification of The Bouncing Ball Model

```
Program StudyOfBouncingBall
```

```
ContinuousModel BouncingBall
```

```
StaticStructure
```

```
States Y1,Y2      (* Y1 vertical velocity      *)
```

```
Outputs Y2        (* Y2 height                *)
```

```
Constants G,K
```

```
G = 9.807         (* G gravity constant      *)
```

```
K = 0.8           (* K bouncing constant     *)
```

```
EndConstants
```

```
EndStaticStructure
```

```
DynamicStructure
```

```
Derivatives
```

```
Y1' = -G
```

```
Y2' = Y1
```

```
EndDerivatives
```

```
Updates
```

```
When Y2 Crosses 0.0 ( Tolerance 0.01 ),
```

```
Y1 = -K*Y1 ,
```

```
Y2 = 0
```

```
EndUpdates
```

```
EndDynamicStructure
```

```
EndModel BouncingBall
```

```
Experiment 1
```

```
TimeUnitIs Second
```

```
InitialStates
```

```
Y1 = 0
```

```
Y2 = 10.0
```

```
EndInitialStates
```

```
IntegrateBy DiscontinuityProcessingAlgorithm
```

```
Communicate at every 0.1 Second
```

```
Display OutputModule 1 on Screen and on LaserQMS
```

```
SimulateUntil Time = 10.0 Seconds
```

```
EndExperiment 1
```

```
Run 1
```

```
ToObserve BouncingBall
```

```
InExperiment 1
```

```
EndRun 1
```

```
OutputModule 1
```

```
Heading ForFirstPage 1 Line
```

```
StudyOfBouncingBall
```

```
PlotAndList Y2 Versus Time
```

```
EndOutputModule 1
```

```
EndProgram StudyOfbouncingBall
```

C	D.3	EQUIVALENT FORTRAN PROGRAM WITH RESULTS	BAL00030
C		FOR BOUNCING BALL MODEL	BAL00040
			BAL00050
			BAL00060
			BAL00070
C		Variable List	BAL00080
C			BAL00090
C	Input	: N --Dimension of the Vector of State Variables	BAL00100
C			BAL00110
C		NDF --Dimension of the Vector of Discontinuity	BAL00120
C		Functions	BAL00130
C			BAL00140
C		Y(1)-Y(N) --Initial Values of State Variables	BAL00150
C			BAL00160
C		G --Constant used in differential equation for V	BAL00170
C			BAL00180
C		K --Constant used in Model Update	BAL00190
C			BAL00200
C		T --Computational Time	BAL00210
C			BAL00220
C		TINIT --Initial Time Of Simulation	BAL00230
C			BAL00240
C		TFIN --End Time of Simulation	BAL00250
C			BAL00260
C		TCOM --Communication Time	BAL00270
C			BAL00280
C		COMINT --Communication Interval	BAL00290
C			BAL00300
C		TE --Vector Of Times At Which Time	BAL00310
C		Events Occur	BAL00320
C			BAL00330
C		THOR --Horizon Time	BAL00340
C			BAL00350
C		H --Integration Step Size	BAL00360
C			BAL00370
C		HINIT --Starting Integration Step Size	BAL00380
C			BAL00390
C		HMAX --Maximum step size integration is	BAL00400
C		allowed to proceed at	BAL00410
C			BAL00420
C		HBOUND --Upper Bound On Initial Step Size	BAL00430
C			BAL00440
C		HMIN --Minimum step size integration is	BAL00450
C		allowed to proceed at	BAL00460
C			BAL00470
C		TOL --Tolerance or Accuracy specified by user	BAL00480
C			BAL00490
C		NORD --Order of the Integration Method	BAL00500
C			BAL00510
C	COUPTUT	:T --Vector of times of Output Values	BAL00520
C			BAL00530
C		YVAL(N) --Vector of Output at Output Points	BAL00540
C			BAL00550
C		YVAL1(N) --Vector of Output at Output Points	BAL00560
C			BAL00570
C	PROGRAM VARIABLES :		BAL00580
C		Y(N) --State Variables Vector	BAL00590
C			BAL00600
C		DY(N) --Derivative Vector of State Variables	BAL00610

C	ER(N)	--Vector of Local Error Estimates	BAL00620
C			BAL00630
C	ERMAX	--Variable containing Maximum Error	BAL00640
C			BAL00650
C	HPOS	--Intermediate variable used in determining HINIT	BAL00660
C			BAL00670
C	NPL	--Counter used for Graphics Routine	BAL00680
C			BAL00690
C	YVAL, TIME	--Single-Precision copies of output Vectors needed to run Disspla Graphics Package	BAL00700
C			BAL00710
C	YLAST(N)	--Last Values of State Variables	BAL00720
C			BAL00730
C	DF(DDF)	--Present Values of Discontinuity Functions	BAL00740
C			BAL00750
C	PDF(DDF)	--Previous Values of Discontinuity Functions	BAL00760
C			BAL00770
C	F(10,5)	--Working Arrays used in Aitken Interpolation Table	BAL00780
C			BAL00790
C	TS(10,10)	--Working Arrays used in Aitken Interpolation Table	BAL00800
C			BAL00810
C			BAL00820
C	NUM	--Identifies the Discontinuity Function which has changed its sign in the preceding Step	BAL00830
C			BAL00840
C	NOT	--A Flag used to indicate whether the value of the Discontinuity Function is within the Tolerance Limit	BAL00850
C			BAL00860
C			BAL00870
C			BAL00880
C	NUMTE	--Number of Time Events	BAL00890
C			BAL00900
C	ITER	--Iteration Number	BAL00910
C			BAL00920
C	NPL	--Counter for plot of Output	BAL00930
C			BAL00940
C	NTIMEV	--Flag Showing Time Event Taking Place	BAL00950
C			BAL00960
C	NFIRST	--Flag Showing Initial Step to be Processed	BAL00970
C			BAL00980
C	NTEALL	--Flag Showing Discon. are all Time Events	BAL00990
C			BAL01000
C	NTIMUP	--Flag Showing Time Update took place	BAL01010
C			BAL01020
C	G	--Constant Used In Differential Equation For V	BAL01030
C			BAL01040
C	C	--Parameter Used In Model Update	BAL01050
C			BAL01060
C			BAL01070
C			BAL01080
C			BAL01090
C			BAL01100
C			BAL01110
C			BAL01120
C			BAL01130
C			BAL01140
C			BAL01150
C			BAL01160
C			BAL01170
C			BAL01180
C			BAL01190
C			BAL01200

Variable Declaration

```

IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(5)
REAL*4 TIME1(500), YVAL2(500), YVAL3(500)
COMMON/DIFF/YVAL(500), TIME(500), YVAL1(500), NPL
COMMON/FLAG/NUMTE, NTIMEV, NFIRST, NTEALL
COMMON/CON/G
COMMON/UPD/C

```

COMMON/WHY/COMINT,NOUT,NTIMUP
COMMON/INTEG/ORD
EXTERNAL DERIV

Initialization

Initialize Constants

G = 9.807D0
C = 0.8

Initialize State Variables

Y(1) = 0.0
Y(2) = 10.0

Initialize Run Control Variables

T = 0.0
TFIN = 10.0
HMIN = 0.000001
TOL = 0.00001
ORD = 4
COMINT = 0.10
NDF = 1
N = 2
NPL = 1.
NUMTE = 0
NTIMEV = 0

Flag Showing Initial Step to be Processed

NFIRST = 0

Flag Showing Discon. are all Time Events

NTEALL = 0

Flag Showing Time Update Took Place

NTIMUP = 1

Pre-Run Output :

Set up Output Format

WRITE(8,17)

17 FORMAT(1X,'Problem:',19X,'Study Of Bouncing Ball Model')

WRITE(8,79)

79 FORMAT(1X,'Method:',19X,'Discontinuity Processing Algorithm')

+ /30X,'Based On Runge-Kutta Merson'

+ /10X/1X,'Time',6X,'Height',6X,'Velocity')

PRINT *,

TIME(1) = 0.0

YVAL1(1) = 10.0

CALL DISCON(T,Y,TE,N,TFIN,HMIN,DERIV,TOL,NDF)

DO 33 I = 1,NPL

TIME1(I) = TIME(I)

YVAL2(I) = YVAL(I)

YVAL3(I) = YVAL1(I)

33 CONTINUE

Post Run Output

DO 59 I = 1,NPL

WRITE(8,23) TIME(I),YVAL1(I),YVAL(I)

23 FORMAT(1X,F5.3,5X,F8.3,5X,F8.3)

59 CONTINUE

PRINT*, 'VALUE OF D IS',D

CALL ANYDEV

CALL GRAPH(TIME1,YVAL3,NPL)

BAL01210
BAL01220
BAL01230
BAL01240
BAL01250
BAL01260
BAL01270
BAL01280
BAL01290
BAL01300
BAL01310
BAL01320
BAL01330
BAL01340
BAL01350
BAL01360
BAL01370
BAL01380
BAL01390
BAL01400
BAL01410
BAL01420
BAL01430
BAL01440
BAL01450
BAL01460
BAL01470
BAL01480
BAL01490
BAL01500
BAL01510
BAL01520
BAL01530
BAL01540
BAL01550
BAL01560
BAL01570
BAL01580
BAL01590
BAL01600
BAL01610
BAL01620
BAL01630
BAL01640
BAL01650
BAL01660
BAL01670
BAL01680
BAL01690
BAL01700
BAL01710
BAL01720
BAL01730
BAL01740
BAL01750
BAL01760
BAL01770
BAL01780
BAL01790

```

STOP
END

SUBROUTINE DISFUN(Y,T,M,L,DF)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION DF(L),Y(M)
C      This Subprogram is Responsible For Evaluating The Value
C      of The Discontinuity or Switching Function.The User Creates
C      This Module According to His Model.
DF(1)=Y(2)
RETURN
END

SUBROUTINE DERIV(T,Y,DY,N)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(N),DY(N)
COMMON/CON/G
C      This is the derivative evaluation Subroutine where the
C      user should write the model's system derivatives.

DY(1) = -G
DY(2)= Y(1)
RETURN
END

SUBROUTINE GRAPH(TIME1,YVAL3,NPL)
C      This Subroutine Provides A Graphical Display of The
C      BouncingBall Model.Height is plotted against Time.
DIMENSION TIME1(NPL),YVAL3(NPL)
VALMAX = YVAL3(NPL)
VALMIN = YVAL3(1)
DO 13 I = 1,NPL
  IF (YVAL3(I).GT.VALMAX) THEN
    VALMAX = YVAL3(I)
  ELSE IF(YVAL3(I).LT.VALMIN) THEN
    VALMIN = YVAL3(I)
  ENDIF
13 CONTINUE
MAXVAL = VALMAX + 1
MINVAL = VALMIN - 1
SPAC1 = (TIME1(NPL) - TIME1(1))/10.0
SPAC2 = (MAXVAL - MINVAL)/10.0
CALL HWROT('MOVIE')
CALL SWISSM
CALL PAGE(8.5,11.0)
CALL AREA2D(6.0,8.0)
CALL HEADIN('Study Of Bouncing Ball Model$',100,1.5,3)
CALL HEADIN('Discontinuity Processing Algorithm$',100,1.25,3)
CALL HEADIN('Based On RK-Merson$',100,-1.15,3)
CALL XNAME('TIME(sec)',100)
CALL YNAME('Height(m)',100)
CALL GRAF(TIME1(1),SPAC1,TIME1(NPL),0.0,SPAC2,MAXVAL)
C DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C RATIONAL SPLINE INTERPOLATION
CALL RASPLN (1.5)

```

```

BAL01800
BAL01810
BAL01820
BAL01830
BAL05330
BAL05340
BAL05350
BAL05360
BAL05370
BAL05380
BAL05390
BAL05400
BAL05410
BAL05420
BAL05430
BAL05440
BAL05450
BAL05460
BAL05470
BAL05480
BAL05490
BAL05500
BAL05510
BAL05520
BAL05530
BAL05540
BAL05550
BAL07960
BAL07970
BAL07980
BAL07990
BAL08000
BAL08010
BAL08020
BAL08030
BAL08040
BAL08050
BAL08060
BAL08070
BAL08080
BAL08090
BAL08100
BAL08110
BAL08120
BAL08130
BAL08140
BAL08150
BAL08160
BAL08170
BAL08180
BAL08190
BAL08200
BAL08210
BAL08220
BAL08230
BAL08240
BAL08250
BAL08260
BAL08270

```

```

CALL THKCRV (.015)
CALL THKRND (0.)
CALL CURVE(TIME1,YVAL3,NPL,0)
CALL ENDEPL(0)
RETURN
END

```

```

SUBROUTINE OUTPUT(Y,N,T)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(N)
COMMON/DIFF/YVAL(500),TIME(500),YVAL1(500),NPL

```

```

WRITE(6,23) T,Y(2),Y(1)
23 FORMAT(1X,F5.2,3X,F9.3,3X,F9.3)
NPL = NPL + 1
TIME(NPL) = T
YVAL(NPL) = Y(1)
YVAL1(NPL) = Y(2)
RETURN
END

```

```

SUBROUTINE MODUPD(DF,NDF,T,Y,N,TOL)

```

```

C      This subroutine is model dependent and is supplied by
C      the user. It contains all time and state events for
C      the model involved.

```

```

DIMENSION Y(N),DF(N)
COMMON/UPD/C
IF ((DF(1).GE.-TOL) .AND. (DF(1).LE.0)) THEN
    Y(1) = -(C * Y(1))
    Y(2) = 0.0
ENDIF
RETURN
END

```

```

BAL08280
BAL08290
BAL08300
BAL08310
BAL08320
BAL08330
BAL08340
BAL08350
BAL08360
BAL08370
BAL08380
BAL08390
BAL08400
BAL08410
BAL08420
BAL08430
BAL08440
BAL08450
BAL08460
BAL08470
BAL08480
BAL08490
BAL08500
BAL08510
BAL08520
BAL08530
BAL08540
BAL08550
BAL08560
BAL08570
BAL08580
BAL08590
BAL08600
BAL08610
BAL08620
BAL08630
BAL08640

```

Method: Discontinuity Processing Algorithm
Based On Runge-Kutta Merson

Problem: Study Of Bouncing Ball Model

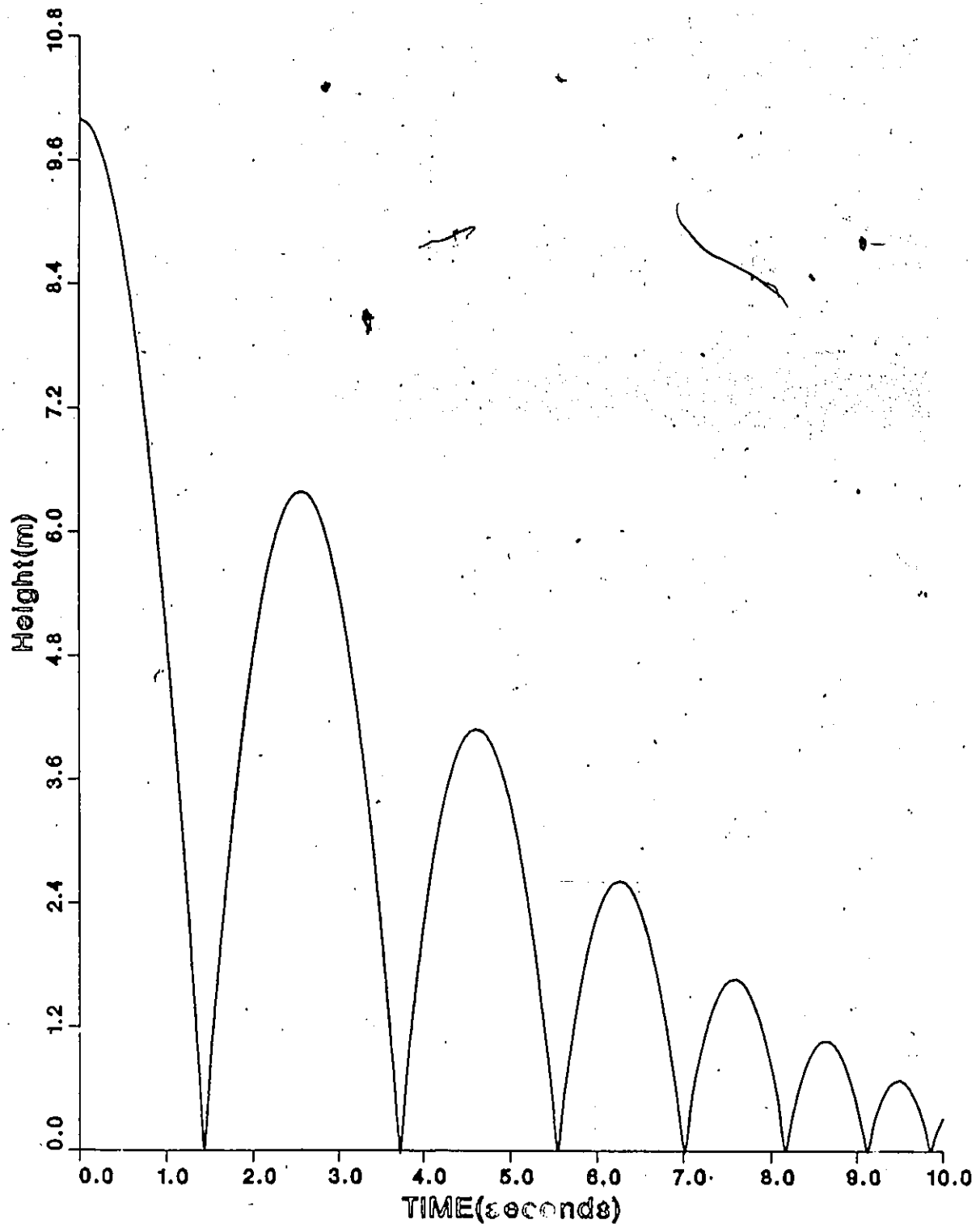
Time (T)	Height (Y2)
0.000	10.000
0.100	9.951
0.200	9.804
0.300	9.559
0.400	9.215
0.500	8.774
0.600	8.235
0.700	7.597
0.800	6.862
0.900	6.028
1.000	5.096
1.100	4.067
1.200	2.939
1.300	1.713
1.400	0.389
1.428	0.000
1.500	0.781
1.600	1.781
1.700	2.684
1.800	3.489
1.900	4.195
2.000	4.804
2.100	5.314
2.200	5.727
2.300	6.041
2.400	6.257
2.500	6.376
2.600	6.396
2.700	6.318
2.800	6.142
2.900	5.868
3.000	5.495
3.100	5.025
3.200	4.457
3.300	3.791
3.400	3.026
3.500	2.164
3.600	1.203
3.700	0.144
3.713	0.000
3.800	0.743
3.900	1.503
4.000	2.169
4.100	2.735
4.200	3.202
4.300	3.572
4.400	3.844
4.500	4.017
4.600	4.092
4.700	4.070
4.800	3.949
4.900	3.730
5.000	3.413
5.100	2.999
5.200	2.486
5.300	1.875
5.400	1.165
5.500	0.358

Method: Discontinuity Processing Algorithm
Based On Runge-Kutta Merson

Problem: Study Of Bouncing Ball Model

Time	Height
5.541	0.000
5.600	0.407
5.700	1.017
5.800	1.529
5.900	1.943
6.000	2.259
6.100	2.476
6.200	2.596
6.300	2.618
6.400	2.541
6.500	2.367
6.600	2.094
6.700	1.723
6.800	1.255
6.900	0.688
7.000	0.023
7.003	0.000
7.100	0.509
7.200	0.939
7.300	1.271
7.400	1.504
7.500	1.640
7.600	1.677
7.700	1.616
7.800	1.458
7.900	1.201
8.000	0.846
8.100	0.393
8.173	0.000
8.200	0.120
8.300	0.503
8.400	0.789
8.500	0.976
8.600	1.065
8.700	1.057
8.800	0.950
8.900	0.745
9.000	0.442
9.100	0.041
9.109	0.000
9.200	0.294
9.300	0.522
9.400	0.653
9.500	0.686

Study Of Bouncing Ball Model
Discontinuity Processing Algorithm
Based On RK-Merson



Appendix. E THE SAFETY PARACHUTE MODEL

E.1 Problem Definition

This model illustrates the use of the discontinuity processing algorithm in the processing of time and state events. The simulation simulates the trajectory of a parachutist starting at a height of 1000m at the point of leaving the aeroplane, to the specific time of popping the parachute at $T = 5$ seconds, to the point when the emergency parachute pops at a height of 900m, and the subsequent descent. The aeroplane is assumed to be flying at a fairly level trajectory before allowing the parachutist to jump. Thus the initial horizontal component of velocity is given to be large as opposed to the upward vertical component of velocity which is very small. The world view taken is that the upward vertical velocity and the easterly horizontal component of velocity, were both positive. The reverse directions were negative. The results displayed by the simulation are as expected. They indicate a drastic reduction in the horizontal component of the velocity and a quick change of an upward to a downward component of velocity in the first second. The horizontal component of velocity continues to fall at a reduced rate while the downward vertical component of velocity increases rapidly and gradually levels off. At the time of the first discontinuity, it is assumed that the parachute fails

opening only partially and hence increasing the drag coefficient slightly. This point occurs at $T = 5$ where the vertical component of velocity decreases only slightly. When the safety parachute is pulled, the drag coefficient increases and the vertical component of velocity reduces sharply. The descent hereafter sees the horizontal component diminish to zero over time with the vertical component stabilizing at a constant velocity until the parachutist finally lands.

E.2 Gtest Specification of The Safety Parachute Model

```

Program StudyOfSafetyParachute.

ContinuousModel SafetyParachute
  StaticStructure
    States Y1,Y2,Y3          (* Y2 Vertical Component of Velocity *)
    Outputs Y1,Y2            (* Y1 Horizontal Component of Velocity *)
    AuxiliaryVariables V      (* V Velocity , Y3 Height *)
    Constants G
      G = 9.807
    EndConstants
    Parameters M,D,TE        (* TE Parachute Opening Time (s)
                              D Drag Coef. (kg/m)
                              M Mass (kg) *)
  EndStaticStructure

  DynamicStructure
    Derivatives
      Y1' = -(D*V*Y1)/M
      Y2' = -G-(D*V*Y2)/M
      V = Sqrt(Y1**2+Y2**2)
      Y3' = Y2
    EndDerivatives
    Updates
      When Time = TE
        D = 1.5          (* Update of parameter *)
      When Y3 = 900
        D = 7.0          (* Update of parameter *)
    EndUpdates
  EndDynamicStructure
EndModel SafetyParachute

ParameterSet 1
  Model Parachute
    Parameters
      TE = 5.0
      M = 70
      D = 0.7
    EndParameters
  EndModel Parachute
EndParameterSet1

Experiment 1
  TimeUnitIs Second
  InitialStates
    Y1 = 800.0
    Y2 = 10.0
    Y3 = 1000.0
  EndInitialStates
  IntegrateBy Discontinuity Algorithm
  Communicate at every 0.3 Second
  Display OutputModule 1 on Screen and on LaserQMS
  SimulateUntil Time = 20.0
EndExperiment 1

```

Run 1
 ToObserve Parachute
 WithParameterSet 1
 InExperiment 1
EndRun 1

OutputModule 1
 NewPage
 Heading ForFirstPage 1 Line
 StudyofSafetyParachute
 PlotandList Y1,Y2,Y3 Versus Time
EndOutputModule 1

EndProgram StudyOfFaultyParachute

C	E.3	Equivalent Fortran Program With Results	SAF00010
C		For Safety Parachute Model	SAF00020
			SAF00030
			SAF00040
			SAF00050
			SAF00060
			SAF00070
			SAF00080
			SAF00090
			SAF00100
			SAF00110
			SAF00120
			SAF00130
			SAF00140
			SAF00150
			SAF00160
			SAF00170
			SAF00180
			SAF00190
			SAF00200
			SAF00210
			SAF00220
			SAF00230
			SAF00240
			SAF00250
			SAF00260
			SAF00270
			SAF00280
			SAF00290
			SAF00300
			SAF00310
			SAF00320
			SAF00330
			SAF00340
			SAF00350
			SAF00360
			SAF00370
			SAF00380
			SAF00390
			SAF00400
			SAF00410
			SAF00420
			SAF00430
			SAF00440
			SAF00450
			SAF00460
			SAF00470
			SAF00480
			SAF00490
			SAF00500
			SAF00510
			SAF00520
			SAF00530
			SAF00540
			SAF00550
			SAF00560
			SAF00570
			SAF00580
			SAF00590
			SAF00600
			SAF00610
			SAF00620
			SAF00630
			SAF00640

C		Variable List	
C			
C	Input	: N	--Dimension of the Vector of State Variables
C			
C		NDF	--Dimension of the Vector of Discontinuity Functions
C			
C		Y(1)-Y(N)	--Initial Values of State Variables
C			
C		G	--Constant used in differential equation for V
C			
C		K	--Constant used in Model Update
C			
C		T	--Computational Time
C			
C		TINIT	--Initial Time Of Simulation
C			
C		TFIN	--End Time of Simulation
C			
C		TCOM	--Communication Time
C			
C		COMINT	--Communication Interval
C			
C		TE	--Vector Of Times At Which Time Events Occur
C			
C		THOR	--Horizon Time
C			
C		H	--Integration Step Size
C			
C		HINIT	--Starting Integration Step Size
C			
C		HMAX	--Maximum step size integration is allowed to proceed at
C			
C		HBOUND	--Upper Bound On Initial Step Size
C			
C		HMIN	--Minimum step size integration is allowed to proceed at
C			
C		TOL	--Tolerance or Accuracy specified by user
C			
C		NORD	--Order of the Integration Method
C			
C	COUTPUT	:T	--Vector of times of Output Values
C			
C		YVAL(N)	--Vector of Output at Output Points
C			
C		YVAL1(N)	--Vector of Output at Output Points
C			
C	CPROGRAM	VARIABLES :	
C		Y(N)	--State Variables Vector
C			
C		DY(N)	--Derivative Vector of State Variables
C			
C		ER(N)	--Vector of Local Error Estimates
C			
C		ERMAX	--Variable containing Maximum Error

C	HPOS	--Intermediate variable used in determining HINIT	SAF00650
C	NPL	--Counter used for Graphics Routine	SAF00660
C			SAF00670
C	YVAL, TIME	--Single Precision copies of output Vectors needed to run Disspla Graphics Package	SAF00680
C			SAF00690
C	YLAST(N)	--Last Values of State Variables	SAF00700
C			SAF00710
C	DF(DDF)	--Present Values of Discontinuity Functions	SAF00720
C			SAF00730
C	PDF(DDF)	--Previous Values of Discontinuity Functions	SAF00740
C			SAF00750
C	F(10,5)	--Working Arrays used in Aitken Interpolation Table	SAF00760
C			SAF00770
C	TS(10,10)	--Working Arrays used in Aitken Interpolation Table	SAF00780
C			SAF00790
C	NUM	--Identifies the Discontinuity Function which has changed its sign in the preceding Step	SAF00800
C			SAF00810
C	NOT	--A Flag used to indicate whether the value of the Discontinuity Function is within the Tolerance Limit	SAF00820
C			SAF00830
C	NUMTE	--Number of Time Events	SAF00840
C			SAF00850
C	ITER	--Iteration Number	SAF00860
C			SAF00870
C	NPL	--Counter for plot of Output	SAF00880
C			SAF00890
C	NTIMEV	--Flag Showing Time Event Taking Place	SAF00900
C			SAF00910
C	NFIRST	--Flag Showing Initial Step to be Processed	SAF00920
C			SAF00930
C	NTEALL	--Flag Showing Discon. are all Time Events	SAF00940
C			SAF00950
C	NTIMUP	--Flag Showing Time Update took place	SAF00960
C			SAF00970
C			SAF00980
C			SAF00990
C			SAF01000
C			SAF01010
C			SAF01020
C			SAF01030
C			SAF01040
C			SAF01050
C			SAF01060
C			SAF01070
C			SAF01080
C			SAF01090
C			SAF01100
C			SAF01110
C			SAF01120
C			SAF01130
C			SAF01140
C			SAF01150
C			SAF01160
C			SAF01170
C			SAF01180
C			SAF01190
C			SAF01200
C			SAF01210
C			SAF01220
C			SAF01230
C			SAF01240
C			SAF01250
C			SAF01260
C			SAF01270
C			SAF01280
C			SAF01290
C			SAF01300

Variable Declaration.

```

IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(5), TE(5)
REAL*4 TIME1(500), YVAL2(500), YVAL3(500), YVAL4(500)
COMMON/DIFF/YVAL(500), TIME(500), YVAL1(500), Y4(500), NPL
COMMON/FLAG/NUMTE, NTIMEV, NFIRST, NTEALL
COMMON/DER/D, G, M
COMMON/WHY/COMINT, NOUT, NTIMUP
COMMON/INTEG/NORD
EXTERNAL DERIV

```

Initialization

Initialize Constants

```

M      = 70.
G      = 9.807D0
D      = 0.7

```

Initialize State Variables

```

Y(1) = 800.0
Y(2) = 10.0
Y(3) = 1000.0

```

Initialize Run Control Variables

```

T      = 0.0-
TFIN   = 20.0
TE(1)  = 5.0

```

```

C      TE(2) = 7.02
      COMINT = 0.3
      HMIN  = 0.0000001
      TOL   = 0.00001
      NORD  = 4
      NDF   = 1
      N     = 3
      NPL   = 1
      NUMTE = 1
C
C      FLAG SHOWING TIME EVENT TAKING PLACE
      NTIMEV = 0
C
C      FLAG SHOWING INITIAL STEP TO BE PROCESSED
      NFIRST = 0
C
C      FLAG SHOWING DISCON. ARE ALL TIME EVENTS
      NTEALL = 0
C
C      FLAG SHOWING TIME UPDATE TOOK PLACE
      NTIMUP = 1
C
C      Pre-Run Output :
      Set up Output Format
C
      WRITE(8,17)
17  FORMAT(1X,'Problem:',1X,'Study Of Safety Parachute Model'
+ /13X,'Time And State Events')
      WRITE(8,11)
11  FORMAT(1X,'Method:',1X,'Discontinuity Processing Algorithm')
C
      PRINT *, '
C
      TIME(1) = 0.0
      YVAL(1) = 800.0
      YVAL1(1) = 10.0
      Y4(1) = 1000.0
      CALL DISCON(T,Y,TE,N,TFIN,HMIN,DERIV,TOL,NDF)
C
      DO 33 I = 1,NPL
        TIME1(I) = TIME(I)
        YVAL2(I) = YVAL(I)
        YVAL3(I) = YVAL1(I)
        YVAL4(I) = Y4(I)
33  CONTINUE
C
C      Post Run Output
      DO 59 I = 1,NPL
        WRITE(8,23) TIME(I),YVAL(I),YVAL1(I),Y4(I)
23  FORMAT(1X,F6.2,5X,F8.3,5X,F8.3,5X,F8.3)
59  CONTINUE
C
      PRINT*, 'VALUE OF D IS',D
      CALL ANYDEV
      CALL GRAPH(TIME1,YVAL3,NPL)
      CALL GRAPH(TIME1,YVAL2,NPL)
      CALL GRAPH(TIME1,YVAL4,NPL)
      STOP
      END
C
      SUBROUTINE DISFUN(Y,T,M,L,DF)
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION DF(L),Y(M)
C      This subprogram is responsible for evaluating the value
C      of the discontinuity or switching function. The user creates
C      this module according to his model.
C
      DF(1) = Y(3) - 900
      RETURN

```

SAF01310
SAF01320
SAF01330
SAF01340
SAF01350
SAF01360
SAF01370
SAF01380
SAF01390
SAF01400
SAF01410
SAF01420
SAF01430
SAF01440
SAF01450
SAF01460
SAF01470
SAF01480
SAF01490
SAF01500
SAF01510
SAF01520
SAF01530
SAF01540
SAF01550
SAF01560
SAF01570
SAF01580
SAF01590
SAF01600
SAF01610
SAF01620
SAF01630
SAF01640
SAF01650
SAF01660
SAF01670
SAF01680
SAF01690
SAF01700
SAF01710
SAF01720
SAF01730
SAF01740
SAF01750
SAF01760
SAF01770
SAF01780
SAF01790
SAF01800
SAF01810
SAF01820
SAF01830
SAF01840
SAF01850
SAF01860
SAF05340
SAF05350
SAF05360
SAF05370
SAF05380
SAF05390
SAF05400
SAF05410
SAF05420
SAF05430

END

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SUBROUTINE DERIV(T,Y,DY,N)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(N),DY(N)
COMMON/DER/D,G,M

This is the derivative evaluation
subroutine where the user should
write the model's system derivatives.

V = SQRT(Y(1)*Y(1)+Y(2)*Y(2))
DY(1) = -(D*V*Y(1))/M
DY(2) = -G - (D*V*Y(2))/M
DY(3) = Y(2)
RETURN
END

SUBROUTINE GRAPH(TIME1,YVAL3,NPL)

This Subroutine Provides A Graphical Display of The
Bouncing Ball Model. Height is plotted against Time.

DIMENSION TIME1(NPL),YVAL3(NPL)

VALMAX = YVAL3(NPL)

VALMIN = YVAL3(1)

DO 13 I = 1,NPL

IF (YVAL3(I).GT.VALMAX) THEN

VALMAX = YVAL3(I)

ELSE IF (YVAL3(I).LT.VALMIN) THEN

VALMIN = YVAL3(I)

ENDIF

13 CONTINUE

MAXVAL = VALMAX + 1

MINVAL = VALMIN - 1

SPAC1 = (TIME1(NPL) - TIME1(1))/10.0

SPAC2 = (MAXVAL - MINVAL)/10.0

CALL HWROT('MOVIE')

CALL SWISSM

CALL PAGE(8.5,11.0)

CALL AREA2D(6.0,8.0)

CALL HEADIN('Study Of Safety Parachute Model\$',100,1.5,3)

CALL HEADIN('Discontinuity Processing Algorithm\$',100,1.25,3)

CALL HEADIN('Based On RK-Merson\$',100,-1.15,3)

CALL XNAME('Time (seconds) \$',100)

CALL YNAME('Height (m) \$',100)

CALL GRAF(TIME1(1),SPAC1,TIME1(NPL),MINVAL,SPAC2,MAXVAL)

C DRAW CURVE WITH ROUNDED AND THICKENED LINE AND

C RATIONAL SPLINE INTERPOLATION

CALL RASPLN (1.5)

CALL THKCRV (.015)

CALL THKRND (0.)

CALL CURVE(TIME1,YVAL3,NPL,0)

CALL ENDPL(0)

RETURN

END

SUBROUTINE OUTPUT(Y,N,T)

IMPLICIT REAL*8 (A-H,O-Z)

DIMENSION Y(N)

COMMON/DIFF/YVAL(500),TIME(500),YVAL1(500),Y4(500),NPL

WRITE(6,23) T,Y(2),Y(1)

23 FORMAT(1X,F5.2,3X,F9.3,3X,F9.3)

SAF05440
SAF05450
SAF05460
SAF05470
SAF05480
SAF05490
SAF05500
SAF05510
SAF05520
SAF05530
SAF05540
SAF05550
SAF05560
SAF05570
SAF05580
SAF05590
SAF05600
SAF05610
SAF05620
SAF08020
SAF08030
SAF08040
SAF08050
SAF08060
SAF08070
SAF08080
SAF08090
SAF08100
SAF08110
SAF08120
SAF08130
SAF08140
SAF08150
SAF08160
SAF08170
SAF08180
SAF08190
SAF08200
SAF08210
SAF08220
SAF08230
SAF08240
SAF08250
SAF08260
SAF08270
SAF08280
SAF08290
SAF08300
SAF08310
SAF08320
SAF08330
SAF08340
SAF08350
SAF08360
SAF08370
SAF08380
SAF08390
SAF08400
SAF08410
SAF08420
SAF08430
SAF08440
SAF08450
SAF08460
SAF08470
SAF08480

```
NPL = NPL + 1
TIME(NPL) = T
YVAL(NPL) = Y(1)
YVAL1(NPL) = Y(2)
Y4(NPL) = Y(3)
RETURN
END
```

```
SUBROUTINE MODUPD(DF,NDF,T,Y,N,TOL)
```

```
C      This subroutine is model dependent and is supplied by
C      the user. It contains all time and state events for
C      the model involved.
```

```
DIMENSION Y(N),DF(N)
COMMON/DER/D,G,M
```

```
IF (T.EQ.5.0) THEN
  D = 1.5
ENDIF
```

```
IF ((DF(1).GE.-TOL ) .AND. (DF(1).LE.0 )) THEN
  D = 7.0
ENDIF
RETURN
END
```

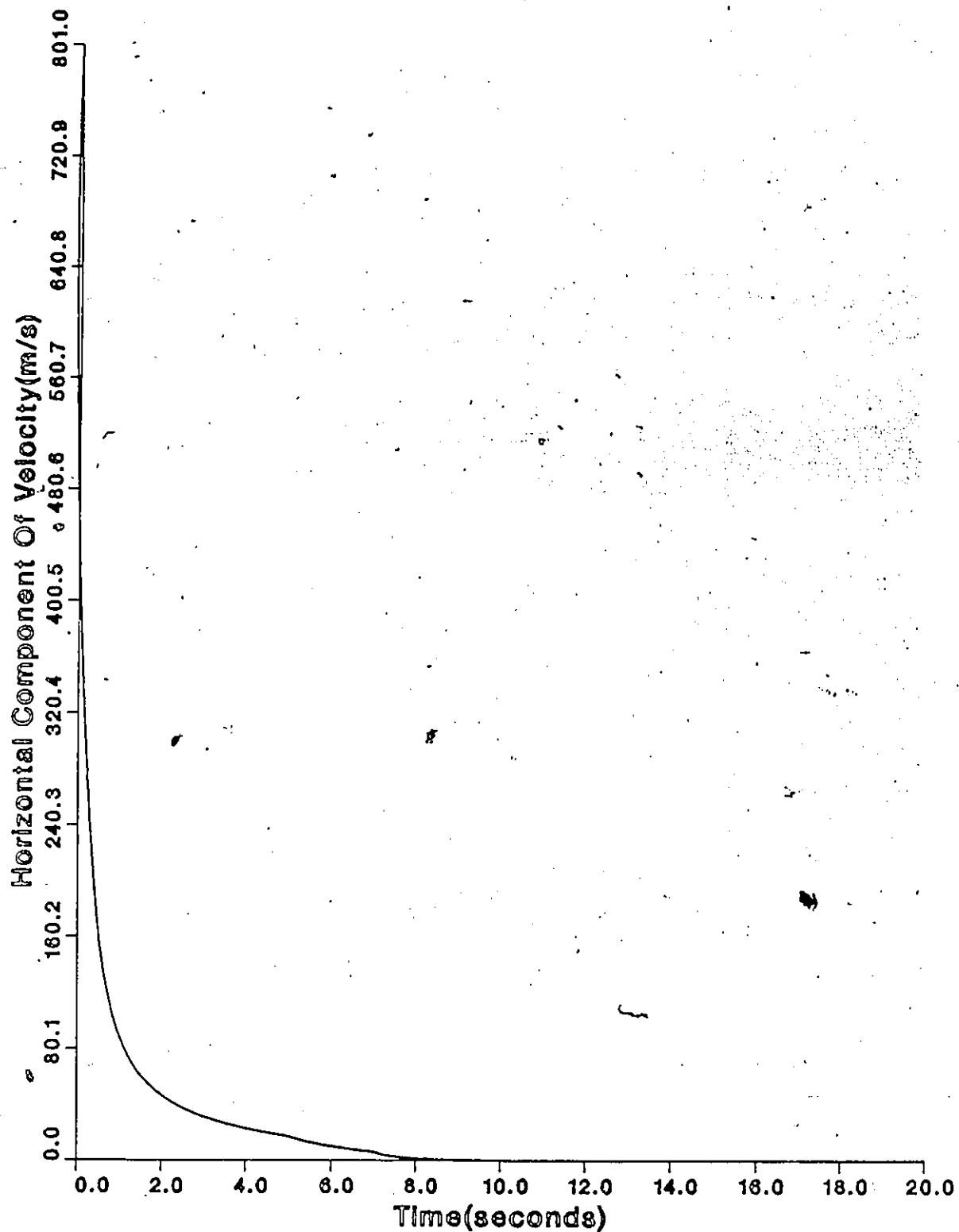
```
SAF08490
SAF08500
SAF08510
SAF08520
SAF08530
SAF08540
SAF08550
SAF08560
SAF08570
SAF08580
SAF08590
SAF08600
SAF08610
SAF08620
SAF08630
SAF08640
SAF08650
SAF08660
SAF08670
SAF08680
SAF08690
SAF08700
SAF08710
SAF08720
SAF08730
SAF08740
```

Problem: Study Of Safety Parachute Model
Time And State Events

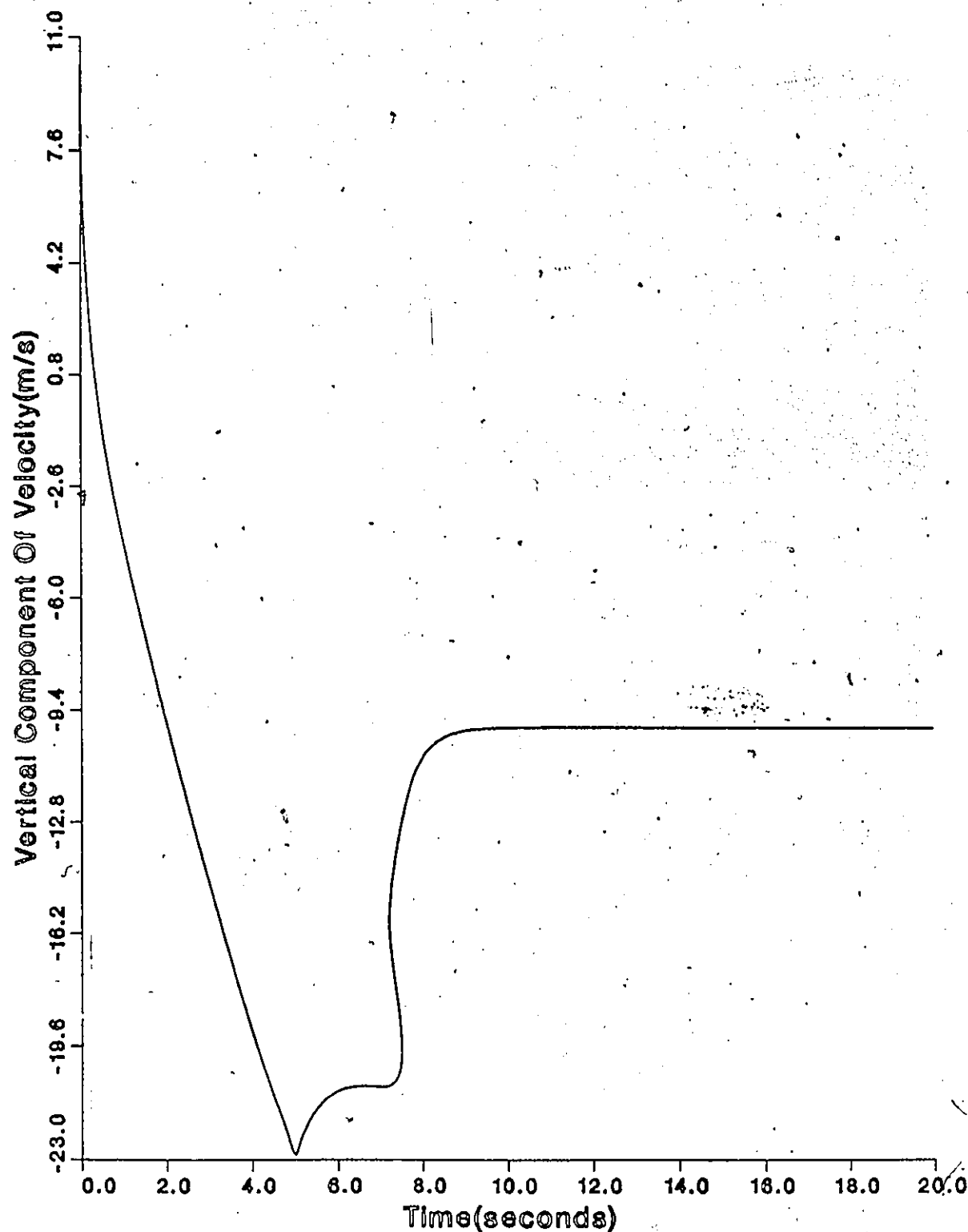
Method: Discontinuity Processing Method

Time (T)	Velocity (Y1)	Velocity (Y2)	Height (Y3)
0.00	800.000	10.000	1000.000
0.30	235.299	1.038	1001.219
0.60	137.933	-1.725	1001.082
0.90	97.553	-3.732	1000.254
1.20	75.440	-5.494	998.866
1.50	61.467	-7.146	996.968
1.80	51.816	-8.735	994.585
2.10	44.726	-10.280	991.731
2.40	39.275	-11.789	988.420
2.70	34.928	-13.263	984.661
3.00	31.359	-14.699	980.466
3.30	28.355	-16.091	975.846
3.60	25.773	-17.433	970.816
3.90	23.516	-18.718	965.392
4.20	21.513	-19.940	959.592
4.50	19.716	-21.091	953.435
4.80	18.088	-22.169	946.944
5.00	17.083	-22.844	942.442
5.10	16.086	-22.463	940.178
5.40	13.565	-21.650	933.571
5.70	11.566	-21.181	927.154
6.00	9.937	-20.928	920.841
6.30	8.581	-20.811	914.583
6.60	7.436	-20.776	908.347
6.90	6.459	-20.791	902.112
7.00	6.161	-20.804	900.000
7.20	4.244	-15.968	896.412
7.50	2.745	-12.734	892.178
7.80	1.906	-11.318	888.597
8.10	1.368	-10.632	885.316
8.40	0.998	-10.284	882.185
8.70	0.735	-10.103	879.130
9.00	0.543	-10.009	876.114
9.30	0.402	-9.959	873.120
9.60	0.299	-9.932	870.137
9.90	0.222	-9.919	867.159
10.20	0.165	-9.911	864.185
10.50	0.122	-9.907	861.212
10.80	0.091	-9.905	858.240
11.10	0.067	-9.904	855.269
11.40	0.050	-9.904	852.298
11.70	0.037	-9.903	849.327
12.00	0.028	-9.903	846.356
12.30	0.021	-9.903	843.385
12.60	0.015	-9.903	840.414
12.90	0.011	-9.903	837.443
13.20	0.008	-9.903	834.472
13.50	0.006	-9.903	831.501
13.80	0.005	-9.903	828.530
14.10	0.003	-9.903	825.559
14.40	0.003	-9.903	822.588
14.70	0.002	-9.903	819.618
15.00	0.001	-9.903	816.647
15.30	0.001	-9.903	813.676
15.60	0.001	-9.903	810.705
15.90	0.001	-9.903	807.734
16.20	0.000	-9.903	804.763
16.50	0.000	-9.903	801.792
16.80	0.000	-9.903	798.821
17.10	0.000	-9.903	795.850
17.40	0.000	-9.903	792.879
17.70	0.000	-9.903	789.908
18.00	0.000	-9.903	786.938
18.30	0.000	-9.903	783.967
18.60	0.000	-9.903	780.996
18.90	0.000	-9.903	778.025
19.20	0.000	-9.903	775.054
19.50	0.000	-9.903	772.083
19.80	0.000	-9.903	769.112
20.00	0.000	-9.903	767.132

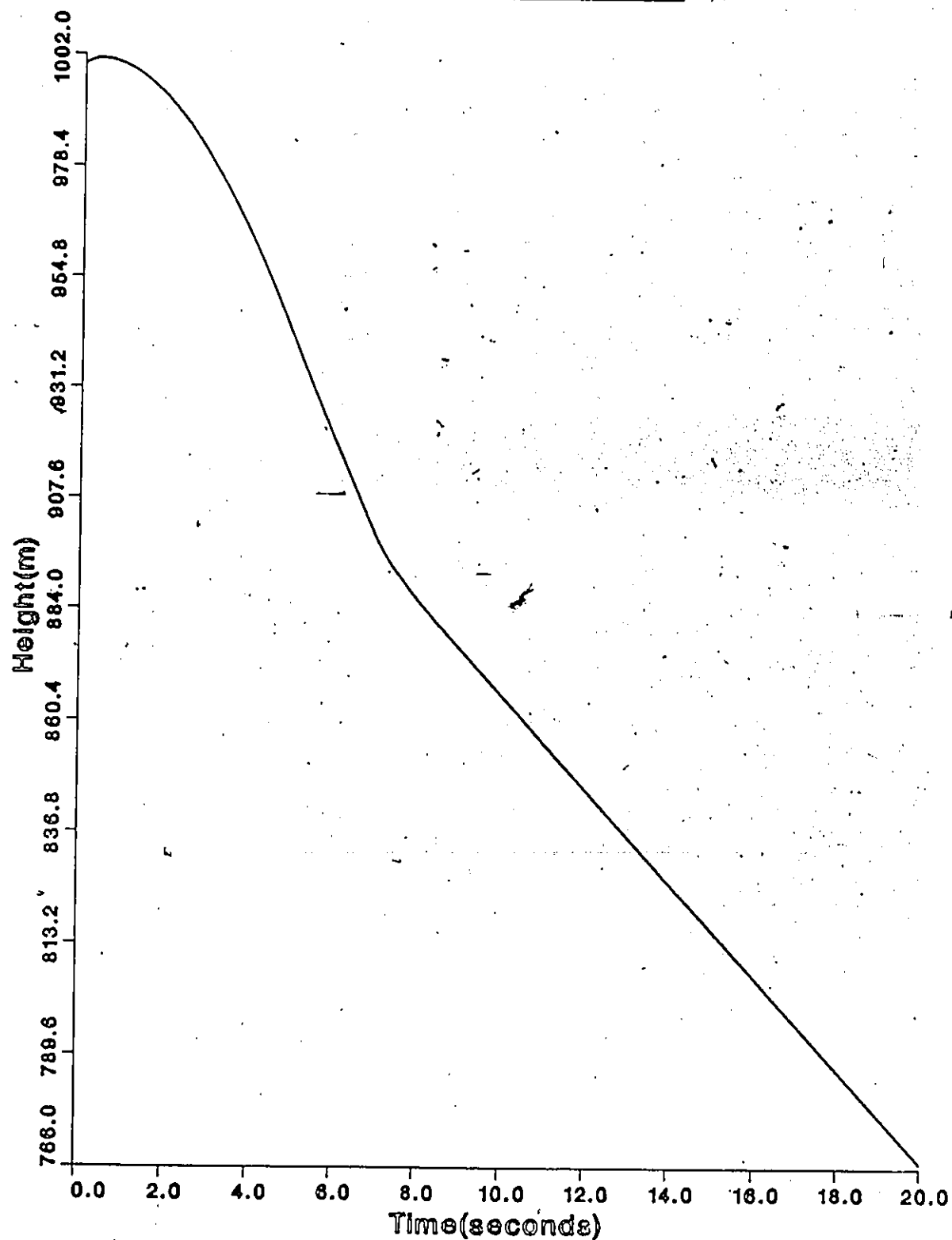
Study Of Safety Parachute Model
Discontinuity Processing Algorithm
Based On RK-Merson



Study Of Safety Parachute Model
Discontinuity Processing Algorithm
Based On RK-Merson



Study Of Safety Parachute Model
Discontinuity Processing Algorithm
Based On RK-Merson



Appendix. F THE TREE BIOMASS MODEL

F.1 Problem Description

This simulation is fully described by Goldstein and Harris (1973). It is a deterministic model to simulate tree biomass dynamics of a closed canopy, forested watershed on a year to year basis. The model is conceived on the basis of measurable forest processes influencing change in biomass. Trees are divided into three size classes: 1.3-8.8, 8.9-23.8 and >23.8 dbh (diameter at breast height) and the resulting coupling between the different compartments is as shown in Figure F.1. The live above ground biomasses are designated Y1, Y2 and Y3 respectively. There are three variables Y4, Y5 and Y6 for the three size classes of standing dead material and Y7 is the total live root biomass in all the classes. The equations defining the rate of change of these variables and all other model information is shown in the Gest specification in section F.2. The simulation is carried out over a 300 year period with the following initial conditions for each sector Y1: 10000, 30000, 60000, 2500, 2000 and 32000 (measured in kilograms per hectare). The results are similar to those shown in the article by Goldstein and Harris (1973).

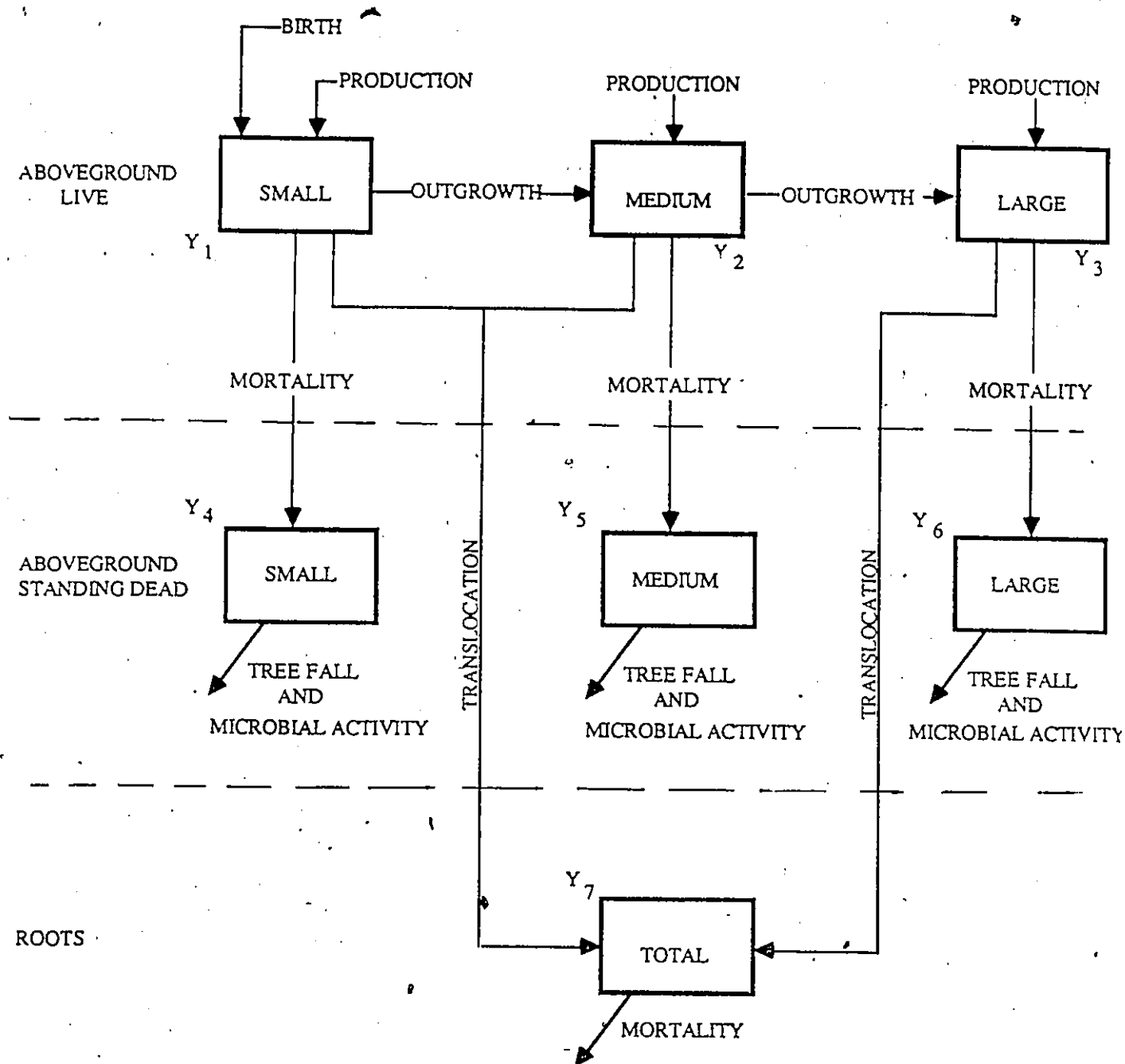


Figure F.1 Schematic diagram depicting compartments and transfers of nonfoliar biomass for SERENDIPITY

F.2 Gest Specification of The Tree Biomass Model

Program StudyOfTreeBiomassDynamics .

CoupledModel ForestBiomass

ComponentModels

LiveAbovegroundBiomass

StandingDeadCompartments

RootBiomass

EndComponentModels

ContinuousModel LiveAbovegroundBiomass

StaticStructure

States

Y1,

(* Live Aboveground Biomass of the
small size class *)

Y2,

(* Live Aboveground Biomass of the
medium size class *)

Y3

(* Live Aboveground Biomass of the
large size class *)

Outputs

Y1,

Y2,

Y3,

BIOSUM

(* Total Aboveground_Biomass *)

AuxiliaryVariables

PY2[3],

(* Live Aboveground_Biomass of the
medium size class in the last
3 consecutive years *)

PY3[3]

(* Live Aboveground_Biomass of the
large size class in the last
3 consecutive years *)

Parameters

ProdS,

(* Production rate in small size
class *)

ProdM,

(* Production rate in medium size
class *)

ProdL,

(* Production rate in large size
class *)

OutgS,

(* Outgrowth from small size class *)

OutgM,

(* Outgrowth from medium size class *)

OutgL,

(* Outgrowth from large size class *)

MortS,

(* Mortality from small size class *)

MortM,

(* Mortality from medium size class *)

MortL,

(* Mortality from large size class *)

YMAX,

(* Maximum Aboveground_Live_Biomass
Density *)

I

(* Ingrowth rate coefficient *)

EndStaticStructure

DynamicStructure

Derivatives

$$Y1' = (ProdS - OutgS) * Y1 * (1 - (Y1 + Y2 + Y3)/YMAX) - MortS * Y1 * (1 + (Y1 + Y2 + Y3)/YMAX) + I * (PY2[3] + PY3[3]) * (1 - (Y1 + Y2 + Y3)/YMAX)$$

$$Y2' = (ProdM - OutgM) * Y2 * (1 - (Y1 + Y2 + Y3)/YMAX) - MortM * Y2 * (1 + (Y1 + Y2 + Y3)/YMAX) + OutgS * Y1 * (1 - (Y1 + Y2 + Y3)/YMAX)$$

$$Y3' = ProdS * Y3 * (1 - (Y1 + Y2 + Y3)/YMAX) - MortL * Y3 * (1 + (Y1 + Y2 + Y3)/YMAX) + OutgM$$

$$*Y2 * (1 - (Y1 + Y2 + Y3)/YMAX)$$

```

PY2[3] = PY2[2]
PY2[2] = PY2[1]
PY2[1] = Y2
PY3[3] = PY3[2]
PY3[2] = PY3[1]
PY3[1] = Y3

```

```

EndDerivatives
OutputFunctions
  BIOSUM = Y1 + Y2 + Y3
EndOutputFunctions
EndDynamicStructure
EndModel LiveAbovegroundBiomass

```

ContinuousModel StandingDeadCompartments

StaticStructure

Inputs

Y1,
Y2,
Y3

States

Y4,

(* Standing dead material for small
size class *)

Y5,

(* Standing dead material for medium
size class *)

Y6

(* Standing dead material for large
size class *)

Outputs

Y4,
Y5,
Y6

Parameters

MortS,
MortM,
MortL,
YMAX,
MdS,

(* Microbial decay rate of 'small'
standing dead *)

MdM,

(* Microbial decay rate of 'medium'
standing dead *)

MdL,

(* Microbial decay rate of 'large'
standing dead *)

FfmS,

(* Movement small standing dead to
forest floor *)

FfmM,

(* Movement medium standing dead to
forest floor *)

FfmL

(* Movement large standing dead to
forest floor *)

EndStaticStructure

DynamicStructure

Derivatives

$$Y4' = MortS * Y1 * (1 + (Y1 + Y2 + Y3)/YMAX) - (MdS + FfmS) * Y4$$

$$Y5' = MortM * Y2 * (1 + (Y1 + Y2 + Y3)/YMAX) - (MdM + FfmM) * Y5$$

$$Y6' = MortL * Y3 * (1 + (Y1 + Y2 + Y3)/YMAX) - (MdL + FfmL) * Y6$$

EndDerivatives

EndDynamicStructure

EndModel StandingDeadCompartments

ContinuousModel RootBiomass

StaticStructure

Inputs

Y1,
Y2,
Y3,
BIOSUM,
PY2[3],
PY3[3]

States

Y7

(* Total live root biomass in all
dbh classes *)

Outputs

Y7,

Ratio

(* Root/Shoot Ratio *)

Parameters

MortS,
MortM,
MortL,
YMAX,
ProdS,
ProdM,
ProdL,
I,
RT,
E

(* Root Turnover *)

(* Ratio of biomass translocated to
the roots to aboveground prodn. *)

EndStaticStructure

DynamicStructure

Derivatives

$$Y7' = E * (ProdS*Y1 + ProdM*Y2 + ProdL*Y3 + I * \\ (PY2[3] + PY3[3]) * (1 - (Y1 + Y2 + Y3)/YMAX) - \\ (MortS*Y1 + MortM*Y2 + MortL*Y3) * (1 + \\ (Y1 + Y2 + Y3)/YMAX) * (Y7/(Y1 + Y2 + Y3))) - RT*Y7$$

EndDerivatives

OutputFunctions

Ratio = Y7/BIOSUM

EndOutputFunctions

EndDynamicStructure

EndModel RootBiomass

InternalCoupling

RootBiomass.Y1 <-- LiveAbovegroundBiomass.Y1
RootBiomass.Y2 <-- LiveAbovegroundBiomass.Y2
RootBiomass.Y3 <-- LiveAbovegroundBiomass.Y3
RootBiomass.PY2[3] <-- LiveAbovegroundBiomass.PY2[3]
RootBiomass.PY3[3] <-- LiveAbovegroundBiomass.PY3[3]
StandingDeadCompartments.Y1 <-- LiveAbovegroundBiomass.Y1
StandingDeadCompartments.Y2 <-- LiveAbovegroundBiomass.Y2
StandingDeadCompartments.Y3 <-- LiveAbovegroundBiomass.Y3

EndInternalCoupling

ParameterSet 1

Model LiveAbovegroundBiomass

Parameters

ProdS = 0.12
ProdM = 0.05
ProdL = 0.03
OutgS = 0.10
OutgM = 0.025
MortS = 0.020
MortM = 0.010
MortL = 0.005
I = 0.001
YMAX = 400000

EndParameters

Model StandingDeadCompartments
Parameters

MdS = 0.0001
MdM = 0.0001
MdL = 0.0001
FfmS = 0.2000
FfmM = 0.2000
FfmL = 0.2000
MortS = 0.0200
MortM = 0.0100
MortL = 0.0050
YMAX = 400000

EndParameters

EndModel StandingDeadCompartments

Model RootBiomass

Parameters

ProdS = 0.12
ProdM = 0.05
ProdL = 0.03
MortS = 0.020
MortM = 0.010
MortL = 0.005
I = 0.001
RT = 0.266
E = 2.0
YMAX = 400000

EndParameters

EndModel RootBiomass

EndParameterSet 1

Experiment 1

TimeUnitIs Year

StartTime = 0.0

IntegrateBy Runge-KuttaFehlberg

Tol = 0.000001

Communicate at every 3 Years

SimulateUntil Time = 300.0

Model LiveAbovegroundBiomass

InitialStates

Y1 = 10000.0
Y2 = 30000.0
Y3 = 60000.0
PY2[1] = 30000.0
PY2[2] = 30000.0
PY2[3] = 30000.0
PY3[1] = 60000.0
PY3[2] = 60000.0
PY3[3] = 60000.0

EndInitialStates

SaveOutputs Y1,Y2,Y3,BIOSUM

EndModel LiveAbovegroundBiomass

Model StandingDeadCompartments

InitialStates

Y4 = 2500.0
Y5 = 2000.0
Y6 = 2000.0

EndInitialStates

SaveOutputs Y4,Y5,Y6

EndModel StandingDeadCompartments

Model RootBiomass

InitialStates

Y7 = 32000.0

EndInitialStates

SaveOutputs Y7,RATIO
EndModel RootBiomass
EndExperiment 1

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Run 1
 ToObserve ForestBiomass
 WithParameterSet 1
 InExperiment 1
 WithPostRun
 OutputModule 1 On Printer
 OutputModule 2 On Printer
 OutputModule 3 On Printer
 EndPostRun
EndRun 1

OutputModule 1
 New Page
 Heading ForFirstPage 1 Line
 - 'Study of Aboveground_Live_Compartments'
 List Parameters And InitialConditions
 PlotandList Y1,Y2,Y3
EndOutputModule 1

OutputModule 2
 New Page
 Heading ForFirstPage 1 Line
 'Study of Aboveground_Standing_Dead_Compartments'
 PlotandList Y4,Y5,Y6
EndOutputModule 2

OutputModule 3
 New Page
 Heading ForFirstPage 1 Line
 'Study of Root_Biomass'
 List Y7,BIOSUM,RATIO
EndOutputModule 3
EndProgram StudyOfTreeBiomassDynamics

C F.3 Equivalent Fortran Program With Results
C For Tree Biomass Model

Variable List

C Input : N --Dimension of the Vector of State Variables
C Y(1)-Y(N) --Initial Values of State Variables
C T --Computational Time
C TINIT --Initial Time of Simulation
C TFIN --End Time of Simulation
C TCOM --Communication Time
C COMINT --Communication Interval
C
C H --Current Integration Step Size
C HINIT --Starting Integration Step Size
C HBOUND --Upper Bound on Initial Step Size
C HMIN --Minimum step size integration is
C Variable List
C
C TOL --Tolerance or Accuracy specified by user
C
C Output : TIME --Vector of times of Output Values
C Y(1)-Y(7) --Vector of values of Y at Output Points
C BIOSUM --Total Aboveground Production of Biomass
C RATIO --Biomass Transported to Biomass Production
C
C Program Variables :
C Y(N) --State Variables Vector
C DY(N) --Derivative Vector of State Variables
C DY1(15)-DY4(15) --Working Vectors in Integration Routine
C capable of Integration systems with up
C to 15 state variables.
C F1(15)-F3(15) --Working Vectors in Integration Routine
C capable of Integrating systems with up
C to 15 state variables.
C
C NFLAG --Flag Which Signals Collection of Output
C Variables.
C
C HPOS --Intermediate variable used in computing HINIT

C	NPL	--Counter used for Graphics Routine.	RKB00630
C			RKB00640
C	FDER	--Maximum value of derivative functions at	RKB00650
C		initial time	RKB00660
C			RKB00670
C	This Test Program Demonstrates the use of the Fourth		RKB00680
C	Order Runge-Kutta Integration Algorithm in the		RKB00690
C	Simulation of Coupled Model Tree Biomass		RKB00700
			RKB00710
	PROGRAM MAIN		RKB00720
	IMPLICIT REAL*4 (A-H,O-Z)		RKB00730
	DIMENSION Y(10),DY(10),ERR(10)		RKB00740
	COMMON/DIFF/TIME(400),Y1(400),Y2(400),Y3(400),Y4(400),Y5(400)		RKB00750
	COMMON/DIFF1/Y6(400),Y7(400),BIO(400),RAT(400)		RKB00760
	COMMON/PARS/DMORTS,DMORTM,DMORTL,YMAX,DMS,DMDM,DMDL,FFMS,FFMM		RKB00770
	COMMON/PARS1/PRODS,PRODM,PRODL,DI,RT,E,OUTGS,OUTGM,FFML,H		RKB00780
	COMMON/COUNT/NK,PREVY2,PREVY3,P2(3),P3(3)		RKB00790
	COMMON/GRA/NPL		RKB00800
	COMMON/XMEN/PU(32)		RKB00810
	CHARACTER*1 CHOICE		RKB00820
	EXTERNAL DERIV		RKB00830
			RKB00840
	PRINT*,'Welcome to the Tree Biomass Model'		RKB00850
	PRINT*,' '		RKB00860
	PRINT*,'Would You Like To Perform a Simulation ? (Y/N) '		RKB00870
	READ*, CHOICE		RKB00880
	IF (CHOICE .EQ. 'Y') THEN		RKB00890
	CALL INIT		RKB00900
			RKB00910
			RKB00920
		Initialization from Menu	RKB00930
			RKB00940
		Initialize Parameters	RKB00950
			RKB00960
199	DMORTS = PU(1)		RKB00970
	DMORTM = PU(2)		RKB00980
	DMORTL = PU(3)		RKB00990
	YMAX = PU(4)		RKB01000
	DMS = PU(5)		RKB01010
	DMDM = PU(6)		RKB01020
	DMDL = PU(7)		RKB01030
	FFMS = PU(8)		RKB01040
	FFMM = PU(9)		RKB01050
	FFML = PU(10)		RKB01060
	PRODS = PU(11)		RKB01070
	PRODM = PU(12)		RKB01080
	PRODL = PU(13)		RKB01090
	DI = PU(14)		RKB01100
	RT = PU(15)		RKB01110
	E = PU(16)		RKB01120
	OUTGS = PU(17)		RKB01130
	OUTGM = PU(18)		RKB01140
			RKB01150
			RKB01160
		Initialize State Variables	RKB01170
	N = 7		RKB01180
	Y(1) = PU(19)		RKB01190
	Y(2) = PU(20)		RKB01200
	Y(3) = PU(21)		RKB01210

Y(4) = PU(22)
 Y(5) = PU(23)
 Y(6) = PU(24)
 Y(7) = PU(25)

RKB01220
 RKB01230
 RKB01240

RKB01250

RKB01260

RKB01270

RKB01280

RKB01290

RKB01300

RKB01310

RKB01320

RKB01330

RKB01340

RKB01350

RKB01360

RKB01370

RKB01380

RKB01390

RKB01400

RKB01410

RKB01420

RKB01430

RKB01440

RKB01450

RKB01460

RKB01470

RKB01480

RKB01490

RKB01500

RKB01510

RKB01520

RKB01530

RKB01540

RKB01550

RKB01560

RKB01570

RKB01580

RKB01590

RKB01600

RKB01610

RKB01620

RKB01630

RKB01640

RKB01650

RKB01660

RKB01670

RKB01680

RKB01690

RKB01700

RKB01710

RKB01720

RKB01730

RKB01740

RKB01750

RKB01760

RKB01770

RKB01780

RKB01790

RKB01800

Initialize Run Control Variables

T = PU(26)
 TFIN = PU(27)
 COMINT = PU(28)
 TOL = PU(29)
 HBOUND = PU(30)
 HMIN = PU(31)
 HINIT = PU(32)

NPL = 1

NK = 1

BIOSUM = Y(1) + Y(2) + Y(3)

RATIO = BIOSUM / Y(7)

DO 37 I = 1, 3

P2(I) = 30000.0

P3(I) = 60000.0

37 CONTINUE

PREVY2 = 30000.0

PREVY3 = 60000.0

Pre-Run Output :

Set Up Output Format and Output Initial Values of T and

WRITE(8,17)

17 FORMAT(1X, 'Method:', 10X, 'Fourth Order Runge-Kutta' / 10X /
 + 1X, 'Problem:', 10X, 'Coupled Model TreeBiomass' / 10X / 1X,
 + 'TIME', 6X, 'Y1', 6X, 'Y2', 6X, 'Y3', 6X, 'Y4', 6X, 'Y5', 6X, 'Y6')

PRINT*,

WRITE(8,17)

17 FORMAT(1X, 'METHOD:', 10X, 'Fourth Order Runge-Kutta' / 10X /
 + 1X, 'Problem:', 10X, 'Coupled Model TreeBiomass' / 10X / 1X,
 + 'TIME', 9X, 'Y7', 9X, 'BIOSUM', 9X, 'RATIO')

PRINT*,

WRITE(8,21) T, Y(1), Y(2), Y(3), Y(4), Y(5), Y(6)

21 FORMAT(F6.2, 2X, F9.1, 2X, F9.1, 2X, F9.1, 2X, F7.1, 2X, F7.1, 2X, F7.1)

WRITE(8,21) T, Y(7), BIOSUM, RATIO

21 FORMAT(1X, F6.2, 1X, F9.1, 1X, F9.1, 1X, F6.3)

TIME(1) = T

Y1(1) = Y(1)

Y2(1) = Y(2)

Y3(1) = Y(3)

Y4(1) = Y(4)

```

Y5(1) = Y(5)
Y6(1) = Y(6)
Y7(1) = Y(7)
BIO(1) = BIOSUM
RAT(1) = RATIO

```

```
CALL RK4(T,Y,N,TFIN,H,HINIT,HBOUND,HMIN,TOL,COMINT,DERIV)
```

Post-Run Output:

```

Tabulate Values of State
Variables and Time at
Output Points

```

```

C      DO 99 I = 2,NPL
C      WRITE(8,87)TIME(I),Y1(I),Y2(I),Y3(I),Y4(I),Y5(I),Y6(I)
C 87   FORMAT(F6.2,2X,F9.1,2X,F9.1,2X,F9.1,2X,F6.1,2X,F6.1,2X,F8.1)
C      PRINT*,' '
C 99 CONTINUE

```

```

      DO 97 I = 2,NPL
      WRITE(8,67)TIME(I),Y7(I),BIO(I),RAT(I)
67   FORMAT(F6.2,3X,F9.1,3X,F9.1,3X,F6.3)
      PRINT*,' '
97 CONTINUE

```

```

Plot Values of State
Variables with Time

```

```

C      CALL ANYDEV
C      CALL GRAPH(Y1,TIME,NPL)
      CALL GRAPH(Y2,TIME,NPL)
      CALL GRAPH(Y3,TIME,NPL)
      CALL GRAPH(Y4,TIME,NPL)
      CALL GRAPH(Y5,TIME,NPL)
      CALL GRAPH(Y6,TIME,NPL)
      PRINT*,'Do you wish to carry out another simulation (Y/N) ?'
      READ*,CHOICE
      IF (CHOICE.EQ.'Y') THEN
        CALL INIT
        GOTO 199
      ENDIF
    ENDIF
  STOP
END

```

```
SUBROUTINE GRAPH(Y1,TIME,NPL)
```

```

  This Subroutine Provides A Graphical Display Of The
  Outputs Of The Component Model With Time

```

```

C      DIMENSION Y1(NPL),TIME (NPL)
C      MINT = TIME(1)
      MAXT = TIME(NPL)
      VALMAX = Y1 (NPL)
      VALMIN = Y1 (1)
      DO 14 I = 1,NPL
        IF (Y1 (I).GT.VALMAX) THEN
          VALMAX = Y1 (I)
        ELSE IF (Y1 (I).LT.VALMIN) THEN
          VALMIN = Y1 (I)
        
```

```

RKB01810
RKB01820
RKB01830
RKB01840
RKB01850
RKB01860
RKB01870
RKB01880
RKB01890
RKB01900
RKB01910
RKB01920
RKB01930
RKB01940
RKB01950
RKB01960
RKB01970
RKB01980
RKB01990
RKB02000
RKB02010
RKB02020
RKB02030
RKB02040
RKB02050
RKB02060
RKB02070
RKB02080
RKB02090
RKB02100
RKB02110
RKB02120
RKB02130
RKB02140
RKB02150
RKB02160
RKB02170
RKB02180
RKB02190
RKB02200
RKB02210
RKB02220
RKB02230
RKB02240
RKB02250
RKB03270
RKB03280
RKB03290
RKB03300
RKB03310
RKB03320
RKB03330
RKB03340
RKB03350
RKB03360
RKB03370
RKB03380
RKB03390
RKB03400

```

```

      END IF
14  CONTINUE
      MAXVAL = VALMAX + 1
      MINVAL = VALMIN - 1
      SPAC1 = (MAXT - MINT)/10.0
      SPAC2 = (MAXVAL - MINVAL)/10.0
      CALL HWROT('MOVIE')
      CALL PAGE(8.5,11.0)
      CALL AREA2D(6.0,8.0)
      CALL SWISSM
      CALL HEADIN('TreeBiomass Model$',100,1.5,2)
      CALL HEADIN('Fourth-Order Runge-Kutta Method$',100,-1.25,2)
      CALL XNAME('Time(years)$',100)
      CALL YNAME('Large Trees (kg/ha)$',100)
      CALL GRAF(MINT,SPAC1,MAXT,MINVAL,SPAC2,MAXVAL)
C   Draw Curve with Rounded and Thickened Line and
C   Rational Spline Interpolation
      CALL RASPLN (1.5)
      CALL THKCRV (.015)
      CALL THKRND (0.)
      CALL CURVE(TIME,Y1,NPL,0)
      CALL ENDPL(0)
      RETURN
      END

      SUBROUTINE OUTPUT(Y,N,T)
C   This Subroutine stores values of Output Variables
C   at communication times. Additionally, it provides
C   an interactive tabular display of the results.

      IMPLICIT REAL*4 (A-H,O-Z)
      DIMENSION Y(N)
      COMMON/DIFF/TIME(400),Y1(400),Y2(400),Y3(400),Y4(400),Y5(400)
      COMMON/DIFF1/Y6(400),Y7(400),BIO(400),RAT(400)
      COMMON/GRA/NPL
      COMMON/OUTP/BIOSUM,RATIO

      WRITE(6,23) T,Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7)
23  FORMAT(1X,F6.2,1X,F9.2,1X,F9.2,1X,F9.2,1X,F8.2,1X,F8.2,1X,F8.2,
+       1X,F8.2)
      NPL = NPL + 1
      TIME(NPL) = T
      Y1(NPL) = Y(1)
      Y2(NPL) = Y(2)
      Y3(NPL) = Y(3)
      Y4(NPL) = Y(4)
      Y5(NPL) = Y(5)
      Y6(NPL) = Y(6)
      Y7(NPL) = Y(7)
      BIO(NPL) = BIOSUM
      RAT(NPL) = RATIO
      RETURN
      END

      SUBROUTINE DERIV(T,Y,DY,N)
      IMPLICIT REAL*4 (A-H,O-Z)
      DIMENSION Y(N),DY(N)

```

RKB03410
 RKB03420
 RKB03430
 RKB03440
 RKB03450
 RKB03460
 RKB03470
 RKB03480
 RKB03490
 RKB03500
 RKB03510
 RKB03520
 RKB03530
 RKB03540
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 RKB03560
 RKB03570
 RKB03580
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 RKB03600
 RKB03610
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 RKB03680
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 RKB03880
 RKB03890
 RKB03900
 RKB03910
 RKB03920
 RKB03930
 RKB03940
 RKB03950
 RKB03960
 RKB03970
 RKB03980
 RKB03990

COMMON/PARS/DMORTS, DMORTM, DMORTL, YMAX, DMDS, DMDM, DMDL, FFMS, FFMM
 COMMON/PARS1/PRODS, PRODM, PRODL, DI, RT, E, OUTGS, OUTGM, FFML, H
 COMMON/GRA/NPL
 COMMON/COUNT/NK, PREVY2, PREVY3, P2(3), P3(3)
 COMMON/OUTP/BIOSUM, RATIO

RKB04000
 RKB04010
 RKB04020
 RKB04030
 RKB04040
 RKB04050
 RKB04060
 RKB04070
 RKB04080
 RKB04090
 RKB04100
 RKB04110
 RKB04120
 RKB04130
 RKB04140
 RKB04150
 RKB04160
 RKB04170
 RKB04180
 RKB04190
 RKB04200
 RKB04210
 RKB04220
 RKB04230
 RKB04240
 RKB04250
 RKB04260
 RKB04270
 RKB04280
 RKB04290
 RKB04300
 RKB04310
 RKB04320
 RKB04330
 RKB04340
 RKB04350
 RKB04360
 RKB04370
 RKB04380
 RKB04390
 RKB04400
 RKB04410
 RKB04420
 RKB04430
 RKB0444Q
 RKB04450
 RKB04460
 RKB04470
 RKB04480
 RKB04490
 RKB04500
 RKB04510
 RKB04520
 RKB04530
 RKB04540
 RKB04550
 RKB04560
 RKB04570
 RKB04580

Subroutine consists of Slow System
 Derivatives which are specified by
 the user for his particular model.

BIOSUM = Y(1) + Y(2) + Y(3)

RATIO = Y(7)/BIOSUM

BOUND = ((100 * H * NK) + 0.000000001)
 BOUND1 = ((100 * H * NK) - 0.000000001)

IF ((T.GT.BOUND1).AND.(T.LT.BOUND)) THEN

P2(1) = Y(2)

P2(2) = P2(1)

P2(3) = P2(2)

PREVY2 = P2(3)

P3(1) = Y(3)

P3(2) = P3(1)

P3(3) = P3(2)

PREVY3 = P3(3)

NK = NK + 1

NC = NC + 1

ENDIF

DY(1) = (PRODS - OUTGS) * Y(1) * (1-(Y(1)+Y(2)+Y(3))/YMAX)
 + - DMORTS * Y(1) * (1+(Y(1)+Y(2)+Y(3))/YMAX)
 + + DI * (PREVY2+PREVY3) * (1-(Y(1)+Y(2)+Y(3))/YMAX)

DY(2) = (PRODM - OUTGM) * Y(2) * (1-(Y(1)+Y(2)+Y(3))/YMAX)
 + - DMORTM * Y(2) * (1+(Y(1)+Y(2)+Y(3))/YMAX)
 + + OUTGS * Y(1) * (1-(Y(1)+Y(2)+Y(3))/YMAX)

DY(3) = PRODS * Y(3) * (1-(Y(1)+Y(2)+Y(3))/YMAX)
 + - DMORTL * Y(3) * (1+(Y(1)+Y(2)+Y(3))/YMAX)
 + + OUTGM * Y(2) * (1-(Y(1)+Y(2)+Y(3))/YMAX)

DY(4) = DMORTS * Y(1) * (1+(Y(1)+Y(2)+Y(3))/YMAX) - (DMDS+FFMS) * Y(4)
 DY(5) = DMORTM * Y(2) * (1+(Y(1)+Y(2)+Y(3))/YMAX) - (DMDM+FFMM) * Y(5)
 DY(6) = DMORTL * Y(3) * (1+(Y(1)+Y(2)+Y(3))/YMAX) - (DMDL+FFML) * Y(6)

DY(7) = E * (PRODS * Y(1)+PRODM * Y(2)+ PRODL*Y(3) + DI *
 + (PREVY2+PREVY3) * (1-(Y(1)+Y(2)+Y(3))/YMAX)) - (DMORTS *
 + Y(1)+DMORTM*Y(2)+DMORTL*Y(3)) * (1+(Y(1)+Y(2)+Y(3))/YMAX)
 + * (Y(7) / (Y(1)+Y(2)+Y(3))) - RT * Y(7)

RETURN
END

SUBROUTINE INIT

INTEGER NUM, RC, RLEN
CHARACTER*8 KEY, MENUN
CHARACTER*8 FLDN(32)
CHARACTER*4 CC
COMMON/XMEN/PU(32)

C Xmenu used for Parameters and Initial Conditions

FLDN(1) = 'MORTS'
FLDN(2) = 'MORTM'
FLDN(3) = 'MORTL'
FLDN(4) = 'YMAX'
FLDN(5) = 'MDS'
FLDN(6) = 'MDM'
FLDN(7) = 'MDL'
FLDN(8) = 'FFMS'
FLDN(9) = 'FFMM'
FLDN(10) = 'FFML'
FLDN(11) = 'PRODS'
FLDN(12) = 'PRODM'
FLDN(13) = 'PRODL'
FLDN(14) = 'I'
FLDN(15) = 'RT'
FLDN(16) = 'E'
FLDN(17) = 'OUTGS'
FLDN(18) = 'OUTGM'
FLDN(19) = 'Y1'
FLDN(20) = 'Y2'
FLDN(21) = 'Y3'
FLDN(22) = 'Y4'
FLDN(23) = 'Y5'
FLDN(24) = 'Y6'
FLDN(25) = 'Y7'
FLDN(26) = 'TINIT'
FLDN(27) = 'TFIN'
FLDN(28) = 'COMINT'
FLDN(29) = 'TOL'
FLDN(30) = 'HBOUND'
FLDN(31) = 'HMIN'
FLDN(32) = 'HINIT'

MENUN = 'BIOMASS'
CALL MCLSCR(NUM, RC)
CALL MLOAD(NUM, RC, MENUN)
CALL MPFMAP(NUM, RC, 1)
CALL MALARM(NUM, RC, 1)
CALL MPRINT(NUM, RC, 2, PROUT)
CALL MDSPRD(NUM, RC, KEY)

RKB04590
RKB04600
RKB04610
RKB04620
RKB04630
RKB04640
RKB04650
RKB04660
RKB04670
RKB04680
RKB04690
RKB04700
RKB04710
RKB04720
RKB04730
RKB04740
RKB04750
RKB04760
RKB04770
RKB04780
RKB04790
RKB04800
RKB04810
RKB04820
RKB04830
RKB04840
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RKB04860
RKB04870
RKB04880
RKB04890
RKB04900
RKB04910
RKB04920
RKB04930
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RKB04970
RKB04980
RKB04990
RKB05000
RKB05010
RKB05020
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RKB05080
RKB05090
RKB05100
RKB05110
RKB05120
RKB05130
RKB05140
RKB05150
RKB05160
RKB05170

```
C      CALL MEXIT(NUM,RC)
      IF (KEY .EQ. 'PF10') GOTO 25
      IF (KEY .EQ. 'PF12') STOP
25     DO 23 I = 1,32
          CALL MSCR2D(NUM,RC,FLDN(I),CC,7,RLEN)
          CALL MCVTCF(PU(I),RC,CC,7,1)
23     CONTINUE
      RETURN
      END
```

```
RKB05180
RKB05190
RKB05200
RKB05210
RKB05220
RKB05230
RKB05240
RKB05250
RKB05260
RKB05270
RKB05280
```

```

1 .....1.....2.....3.....4.....5.....6.....7.....8+
2
3
4
5
6
7
8
9
10
11
12
13
14
15
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17
18
19
20
21
22
23
24

```

INITIALIZATION

KINDLY INITIALIZE VARIABLES

Model Parameters	Experimentation Variables
MTS = 0.020 MTM = 0.010 MTL = 0.005	Initial States Control Variables Y1(0) = 10000.0
YM = 400000. MDS = 0.0001 MDM = 0.0001	Y2(0) = 30000. TINIT = 0.00
MDL = 0.0001 FMS = 0.200 FMM = 0.200	Y3(0) = 60000. TFIN = 24.0
FML = 0.200 PDS = 0.120 PDM = 0.050	Y4(0) = 2500.0 COMINT = 1.00
PDL = 0.030 I = 0.0010 RT = 0.266	Y5(0) = 2000.0 TOL = 0.00010
E = 2.00 OGS = 0.100 OGM = 0.0250	Y6(0) = 2000.0 HBOUND = 0.2000
	Y7(0) = 32000.0 HMIN = 0.00001

Press: PF10 - to start simulation PF12 - to quit

```

1 .....1.....2.....3.....4.....5.....6.....7.....8+
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24

```

Menu For Tree Biomass Model

METHOD: Fourth Order Runge-Kutta
 Problem: Coupled Model TreeBiomass

TIME	Y1	Y2	Y3	Y4	Y5	Y6
0.00	10000.0	30000.0	60000.0	2500.0	2000.0	2000.0
3.00	9888.3	32664.3	78320.3	1944.7	2005.4	2104.5
6.00	9743.5	34980.5	99567.7	1657.3	2122.5	2506.4
9.00	9556.9	36877.9	123168.4	1516.3	2299.6	3144.9
12.00	9320.9	38304.9	148201.9	1453.0	2503.4	3980.5
15.00	9031.1	39238.6	173532.9	1427.9	2710.7	4974.7
18.00	8687.6	39688.7	198020.6	1417.3	2903.7	6083.2
21.00	8295.7	39694.7	220699.1	1407.3	3069.1	7252.4
24.00	7865.5	39317.5	240922.1	1390.0	3198.3	8426.3
27.00	7409.3	38629.5	258400.5	1361.5	3286.8	9554.1
30.00	6940.6	37703.7	273144.7	1321.2	3334.5	10597.0
33.00	6471.6	36606.8	285369.9	1270.3	3344.3	11530.1
36.00	6012.4	35395.3	295400.6	1211.1	3321.1	12343.1
39.00	5570.8	34114.4	303594.9	1146.1	3270.8	13036.5
42.00	5152.2	32798.9	310295.2	1078.0	3199.4	13618.9
45.00	4759.9	31474.5	315804.4	1009.0	3112.4	14103.0
48.00	4395.5	30159.6	320375.1	940.9	3014.5	14503.2
51.00	4059.4	28867.2	324211.3	875.1	2909.5	14833.8
54.00	3751.5	27606.0	327474.1	812.5	2800.5	15107.5
57.00	3470.2	26381.9	330287.8	753.6	2689.9	15335.6
60.00	3214.0	25198.3	332747.8	698.9	2579.4	15527.3
63.00	2981.3	24057.3	334926.9	648.3	2470.2	15690.3
66.00	2770.4	22959.8	336879.8	601.9	2363.3	15830.5
69.00	2579.5	21906.0	338648.4	559.4	2259.2	15952.6
72.00	2407.0	20895.4	340264.7	520.7	2158.4	16060.3
75.00	2251.1	19927.3	341752.0	485.5	2061.0	16156.4
78.00	2110.4	19000.8	343129.7	453.5	1967.3	16243.1
81.00	1983.5	18114.7	344411.8	424.6	1877.2	16321.9
84.00	1869.0	17267.7	345610.1	398.5	1790.7	16394.2
87.00	1765.8	16458.6	346732.9	374.8	1707.9	16461.0
90.00	1672.7	15686.0	347788.9	353.5	1628.6	16522.9
93.00	1588.8	14948.5	348782.6	334.2	1552.7	16580.7
96.00	1513.2	14244.7	349719.9	316.9	1480.2	16634.8
99.00	1445.1	13573.4	350603.8	301.2	1411.0	16685.6
102.00	1383.6	12933.2	351440.2	287.0	1344.9	16733.4
105.00	1328.2	12322.9	352230.5	274.3	1281.7	16778.3
108.00	1278.3	11741.1	352978.9	262.8	1221.5	16820.7
111.00	1233.3	11186.7	353687.5	252.4	1164.1	16860.8
114.00	1192.6	10658.4	354358.2	243.1	1109.3	16898.7
117.00	1156.0	10155.2	354993.7	234.7	1057.1	16934.5
120.00	1122.9	9675.9	355596.6	227.1	1007.3	16968.4
123.00	1093.0	9219.5	356168.0	220.2	959.9	17000.6
126.00	1066.1	8784.9	356708.7	214.0	914.7	17031.0
129.00	1041.7	8371.2	357222.8	208.4	871.7	17059.8
132.00	1019.7	7977.4	357709.3	203.3	830.7	17087.2
135.00	999.8	7602.5	358170.6	198.8	791.7	17113.2
138.00	981.8	7245.8	358608.9	194.7	754.6	17137.7
141.00	965.6	6906.3	359025.3	190.9	719.1	17161.0
144.00	950.8	6583.3	359419.9	187.6	685.5	17183.1
147.00	937.5	6276.1	359793.6	184.5	653.4	17204.1
150.00	925.4	5983.7	360148.6	181.7	622.9	17224.1
153.00	914.5	5705.7	360485.9	179.2	593.9	17242.8

METHOD: Fourth Order Runge-Kutta
 Problem: Coupled Model TreeBiomass

TIME	Y1	Y2	Y3	Y4	Y5	Y6
155.00	904.6	5441.2	360804.8	177.0	566.3	17260.6
159.00	895.6	5189.6	361107.0	174.9	540.0	17277.6
162.00	887.4	4950.4	361394.1	173.1	515.0	17293.7
165.00	880.0	4722.8	361667.7	171.4	491.3	17309.0
168.00	873.3	4506.5	361929.4	169.9	468.7	17323.4
171.00	867.2	4300.8	362173.3	168.5	447.2	17337.3
174.00	861.6	4105.2	362406.5	167.2	426.7	17350.2
177.00	856.5	3919.7	362631.5	166.1	407.3	17362.7
180.00	851.9	3743.4	362838.2	165.0	388.8	17374.5
183.00	847.7	3575.7	363039.9	164.1	371.3	17385.8
186.00	843.9	3416.4	363227.4	163.2	354.6	17396.3
189.00	840.4	3264.9	363408.9	162.4	338.8	17406.6
192.00	837.2	3120.9	363577.6	161.7	323.7	17415.9
195.00	834.2	2984.0	363743.0	161.0	309.4	17425.3
198.00	831.6	2853.9	363893.0	160.4	295.7	17433.5
201.00	829.1	2730.2	364043.0	159.9	282.8	17441.7
204.00	826.9	2612.7	364178.5	159.4	270.5	17449.6
207.00	824.8	2501.0	364309.7	158.9	258.8	17456.6
210.00	822.9	2394.8	364440.7	158.5	247.7	17463.7
213.00	821.2	2293.9	364553.2	158.1	237.1	17470.6
216.00	819.6	2198.1	364665.7	157.8	227.1	17476.4
219.00	818.1	2106.9	364778.2	157.5	217.6	17482.3
222.00	816.8	2020.4	364875.9	157.2	208.5	17488.1
225.00	815.6	1938.1	364969.7	156.9	199.9	17493.7
228.00	814.4	1859.9	365063.4	156.6	191.7	17498.5
231.00	813.4	1785.6	365157.2	156.4	183.9	17503.5
234.00	812.4	1715.0	365233.6	156.2	176.5	17508.2
237.00	811.5	1647.9	365308.6	156.0	169.5	17512.9
240.00	810.7	1584.2	365383.6	155.8	162.8	17516.8
243.00	809.9	1523.6	365458.6	155.6	156.4	17520.7
246.00	809.2	1466.0	365531.9	155.5	150.4	17524.6
249.00	808.5	1411.4	365588.1	155.3	144.7	17528.1
252.00	807.9	1359.4	365644.4	155.2	139.2	17531.7
255.00	807.3	1310.0	365700.6	155.1	134.1	17534.8
258.00	806.8	1262.4	365757.7	155.0	129.1	17537.8
261.00	806.3	1216.9	365815.3	154.9	124.3	17540.8
264.00	805.8	1173.7	365872.9	154.8	119.8	17543.9
267.00	805.4	1132.6	365917.9	154.7	115.5	17546.5
270.00	805.0	1093.7	365956.8	154.6	111.4	17548.9
273.00	804.6	1056.8	365995.2	154.5	107.5	17551.3
276.00	804.3	1021.8	366033.6	154.4	103.8	17553.7
279.00	804.0	988.5	366071.9	154.4	100.4	17555.7
282.00	803.7	957.0	366110.3	154.3	97.0	17557.7
285.00	803.4	927.0	366148.7	154.2	93.9	17559.7
288.00	803.1	898.6	366187.1	154.2	90.9	17561.7
291.00	802.8	871.6	366225.4	154.1	88.1	17563.8
294.00	802.5	846.0	366257.1	154.1	85.4	17565.5
297.00	802.3	821.7	366281.2	154.0	82.9	17566.7
300.00	802.1	798.7	366304.1	154.0	80.5	17567.9

METHOD: Fourth Order Runge-Kutta
 Problem: Coupled Model TreeBiomass

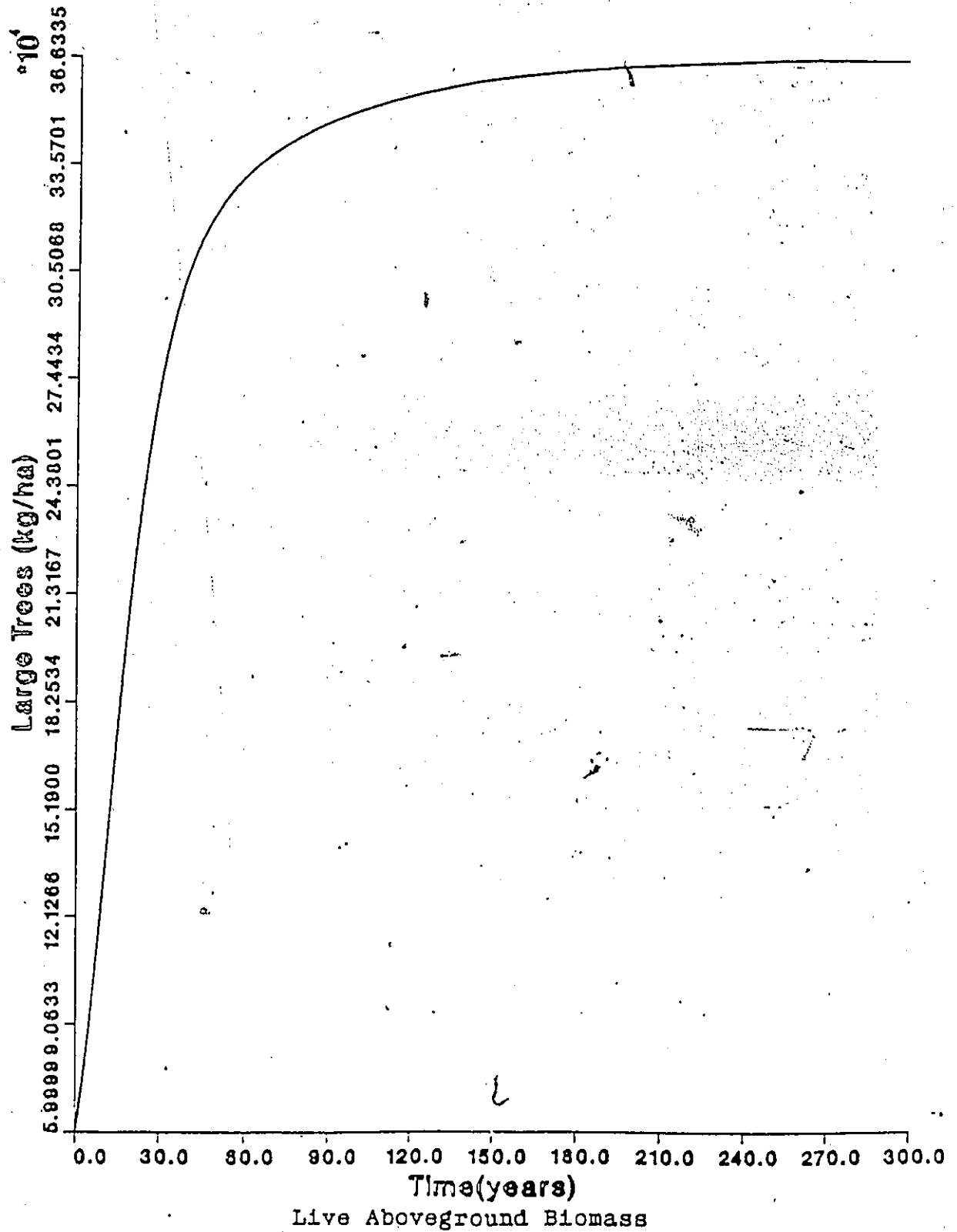
TIME	Y7	BIOSUM	RATIO
0.00	32000.0	100000.0	3.125
3.00	34419.3	120872.9	0.285
6.00	38419.5	144291.7	0.266
9.00	43326.7	169603.2	0.255
12.00	48726.8	195827.7	0.249
15.00	54295.1	221802.6	0.245
18.00	59747.4	246396.8	0.242
21.00	64839.2	268689.4	0.241
24.00	69381.4	288105.0	0.241
27.00	73273.7	304439.4	0.241
30.00	76480.9	317789.1	0.241
33.00	79027.5	328448.2	0.241
36.00	80978.8	336808.2	0.240
39.00	82420.8	343280.1	0.240
42.00	83445.2	348246.3	0.240
45.00	84139.2	352038.8	0.239
48.00	84578.4	354930.1	0.238
51.00	84826.6	357137.9	0.238
54.00	84935.1	358831.6	0.237
57.00	84944.3	360139.8	0.236
60.00	84883.5	361160.1	0.235
63.00	84775.4	361965.5	0.234
66.00	84635.9	362610.0	0.233
69.00	84479.2	363133.9	0.233
72.00	84310.4	363567.0	0.232
75.00	84141.5	363930.4	0.231
78.00	83972.6	364240.9	0.231
81.00	83807.3	364509.9	0.230
84.00	83654.6	364746.7	0.229
87.00	83504.4	364957.2	0.229
90.00	83354.3	365147.5	0.228
93.00	83217.7	365319.8	0.228
96.00	83086.3	365477.8	0.227
99.00	82958.5	365622.2	0.227
102.00	82845.9	365757.0	0.227
105.00	82733.2	365881.6	0.226
108.00	82628.4	365998.3	0.226
111.00	82534.6	366107.4	0.225
114.00	82440.7	366209.2	0.225
117.00	82349.8	366304.9	0.225
120.00	82273.9	366395.4	0.225
123.00	82198.8	366480.5	0.224
126.00	82123.7	366559.6	0.224
129.00	82050.9	366635.7	0.224
132.00	81991.6	366706.4	0.224
135.00	81934.9	366772.9	0.223
138.00	81878.6	366836.6	0.223
141.00	81822.2	366897.2	0.223
144.00	81765.8	366954.1	0.223
147.00	81719.4	367007.1	0.223
150.00	81677.7	367057.7	0.223
153.00	81638.2	367106.1	0.222
156.00	81600.1	367150.6	0.222
159.00	81562.4	367192.2	0.222
162.00	81524.8	367231.9	0.222
165.00	81487.2	367270.5	0.222
168.00	81449.6	367309.2	0.222
171.00	81419.9	367341.2	0.222

METHOD: Fourth Order Runge-Kutta
 Problem: Coupled Model TreeBiomass

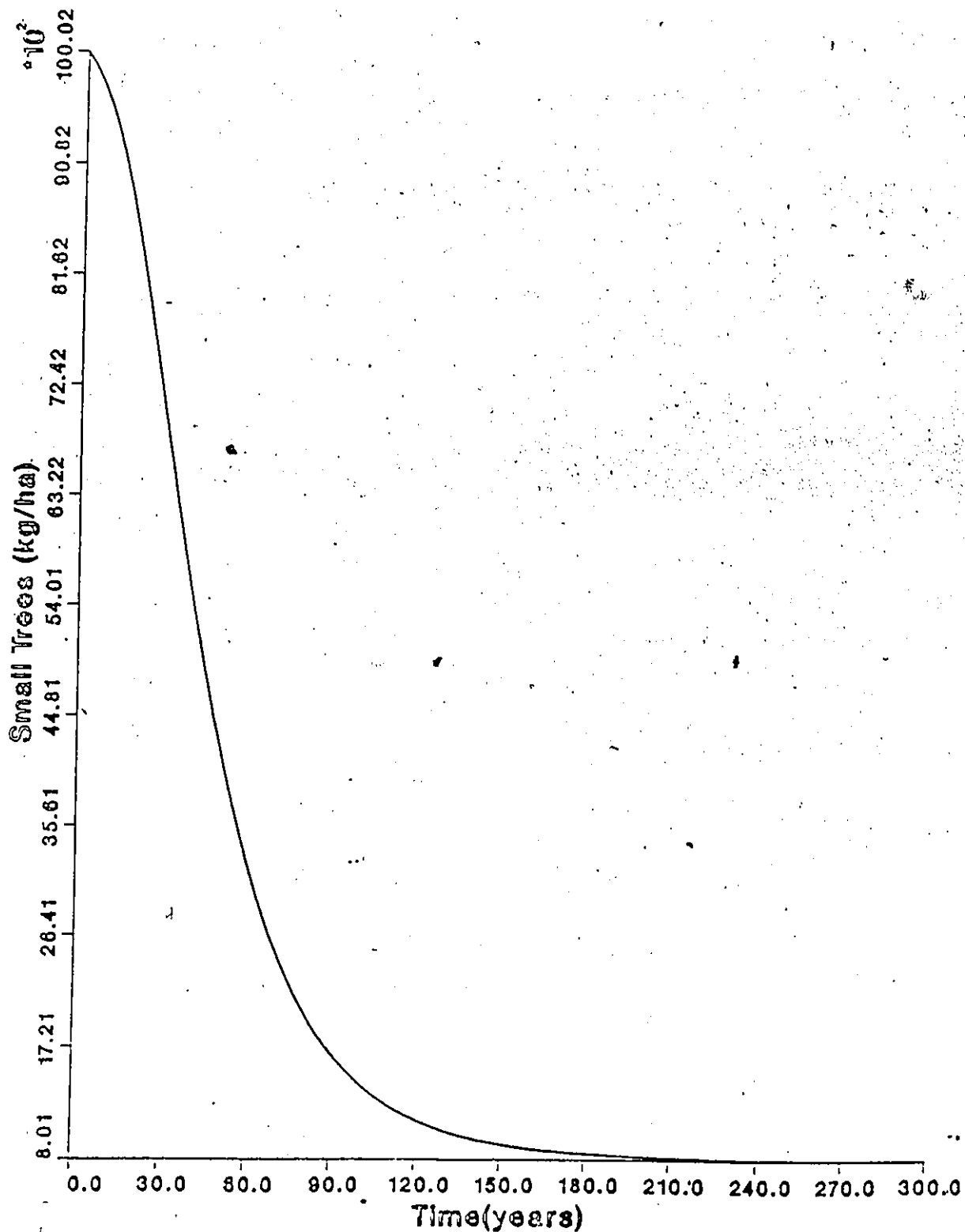
TIME	Y7	BIO SUM	RATIO
174.00	81393.2	367373.3	0.222
177.00	81368.8	367407.7	0.221
180.00	81344.3	367433.4	0.221
183.00	81322.2	367463.2	0.221
186.00	81300.5	367487.6	0.221
189.00	81280.6	367514.1	0.221
192.00	81261.0	367535.6	0.221
195.00	81242.1	367561.2	0.221
198.00	81223.2	367578.4	0.221
201.00	81204.4	367602.3	0.221
204.00	81185.6	367618.0	0.221
207.00	81166.9	367635.5	0.221
210.00	81148.1	367658.4	0.221
213.00	81129.7	367668.3	0.221
216.00	81117.2	367683.4	0.221
219.00	81106.4	367703.3	0.221
222.00	81094.4	367713.1	0.221
225.00	81083.2	367723.2	0.221
228.00	81073.5	367737.7	0.220
231.00	81065.3	367756.1	0.220
234.00	81054.9	367760.9	0.220
237.00	81045.6	367767.9	0.220
240.00	81037.4	367778.4	0.220
243.00	81030.6	367792.0	0.220
246.00	81024.4	367807.1	0.220
249.00	81015.8	367807.9	0.220
252.00	81008.3	367811.6	0.220
255.00	81001.7	367817.9	0.220
258.00	80996.0	367826.9	0.220
261.00	80991.1	367838.4	0.220
264.00	80987.1	367852.4	0.220
267.00	80981.3	367855.9	0.220
270.00	80975.0	367855.5	0.220
273.00	80969.3	367856.6	0.220
276.00	80964.4	367859.8	0.220
279.00	80960.1	367864.4	0.220
282.00	80956.4	367870.9	0.220
285.00	80953.4	367879.1	0.220
288.00	80950.9	367888.7	0.220
291.00	80948.9	367899.8	0.220
294.00	80946.0	367905.6	0.220
297.00	80942.1	367905.2	0.220
300.00	80938.3	367904.8	0.220

TreeBiomass Model

Fourth-Order Runge-Kutta Method

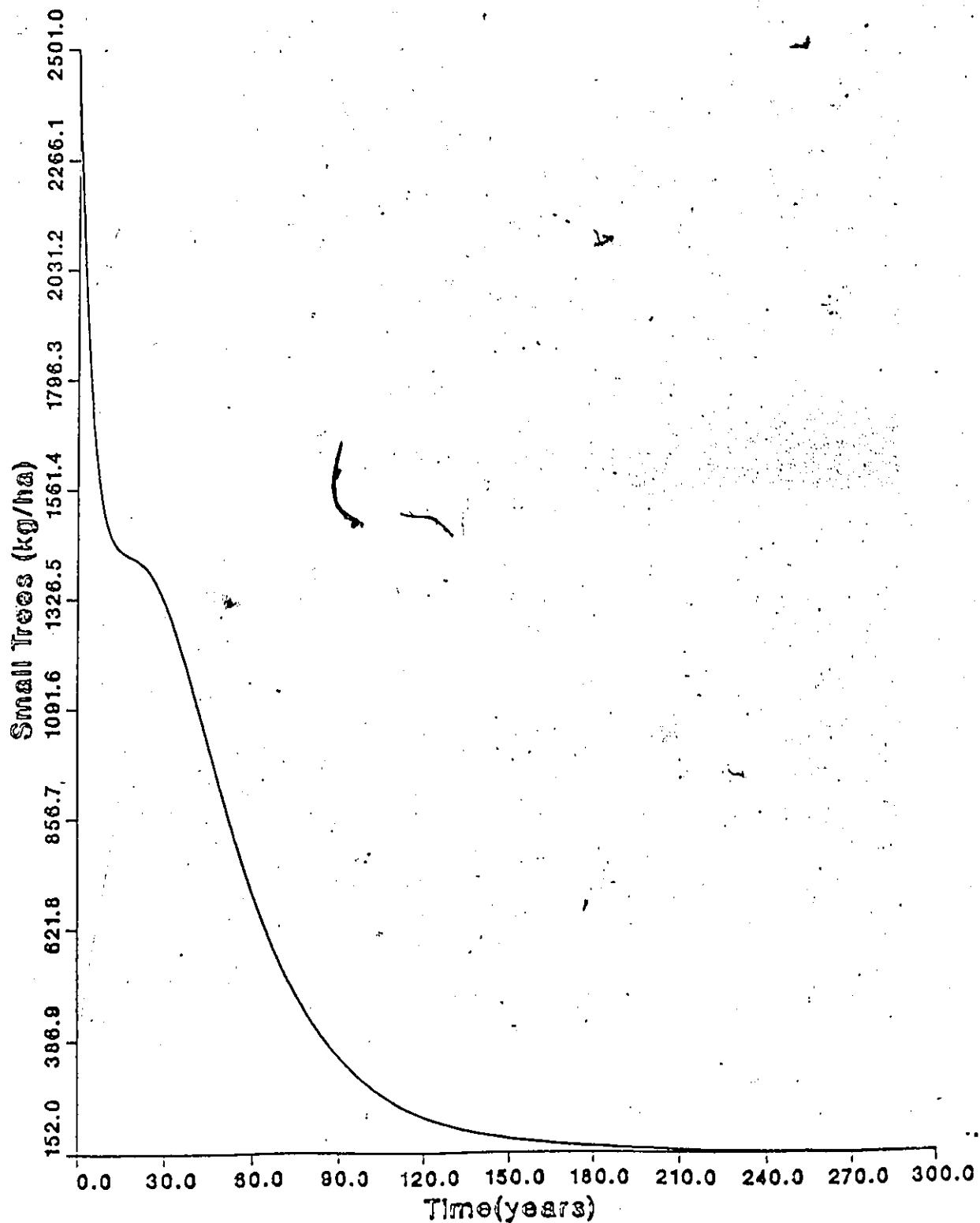


TreeBiomass Model Fourth-Order Runge-Kutta Method



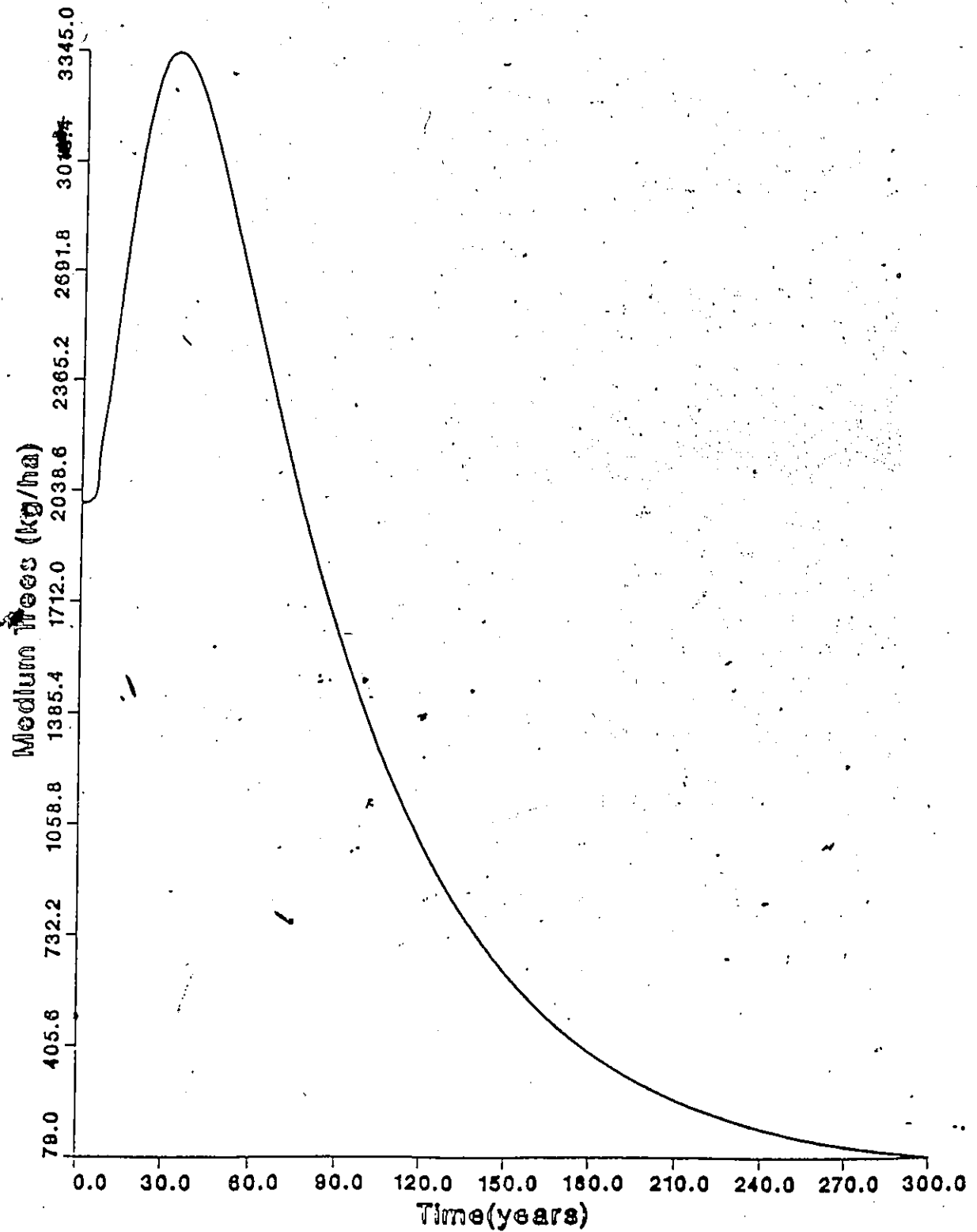
Live Aboveground Biomass

TreeBiomass Model
Fourth-Order Runge-Kutta Method



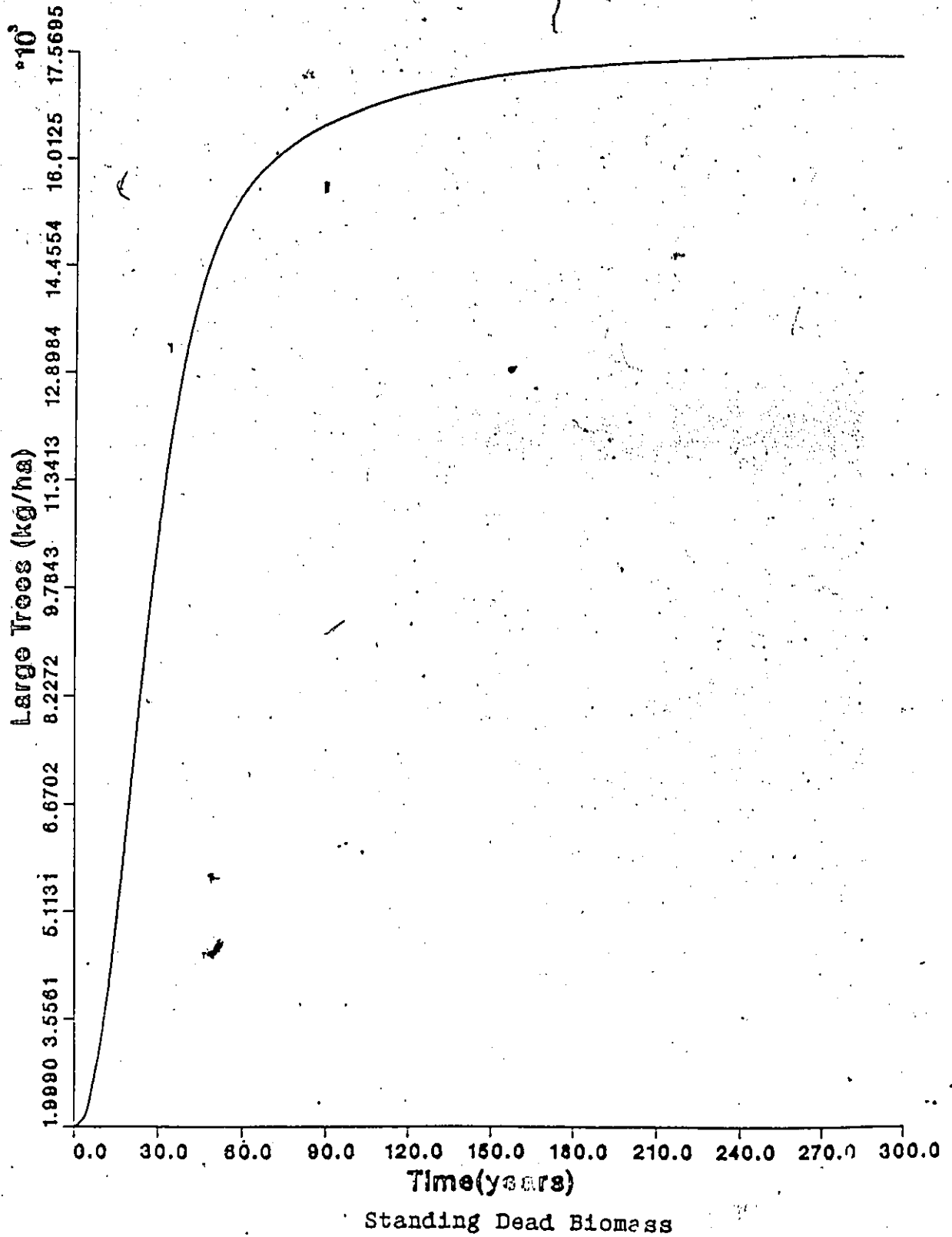
Standing Dead Biomass

TreeBiomass Model
Fourth-Order Runge-Kutta Method



Standing Dead Biomass

TreeBiomass Model Fourth-Order Runge-Kutta Method



Appendix G. THE ELECTRONIC OSCILLATOR MODEL (Revisited)

G.1 Problem Definition

This test example utilizes the multi-rate integration algorithm of the run-time library in the revisitation of the electronic oscillator model as described in Appendix B. A block diagram of the partitioned model for use of the multi-rate algorithm is shown in Figure G.1. The full details of the specification of this multi-rate model is given in Section G.2. As can be seen, the results follow closely to those in Appendix B the algorithm requiring significantly lower CPU-time.

Fast Routine

$$Y1' = Y2$$

$$Y2' = -64Y1 + 7.5(2 + w1 - Y1)Y2^2$$

$$X1' = \frac{2}{R1} Y1Y2 + \frac{1}{R1C1} (X2 - X1)$$

$$X2' = \frac{1}{R2C1} X1 - \left(\frac{1}{R2C1} + \frac{1}{R2C2} \right) X2 + \frac{1}{R1C1} W2 \quad X2$$

$$W1 = S$$

$$W2 = X3$$

Slow Routine

$$X3' = \frac{1}{R3C2} X2 - \left(\frac{1}{R3C2} + \frac{1}{R3C3} \right) X2 + \frac{1}{R3C3} X4$$

$$X4' = \frac{1}{R4C3} X3 - \left(\frac{1}{R4C3} + \frac{1}{R4C4} \right) X4 + \frac{1}{R4C4} X5$$

$$X5' = \frac{1}{R5C4} X4 - \left(\frac{1}{R5C4} + \frac{1}{R5C5} \right) X5 + \frac{1}{R5C5} X6$$

$$X6' = \frac{1}{R6C5} X5 - \left(\frac{1}{R6C5} + \frac{1}{R6C6} \right) X6$$

$$V' = \frac{1}{C6} X6$$

$$S' = 0.02 |36 - 5.29 (|V|)^{.5}|^{1.2} \text{ sign } |36 -$$

$$5.29 (|V|)^{.5}| - 0.02s$$

Figure G.1 Partitioned Model Of Electronic Oscillator

G.2 Gest Specification of The Electronic Oscillator Model (Revisited)

Program StudyOfElectronicOscillator

```

MutirateModel ElectronicOscillator
  ComponentModels
    SlowContinuousModel Slow
    FastContinuousModel Fast
  EndComponentModels

  ContinuousModel Slow
    StaticStructure
      Inputs
        X2
      States
        X3,
        X4,
        X5,
        X6,
        V,
        S
      Outputs
        X3,
        S
      Parameters
        R3, (* Resistance in kOhms *)
        R4, (* Resistance in kOhms *)
        R5, (* Resistance in kOhms *)
        R6, (* Resistance in kOhms *)
        C2, (* Capacitance in microFarads *)
        C3, (* Capacitance in microFarads *)
        C4, (* Capacitance in microFarads *)
        C5, (* Capacitance in microFarads *)
        C6, (* Capacitance in microFarads *)
      EndStaticStructure
    DynamicStructure
      Derivatives
        X3' = X2/R3*C2 - (1/R3*C2 + 1/R3*C3)*X3 + X4/R3*C3
        X4' = X3/R4*C3 - (1/R4*C3 + 1/R4*C4)*X4 + X5/R4*C4
        X5' = X4/R5*C4 - (1/R5*C4 + 1/R5*C5)*X5 + X6/R5*C5
        X6' = X5/R6*C5 - (1/R6*C5 + 1/R6*C6)*X6
        V' = X6/C6
        S' = 0.02*Abs(36 - 5.29 * Sqrt(Abs(V))) ** 1.2 *
            Sign(Abs(36 - 5.29 * Sqrt(Abs(V))) - 0.02*S)
      EndDerivatives
    EndDynamicStructure
  EndModel Slow

ContinuousModel Fast
  StaticStructure
    Inputs
      S,
      X3
    States
      Y1,
      Y2,
      X1,
      X2
    Outputs
      X2
    Parameters
      R1, (* Resistance in kOhms *)

```

```

      R2,          (* Resistance in kOhms          *)
      C1,          (* Capacitance in microFarads   *)
      C2,          (* Capacitance in microFarads   *)
EndStaticStructure
DynamicStructure
  Derivatives
    Y1' = Y2
    Y2' = -64*Y1 + 7.5*(2 + S - Y1**2.0) * Y2
    X1' = 2*Y1*Y2/R1 + (X2-X1)/R1*C1
    X2' = X1/R2*C1 - (1/R2*C1 + 1/R2*C2)*X2 + X3/R1*C1
  EndDerivatives
EndDynamicStructure
EndModel Fast

InternalCoupling
  Slow.X2 <-- Fast.X2
  Fast.S <-- Slow.S
  Fast.X3 <-- Slow.X3
EndInternalCoupling
EndModel ElectronicOscillator

```

```

ParameterSet 1
  Model Slow
  Parameters
    R3 = 8.0
    R4 = 8.0
    R5 = 8.0
    R6 = 8.0
    C2 = 4.25
    C3 = 1.25
    C4 = 1.25
    C5 = 1.25
    C6 = 1.25
  EndParameters
EndModel

```

```

Model Fast
  Parameters
    R1 = 8.0
    R2 = 8.0
    C1 = 6.25
    C2 = 4.25
  EndParameters
EndModel
EndParameterSet 1

```

```

Experiment 1
  Global
    TimeUnitIs Second
    StartTime = 0.0
    IntegrateBy Multi-Rate Integration
    Communicate AtEvery 0.2 Second
    SimulateUntil Time = 20.0
  EndGlobal

```

```

Model Slow
  InitialStates
    X3 = 40.0
    X4 = 45.0
    X5 = 50.0
    X6 = 55.0
    V = 60.0
    S = 65.0
  EndInitialStates

```

Tolers = 0.50
SaveOutputs X3,S
EndModel Slow

Model Fast
InitialStates
Y1 = 60.0
Y2 = 70.0
X1 = 80.0
X2 = 85.0
EndInitialStates
Tolerf = 0.01
EndModel Fast
EndExperiment 1

Run 1
ToObserve ElectronicOscillator
WithParameterSet 1
●InExperiment 1
WithPostRun
OutputModule 1 On Printer
EndPostRun
EndRun 1

OutputModule 1
New Page
Heading ForFirstPage 1 Line
'Study of ElectronicOscillator'
List Parameters And InitialConditions
PlotandList X3,S
EndOutputModule 1

EndProgram StudyOfElectronicOscillator

G.3. Equivalent Fortran Program With Results For
Electronic Oscillator Model: Revisited

Variable List

C	CINPOT: NS-- The Dimension of the Vector of Slow System State Variables	MUL00020
C		MUL00030
C		MUL00040
C		MUL00050
C		MUL00060
C		MUL00070
C		MUL00080
C		MUL00090
C	NF-- The Dimension of the Vector of Fast System State Variables	MUL00100
C		MUL00110
C	S(1)..S(N)-- Initial values of Slow System State Variables	MUL00120
C		MUL00130
C	F(1)..F(M)-- Initial values of Fast System State Variables	MUL00140
C		MUL00150
C		MUL00160
C	W1..W4-- Dummy Arrays	MUL00170
C		MUL00180
C	DF1..DF5 Required For RK-Merson Integration	MUL00190
C		MUL00200
C	HS-- Slow System Integration Step Size	MUL00210
C		MUL00220
C	HSMIN -- Minimum Allowable Slow System Integration Step Size	MUL00230
C		MUL00240
C	HBOUND-- Upper Bound On Initial Step Size	MUL00250
C		MUL00260
C	HF -- Fast System Integration Step Size	MUL00270
C		MUL00280
C	HFMIN -- Minimum Allowable Fast System Integration Step Size	MUL00290
C		MUL00300
C	TOLERS-- User Tolerance for Slow System	MUL00310
C		MUL00320
C	TOLERF-- User Tolerance for Fast System	MUL00330
C		MUL00340
C	T --Computational Time	MUL00350
C		MUL00360
C	TINIT -- Initial Value of Time	MUL00370
C		MUL00380
C	TFIN -- End Time of Simulation	MUL00390
C		MUL00400
C	TCOM -- Communication Time	MUL00410
C		MUL00420
C	COMINT-- Communication Interval	MUL00430
C		MUL00440
C	Output: T-- Time at Output Points	MUL00450
C		MUL00460
C	S(K)-- Values of Slow System Variable at Output points	MUL00470
C		MUL00480
C	Program Variables :	MUL00490
C	S(NS) --State Variables Vector	MUL00500
C		MUL00510
C	DS(NS)--Vector of Derivatives of Slow System State Variables	MUL00520
C		MUL00530
C	PS(NS)--Vector of Predicted Slow System State Variables at	MUL00540
C	TN+HS/3	MUL00550
C		MUL00560
C	DPS(NS)--Vector of Derivatives of Slow System State Variables	MUL00570
C	at TN+HS/3 using Predicted Values	MUL00580
C		MUL00590
C		MUL00600

P1S(NS)--Vector of Corrected Slow System State Variables at TN+HS/3	MUL00610 MUL00620 MUL00630
DP1S(NS)--Vector of Derivatives of Slow System State Variables at TN+HS/3	MUL00640 MUL00650 MUL00660
P2S(NS)--Vector of Estimates of State Variable Values at TN + HS/2	MUL00670 MUL00680 MUL00690
DP2S(NS)--Vector of Derivatives of Slow System State Variables at TN+HS/2	MUL00700 MUL00710 MUL00720
P3S(NS)--Vector of Estimates of State Variable Values at TN + HS	MUL00730 MUL00740 MUL00750
DP3S(NS)--Vector of Derivatives of Slow System State Variables at TN+HS	MUL00760 MUL00770 MUL00780
INTS(2)--Vector of Interpolated/Extrapolated Values of Slow System Variables involved in coupling between TN and TN + HS	MUL00790 MUL00800 MUL00810 MUL00820 MUL00830 MUL00840 MUL00850 MUL00860
ERR(NS)--Vector of Local Error Estimates For Slow System Variables	MUL00870 MUL00880 MUL00890
ERRMAX--Variable containing Maximum Error For Slow System Variables	MUL00900 MUL00910 MUL00920
ER(NF)--Vector of Local Error Estimates For Fast System Variables	MUL00930 MUL00940 MUL00950
ERMAX--Variable containing Maximum Error	MUL00960 MUL00970
HPOS --Intermediate Variable Used in determining HINIT	MUL00980 MUL00990
NPL --Counter used for Graphics Routine	MUL01000 MUL01010
FDER --Maximum value of Derivative Functions at Initial Time	MUL01020 MUL01030 MUL01040
NFLAG--Signals The Detection Of A Communication Time	MUL01050 MUL01060 MUL01070 MUL01080
PROGRAM MAIN	MUL01090 MUL01100
Main Program	MUL01110 MUL01120 MUL01130 MUL01140 MUL01150 MUL01160 MUL01170
This program utilizes a Multi- Rate Integration Algorithm based on Runge-Kutta Merson's to simulate a particular electronic oscillator model.	MUL01180 MUL01190
Variable Declaration	

```

IMPLICIT REAL(A-H,O-Z)
REAL S(8),F(6)
CHARACTER*1 CHOICE
COMMON/DIFF/PU(29)
COMMON/PARS/C1,C2,C3,C4,C5,C6,R1,R2,R3,R4,R5,R6
COMMON/FAST/TOLERF,HFMAX,HFMIN
COMMON/SLOW/TOLERS,HSMAX,HSMIN,COMINT
COMMON/OUT/NPL,SVAL(400),TIME(400),SVAL1(400)
EXTERNAL DERIVS

```

```

PRINT*,'Welcome to the Electronic Oscillator Model'
PRINT*,'
PRINT*,'Would You Like To Perform a Simulation ? (Y/N).'
READ*,CHOICE
IF (CHOICE.EQ.'Y') THEN
  CALL INIT

```

Initialization from Menu

Initialize Parameters

199

```

R1 = PU(1)
R2 = PU(2)
R3 = PU(3)
R4 = PU(4)
R5 = PU(5)
R6 = PU(6)
C1 = PU(7)
C2 = PU(8)
C3 = PU(9)
C4 = PU(10)
C5 = PU(11)
C6 = PU(12)

```

Initialize State Variables

```

S(1) = PU(13)
S(2) = PU(14)
S(3) = PU(15)
S(4) = PU(16)
S(5) = PU(17)
S(6) = PU(18)
F(1) = PU(19)
F(2) = PU(20)
F(3) = PU(21)
F(4) = PU(22)

```

Initialize Time

```

T = PU(23)
TFIN = PU(24)
TOLERF = PU(25)
TOLERS = PU(26)
HSMIN = PU(27)
HFMIN = PU(28)
COMINT = PU(29)
ORD = 5

```

Add Dimensions of Fast System
and Slow System

NF = 4

MUL01200
MUL01210
MUL01220
MUL01230
MUL01240
MUL01250
MUL01260
MUL01270
MUL01280
MUL01290
MUL01300
MUL01310
MUL01320
MUL01330
MUL01340
MUL01350
MUL01360
MUL01370
MUL01380
MUL01390
MUL01400
MUL01410
MUL01420
MUL01430
MUL01440
MUL01450
MUL01460
MUL01470
MUL01480
MUL01490
MUL01500
MUL01510
MUL01520
MUL01530
MUL01540
MUL01550
MUL01560
MUL01570
MUL01580
MUL01590
MUL01600
MUL01610
MUL01620
MUL01630
MUL01640
MUL01650
MUL01660
MUL01670
MUL01680
MUL01690
MUL01700
MUL01710
MUL01720
MUL01730
MUL01740
MUL01750
MUL01760
MUL01770
MUL01780

C	NS = 6		MUL01790
		Add Graphics Counter	MUL01800
	NPL = 1		MUL01810
C			MUL01820
C		Results For Slow Routine at	MUL01830
		the end of the simulation.	MUL01840
			MUL01850
			MUL01860
			MUL01870
17	WRITE(8,17)		MUL01880
+	FORMAT(1X,'Method:',19X,'Multi-Rate Algorithm Based on		MUL01890
+	/28X,'Runge-Kutta Merson'/10X/1X,'Study Of Electronic		MUL01900
+	Oscillator',14X,'Slow Routine'/10X/1X,'Time',17X,		MUL01910
	'Input To Fast Routine'/3X,'T',16X,'X3',14X,'S')		MUL01920
	PRINT*,		MUL01930
	WRITE(8,3)T,S(1),S(6)		MUL01940
3	FORMAT(1X,F5.1,10X,F7.3,10X,F7.3)		MUL01950
	TIME (NPL)= T		MUL01960
	SVAL (NPL)= S(1)		MUL01970
	SVAL1 (NPL) = S(6)		MUL01980
	CALL SRATE(NS,NF,S,F,HS,DERIVS,T,TFIN)		MUL01990
C		Post-Run Output:	MUL02000
C		Tabulate Values of State	MUL02010
C		Variables and Time at	MUL02020
		Output Points	MUL02030
	DO 99 I = 2,NPL		MUL02040
	WRITE(8,87)TIME(I),SVAL(I),SVAL1(I)		MUL02050
87	FORMAT(1X,F5.1,5X,F8.3,5X,F8.3)		MUL02060
	PRINT*,		MUL02070
99	CONTINUE		MUL02080
C		Plot results of outputs from	MUL02090
C		the two routines	MUL02100
	CALL ANYDEV		MUL02110
	CALL GRAPH(TIME,SVAL,NPL)		MUL02120
	CALL GRAPH(TIME,SVAL1,NPL)		MUL02130
	PRINT*,'Do you wish to carry out another simulation (Y/N) ?'		MUL02140
	READ*,CHOICE		MUL02150
	IF (CHOICE.EQ.'Y') THEN		MUL02160
	CALL INIT		MUL02170
	GOTO 199		MUL02180
	ENDIF		MUL02190
	ENDIF		MUL02200
	END		MUL02210
			MUL05370
			MUL05380
			MUL05390
C	SUBROUTINE GRAPH(TVAL,SVALU,NPL)		MUL05400
C	This Subroutine Provides A Graphical Display of Component		MUL05410
	Model Master Routine. Output X3 is plotted against Time.		MUL05420
	DIMENSION TVAL(NPL),SVALU(NPL)		MUL05430
	MINT = TVAL(1)		MUL05440
	MAXT = TVAL(NPL) + 1		MUL05450
	VALMAX = SVALU(NPL)		MUL05460
	VALMIN = SVALU(1)		MUL05470
	DO 13 I = 1,NPL		MUL05480
	IF (SVALU(I).GT.VALMAX) THEN		MUL05490
	VALMAX = SVALU(I)		MUL05500
	ELSE IF (SVALU(I).LT.VALMIN) THEN		MUL05510
	VALMIN = SVALU(I)		MUL05520
	ENDIF		

```

13 CONTINUE
  MAXVAL = VALMAX + 1
  MINVAL = VALMIN - 1
  SPAC1 = (MAXT - MINT)/10.0
  SPAC2 = (MAXVAL - MINVAL)/10.0
  CALL HWROT('MOVIE')
  CALL PAGE(8.5,11.0)
  CALL SWISSM
  CALL AREA2D(6.0,8.0)
  CALL HEADIN('STUDY OF ELECTRONIC OSCILLATOR MODELS',100,1.5,2)
  CALL HEADIN('MULTI-RATE INTEGRATION METHODS',100,-1.15,2)
  CALL XNAME('TIME(SECS)',100)
  CALL YNAME('VALUE OF X3',100)
  CALL GRAF(MINT,SPAC1,MAXT,MINVAL,SPAC2,MAXVAL)
C  DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C  RATIONAL SPLINE INTERPOLATION
  CALL RASPLN (1.5)
  CALL THKCRV (.015)
  CALL THKRND (0.)
  CALL CURVE(TVAL,SVALU,NPL,1)
  CALL ENDEPL(0)
  RETURN
END

SUBROUTINE GRAPH1(TVAL,SVALU,NPL)
C  THIS SUBROUTINE PROVIDES A GRAPHICAL DISPLAY OF COMPONENT
C  MODEL MASTER ROUTINE. OUTPUT S IS PLOTTED AGAINST TIME.

  DIMENSION TVAL(NPL),SVALU(NPL)
  MINT = TVAL(1)
  MAXT = TVAL(NPL) + 1
  VALMAX = SVALU(NPL)
  VALMIN = SVALU(1)
  DO 13 I = 1,NPL
    IF (SVALU(I).GT.VALMAX) THEN
      VALMAX = SVALU(I)
    ELSE IF (SVALU(I).LT.VALMIN) THEN
      VALMIN = SVALU(I)
    ENDIF
  13 CONTINUE
  MAXVAL = VALMAX + 1
  MINVAL = VALMIN - 1
  SPAC1 = (MAXT - MINT)/10.0
  SPAC2 = (MAXVAL - MINVAL)/10.0
  CALL HWROT('MOVIE')

  CALL PAGE(8.5,11.0)
  CALL AREA2D(6.0,8.0)
  CALL SWISSM
  CALL HEADIN('STUDY OF ELECTRONIC OSCILLATOR MODELS',100,1.5,2)
  CALL HEADIN('MULTI-RATE INTEGRATION METHODS',100,-1.15,2)
  CALL XNAME('TIME(SECS)',100)
  CALL YNAME('VALUES OF S',100)
  CALL GRAF(MINT,SPAC1,MAXT,MINVAL,SPAC2,MAXVAL)
C  DRAW CURVE WITH ROUNDED AND THICKENED LINE AND
C  RATIONAL SPLINE INTERPOLATION
  CALL RASPLN (1.5)
  CALL THKCRV (.015)
  CALL THKRND (0.)

```

MUL05530
 MUL05540
 MUL05550
 MUL05560
 MUL05570
 MUL05580
 MUL05590
 MUL05600
 MUL05610
 MUL05620
 MUL05630
 MUL05640
 MUL05650
 MUL05660
 MUL05670
 MUL05680
 MUL05690
 MUL05700
 MUL05710
 MUL05720
 MUL05730
 MUL05740
 MUL05750
 MUL05760
 MUL05770
 MUL05780
 MUL05790
 MUL05800
 MUL05810
 MUL05820
 MUL05830
 MUL05840
 MUL05850
 MUL05860
 MUL05870
 MUL05880
 MUL05890
 MUL05900
 MUL05910
 MUL05920
 MUL05930
 MUL05940
 MUL05950
 MUL05960
 MUL05970
 MUL05980
 MUL05990
 MUL06000
 MUL06010
 MUL06020
 MUL06030
 MUL06040
 MUL06050
 MUL06060
 MUL06070
 MUL06080
 MUL06090
 MUL06100
 MUL06110

```

CALL CURVE(TVAL,SVALU,NPL,1)
CALL ENDPL(0)
RETURN
END

```

```

SUBROUTINE DERIVS(S,DS,NF,NS,F)

```

```

IMPLICIT REAL(A-H,O-Z)

```

```

REAL S(NS),DS(NS),F(NF)

```

```

COMMON/PARS/C1,C2,C3,C4,C5,C6,R1,R2,R3,R4,R5,R6

```

C Subroutine consists of Slow System Derivatives which are
C specified by the user for his particular model.

```

DS(1) = F(4)/(R3*C2) - (1/(R3*C2) + 1/(R3*C3))*S(1) + S(2)/(R3*C3)
DS(2) = S(1)/(R4*C3) - (1/(R4*C3) + 1.0/(R4*C4))*S(2) + S(3)/(R4*C4)
DS(3) = S(2)/(R5*C4) - (1/(R5*C4) + 1/(R5*C5))*S(3) + S(4)/(R5*C5)
DS(4) = S(3)/(R6*C5) - (1.0/(R6*C5) + 1.0/(R6*C6))*S(4)
DS(5) = S(4)/C6
DS(6) = 0.02 * ABS(36.0 - 5.29*SQRT(ABS(S(5))))**1.2*
+ SIGN(1.0,ABS(36.0-5.29*SQRT(ABS(S(5))))) - 0.02*S(6)
RETURN
END

```

```

SUBROUTINE DERIVF(F,DF,NF,NS,INTS)

```

```

IMPLICIT REAL(A-H,O-Z)

```

```

REAL F(NF),DF(NF),INTS(2)

```

```

COMMON/PARS/C1,C2,C3,C4,C5,C6,R1,R2,R3,R4,R5,R6

```

C Subroutine consists of Fast System Derivatives which are
C specified by the user for his particular model.

```

DF(1) = F(2)
DF(2) = -64.0*F(1) + 7.5*(2.0+INTS(1)-(F(1)*F(1)))*F(2)
DF(3) = 2.0*F(1)*F(2)/R1 + (F(4)-F(3))/(R1*C1)
DF(4) = F(3)/(R2*C1) - F(4)*(1.0/(R2*C1) + 1.0/(R2*C2)) + INTS(2)/(R1*C1)
RETURN
END

```

```

SUBROUTINE INIT

```

```

INTEGER NUM,RC,RLEN

```

```

REAL RES1

```

```

CHARACTER*8 KEY,MENUN

```

```

CHARACTER*8 FLDN(29)

```

```

CHARACTER*4 CC

```

MUL06120
MUL06130
MUL06140
MUL06150
MUL06160
MUL06170
MUL06180
MUL06190
MUL06200
MUL06210
MUL06220
MUL06230
MUL06240
MUL06250
MUL06260
MUL06270
MUL06280
MUL06290
MUL06300
MUL06310
MUL06320
MUL06330
MUL06340
MUL06350
MUL06360
MUL06370
MUL06380
MUL06390
MUL06400
MUL06410
MUL06420
MUL06430
MUL06440
MUL06450
MUL06460
MUL06470
MUL06480
MUL06490
MUL06500
MUL06510
MUL06520
MUL06530
MUL06540
MUL06550
MUL06560
MUL06570
MUL06580
MUL06590
MUL06600
MUL06610
MUL06630
MUL07050
MUL07060
MUL07070
MUL07080
MUL07090
MUL07100
MUL07110
MUL07120

COMMON/DIFF/PU(29)

C Xmenu used for Parameters and Initial Conditions

```

FLDN(1) = 'R1'
FLDN(2) = 'R2'
FLDN(3) = 'R3'
FLDN(4) = 'R4'
FLDN(5) = 'R5'
FLDN(6) = 'R6'
FLDN(7) = 'C1'
FLDN(8) = 'C2'
FLDN(9) = 'C3'
FLDN(10) = 'C4'
FLDN(11) = 'C5'
FLDN(12) = 'C6'
FLDN(13) = 'X3'
FLDN(14) = 'X4'
FLDN(15) = 'X5'
FLDN(16) = 'X6'
FLDN(17) = 'V'
FLDN(18) = 'S'
FLDN(19) = 'Y1'
FLDN(20) = 'Y2'
FLDN(21) = 'X1'
FLDN(22) = 'X2'
FLDN(23) = 'TINIT'
FLDN(24) = 'TFIN'
FLDN(25) = 'TOLERF'
FLDN(26) = 'TOLERS'
FLDN(27) = 'HSMIN'
FLDN(28) = 'HFMIN'
FLDN(29) = 'COMINT'

```

MENUN = 'OSCIL5'

CALL MCLSCR(NUM,RC)

CALL MLOAD(NUM,RC,MENUN)

CALL MPFMAP(NUM,RC,1)

CALL MALARM(NUM,RC,1)

CALL MPRINT(NUM,RC,2,PROUT)

CALL MDSPRD(NUM,RC,KEY)

CALL MEXIT(NUM,RC)

IF (KEY.EQ.'PF10') GOTO 25

IF (KEY.EQ.'PF12') STOP

25 DO 23 I = 1,22

CALL MSCR2D(NUM,RC,FLDN(I),CC,4,RLEN)

CALL MCVTCTF(PU(I),RC,CC,4,2)

23 CONTINUE

DO 28 I = 23,29

CALL MSCR2D(NUM,RC,FLDN(I),CC,7,RLEN)

CALL MCVTCTF(PU(I),RC,CC,7,2)

28 CONTINUE

RETURN

END

SUBROUTINE OUTPUT(T,S,NS)

IMPLICIT REAL(A-H,O-Z)

REAL S(NS)

```

MUL07130
MUL07140
MUL07150
MUL07160
MUL07170
MUL07180
MUL07190
MUL07200
MUL07210
MUL07220
MUL07230
MUL07240
MUL07250
MUL07260
MUL07270
MUL07280
MUL07290
MUL07300
MUL07310
MUL07320
MUL07330
MUL07340
MUL07350
MUL07360
MUL07370
MUL07380
MUL07390
MUL07400
MUL07410
MUL07420
MUL07430
MUL07440
MUL07450
MUL07460
MUL07470
MUL07480
MUL07490
MUL07500
MUL07510
MUL07520
MUL07530
MUL07540
MUL07550
MUL07560
MUL07570
MUL07580
MUL07590
MUL07600
MUL07610
MUL07620
MUL07630
MUL07640
MUL07650
MUL07660
MUL07670
MUL07680
MUL07690
MUL07700
MUL07710

```

COMMON/OUT/NPL,SVAL(400), TIME(400), SVAL1(400)

C Display values of Slow System Outputs in Tabular Form

NPL = NPL + 1

WRITE(6,98)T,S(1),S(6)

98 FORMAT(1X,F5.2,10X,F7.3,10X,F7.3)

SVAL (NPL) = S(1)

SVAL1(NPL) = S(6)

TIME(NPL) = T

RETURN

END

MUL07720

MUL07730

MUL07740

MUL07750

MUL07760

MUL07770

MUL07780

MUL07790

MUL07800

MUL07810

```

+....+....1....+....2....+....3....+....4....+....5....+....6....+....7....+....8+
1      /INITIALIZATION
2
3
4      KINDLY INITIALIZE VARIABLES.
5
6      Model Parameters      Experimentation Variables
7
8      Initial States      Control Variables
9      S.System      F.System
10
11      C1 = 6.25 mF  R1 = 8.00 kOhms X3(0) = 40.0 Y1(0) = 20.0  TINIT = 0.00
12
13      C2 = 4.25 mF  R2 = 8.00 kOhms X4(0) = 45.0 Y2(0) = 70.0  TFIN = 20.0
14
15      C3 = 1.25 mF  R3 = 8.00 kOhms X5(0) = 50.0 X1(0) = 80.0  TOLERF = 0.01
16
17      C4 = 1.25 mF  R4 = 8.00 kOhms X6(0) = 55.0 X2(0) = 85.0  TOLERS = 0.50
18
19      C5 = 1.25 mF  R5 = 8.00 kOhms V(0) = 60.0              HSMIN = 0.0001
20
21      C6 = 1.25 mF  R6 = 8.00 kOhms S(0) = 65.0              HFMIN = 0.00001
22
23                                     HBOUND = 0.10
24                                     COMINT = 0.20
25
26      Press: PF10 - to start simulation  PF12 - to quit
27
+....+....1....+....2....+....3....+....4....+....5....+....6....+....7....+....8+

```

Menu For Electronic Oscillator
Model: Multi-Rate Integration

Problem: Study Of Electronic Oscillator

Method: Multi-Rate Algorithm Based on
Runge-Kutta Merson

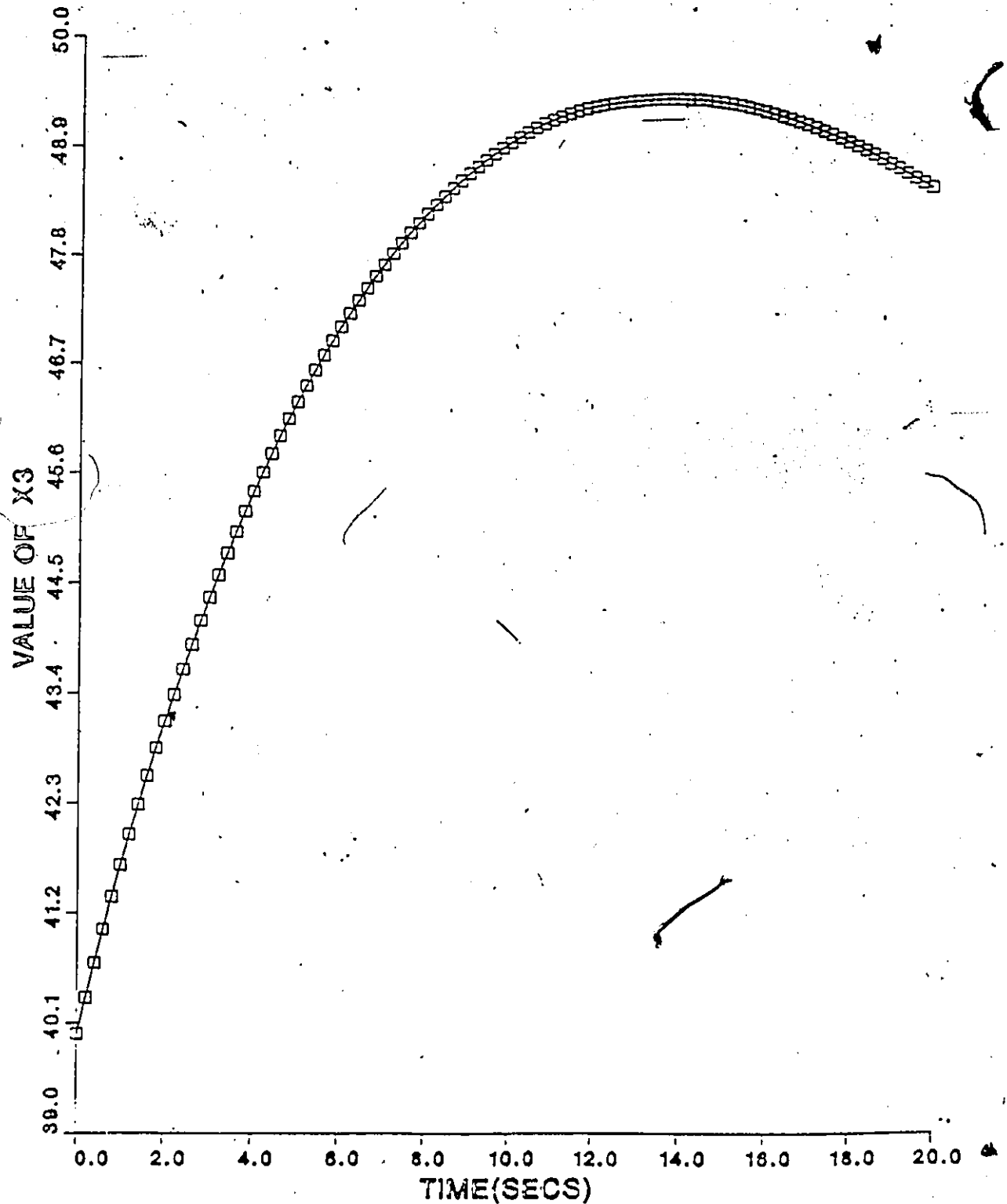
Time T	Inputs To Fast Routine X3	S
0.0	40.000	65.000
0.2	40.469	64.713
0.4	40.707	64.576
0.6	41.178	64.327
0.8	41.371	64.234
1.0	41.688	64.091
1.2	41.995	63.966
1.4	42.293	63.859
1.6	42.582	63.769
1.8	42.862	63.695
2.0	43.222	63.621
2.2	43.398	63.594
2.4	43.653	63.566
2.6	43.901	63.551
2.8	44.142	63.551
3.0	44.448	63.570
3.2	44.601	63.589
3.4	44.819	63.626
3.6	45.032	63.676
3.8	45.237	63.737
4.0	45.436	63.810
4.2	45.692	63.924
4.4	45.815	63.988
4.6	46.069	64.139
4.8	46.170	64.207
5.0	46.338	64.332
5.2	46.501	64.466
5.4	46.715	64.663
5.6	46.811	64.761
5.8	47.019	64.995
6.0	47.099	65.092
6.2	47.238	65.270
6.4	47.372	65.457
6.6	47.502	65.651
6.8	47.668	65.919
7.0	47.751	66.063
7.2	47.870	66.280
7.4	47.985	66.504
7.6	48.136	66.819
7.8	48.205	66.974
8.0	48.353	67.326
8.2	48.411	67.471
8.4	48.508	67.729
8.6	48.627	68.066
8.8	48.694	68.264
9.0	48.814	68.649
9.2	48.866	68.824
9.4	48.947	69.112
9.6	49.025	69.407
9.8	49.126	69.816
10.0	49.172	70.012
10.3	49.270	70.457
10.4	49.307	70.638
10.6	49.398	71.110
10.8	49.430	71.285
11.0	49.488	71.616
11.2	49.542	71.951
11.5	49.609	72.392
11.6	49.644	72.637
11.8	49.690	72.986
12.0	49.747	73.448
12.2	49.776	73.699
12.4	49.815	74.062
12.7	49.862	74.539
12.8	49.885	74.800
13.0	49.929	75.326
13.2	49.946	75.554

Problem: Study Of Electronic Oscillator

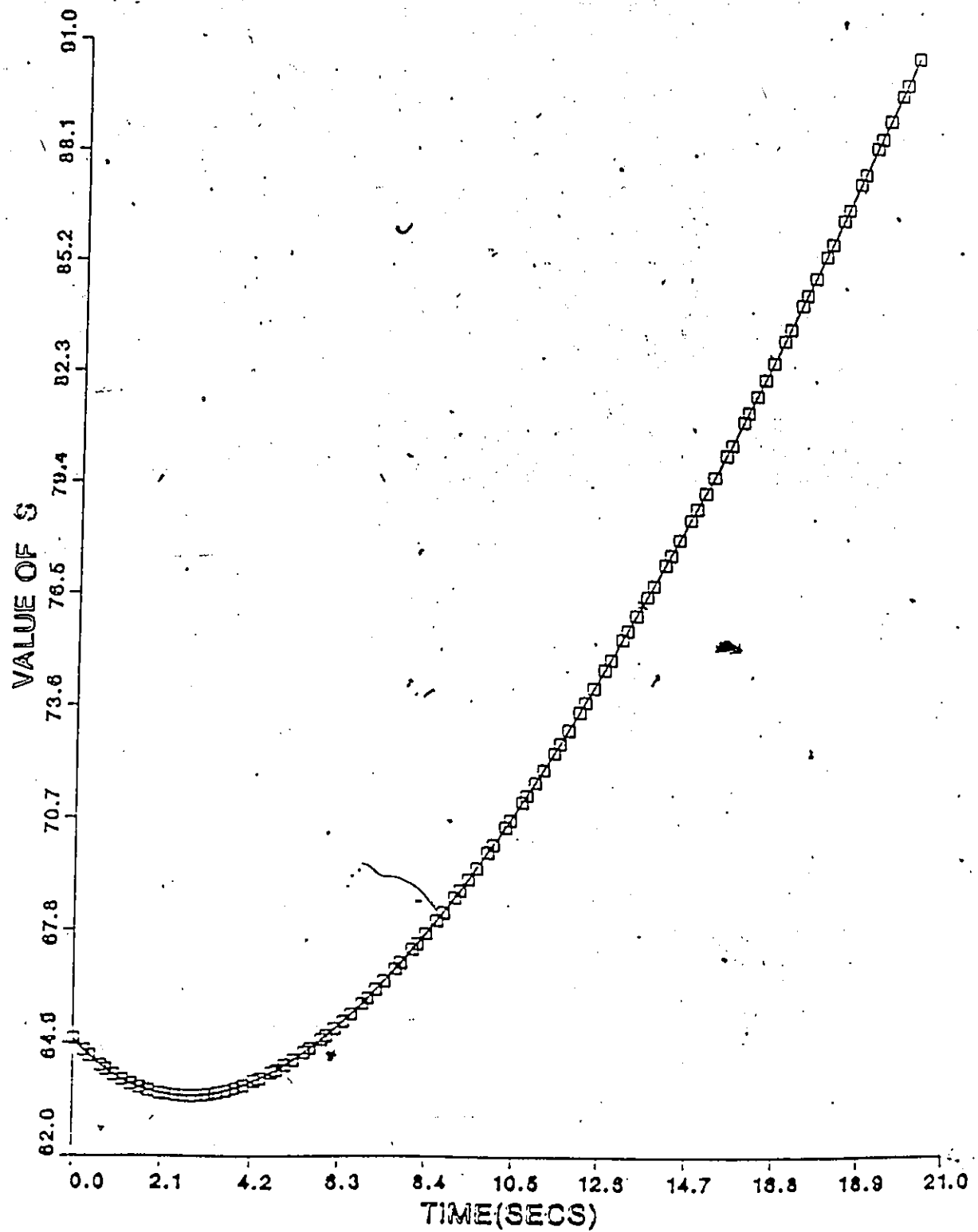
Method: Multi-Rate Algorithm Based on:
Runge-Kutta Merson

Time T	Inputs To Fast Routine X3	S
13.4	49.973	75.937
13.6	50.004	76.431
13.8	50.020	76.715
14.0	50.048	77.263
14.2	50.059	77.507
14.4	50.075	77.909
14.6	50.092	78.427
14.8	50.101	78.723
15.0	50.110	79.134
15.2	50.118	79.550
15.5	50.126	80.114
15.6	50.128	80.390
15.9	50.131	80.996
16.0	50.131	81.243
16.2	50.129	81.674
16.4	50.126	82.108
16.6	50.121	82.545
16.9	50.111	83.125
17.0	50.105	83.427
17.2	50.089	84.056
17.4	50.082	84.321
17.6	50.068	84.772
17.9	50.047	85.350
18.0	50.035	85.682
18.2	50.008	86.319
18.4	49.995	86.602
18.6	49.963	87.272
18.8	49.950	87.532
19.1	49.912	88.222
19.2	49.898	88.472
19.4	49.870	88.945
19.6	49.830	89.604
19.8	49.811	89.898
20.0	49.764	90.591

ELECTRONIC OSCILLATOR MODEL MULTI-RATE INTEGRATION METHOD



STUDY OF ELECTRONIC OSCILLATOR MODEL MULTI-RATE INTEGRATION METHOD



Appendix H. INTEGRATION ROUTINES FOR THE GEST RUN TIME LIBRARY

H.1. The Fourth Order Runge Kutta Algorithm

	SUBROUTINE RK4(T,Y,N,TFIN,H,HINIT,HBOUND,HMIN,TOL,COMINT,DERIV)	DIA01830.
C	Fourth - Order Runge Kutta Method Used To	DIA01840
C	Integrate Systems Having Frequent	DIA01850
C	Output Points But Not Requiring A	DIA01860
C	High Level Of Accuracy.	DIA01870
		DIA01880
C	Variable Declaration	DIA01890
	IMPLICIT REAL (A-H,O-Z)	DIA01900
	DIMENSION Y(N),DY1(15),DY2(15),DY3(15),DY4(15),F1(15),F2(15),	DIA01910
	+F3(15),DY(15)	DIA01920
	EXTERNAL DERIV	DIA01930
	CHARACTER*1 CHOICE	DIA01940
		DIA01950
C	Calculating Starting Step Size	DIA01960
	CALL DERIV(T,Y,DY,N)	DIA01970
	FDER = 0.0	DIA01980
	DO 29 I = 1,N	DIA01990
	IF (ABS(DY(I)).GT.FDER) THEN	DIA02000
	FDER = ABS(DY(I))	DIA02010
	ENDIF	DIA02020
29	CONTINUE	DIA02030
	IF (FDER.NE.0.0) THEN	DIA02040
	HPOS = SQRT(0.5 * TOL/FDER)	DIA02050
	IF (HBOUND.LE.0.0) THEN	DIA02060
	HBOUND = 0.1	DIA02070
	ENDIF	DIA02080
	IF (HPOS.GT.HBOUND) THEN	DIA02090
	HSTART = HBOUND	DIA02100
	ELSE	DIA02110
	HSTART = HPOS	DIA02120
	ENDIF	DIA02130
	ELSE	DIA02140
	IF (HBOUND.LE.0.0) THEN	DIA02150
	HBOUND = 0.1	DIA02160
	ENDIF	DIA02170
	HSTART = HBOUND	DIA02180
	ENDIF	DIA02190
	IF (HINIT.NE.0.0) THEN	DIA02200
	H = HINIT	DIA02210
	ELSE	DIA02220
	HINIT = HSTART	DIA02230
	H = HINIT	DIA02240
	ENDIF	DIA02250
		DIA02260
	IF (H.GT.HBOUND) THEN	DIA02270
	PRINT*,'HINIT > HBOUND. DO YOU WISH TO CARRY OUT INTEGRATION	DIA02280
	+ WITH THIS HINIT (Y) OR HBOUND (N)?'	DIA02290
	READ*, CHOICE	DIA02300
	IF (CHOICE.EQ.'Y') THEN	DIA02310
	H = HINIT	DIA02320
	ELSE	DIA02330
	H = HBOUND	DIA02340
	HINIT = HBOUND	DIA02350
	ENDIF	DIA02360
	ENDIF	DIA02370

```

IF (COMINT.LE.0) THEN
  COMINT = (TFIN - T)/100
ENDIF
IF (HMIN.LE.0.0) THEN
  HMIN = HINIT/10000
ENDIF
NFLAG = 0
TCOM = T + COMINT

```

Integrate system

```

99 IF (T.LT.TFIN) THEN
88   IF (T.LT.TCOM) THEN
      IF (((TCOM - T).LE.(HINIT+ HMIN)).AND.
+      (NFLAG.EQ. 0)) THEN
        H = (TCOM - T)/2.0
        NFLAG= 1
      ENDIF
      H1 = H * 0.5
      CALL DERIV(T,Y,DY1,N)
      DO 6 I = 1,N
        F1(I) = DY1(I) * H/2.0 + Y(I)
6      CONTINUE
      CALL DERIV(H1 + T,F1,DY2,N)
      DO 8 I = 1,N
        F2(I) = H * DY2(I)/2.0 + Y(I)
8      CONTINUE
      CALL DERIV(H1 + T,F2,DY3,N)
      DO 10 I = 1,N
        F3(I) = H*DY3(I) + Y(I)
10     CONTINUE
      CALL DERIV(H + T,F3,DY4,N)
      DO 16 I =1,N
        Y(I)=Y(I)+(DY1(I)+2.0*DY2(I)+2.0*DY3(I)+DY4(I))*H/6.0
16     CONTINUE
      T = T +H

```

Output Values Of Y and T at
each point of TOUT

```

C
C
ELSE
  CALL OUTPUT(Y,N,T)
  TCOM = TCOM + COMINT
  IF (TCOM.GE.TFIN) THEN
    TCOM = TFIN
  ENDIF
  NFLAG = 0
  H = HINIT
  GOTO 88
ENDIF
GOTO 99
ENDIF
CALL OUTPUT(Y,N,T)
RETURN
END

```

DIA02380
 DIA02390
 DIA02400
 DIA02410
 DIA02420
 DIA02430
 DIA02440
 DIA02450
 DIA02460
 DIA02470
 DIA02480
 DIA02490
 DIA02500
 DIA02510
 DIA02520
 DIA02530
 DIA02540
 DIA02550
 DIA02560
 DIA02570
 DIA02580
 DIA02590
 DIA02600
 DIA02610
 DIA02620
 DIA02630
 DIA02640
 DIA02650
 DIA02660
 DIA02670
 DIA02680
 DIA02690
 DIA02700
 DIA02710
 DIA02720
 DIA02730
 DIA02740
 DIA02750
 DIA02760
 DIA02770
 DIA02780
 DIA02790
 DIA02800
 DIA02810
 DIA02820
 DIA02830
 DIA02840
 DIA02850
 DIA02860
 DIA02870
 DIA02880

H.2 The Runge Kutta Fehlberg Algorithm

```

SUBROUTINE RKFEL(T,Y,N,TFIN,H,ORD,HBOUND,HMIN,COMINT,DERIV,TOL)
C      Sixth Order Variable Step R-K Felberg
C      used to integrate systems with
C      infrequent output to a high level of
C      accuracy.
C
C      Variable Declaration
IMPLICIT REAL*4 (A-H,O-Z)
DIMENSION Y(10),DY(10),DY1(10),DY2(10),DY3(10),DY4(10),DY5(10),
+ F(10),F1(10),F2(10),F3(10),F4(10),ERR(10)
CHARACTER*1 CHOICE
REAL NUVAL
IF (COMINT.EQ.0) COMINT = (TFIN-T)/70
NFLAG= 0
TCOM = T + COMINT
C      Calculate Starting Step Size
CALL DERIV(T,Y,DY,N)
FDER = 0.0
DO 29 I = 1,N
  IF (ABS(DY(I)).GT.FDER) THEN
    FDER = ABS(DY(I))
  ENDIF
29 CONTINUE
IF (FDER.NE.0.0) THEN
  HPOS = SQRT(0.5 * TOL/FDER)
  IF (HBOUND.LE.0.0) THEN
    HBOUND = 0.1
  ENDIF
  IF (HPOS.GT.HBOUND) THEN
    HSTART = HBOUND
  ELSE
    HSTART = HPOS
  ENDIF
ELSE
  IF (HBOUND.LE.0.0) THEN
    HBOUND = 0.1
  ENDIF
  HSTART = HBOUND
ENDIF
IF (HINIT.NE.0.0) THEN
  H = HINIT
ELSE
  HINIT = HSTART
  H = HINIT
ENDIF

IF (H.GT.HBOUND) THEN
  PRINT*, 'HINIT > HBOUND. DO YOU WISH TO CARRY OUT INTEGRATION
+ WITH THIS HINIT (Y) OR HBOUND (N) ?'
  READ*, CHOICE
  IF (CHOICE.EQ.'Y') THEN
    H = HINIT
  ELSE
    H = HBOUND
    HINIT = HBOUND
  ENDIF

```

```

ENDIF
IF (COMINT.LE.0.0) THEN /
  COMINT = (TFIN - T)/100
ENDIF
IF (HMIN.LE.0.0) THEN
  HMIN = HINIT /1000
ENDIF

```

Integrate system

```

C
88 IF (T.LT.TFIN) THEN
188 IF (T.LT.TCOM) THEN
  IF (((TCOM - T).LE.(H + HMIN)) .AND. (NFLAG.EQ.0)) THEN
    H = (TCOM - T)/2
    NFLAG = 1
  ENDIF
  CALL DERIV(T,Y,DY,N)
  DO 6 I = 1,N
    F(I) = DY(I) * H/4.0 + Y(I)
  CONTINUE
  CALL DERIV(H/4.0 + T,F,DY1,N)
  DO 8 I = 1,N
    F1(I) = (3.0*DY(I) + 9.0 * DY1(I))*H/32.0 + Y(I)
  CONTINUE
  CALL DERIV(3.0*H/8.0 + T,F1,DY2,N)
  DO 10 I = 1,N
    F2(I) = (1932.0*DY(I) + 7296.0*DY2(I) - 7200.0*DY1(I))
    *H/2197.0 + Y(I)
  CONTINUE
  CALL DERIV(12*H/13.0 + T,F2,DY3,N)
  DO 12 I = 1,N
    F3(I) = H*(439.0*DY(I)/216.0 - 8.0*DY1(I) + 3680.0*DY2(I)
    /513.0 - 845.0*DY3(I)/4104.0) + Y(I)
  CONTINUE
  CALL DERIV(T + H,F3,DY4,N)
  DO 14 I = 1,N
    F4(I) = H*(-8.0*DY(I)/27.0 + 2.0*DY1(I) - 3544.0 * DY2(I)/
    2565.0 + 1859.0*DY3(I)/4104.0 - 11.0*DY4(I)/40.0) + Y(I)
  CONTINUE
  CALL DERIV(T+H/2.0,F4,DY5,N)
  ERRMAX = 0.0
  DO 40 I = 1,N
    ERR(I) = ABS(DY(I)/360.0 - 128.0*DY2(I)/4275.0 - 2197.0
    *DY3(I)/75240.0 + DY4(I)/50.0 + 2.0*DY5(I)/55.0)
    IF (ERR(I).GT.ERRMAX) THEN
      ERRMAX = ERR(I)
    ENDIF
  CONTINUE
  IF (ERRMAX.LE.TOL) THEN
    T = T + H
    DO 16 I = 1,N
      Y(I) = Y(I) + H*(25.0*DY(I)/216.0 + 1408.0*DY2(I)/
      2565.0 + 2197.0 * DY3(I)/4104.0 - DY4(I)/5.0)
    CONTINUE
  ENDIF
  IF (NFLAG.EQ.0) THEN

```

```

FEL02240
FEL02250
FEL02260
FEL02270
FEL02280
FEL02290
FEL02300
FEL02310
FEL02320
FEL02330
FEL02340
FEL02350
FEL02360
FEL02370
FEL02380
FEL02390
FEL02400
FEL02410
FEL02420
FEL02430
FEL02440
FEL02450
FEL02460
FEL02470
FEL02480
FEL02490
FEL02500
FEL02510
FEL02520
FEL02530
FEL02540
FEL02550
FEL02560
FEL02570
FEL02580
FEL02590
FEL02600
FEL02610
FEL02620
FEL02630
FEL02640
FEL02650
FEL02660
FEL02670
FEL02680
FEL02690
FEL02700
FEL02710
FEL02720
FEL02730
FEL02740
FEL02750
FEL02760
FEL02770
FEL02780
FEL02790
FEL02800
FEL02810
FEL02820

```

```

      H = 0.9 * H * (TOL/ERRMAX) ** (1/ORD)
      IF (H.LT.HMIN) THEN
        PRINT*, 'HMIN Exceeded. Do you wish to change value of
+ HMIN (Y) or would you rather halt the integration and further
+investigate the model (N) ?'
        READ*, CHOICE
        IF (CHOICE.EQ.'Y') THEN
          PRINT*, 'Please enter new value of HMIN. Note that
+for integration to proceed, it should be less than', H
          READ*, NUVAL
          HMIN = NUVAL
        ELSE
          STOP
        ENDIF
      ENDIF
      IF (H.GT.HMAX) THEN
        H = HMAX
      ENDIF
    ENDIF
  ELSE
    CALL OUTPUT(Y,N,T)
    TCOM = TCOM + COMINT
    IF ((TCOM.GE.TFIN) .AND. (T.NE.TFIN)) THEN
      TCOM = TFIN
    ENDIF
    NFLAG = 0
    GOTO 88
  ENDIF
  GOTO 188
ENDIF
CALL OUTPUT(Y,N,T)
RETURN
END

```

```

FEL02830
FEL02840
FEL02850
FEL02860
FEL02870
FEL02880
FEL02890
FEL02900
FEL02910
FEL02920
FEL02930
FEL02940
FEL02950
FEL02960
FEL02970
FEL02980
FEL02990
FEL03000
FEL03010
FEL03020
FEL03030
FEL03040
FEL03050
FEL03060
FEL03070
FEL03080
FEL03090
FEL03100
FEL03110
FEL03120
FEL03130
FEL03140
FEL03150

```

C
C
C

H.3 The Fourth Order Adams Algorithm

```

SUBROUTINE ADAMS(T,Y,N,TFIN,H,NORD,HBOUND,HMIN,DERIV,COMINT,TOL,K) ADA01860
C      FourthOrder Variable Step Adams Predictor Corrector Method ADA01870
C      used to integrate systems to a high level of accuracy. ADA01880
C
C      Variable Declaration ADA01890
      IMPLICIT REAL*4(A-H,O-Z) ADA01900
      DIMENSION T(6000),Y(6000,5),Y1(5),Y2(5),Y3(5), ADA01910
+      Y4(5),VC(6000,5),TIME(300),YVAL1(300),YVAL2(300), ADA01920
+      DY(6000,5) ADA01930
      ADA01940
      ADA01950
      EXTERNAL DERIV ADA01960
      COMMON/STIFF/NCHECK ADA01970
      CHARACTER*1 CHOICE ADA01980
      REAL NUVAL ADA01990
      ADA02000
      K = 1 ADA02010
C      CALCULATING STARTING STEP SIZE ADA02020
      CALL DERIV(T,Y,DY,N,K) ADA02030
      FDER = 0.0 ADA02040
      DO 29 I = 1,N ADA02050
        IF (ABS(DY(1,I)).GT.FDER) THEN ADA02060
          FDER = ABS(DY(1,I)) ADA02070
        ENDIF ADA02080
29 CONTINUE ADA02090
      IF (FDER.NE.0.0) THEN ADA02100
        HPOS = SQRT(0.5 * TOL/FDER) ADA02110
        IF (HBOUND.LE.0.0) THEN ADA02120
          HBOUND = 0.1 ADA02130
        ENDIF ADA02140
        IF (HPOS.GT.HBOUND) THEN ADA02150
          HSTART = HBOUND ADA02160
        ELSE ADA02170
          HSTART = HPOS ADA02180
        ENDIF ADA02190
      ELSE ADA02200
        IF (HBOUND.LE.0.0) THEN ADA02210
          HBOUND = 0.1 ADA02220
        ENDIF ADA02230
        HSTART = HBOUND ADA02240
      ENDIF ADA02250
      IF (HINIT.NE.0.0) THEN ADA02260
        H = HINIT ADA02270
      ELSE ADA02280
        HINIT = HSTART ADA02290
        H = HINIT ADA02300
      ENDIF ADA02310
      IF (H.GT.HBOUND) THEN ADA02320
        PRINT*,'HINIT > HBOUND. DO YOU WISH TO CARRY OUT INTEGRATION ADA02330
+ WITH THIS HINIT (Y) OR HBOUND (N)?' ADA02340
        READ*, CHOICE ADA02350
        IF (CHOICE.EQ.'Y') THEN ADA02360
          H = HINIT ADA02370
        ELSE ADA02380
          H = HBOUND ADA02390
          HINIT = HBOUND ADA02400
        ENDIF ADA02410

```

ENDIF	ADA02420
ENDIF	ADA02430
IF (COMINT.LE.0) THEN	ADA02440
COMINT = (TFIN - T(1))/30	ADA02450
ENDIF	ADA02460
IF (HMIN.LE.0.0) THEN	ADA02470
HMIN = HINIT/10000	ADA02480
ENDIF	ADA02490
TCOM = TCOM + COMINT	ADA02500
T1 = T(1)	ADA02510
Compute steps for stiffness check	ADA02520
NSTEPS = (TFIN-T1)/HINIT * 10	ADA02530
Compute the first three	ADA02540
values by Fourth-Order	ADA02550
Runge Kutta	ADA02560
CALL RK4(H,Y,K,T1,DERIV,Y2,T2,Y3,T3,Y4,T4,N)	ADA02570
NFLG = 1	ADA02580
MFLG = 1	ADA02590
NFLAG = 0	ADA02600
K = 5	ADA02610
DO 62 I = 1,N	ADA02620
Y(K-1,I) = Y4(I)	ADA02630
Y(K-2,I) = Y3(I)	ADA02640
Y(K-3,I) = Y2(I)	ADA02650
62 CONTINUE	ADA02660
T(K-1) = T4	ADA02670
T(K-2) = T3	ADA02680
T(K-3) = T2	ADA02690
TNOW = T(K-1) + H	ADA02700
99 IF (T(K-1).LE.TFIN) THEN	ADA02710
88 IF ((T(K-1).LE.TCOM) .OR. (MFLG.EQ.1)) THEN	ADA02720
IF ((TCOM - T(K-1)).LE.(H+ HMIN)) .AND. (NFLAG.EQ.0)) THEN	ADA02730
H = (TCOM - T(K-1))/2.0	ADA02740
NFLAG = 1	ADA02750
ENDIF	ADA02760
CALL ADCOMP(H,Y,T,N,K,ERRMAX,VC)	ADA02770
NCHECK = NCHECK + 1	ADA02780
IF (ERRMAX.LE.TOL) THEN	ADA02790
DO 101 I = 1,N	ADA02800
Y(K,I) = VC(K,I)	ADA02810
101 CONTINUE	ADA02820
T(K) = TNOW	ADA02830
MFLG = 0	ADA02840
NFLAG = 0	ADA02850
K = K + 1	ADA02860
ENDIF	ADA02870
IF (ERRMAX .GT. 0.0) THEN	ADA02880
IF ((ERRMAX.LE.(0.9*TOL)) .AND. (NFLAG.EQ.0)) THEN	ADA02890
HOLD = H	ADA02900
H = 0.9 * H * (TOL/ERRMAX) ** (1/ORD)	ADA02910
IF ((T(K-1) + 3*H).GE.TCOM) THEN	ADA02920
HOLD = TCOM - T(K-1)	ADA02930
H = HOLD	ADA02940
ENDIF	ADA02950
NFLAG = 1	ADA02960
DO 59 I = 1,N	ADA02970
Y(K,I) = Y(K-1,I)	ADA02980
59 CONTINUE	ADA02990
T1 = T(K-1)	ADA03000

```

CALL RK4(H,Y,K,T1,DERIV,Y2,T2,Y3,T3,Y4,T4,N)
DO 65 I = 1,N
    Y(K+2,I) = Y4(I)
    Y(K+1,I) = Y3(I)
    Y(K,I) = Y2(I)
65 CONTINUE
    T(K+2) = T4
    T(K+1) = T3
    T(K) = T2
    K = K + 3
ENDIF
ENDIF
IF (ERRMAX.GT.TOL) THEN
    MFLG = 1
    H = 0.9 * H * (TOL/ERRMAX) ** (1/NORD)
    IF (H.LT.HMIN) THEN
        PRINT*,'HMIN Exceeded. Do you wish to change value of
+ HMIN (Y) or would you rather halt the integration and further
+investigate the model (N) ?'
        READ*,CHOICE
        IF (CHOICE.EQ.'Y') THEN
            PRINT*,'Please enter new value of HMIN. Note that
+for integration to proceed, it should be less than',H
            READ*,NUVAL
            HMIN = NUVAL
        ELSE
            STOP
        ENDIF
    ENDIF
    IF (NFLG.EQ.1) K = K-3
    DO 150 I = 1,N
        Y(K,I)=Y(K-1,I)
150 CONTINUE
    T1 = T(K-1)
    CALL RK4(H,Y,K,T1,DERIV,Y2,T2,Y3,T3,Y4,T4,N)
    DO 67 I = 1,N
        Y(K+2,I) = Y4(I)
        Y(K+1,I) = Y3(I)
        Y(K,I) = Y2(I)
67 CONTINUE
    T(K+2) = T4
    T(K+1) = T3
    T(K) = T2
    K = K + 3
    NFLG = 1
ENDIF
TNOW = T(K-1) + H
T(K) = T(K-1) + H
C PRINT*,'TNOW = ',TNOW
C PRINT*,'Y(K,1) = ',Y(K,1)
C PRINT*,'Y(K,2) = ',Y(K,2)
C PRINT*,'H = ',H
ELSE
    CALL OUTPUT(Y,N,TNOW,K)
    TCOM = TCOM + COMINT
    IF ((TCOM.GE.TFIN) .AND. (TNOW.NE.TFIN)) THEN
        TCOM = TFIN
    ENDIF

```

ADA03010
 ADA03020
 ADA03030
 ADA03040
 ADA03050
 ADA03060
 ADA03070
 ADA03080
 ADA03090
 ADA03100
 ADA03110
 ADA03120
 ADA03130
 ADA03140
 ADA03150
 ADA03160
 ADA03170
 ADA03180
 ADA03190
 ADA03200
 ADA03210
 ADA03220
 ADA03230
 ADA03240
 ADA03250
 ADA03260
 ADA03270
 ADA03280
 ADA03290
 ADA03300
 ADA03310
 ADA03320
 ADA03330
 ADA03340
 ADA03350
 ADA03360
 ADA03370
 ADA03380
 ADA03390
 ADA03400
 ADA03410
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 ADA03450
 ADA03460
 ADA03470
 ADA03480
 ADA03490
 ADA03500
 ADA03510
 ADA03520
 ADA03530
 ADA03540
 ADA03550
 ADA03560
 ADA03570
 ADA03580
 ADA03590

```

      NFLAG = 0
      GOTO 88
    ENDIF
    GOTO 99
  ENDIF
  CALL OUTPUT(Y,N,TNOW,K)
  IF (NCHECK.GT.NSTEPS) THEN
    PRINT*,'Test suspects Model to be stiff with time constants
+varying greatly'
  ENDIF
  RETURN
END

```

ADA03600
ADA03610
ADA03620
ADA03630
ADA03640
ADA03650
ADA03660
ADA03670
ADA03680
ADA03690
ADA03700
ADA03710
ADA03720
ADA03730
ADA03740
ADA03750
ADA03760
ADA03770
ADA03780
ADA03790
ADA03800
ADA03810
ADA03820
ADA03830
ADA03840
ADA03850
ADA03860
ADA03870
ADA03880
ADA03890
ADA03900
ADA03910
ADA03920
ADA03930
ADA03940
ADA03950
ADA03960
ADA03970
ADA03980
ADA03990
ADA04000
ADA04010
ADA04020
ADA04030
ADA04040
ADA04050
ADA04060
ADA04070
ADA04080
ADA04090
ADA04100
ADA04110
ADA04120
ADA04130
ADA04140
ADA04150
ADA04160
ADA04170
ADA04180

```

SUBROUTINE RK4(H,Y,K,T1,DERIV,Y2,T2,Y3,T3,Y4,T4,N)

C   The Fourth-Order Runge-Kutta Method
C   is used as a starter to determine
C   the four previous function evaluations
C   needed by the Adams Method. It is
C   invoked at the beginning of the simul-
C   ation and at each step size change.

C                                     Variable Declaration

      IMPLICIT REAL*4 (A-H,O-Z)
      DIMENSION Y(6000,5),DY1(6000,5),DY2(6000,5),DY3(6000,5),
+ DY4(6000,5),P1(6000,5),P2(6000,5),P3(6000,5),Y2(5),Y3(5),Y4(5)
      COMMON/STIFF/NCHECK
      EXTERNAL DERIV

      H1 = H * 0.5
      KC = 1
      DO 5 KC = 1,3
        CALL DERIV(T1,Y,DY1,N,K)
        DO 6 I = 1,N
          P1(K,I) = (DY1(K,I)*H/2.0) + Y(K,I)
6        CONTINUE
        CALL DERIV(H1 + T1,P1,DY2,N,K)
        DO 8 I = 1,N
          P2(K,I) = H * DY2(K,I)/2.0 + Y(K,I)
8        CONTINUE
        CALL DERIV(H1 + T1,P2,DY3,N,K)
        DO 10 I = 1,N
          P3(K,I) = H*DY3(K,I) + Y(K,I)
10       CONTINUE
        CALL DERIV(H + T1,P3,DY4,N,K)
        DO 16 I = 1,N
          Y(K,I) = Y(K,I) + (DY1(K,I) + 2.0*DY2(K,I)
+          + 2.0*DY3(K,I) + DY4(K,I)) *H/6.0
16       CONTINUE
        IF (KC.EQ.1) THEN
          DO 11 I = 1,N
            Y2(I) = Y(K,I)
11          CONTINUE
          T2 = T1 + H
        ELSEIF (KC.EQ.2) THEN
          DO 12 I = 1,N

```

	Y3(I) = Y(K,I)	ADA04190
12	CONTINUE	ADA04200
	T3 = T1 + H	ADA04210
	ELSEIF (KC.EQ.3) THEN	ADA04220
	DO 13 I = 1,N	ADA04230
	Y4(I) = Y(K,I)	ADA04240
13	CONTINUE	ADA04250
	T4 = T1	ADA04260
	ENDIF	ADA04270
	T1 = T1 + (KC) * H	ADA04280
5	CONTINUE	ADA04290
	NCHECK = NCHECK + 3	ADA04300
	RETURN	ADA04310
	END	ADA04320
		ADA04330
		ADA04570
	SUBROUTINE ADCOMP (H,Y,T,N,K,ERRMAX,VC)	ADA04580
	IMPLICIT REAL*4 (A-H,O-Z)	ADA04590
	DIMENSION Y(6000,5),T(6000),VP(6000,5),VC(6000,5),ERR(5),	ADA04600
+	DY(6000,5),DVP(6000,5)	ADA04610
		ADA04620
C	This subroutine performs the calculations	ADA04630
C	of the predictor and corrector for the	ADA04640
C	Adams Method.	ADA04650
		ADA04660
	CALL DERIV(T,Y,DY,N,K-1)	ADA04670
	CALL DERIV(T,Y,DY,N,K-2)	ADA04680
	CALL DERIV(T,Y,DY,N,K-3)	ADA04690
	CALL DERIV(T,Y,DY,N,K-4)	ADA04700
		ADA04710
	DO 50 I = 1,N	ADA04720
	VP(K,I) = Y(K-1,I) + H/24.0 *(55.0*DY(K-1,I) - 59.0*DY(K-2,I)	ADA04730
+	+ 37.0*DY(K-3,I) - 9.0*DY(K-4,I))	ADA04740
50	CONTINUE	ADA04750
	CALL DERIV(T,VP,DVP,N,K)	ADA04760
	DO 51 I = 1,N	ADA04770
	VC(K,I) = Y(K-1,I) + H/24.0*(9.0*DVP(K,I) + 19.0	ADA04780
+	* DY(K-1,I) - 5.0*DY(K-2,I) + DY(K-3,I))	ADA04790
51	CONTINUE	ADA04800
	ERRMAX= 0.0	ADA04810
	DO 100 I = 1,N	ADA04820
	ERR(I) = ABS(VC(K,I)-VP(K,I))/(10.0*H)	ADA04830
	IF (ERR(I).GT.ERRMAX) THEN	ADA04840
	ERRMAX = ERR(I)	ADA04850
	ENDIF	ADA04860
100	CONTINUE	ADA04870
	RETURN	ADA04880
	END	ADA04890

H.4 The Multi-Rate Integration Algorithm

SUBROUTINE	SRATE(NS,NF,S,F,HS,DERIVS,T,TFIN)	MUL02230
IMPLICIT	REAL(A-H,O-Z)	MUL02240
REAL	F(NF),S(NS),ERR(10),PS(10),P2S(10),P3S(10),DP3S(10)	MUL02250
COMMON/SAME/	DS(10),P1S(10),DPS(10),DP1S(10),DP2S(10)	MUL02260
COMMON/SLOW/TOLERS,	HSMAX,HSMIN,COMINT	MUL02270
EXTERNAL	DERIVF,DERIVS	MUL02280
CHARACTER*1	CHANGE, CHOICE	MUL02290
		MUL02300
	Integration of Slow System	MUL02310
	Utilizing Integration Algorithm	MUL02320
	Based on Runge-Kutta Merson	MUL02330
	Variable Step Method.	MUL02340
	HS- Slow System HF- Fast System	MUL02350
ORD	= 5	MUL02360
IF (COMINT.LE.0.0) THEN		MUL02370
COMINT	= (TFIN - T)/100	MUL02380
ENDIF		MUL02390
TCOM	= T + COMINT	MUL02400
		MUL02410
	Calculate Starting Step Size	MUL02420
CALL	DERIVS(S,DS,NF,NS,F)	MUL02430
FDER	= 0.0	MUL02440
DO 39 I	= 1,N	MUL02450
IF (ABS(DS(I)).GT.FDER) THEN		MUL02460
FDER	= ABS(DS(I))	MUL02470
ENDIF		MUL02480
39 CONTINUE		MUL02490
IF (FDER.NE.0.0) THEN		MUL02500
HPOS	= SQRT(0.5 * TOL/FDER)	MUL02510
IF (HBOUND.LE.0.0) THEN		MUL02520
HBOUND	= 0.1	MUL02530
ENDIF		MUL02540
IF (HPOS.GT.HBOUND) THEN		MUL02550
HSTART	= HBOUND	MUL02560
ELSE		MUL02570
HSTART	= HPOS	MUL02580
ENDIF		MUL02590
ELSE		MUL02600
IF (HBOUND.LE.0.0) THEN		MUL02610
HBOUND	= 0.1	MUL02620
ENDIF		MUL02630
HSTART	= HBOUND	MUL02640
ENDIF		MUL02650
IF (HINIT.NE.0.0) THEN		MUL02660
HS	= HINIT	MUL02670
ELSE		MUL02680
HINIT	= HSTART	MUL02690
HS	= HINIT	MUL02700
ENDIF		MUL02710
		MUL02720
IF (HS.GT.HBOUND) THEN		MUL02730
PRINT*, 'HINIT > HBOUND. DO YOU WISH TO CARRY OUT INTEGRATION		MUL02740
+ WITH THIS HINIT (Y) OR HBOUND (N)?'		MUL02750
READ*, CHOICE		MUL02760
IF (CHOICE.EQ.'Y') THEN		MUL02770
HS	= HINIT	MUL02780

```

ELSE
  HS = HBOUND
  HINIT = HBOUND
ENDIF
ENDIF
IF (COMINT.LE.0) THEN
  COMINT = (TFIN - T)/100
ENDIF
IF (HMIN.LE.0.0) THEN
  HMIN = HINIT/10000
ENDIF

99 IF (T.LT. TFIN) THEN

188 IF (T.LT.TCOM) THEN
  IF (((TCOM - T).LE.(HS + HSMIN)) .AND. (NFLAG.EQ.0)) THEN
    HS = (TCOM - T)/2
    NFLAG = 1
  ENDIF
  TBEG = T

C          Determine K1 for components of
C          Slow System Represented By DS Below
          CALL DERIVS(S,DS,NF,NS,F)

C          Find Predicted Value of Slow
C          System Vector Y for all its
C          Components.
          DO 12 I = 1,NS
            PS(I) = S(I) + HS/3.0 * DS(I)
12 CONTINUE

C          Integrate Fast System between
C          TN and TN + H/3 to determine
C          Components of X involved in
C          Coupling to Slow System
            TF = T + HS/3.0
            CALL FRATE(NS,NF,S,F,HS,DERIVF,TF,T,TBEG)

C          Determine K2 for components of
C          Slow System.
            CALL DERIVS(PS,DPS,NF,NS,F)

C          Determine K3 for components of
C          Slow System.
            DO 14 I =1,NS
              P1S(I) = S(I) + HS/6.0 * (DS(I) + DPS(I))
14 CONTINUE
              CALL DERIVS(P1S,DP1S,NF,NS,F)

C          Integrate Fast System Between
C          TN + H/3 and TN + H/2 to determine
C          Components of X involved in
C          Coupling to Slow System

```

MUL02790
 MUL02800
 MUL02810
 MUL02820
 MUL02830
 MUL02840
 MUL02850
 MUL02860
 MUL02870
 MUL02880
 MUL02890
 MUL02900
 MUL02910
 MUL02920
 MUL02930
 MUL02940
 MUL02950
 MUL02960
 MUL02970
 MUL02980
 MUL02990
 MUL03000
 MUL03010
 MUL03020
 MUL03030
 MUL03040
 MUL03050
 MUL03060
 MUL03070
 MUL03080
 MUL03090
 MUL03100
 MUL03110
 MUL03120
 MUL03130
 MUL03140
 MUL03150
 MUL03160
 MUL03170
 MUL03180
 MUL03190
 MUL03200
 MUL03210
 MUL03220
 MUL03230
 MUL03240
 MUL03250
 MUL03260
 MUL03270
 MUL03280
 MUL03290
 MUL03300
 MUL03310
 MUL03320
 MUL03330
 MUL03340
 MUL03350
 MUL03360
 MUL03370


```

      STOP
    ENDIF
  ENDIF
  IF (HS.GT.HSMAX) THEN
    HS = HSMAX
  ENDIF
ENDIF
ELSE
  CALL OUTPUT(T,S,NS)
  TCOM = TCOM + COMINT
  IF ((TCOM.GE.TFIN) .AND. (T.NE.TFIN)) THEN
    TCOM = TFIN
  ENDIF
  NFLAG = 0
  GOTO 99
ENDIF
GOTO 188
ENDIF
CALL OUTPUT(T,S,NS)
RETURN
END

```

MUL03970
MUL03980
MUL03990
MUL04000
MUL04010
MUL04020
MUL04030
MUL04040
MUL04050
MUL04060
MUL04070
MUL04080
MUL04090
MUL04100
MUL04110
MUL04120
MUL04130
MUL04140
MUL04150
MUL04160
MUL04170
MUL04180
MUL04190
MUL04200
MUL04210
MUL04220
MUL04230
MUL04240
MUL04250
MUL04260
MUL04270
MUL04280
MUL04290
MUL04300
MUL04310
MUL04320
MUL04330
MUL04340
MUL04350
MUL04360
MUL04370
MUL04380
MUL04390
MUL04400
MUL04410
MUL04420
MUL04430
MUL04440
MUL04450
MUL04460
MUL04470
MUL04480
MUL04490
MUL04500
MUL04510
MUL04520
MUL04530
MUL04540
MUL04550

SUBROUTINE FRATE(NS,NF,S,F,HS,DERIVF,TF,T,TBEG)
IMPLICIT REAL(A-H,O-Z)
REAL F(NF),S(NS),W1(10),W2(10),W3(10),W4(10),ERR(10),
+INTS(4),DF1(10),DF2(10),DF3(10),DF4(10),DF5(10),DF(10)
COMMON/SAME/DS(10),P1S(10),DPS(10),DP1S(10),DP2S(10)
COMMON/FAST/TOLERF,HFMAX,HFMIN
CHARACTER*1 CHECK

C Subroutine For Fast Subsystem
C Integration. The Runge-Kutta
C Merson Method Is Utilized.

HFMIN = 0.000000000000000001
ORD = 5
HF = HINIT

TNOW = T

5 IF (T.LT.TF) THEN

C Depending on the time interpolate
C or extrapolate for values of Slow
C System Components involved in coupling

IF (T.LT.TBEG + HS/3.0) THEN
CALL INTER1(T,TNOW,S,DS,NS,INTS)
IF (NFIRST.EQ.0) THEN

C Calculate Starting Step Size
CALL DERIVF(F,DF,NF,NS,INTS)
FDER = 0.0
DO 29 I = 1,NF
IF (ABS(DF(I)).GT.FDER) THEN
FDER = ABS(DF(I))
ENDIF

```

29      CONTINUE
      HPOS = SQRT(0.5 * TOLERF/FDER)
      IF (HFMAX.LE.0.0) THEN
          HFMAX = 0.1
      ENDIF
      IF (HPOS.GT.HFMAX) THEN
          HINIT = HFMAX
      ELSE
          HINIT = HPOS
      ENDIF
      IF (HFMIN.LE.0.0) THEN
          HFMIN = HINIT/10000
      ENDIF
      HF = -HINIT
      ENDIF
      NFIRST = 1
      ELSE IF (T.LT. TBEG + HS/2.0) THEN
          CALL INTER2 (T,TNOW,P1S,DS,DPS,DP1S,NS,INTS)
      ELSE IF (T.LT. TBEG + HS) THEN
          CALL EXTRAP (T,TNOW,P1S,DP2S,NS,INTS)
      ENDIF
      CALL DERIVF (F,DF1,NF,NS,INTS)
      DO 31 I =1,NF
          W1(I) = DF1(I) * HF/3.0 + F(I)
31      CONTINUE
      CALL DERIVF (W1,DF2,NF,NS,INTS)
      DO 33 I=1,NF
          W2(I) = (DF1(I)+DF2(I))*HF/6.0 + F(I)
33      CONTINUE
      CALL DERIVF (W2,DF3,NF,NS,INTS)
      DO 35 I=1,NF
          W3(I) = (DF1(I) + 3.0*DF3(I)) * HF*0.125 +F(I)
35      CONTINUE
      CALL DERIVF (W3,DF4,NF,NS,INTS)
      DO 37 I=1,NF
          W4(I) = DF1(I)*HF*0.5-DF3(I)*HF*1.5+DF4(I)*HF*2.0 +F(I)
37      CONTINUE
      CALL DERIVF (W4,DF5,NF,NS,INTS)
      C
      ERRMAX = 0.0
      DO 41 I =1,NF
          ERR(I) = HF*(DF1(I) *HF/3.0-1.5*HF*DF3(I) +4.0* DF4(I)*HF
          + /3.0 -HF*DF5(I)/6.0)
          IF (ERR(I).GT.ERRMAX) THEN
              ERRMAX = ERR(I)
          ENDIF
41      CONTINUE
      C
      Tolerance Check

      IF (ERRMAX .LE. TOLERF) THEN
          T = T + HF
          DO 39 I=1,NF
              F(I) = (DF1(I) + 4.0*DF4(I)+DF5(I))*HF/6.0+F(I)
39      CONTINUE
      ENDIF
      C
      Adjust Step Size If Necessary

      IF (ERRMAX .GT. 0.0) THEN
          HF= 0.9 * HF* (TOLERF/ERRMAX) ** (1/ORD)
          IF (HF.LT.HFMIN) THEN

```

MUL04560
 MUL04570
 MUL04580
 MUL04590
 MUL04600
 MUL04610
 MUL04620
 MUL04630
 MUL04640
 MUL04650
 MUL04660
 MUL04670
 MUL04680
 MUL04690
 MUL04700
 MUL04710
 MUL04720
 MUL04730
 MUL04740
 MUL04750
 MUL04760
 MUL04770
 MUL04780
 MUL04790
 MUL04800
 MUL04810
 MUL04820
 MUL04830
 MUL04840
 MUL04850
 MUL04860
 MUL04870
 MUL04880
 MUL04890
 MUL04900
 MUL04910
 MUL04920
 MUL04930
 MUL04940
 MUL04950
 MUL04960
 MUL04970
 MUL04980
 MUL04990
 MUL05000
 MUL05010
 MUL05020
 MUL05030
 MUL05040
 MUL05050
 MUL05060
 MUL05070
 MUL05080
 MUL05090
 MUL05100
 MUL05110
 MUL05120
 MUL05130
 MUL05140

```

      PRINT*, 'HFMIN EXCEEDED. DO YOU WISH TO CHANGE VALUE OFMUL05150
+ HFMIN (Y) OR WOULD YOU RATHER HALT THE INTEGRATION AND FURTHER      MUL05160
+INVESTIGATE THE MODEL (N) ?'                                         MUL05170
      READ*, CHECK                                                       MUL05180
      IF (CHECK .EQ. 'Y') THEN                                           MUL05190
        PRINT*, 'PLEASE ENTER NEW VALUE OF HFMIN. NOTE THAT           MUL05200
+FOR INTEGRATION TO PROCEED, IT SHOULD BE LESS THAN', HF              MUL05210
        READ*, NUVAL                                                     MUL05220
        HFMIN = NUVAL                                                    MUL05230
      ELSE                                                                MUL05240
        STOP                                                             MUL05250
      ENDIF                                                              MUL05260
    ENDIF                                                                MUL05270
    IF (HF.GT.HFMAX) THEN                                                MUL05280
      HF = HFMAX                                                         MUL05290
    ENDIF                                                                MUL05300
  ENDIF                                                                MUL05310
  IF (HF.GE. TF - T) HF = TF-T                                          MUL05320
  GOTO 5                                                                MUL05330
ENDIF                                                                    MUL05340
RETURN                                                                    MUL05350
END                                                                        MUL05360

```

```

SUBROUTINE INTER1(T, TNOW, S, DS, NS, INTS)
IMPLICIT REAL(A-H, O-Z)
REAL S(NS), DS(NS), INTS(2)

```

C Subroutine that returns values of Slow System components
C involved in coupling between TN and TN + H/3

```
INTS(1) = S(6) + (T-TNOW)* DS(6)
```

```
INTS(2) = S(1) + (TF-T)*DS(1)
```

```
RETURN
END
```

```

SUBROUTINE INTER2(T, TNOW, P1S, DS, DPS, DP1S, NS, INTS)
IMPLICIT REAL(A-H, O-Z)
REAL P1S(NS), DS(NS), DPS(NS), DP1S(NS), INTS(2)

```

C Subroutine that returns values of Slow System components
C involved in coupling between TN + H/3 and TN + H/2

```
INTS(1) = P1S(6) + (T-TNOW)*(-DS(6)/4.0-DPS(6) + 9.0*DP1S(6)/4.0)
```

```
INTS(2) = P1S(1) + (T-TNOW)*(-DS(1)/4.0-DPS(1) + 9.0*DP1S(1)/4.0)
```

```
RETURN
END
```

```

SUBROUTINE EXTRAP(T, TNOW, P1S, DP2S, NS, INTS)
IMPLICIT REAL(A-H, O-Z)
REAL P1S(NS), DP2S(NS), INTS(2)

```

C Subroutine that returns values of Slow System components

C involved in coupling between $TN + H/2$ and $TN + H$

$INTS(1) = P1S(6) + (T-TNOW)*DP2S(6)$

$INTS(2) = P1S(1) + (T-TNOW)*DP2S(1)$

RETURN

END

MUL06970
MUL06980
MUL06990
MUL07000
MUL07010
MUL07020
MUL07030
MUL07040
MUL07050

H.5 The Discontinuity Processing Algorithm

```

SUBROUTINE DISCON(T,Y,TE,N,TFIN,HMIN,DERIV,TOL,NDF)
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION DY(5),F(10,10),TS(10,10),W4(9),ERR(9),ERD(9),DF(5)
  +,DY1(9),DY2(9),DY3(9),DY4(9),W1(9),W2(9),W3(9),Y(5),PDF(5),TE(5)
  COMMON/HOPE/YLAST(5),HINIT
  COMMON/TIMVAL/THOR
  COMMON/WHY/COMINT,NOUT,NTIMUP
  COMMON/FLAG/NUMTE,NTIMEV,NFIRST,NTEALL
  COMMON/DIFF/YVAL(500),TIME(500),YVAL1(500),NPL
  EXTERNAL DERIV
  CHARACTER*1 CHOICE

  NOUT = 0

  CALL DERIV(T,Y,DY,N)
  FDER = 0.0
  DO 29 I = 1,N
    IF (ABS(DY(I)).GT.FDER) THEN
      FDER = ABS(DY(I))
    ENDIF
  29 CONTINUE
  IF (FDER.NE.0.0) THEN
    HPOS = SQRT(0.5 * TOL/FDER)
    IF (HBOUND.LE.0.0) THEN
      HBOUND = 0.1
    ENDIF
    IF (HPOS.GT.HBOUND) THEN
      HSTART = HBOUND
    ELSE
      HSTART = HPOS
    ENDIF
  ELSE
    IF (HBOUND.LE.0.0) THEN
      HBOUND = 0.1
    ENDIF
    HSTART = HBOUND
  ENDIF
  IF (HINIT.NE.0.0) THEN
    H = HINIT
  ELSE
    HINIT = HSTART
    H = HINIT
  ENDIF

  IF (H.GT.HBOUND) THEN
    PRINT*,'HINIT > HBOUND. DO YOU WISH TO CARRY OUT INTEGRATION
  + WITH THIS HINIT (Y) OR HBOUND (N)?'
    READ*, CHOICE
    IF (CHOICE.EQ.'Y') THEN
      H = HINIT
    ELSE
      H = HBOUND
      HINIT = HBOUND
    ENDIF
  ENDIF

```

BAL01840
 BAL01850
 BAL01860
 BAL01870
 BAL01880
 BAL01890
 BAL01900
 BAL01910
 BAL01920
 BAL01930
 BAL01940
 BAL01950
 BAL01960
 BAL01970
 BAL01980
 BAL01990
 BAL02000
 BAL02010
 BAL02020
 BAL02030
 BAL02040
 BAL02050
 BAL02060
 BAL02070
 BAL02080
 BAL02090
 BAL02100
 BAL02110
 BAL02120
 BAL02130
 BAL02140
 BAL02150
 BAL02160
 BAL02170
 BAL02180
 BAL02190
 BAL02200
 BAL02210
 BAL02220
 BAL02230
 BAL02240
 BAL02250
 BAL02260
 BAL02270
 BAL02280
 BAL02290
 BAL02300
 BAL02310
 BAL02320
 BAL02330
 BAL02340
 BAL02350
 BAL02360
 BAL02370
 BAL02380
 BAL02390

```

IF (COMINT.LE.0) THEN
  COMINT = (TFIN - T)/100
ENDIF
IF (HMIN.LE.0.0) THEN
  HMIN = HINIT/10000
ENDIF

```

```

IT      = 1
NC      = 1
ITER    = 0
IF (COMINT.EQ.0.0) THEN
  COMINT = (TFIN - T)/100
ENDIF
TCOM = T + COMINT

```

C Determine the current time horizon

```

7 IF (T.LT.TFIN) THEN
  IF ((IT.LE.NUMTE).AND. (NTIMUP.EQ.1)) THEN
    IF (TE(IT).LT.TCOM) THEN
      THOR = TE(IT)
      NTIMUP = 0
    ELSE
      THOR = TCOM
      NTIMUP = 0
    ENDIF
  ENDIF
  IF ((IT.GT.NUMTE).AND. (NTIMUP.EQ.1)) THEN
    IF (TFIN.GT.TCOM) THEN
      THOR = TCOM
      NTIMUP = 0
    ELSE
      THOR = TFIN
      NTIMUP = 0
    ENDIF
  ENDIF

```

```

8 IF ((T + H.LT.THOR) .OR. (NOUT.EQ.1)) THEN
  IF (NTEALL.EQ.1) THEN
    IF (NTIMEV.EQ.1) THEN

```

C

```

      Model Update for Time Events
      CALL MODUPD(DF,NDF,T,Y,N,TOL)
      CALL OUTPUT(Y,N,T)
      NTIMEV = 0
      NOUT = 0
      IT = IT + 1
      NTIMUP = 1
    ENDIF
    CALL NORMIN(Y,H,T,TOL,DF,PDF,TLAST,TCOM,N,NDF,TFIN)
  ELSE
    CALL DISFUN(Y,T,N,NDF,DF)
    NUM = 0
    NOT = 0
    IF (NFIRST.EQ.0) THEN
      NFIRST = 1
      CALL NORMIN(Y,H,T,TOL,DF,PDF,TLAST,TCOM,N,NDF,TFIN)
      CALL DISFUN(Y,T,N,NDF,DF)
    ENDIF

```

C

Detection of Discontinuities

```

2 I      = 1
  IF (I.LE.NDF) THEN
    IF (PDF(I)*DF(I).LT.0.0) THEN

```

```

BAL02400
BAL02410
BAL02420
BAL02430
BAL02440
BAL02450
BAL02460
BAL02470
BAL02480
BAL02490
BAL02500
BAL02510
BAL02520
BAL02530
BAL02540
BAL02550
BAL02560
BAL02570
BAL02580
BAL02590
BAL02600
BAL02610
BAL02620
BAL02630
BAL02640
BAL02650
BAL02660
BAL02670
BAL02680
BAL02690
BAL02700
BAL02710
BAL02720
BAL02730
BAL02740
BAL02750
BAL02760
BAL02770
BAL02780
BAL02790
BAL02800
BAL02810
BAL02820
BAL02830
BAL02840
BAL02850
BAL02860
BAL02870
BAL02880
BAL02890
BAL02900
BAL02910
BAL02920
BAL02930
BAL02940
BAL02950
BAL02960
BAL02970
BAL02980

```

```

      NUM=I
      IF (DABS(DF(I)).GT.TOL) THEN
        NOT=1
      END IF
      END IF
      I=I+1
      GOTO 2
    ENDIF
    IF (ITER.NE.1) THEN
      IF (NUM.EQ.0) THEN
        IF (NTIMEV.EQ.1) THEN
          Model Update As Specified By Time Event
          No State Event In Last Step
          CALL MODUPD(DF,NDF,T,Y,N,TOL)
          CALL OUTPUT(Y,N,T)
          NTIMEV = 0
          NOUT = 0
          IT = IT + 1
          NTIMUP = 1
        ELSE
          CALL NORMIN(Y,H,T,TOL,DF,PDF,TLAST,TCOM,N,NDF,TFIN)
        ENDIF
      ELSE
        I=1
        IF (I.LE.NDF) THEN
          F(1,I)=PDF(I)
          F(2,I)=DF(I)
          I=I+1
          GOTO 83
        ENDIF
        TS(2,1)=T
        TS(1,1)=TLAST
        NC = 2
        J = 2
        NDIS = NUM
        IIME = 0
        CALL AITKEN(NC,J,TS,F,PDF,NDIS)
        HDIS = TS(NC,NC)-TLAST
        ITER = 1
        T = TLAST
        I = 1
        IF (I.LE.N) THEN
          Y(I)=YLAST(I)
          I=I+1
          GOTO 90
        ENDIF
        IIME=IIME+1
        CALL RKD(N,T,Y,HDIS,DERIV,TOL)
      ENDIF
    ELSEIF (NOT.EQ.0.AND.NUM.NE.0) THEN
      Discontinuity present and
      within Tolerance.No interpolation
      required. Model Update done.
      Model Update by State Event
      CALL MODUPD(DF,NDF,T,Y,N,TOL)
      CALL OUTPUT(Y,N,T)
      NOUT = 0
      NC = 1
      ITER = 0

```

```

BAL02990
BAL03000
BAL03010
BAL03020
BAL03030
BAL03040
BAL03050
BAL03060
BAL03070
BAL03080
BAL03090
BAL03100
BAL03110
BAL03120
BAL03130
BAL03140
BAL03150
BAL03160
BAL03170
BAL03180
BAL03190
BAL03200
BAL03210
BAL03220
BAL03230
BAL03240
BAL03250
BAL03260
BAL03270
BAL03280
BAL03290
BAL03300
BAL03310
BAL03320
BAL03330
BAL03340
BAL03350
BAL03360
BAL03370
BAL03380
BAL03390
BAL03400
BAL03410
BAL03420
BAL03430
BAL03440
BAL03450
BAL03460
BAL03470
BAL03480
BAL03490
BAL03500
BAL03510
BAL03520
BAL03530
BAL03540
BAL03550
BAL03560
BAL03570

```

```

IF (NTIMEV.EQ.0) THEN
  CALL NORMIN(Y,H,T,TOL,DF,PDF,TLAST,TCOM,N,NDF,TFIN)
ELSE
  HDIS = THOR - T /
  YVAL(NPL) = Y(1)
  YVAL1(NPL) = Y(2)
  TIME(NPL) = T
  NPL = NPL + 1
  CALL RKD(N,T,Y,HDIS,DERIV,TOL)
  I=1
  IF (I.LE.NDF) THEN
    PDF(I) = DF(I)
    I = I+1
    GOTO 46
  ENDIF
ENDIF
ELSE
  ITER = 1, Discontinuity present,
  value of DY not within tolerance
  Need to interpolate.
  I = 1
  IF (I.LE.NDF) THEN
    F(NC+1,I)=DF(I)
    I = I + 1
    GOTO 4
  ENDIF
  TS(NC+1,1) = T
  NC = NC + 1
  Sort in ascending order of D.F. from
  0, the D.F.'s and their corresponding
  Times.
  CALL SORT(F,TS,NC,NDF)
  CALL SELECT(F,TS,NC,NDIS,PDF,J,NDF)
  CARRY OUT INVERSE AITKEN INTERPOLATION
  CALL AITKEN(NC,J,TS,F,PDF,NDIS)
  HDIS = TS(NC,NC)-TLAST
  ITER = 1
  T = TLAST
  I = 1
  IF (I.LE.N) THEN
    Y(I)=YLAST(I)
    I=I+1
    GOTO 94
  ENDIF
  IIME=IIME+1
  CALL RKD(N,T,Y,HDIS,DERIV,TOL)
ENDIF
ENDIF
GOTO 8
ENDIF
Determine The Step Size needed to
reach the Time Event Discontinuity
or the end time of the Simulation.
Use the Modified R-K Merson to reach
that point exactly
IF (NTIMUP.EQ.0) THEN
  HDIS = THOR - T
  CALL RKD(N,T,Y,HDIS,DERIV,TOL)

```

BAL03580
 BAL03590
 BAL03600
 BAL03610
 BAL03620
 BAL03630
 BAL03640
 BAL03650
 BAL03660
 BAL03670
 BAL03680
 BAL03690
 BAL03700
 BAL03710
 BAL03720
 BAL03730
 BAL03740
 BAL03750
 BAL03760
 BAL03770
 BAL03780
 BAL03790
 BAL03800
 BAL03810
 BAL03820
 BAL03830
 BAL03840
 BAL03850
 BAL03860
 BAL03870
 BAL03880
 BAL03890
 BAL03900
 BAL03910
 BAL03920
 BAL03930
 BAL03940
 BAL03950
 BAL03960
 BAL03970
 BAL03980
 BAL03990
 BAL04000
 BAL04010
 BAL04020
 BAL04030
 BAL04040
 BAL04050
 BAL04060
 BAL04070
 BAL04080
 BAL04090
 BAL04100
 BAL04110
 BAL04120
 BAL04130
 BAL04140
 BAL04150
 BAL04160

```

96      I=1
      IF (I.LE.NDF) THEN
          PDF(I) = DF(I)
          I = I+1
          GOTO 96
      ENDIF
      NOUT = 1
      IF (THOR.EQ.TE(IT)) NTIMEV = 1
      ENDIF
      IF (THOR.EQ.TFIN) THEN
          CALL OUTPUT(Y,N,T)
      ENDIF
      GOTO 7
      ENDIF
      RETURN
      END

      SUBROUTINE AITKEN(NC,J,TS,F,PDF,NDIS)
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION TS(10,10),F(10,5),PDF(5)

      TOL = 0.00001
12      DO 13 K=2,NC
          DO 13 I=K,NC
              TS(I,K) = (TS(K-1,K-1)*(F(I,NDIS)+DSIGN(TOL,PDF(NDIS)))*0.5)
              +-TS(I,K-1)*(F(K-1,NDIS)+0.5*DSIGN(TOL,PDF(NDIS))))
              +/(F(I,NDIS)-F(K-1,NDIS))
13      CONTINUE

      C      Check Validity of Interpolation Table
      C
      IF (TS(NC,NC).GT.TS(J,1).OR.TS(NC,NC).LT.TS(J-1,1)) THEN
          WRITE(6,120) TS(NC,NC)
120         FORMAT(4X,'OUT OF RANGE',F10.8)
          IF (J.EQ.NC) THEN
              I = 1
          60          IF (I.LT.NC) THEN
                      TS(I,1) = TS(I+1,1)
                      N1=1
          70          IF (N1.LE.NDF) THEN
                      F(I,N1) = F(I+1,N1)
                      N1=N1+1
                      GOTO 70
                  ENDIF
                  I=I+1
                  GOTO 60
              ENDIF
              J=J-1
              NC=NC-1
              WRITE(6,130)
130          FORMAT(10X,'ERASE FIRST ROW')
              GOTO 12
          END IF
          IF (J.EQ.2) THEN
              NC=NC-1
              WRITE(6,140)
140          FORMAT(10X,'ERASE LAST ROW')
              GOTO 12
          END IF
          TS(1,1) = TS(J-1,1)

```

BAL04170
 BAL04180
 BAL04190
 BAL04200
 BAL04210
 BAL04220
 BAL04230
 BAL04240
 BAL04250
 BAL04260
 BAL04270
 BAL04280
 BAL04290
 BAL04300
 BAL04310
 BAL04320
 BAL04330
 BAL04340
 BAL04350
 BAL04360
 BAL04370
 BAL04380
 BAL04390
 BAL04400
 BAL04410
 BAL04420
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 BAL04470
 BAL04480
 BAL04490
 BAL04500
 BAL04510
 BAL04520
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 BAL04560
 BAL04570
 BAL04580
 BAL04590
 BAL04600
 BAL04610
 BAL04620
 BAL04630
 BAL04640
 BAL04650
 BAL04660
 BAL04670
 BAL04680
 BAL04690
 BAL04700
 BAL04710
 BAL04720
 BAL04730
 BAL04740
 BAL04750

```

      TS(2,1)=TS(J,1)
      I=1
80    IF (I.LE.DDF) THEN
          F(1,I)=F(J-1,I)
          F(2,I)=F(J,I)
          I=I+1
          GOTO 80
      ENDIF
      NC=2
      J=2
      GOTO 12
END IF
RETURN
END

```

BAL04760
BAL04770
BAL04780
BAL04790
BAL04800
BAL04810
BAL04820
BAL04830
BAL04840
BAL04850
BAL04860
BAL04870
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BAL04890
BAL04900
BAL04910
BAL04920
BAL04930
BAL04940
BAL04950
BAL04960
BAL04970
BAL04980
BAL04990
BAL05000
BAL05010
BAL05020
BAL05030
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BAL05100
BAL05110
BAL05120
BAL05130
BAL05140
BAL05150
BAL05160
BAL05170
BAL05180
BAL05190
BAL05200
BAL05210
BAL05220
BAL05230
BAL05240
BAL05250
BAL05260
BAL05270
BAL05280
BAL05290
BAL05300
BAL05310
BAL05320
BAL05560
BAL05570

```

SUBROUTINE NORMIN(Y,H,T,TOL,DF,PDF,TLAST,TCOM,N,NDF,TFIN)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION Y(5),DF(5),PDF(5)
COMMON/HOPE/YLAST(5),HINIT
COMMON/WHY/COMINT,NOUT,NTIMUP
COMMON/TIMVAL/THOR
EXTERNAL DERIV
HMAX = 0.1
HMIN = 0.0000000001
24 TLAST = T
   I = 1

```

To prevent discontinuity detection hazards

```

95 IF (I.LE.N) THEN
      IF (YLAST(2).LT.0.0) YLAST(2) = 0.0
      YLAST(I) = Y(I)
      I = I+1
      GOTO 95
ENDIF
I=1
96 IF (I.LE.NDF) THEN
      IF (DF(I).LT.0.0) DF(I) = 0.0
      PDF(I) = DF(I)
      I = I+1
      GOTO 96
ENDIF

```

Output Values of Time with Corresponding State Values.
Collect Output Values for plotting

```

IF (NOUT.NE.1) THEN
      CALL RKN(N,T,Y,H,DERIV,TOL,HMAX,HMIN)
ELSE
      CALL OUTPUT(Y,N,T)
      TCOM = T + COMINT
      NOUT = 0
      NTIMUP = 1
ENDIF
RETURN
END

```

SUBROUTINE RKD(N,T,Y,H,DERIV,TOL)

```

      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION Y(N),W1(10),W2(10),W3(10),W4(10),ERD(10),
+DY(10),DY1(10),DY2(10),DY3(10),DY4(10)
      C=1
2    HD=H/C
      C1=0
4    CALL DERIV(T,Y,DY,N)
      DO 6 I=1,N
6    W1(I)=DY(I)*HD/3.0+Y(I)
      CALL DERIV(HD/3.0+T,W1,DY1,N)
      DO 8 I=1,N
8    W2(I)=(DY(I)+DY1(I))*HD/6.0+Y(I)
      CALL DERIV(HD/3.0+T,W2,DY2,N)
      DO 10 I=1,N
10   W3(I)=(DY(I)+3.0*DY2(I))*HD*0.125+Y(I)
      CALL DERIV(HD*0.5+T,W3,DY3,N)
      DO 12 I=1,N
12   W4(I)=DY(I)*HD*0.5-DY2(I)*HD*1.5+DY3(I)*HD*2.0+Y(I)
      CALL DERIV(HC+T,W4,DY4,N)

      ERDMAX = 0.0
      DO 40 I=1,N
      ERD(I)=HD*DABS(DY(I)*HD/3.0-1.5*HD*DY2(I)+4.0*DY3(I)*HD/3.0
+HD*DY4(I)/6.0)
      IF(ERD(I).GT.MAXERD) THEN
        ERDMAX = ERD(I)
      ENDIF
40   CONTINUE

      IF(ERDMAX.LE.TOL)GO TO 18
      HD=HD*0.5
      C=C+C
      C1=C1+C1
      GO TO 4
18   T=T+HD
      DO 14 I=1,N
14   Y(I)=(DY(I)+4.0*DY3(I)+DY4(I))*HD/6.0+Y(I)
      C1=C1+1
      IF(C1.EQ.C)RETURN
      GO TO 4
      END

      SUBROUTINE RKN(N,T,Y,H,DERIV,TOL,HMAX,HMIN)
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION Y(N),W1(10),W2(10),W3(10),W4(10),ERR(10),
+DY(10),DY1(10),DY2(10),DY3(10),DY4(10)
      COMMON/INTEG/ORD
      CHARACTER*1 CHOICE

4    CALL DERIV(T,Y,DY,N)
      DO 6 I=1,N
6    W1(I)=DY(I)*H/3.0+Y(I)
      CALL DERIV(H/3.0+T,W1,DY1,N)
      DO 8 I=1,N
8    W2(I)=(DY(I)+DY1(I))*H/6.0+Y(I)
      CALL DERIV(H/3.0+T,W2,DY2,N)
      DO 10 I=1,N
10   W3(I)=(DY(I)+3.0*DY2(I))*H*0.125+Y(I)

```

BAL05580
 BAL05590
 BAL05600
 BAL05610
 BAL05620
 BAL05630
 BAL05640
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 BAL05670
 BAL05680
 BAL05690
 BAL05700
 BAL05710
 BAL05720
 BAL05730
 BAL05740
 BAL05750
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 BAL05780
 BAL05790
 BAL05800
 BAL05810
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 BAL05970
 BAL05980
 BAL05990
 BAL06000
 BAL06010
 BAL06020
 BAL06030
 BAL06040
 BAL06050
 BAL06060
 BAL06070
 BAL06080
 BAL06090
 BAL06100
 BAL06110
 BAL06120
 BAL06130
 BAL06140
 BAL06150
 BAL06160

```

CALL DERIV(H*0.5+T,W3,DY3,N)
DO 12 I=1,N
12 W4(I)=DY(I)*H*0.5-DY2(I)*H*1.5+DY3(I)*H*2.0+Y(I)
CALL DERIV(HC+T,W4,DY4,N)

ERRMAX = 0.0
DO 40 I=1,N
ERR(I)=H*DABS(DY(I)*H/3.0-1.5*H*DY2(I)+4.0*DY3(I)*H/3.0
+-H*DY4(I)/6.0)
IF(ERR(I).GT.ERRMAX) THEN
ERRMAX = ERR(I)
ENDIF
40 CONTINUE

IF ((ERRMAX.GT.TOL).AND.(ERRMAX.NE.0.0)) THEN
H = 0.9 * H * (TOL/ERRMAX) ** (1/ORD)
IF (H.LT.HMIN) THEN
PRINT*, 'HMIN Exceeded. Do you wish to change value of
+ HMIN (Y) or would you rather halt the integration and further
+investigate the model (N) ?'
READ*, CHOICE
IF (CHOICE.EQ.'Y') THEN
PRINT*, 'Please enter new value of HMIN. Note that
+for integration to proceed, it should be less than', H
READ*, NUVAL
HMIN = NUVAL
ELSE
STOP
ENDIF
ENDIF
GO TO 4
ENDIF
T=T+H
DO 14 I=1,N
14 Y(I)=(DY(I)+4.0*DY3(I)+DY4(I))*H/6.0+Y(I)
IF ((ERRMAX.LT.TOL).AND.(ERRMAX.NE.0.0)) THEN
H = 0.9 * H * (TOL/ERRMAX) ** (1/ORD)
IF (H.GT.HMAX) H = HMAX
ENDIF
RETURN
END

SUBROUTINE SORT(F,TS,NC,NDF)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION F(10,10),TS(10,10),TSMIN(5)

C This subprogram is model independent.
C It is responsible for rearranging
C the interpolation table in descending
C order of Ts after each iterative inter-
C polation.

I=1
52 IF (I.LE.NC-1) THEN
I1=1
54 IF (I1.LE.NDF) THEN
TSMIN(I1)=TS(I,I1)
I1=I1+1

```

BAL06170
 BAL06180
 BAL06190
 BAL06200
 BAL06210
 BAL06220
 BAL06230
 BAL06240
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 BAL06260
 BAL06270
 BAL06280
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 BAL06300
 BAL06310
 BAL06320
 BAL06330
 BAL06340
 BAL06350
 BAL06360
 BAL06370
 BAL06380
 BAL06390
 BAL06400
 BAL06410
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 BAL06490
 BAL06500
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 BAL06580
 BAL06590
 BAL06600
 BAL06610
 BAL06620
 BAL06630
 BAL06640
 BAL06650
 BAL06660
 BAL06670
 BAL06680
 BAL06690
 BAL06700
 BAL06710
 BAL06720
 BAL06730
 BAL06740
 BAL06750

	GOTO 54	BAL06760
	ENDIF	BAL06770
	FMIN=F(I,1)	BAL06780
	JMIN=I	BAL06790
	J=I+1	BAL06800
56	IF (J.LE.NC) THEN	BAL06810
	IF (F(J,1).LT.FMIN) THEN	BAL06820
	I1=1	BAL06830
58	IF (I1.LE.NDF) THEN	BAL06840
	TSMIN(I1)=TS(J,I1)	BAL06850
	I1=I1+1	BAL06860
	GOTO 58	BAL06870
	ENDIF	BAL06880
	JMIN=J	BAL06890
	FMIN=F(J,1)	BAL06900
	END IF	BAL06910
	J=J+1	BAL06920
	GOTO 56	BAL06930
	ENDIF	BAL06940
	I1=1	BAL06950
62	IF (I1.LE.NDF) THEN	BAL06960
	TS(JMIN,I1)=TS(I,I1)	BAL06970
	I1=I1+1	BAL06980
	GOTO 62	BAL06990
	ENDIF	BAL07000
	F(JMIN,1)=F(I,1)	BAL07010
	I1=1	BAL07020
64	IF (I1.LE.NDF) THEN	BAL07030
	TS(I,I1)=TSMIN(I1)	BAL07040
	I1=I1+1	BAL07050
	GOTO 64	BAL07060
	ENDIF	BAL07070
	F(I,1)=FMIN	BAL07080
	I=I+1	BAL07090
	GOTO 52	BAL07100
	ENDIF	BAL07110
	RETURN	BAL07120
	END	BAL07130
		BAL07140
		BAL07150
	SUBROUTINE SELECT(F,TS,NC,NDIS,PDF,J,NDF)	BAL07160
	IMPLICIT REAL*8 (A-H,O-Z)	BAL07170
	DIMENSION F(10,5),TS(10,10),PDF(5),FF(10,5),TTS(10,10)	BAL07180
C	The subprogram selects the useful points which will	BAL07190
C	increase the convergence rate and discards those that	BAL07200
C	will not. It also performs a monotonic check.	BAL07210
C		BAL07220
	I=1	BAL07230
72	IF (I.LE.NC) THEN	BAL07240
	I1=1	BAL07250
74	IF (I1.LE.NDF) THEN	BAL07260
	IF (PDF(I1)*F(I,I1).LT.0.0) THEN	BAL07270
	J=I	BAL07280
	K=I1	BAL07290
	GOTO 2	BAL07300
	END IF	BAL07310
	I1=I1+1	BAL07320
	GOTO 74	BAL07330
	ENDIF	BAL07340

```

      I=I+1
      GOTO 72
    ENDIF
  2  NDIS=K
    I=1
  76  IF (I.LE.NC-2) THEN
      IF ((F(I+2,K)-F(I+1,K))*(F(I+1,K)-F(I,K)).LT.0.0) THEN
        IF (I.LE.J-2) THEN
          K=1
          IF (K.LE.NC-I) THEN
            I1=1
            IF (I1.LE.NDF) THEN
              F(K,I1)=F(I+K,I1)
              I1=I1+1
              GOTO 82
            ENDIF
            TS(K,1)=TS(I+K,1)
            K=K+1
            GOTO 78
          ENDIF
          NC=NC-I
          J=J-I
          WRITE(6,180)
          FORMAT(40X,'CUT OFF HEAD FOR NON-MONOTONY')
          GOTO 4
        ELSE
          NC=NC-1
          WRITE(6,190)
          FORMAT(40X,'NON-MONOTONY ,CUT OFF TAIL')
          GOTO 4
        END IF
      END IF
      I=I+1
      GOTO 76
    ENDIF
  4  IF (NC.EQ.5) THEN
      IF (J.LE.3) THEN
        NC=NC-1
        WRITE(8,200)
        FORMAT(40X,'NC=5,CUT OFF TAIL')
      ELSE
        I=1
        IF (I.LT.NC) THEN
          I1=1
          IF (I1.LE.NDF) THEN
            F(I,I1)=F(I+1,I1)
            I1=I1+1
            GOTO 86
          ENDIF
          TS(I,1)=TS(I+1,1)
          I=I+1
          GOTO 84
        ENDIF
        NC=NC-1
        J=J-1
        WRITE(8,210)
        FORMAT(20X,'NC=5, CUT OFF HEAD')
      END IF
    END IF
  9  RETURN
END

```

```

BAL07350
BAL07360
BAL07370
BAL07380
BAL07390
BAL07400
BAL07410
BAL07420
BAL07430
BAL07440
BAL07450
BAL07460
BAL07470
BAL07480
BAL07490
BAL07500
BAL07510
BAL07520
BAL07530
BAL07540
BAL07550
BAL07560
BAL07570
BAL07580
BAL07590
BAL07600
BAL07610
BAL07620
BAL07630
BAL07640
BAL07650
BAL07660
BAL07670
BAL07680
BAL07690
BAL07700
BAL07710
BAL07720
BAL07730
BAL07740
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BAL07760
BAL07770
BAL07780
BAL07790
BAL07800
BAL07810
BAL07820
BAL07830
BAL07840
BAL07850
BAL07860
BAL07870
BAL07880
BAL07890
BAL07900
BAL07910
BAL07920
BAL07930
BAL07940
BAL07950

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References

- Aytac, Z.K., Ören, T.I. (1986). Magest: A Model-Based Advisor and Certifier for Gert Programs. In: Modelling and Simulation Methodology in the Artificial Intelligence Era, M.S. Elzas, T.I. Ören, B.P. Zeigler (Eds.) ,North Holland, pp. 299-307.
- Bergsten, J.R., Fung, M.G. (1984). XMENU/E User's Guide, Kolinar Corporation, Santa Clara, California.
- Birta, L. (1980). A Quasi-Parallel Method For The Simulation of Loosely Coupled Continuous Subsystems. Mathematics and Computers in Simulation XXII, 189-199.
- Birta, L.G., Ören, T.I., Kettenis, D.L. (1985). A Robust Procedure For Discontinuity Handling In Continuous System Simulation. Transactions of the Society For Computer Simulation, 2:3, 189-205.
- Birtwistle, G.M. (1985). In: AI, Graphics, and Simulation. ScS, San Diego, CA.
- Brosilow, C.B. (1985). Modular Integration Methods for Simulation of Large Scale Dynamics Systems. In: International Seminar on Modern Methods in Dynamic Simulation of Industrial Processes, The Norwegian Institute of Technology, Trondheim, Norway.
- Carver, M.B. (1978). Efficient Integration over Discontinuities in Ordinary Differential Equation Simulations. Mathematics and Computers in Simulation, XX, 190-196.
- Cellier, F.E. (1979). Combined Continuous/Discrete System Simulation By Use of Digital Computers: Techniques And Tools. Doctoral Dissertation ETH No. 6483, Swiss Federal Institute of Technology, Zurich.
- Davies, M.J. (1976) A Differential Model of Diabetes Mellitus. In : Mathematical Modelling, J.G. Andrews, R.R. McLone (Eds.), Butterworths & Co. (Publishers) Ltd., 1976.
- Ellison, D. (1981). Efficient Automatic Integration of Ordinary Differential Equations With Discontinuities. Mathematics and Computers in Simulation, XXIII, 12-22.
- Elzas, M.S. (1979). What is Needed For Robust Simulation. In: Methodology in Systems Modelling and Simulation, B.P. Zeigler, G.J. Klir, M.S. Elzas, T.I. Ören (Eds.), North Holland, Amsterdam, pp. 57-91.
- Elzas, M.S. (1986). The Kinship between Artificial

- Intelligence, Modelling and Simulation: An Appraisal.
In: Modelling and Simulation Methodology in the
Artificial Intelligence Era, M.S. Elzas, T.I. Oren,
B.P. Zeigler (Eds.), North-Holland, Amsterdam, 3-13.
- Elzas, M.S., Oren, T.I., Zeigler, B.P. (Eds.) (1986).
Modelling and simulation methodology in the artificial
intelligence era, North Holland, Amsterdam.
- Fikes, R., Kehler, T. (1985). The Role of Frame-Based
Representation in Reasoning. Communications of the ACM,
28:9.
- Gear, C.W. (1971). The Automatic Integration of Ordinary
Differential Equations. Communications of the ACM, 14:3,
176-190.
- Gear, C.W. (1981). Numerical Solution of Ordinary
Differential Equations: Is there Anything Left to do?
SIAM Review, 23:1, 10-24.
- Gear, C.W., Osterby, O. (1984). Solving Ordinary
Differential Equations With Discontinuities. ACM TOMS
10, pp. 23-44.
- Gerald, C.F., Wheatley, P.O. (1984). Applied Numerical
Analysis, Addison Wesley Publishing Company.
- Goldstein, R.A., Harris, W.F. (1973) Serendipity - A
Watershed Level Simulation Model of Tree Biomass
Dynamics. In : Summer Computer Simulation Conference,
1973, pp. 691-696.
- Guariso, G., Hitz, M., Werthner, H. (1987). An Intelligent
Simulation Model Generator. In: Proceedings of The
European Simulation Multi-Conference Vienna, Austria.
- Harmon, P., King, D. (1985). Expert Systems: - Artificial
Intelligence in Business. John Wiley & Sons, Inc., New
York.
- Henricksen, J. (1983). The Integrated Simulation
Environment, Operations Research. Operations Research,
31:6.
- Holmes, W.M. (Eds.) (1985). Artificial Intelligence and
Simulation, SCS, San Diego, CA.
- Hornbeck, R.W. (1975). Numerical Methods. Prentice-Hall,
Inc., Englewood Cliffs, New Jersey.
- Hull, T.E. (1980). Comparison of Algorithms For Initial
Value Problems. In: Computational Techniques For
Ordinary Differential Equations, I. Gladwell, D.K.

- Sayers (Eds.) Academic Press, London, New York, pp. 143-163.
- Hull, T.E. et al. (1972). Comparing Numerical Methods for Ordinary Differential Equations. SIAM Journal of Numerical Analysis, 9, 603-607.
- I.S.S.C. (1982). Disspla User's Manual. San Diego, CA 92121-1698.
- Jackson, P. (1985). Introduction To Expert Systems. Addison-Wesley Publishing Company, Inc.
- Kerchoffs, E.J.H., Vansteenkiste, G., Zeigler, B.P. (Eds.)(1986). Artificial Intelligence applied to simulation, SCS, San Diego, CA.
- Kettenis, D.L. (1986). Knowledge-Based Model Storage and Retrieval: Problems and Possibilities. In: Modelling and Simulation Methodology in the Artificial Intelligence Era, M.S. Elzas, T.I. Oren, B.P. Zeigler (Eds.), North-Holland, Amsterdam, pp. 101-111.
- Khoshnevis, B., Austin, W.M. (1986). An intelligent interface for systems dynamics modelling. In: Simulation And AI, P.A. Luker, G. Birtwistle (Eds.), SCS, San Diego, CA, 18:3, 81-87.
- Lambert, J.D. (1973). Computational Methods in Ordinary Differential Equations. John Wiley, New York.
- Langer, K., Schmidt, B. (1987). The Simulation System SIMPLEX-II: A Model Construction And Experimentation Environment. In: Proceedings of The European Simulation Multi-Conference, Vienna, Austria.
- Lehmann, A. (1987). Taxonomy and Applications of Expert Systems in Simulation. International Symposium on AI, Expert Systems and Languages in Modelling and Simulation, Barcelona, Spain, June 1987.
- Luker, R.A., Adelsberger, H.H. (Eds.) (1986). Intelligent simulation environments. SCS, San Diego, CA.
- Luker, R.A., Birtwistle, G. (Eds.) (1987). Simulation and AI, SCS, San Diego, CA.
- Ma, J. Lui, W. (1986). Software Requirements of the Simulation of Discontinuous Systems. In: Proceedings of Beijing System Simulation Symposium, pp. 122-125.
- Nielsen, N.R. (1986). The impact of using AI-based techniques in a control system simulator. In: Simulation And AI, P.A. Luker, G. Birtwistle (Eds.),

SCS. 18:3, 72-81.

Ören, T.I. (1984a). "Quality Assurance in Modelling and Simulation: A Taxonomy." In: Simulation and Model-Based Methodologies: An Integrative View, T.I. Ören, B.P. Zeigler, M.S. Elzas (Eds.), Springer Verlag, Heidelberg, W. Germany, pp. 477-517.

Ören, T.I. (1984b). Gest: A Modelling and Simulation Language Based on System Theoretic Concepts. In: Simulation and Model Based Methodologies: An Integrative View, T.I. Ören, B.P. Zeigler, M.S. Elzas (Eds.), Springer Verlag, Heidelberg, W. Germany, pp. 281-335.

Ören, T.I. (1984c). Model-Based Activities: A Paradigm Shift. In: Simulation and Model Based Methodologies: An Integrative View, T.I. Ören, B.P. Zeigler, M.S. Elzas (Eds.), Springer Verlag, Heidelberg, W. Germany, pp. 3-40.

Ören, T.I. (1986a). Artificial Intelligence and Simulation. Artificial Intelligence applied to Simulation, SCS, San Diego, CA.

Ören, T.I. (1986b). Knowledge bases for an advanced simulation environment. In: Intelligent Simulation Environments, P.A. Luker, H.H. Adelsberger (Eds.) SCS, San Diego, CA, pp. 16-22.

Ören, T.I. (1986c). Artificial Intelligence in Quality Assurance of Simulation Studies. In: Modelling and Simulation Methodology in the Artificial Intelligence Era, M.S. Elzas, T.I. Ören, B.P. Zeigler (Eds.), North-Holland, Amsterdam.

Ören, T.I., Ma, J. (1986). An Adaptive Order Discontinuity Algorithm For Simulation of Ordinary Differential Equations. Proceedings JSST Conference on Recent Advances in Simulation of Complex Systems, Tokyo, Japan, pp. 35-38.

Ören, T.I. (1987a). Quality Assurance Paradigms For Artificial Intelligence In Modelling and Simulation. Simulation, 48:4, 149-151.

Ören, T.I. (1987b). Artificial Intelligence In Simulation. In: Proceedings of Measurement, Modelling, and Evaluation of Computer Systems, Erlanger, West Germany, 1987, pp. 375-388.

Ören, T.I. (1987c). Model Update: A Model Specification Formalism With A Generalized View of Discontinuity. Summer Computer Simulation Conference, Montreal, Canada,

July 1987.

- Ören, T.I., Sheng, G. (1988 In Press). Semantic Rules and Facts for an Expert Modelling and Simulation System. In: Preprints of IMACS Congress, Paris, France, July 1988.
- Palusinski, O.A. (1985). Simulation of Dynamic Systems Using Multi-Rate Integration Techniques. Transactions of the Society For Computer Simulation, 2:4, 257-273.
- Reddy, R., Fox, M.S. (1986). The Knowledge-Based Simulation System. IEEE Software, 3, pp. 26-37.
- Reddy, R. (1987). Epistemology of Knowledge-Based Simulation. Simulation, 48:4, 162-166.
- Rich, E., (1984). Natural Language Interfaces, Computer, pp. 39-47.
- Shampine, L.F. (1980). What Everyone Solving Differential Equations Numerically Should Know. In: Computational Techniques For Ordinary Differential Equations, I. Gladwell, D.K. Sayers, (Eds.) Academic Press, London, New York, pp. 1-19.
- Shampine, L.F. Gordon, M.K. (1975). Computer Solution of Ordinary Differential Equations: the initial value problem. W.H. Freeman & Co., San Francisco.
- Shampine, L.F. Gordon, M.K. Wisniewski, J.A. (1980). Variable Order Runge-Kutta Codes. In: Computational Techniques For Ordinary Differential Equations, I. Gladwell, D.K. Sayers, Academic Press, London, New York, 83-103.
- Shannon, R.E. Mayer, R., Adelsberger, H.H. (1985). Expert Systems and Simulation. Simulation, 44:6, 275-284.
- Wagner, H.M. (1975). Principles of Operations Research. Prentice-Hall, NJ.
- Widman, L.A., Loparo, K.A., Helman, d.H. (Eds) (1987). Artificial Intelligence, Simulation, and Modelling, D. Reidel publishing company.
- Wymore, A.W. (1967). A Mathematical Theory of Systems Engineering: The Elements. John Wiley, New York.
- Xiong, G., Song, A. (1986). An Expert System For Dynamic Systems Simulation. In: AI Applied To Simulation, E.G.H. Kerkhoffs, G.C. Vansteenkiste, B.P. Zeigler (Eds.), Simulation Series, 18:1(Feb.), SCS, San Diego,

CA, pp. 106-110.