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# UNCERTAINTY METRICS FOR COUPLED WATERSHED MODELS

by

Geoff Parker

A thesis

submitted under the supervision of

Dr. Ronald L. Droste

and

Dr. Colin D. Rennie

in partial fulfillment of the  
requirements for the degree of

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in

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Cette thèse contient plusieurs pages qui sont illisibles, à partir de l'**Appendix** E.1, page 154- jusqu'à la fin.

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This thesis has many unreadable pages, starting with Appendix E.1, page 154- till the end.

***\*Appendix (en anglais dans le texte)***



THE UNIVERSITY OF OTTAWA-FACULTY OF GRADUATE STUDIES

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The thesis by  
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entitled  
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## ABSTRACT

Predictions of river water quality models are subject to substantial uncertainties, which depend not only on parameterization and calibration strategies but also on the structure of the conceptual model itself. Equally, the uncertainty associated with a non-point source (NPS) model can also be attributed to both the parameterization and model structure. The work presented here evaluated the relative importance of these effects and the associated implications for coupled watershed/water quality models. Particular emphasis was placed on model application and interpretation for stochastic-type problems. Investigations were conducted using real-world data from the non-tidal Potomac basin in the Eastern United States for data analysis and case study purposes.

In the first sub-project, two commonly used conceptual representations of real-world water quality processes were used, and their simulation of dissolved oxygen (DO), biochemical oxygen demand (BOD) and ammonium ( $\text{NH}_4$ ) components were scrutinized. A Generalized Likelihood Uncertainty Estimation (GLUE) approach to the inverse problem was then used to examine how uncertainty changed along the river network for each conceptual model. Differences were observed not only between deterministic instances of each conceptual model, but also between their response surfaces as a whole. In addition, response patterns showed substantial sensitivity to the selection of calibration data used. This methodology was able to identify surface response differences between two conceptual models, and could be used to identify or resolve conceptual model issues for specific applications and/or datasets. Of the two conceptual models examined, the simpler Mike11 model showed marginally better performance at the outlet in most respects, and substantially increased sensitivity to data proximity (i.e. location) throughout the watershed when compared with the more complex QUAL2E representation. Both 'high-fitness' calibrations showed an aggregate coefficient of variation (ACV) of approximately  $7. \times 10^{-2}$  near the outlet.

A second sub-project examined instead the suitability of deterministic calibration criteria for stochastic model calibration and uncertainty analysis. Here, the suitability, relative benefits and substantial disadvantages of 'deterministic-optimization' approaches in stochastic contexts were examined. Three alternate calibration strategies, suitable for water quality modeling under uncertainty, were proposed, and then demonstrated. The proposed strategies, based on absolute relative error (ARE) measures, place increased emphasis on lossless metrics and the inherent subjectivity of any calibration criteria. Calibration based on these criteria generally showed equal

or better performance for stochastic applications when contrasted to root mean square error (RMSE). The findings suggest opportunities for potential improvement in current calibration paradigms can be obtained by using ARE and related strategies..

The areal nature of NPS models and the implications associated with the direct relationship between model structure and parameterization sampling, were examined in a third sub-project. The approach was to find limitations in scale for use of a conceptual model, then examine the scales at which a suitable stochastic depiction of key parameter sets could be obtained. The overlapping regions for model scale are optimal (and possibly the only suitable regions) for conducting meaningful stochastic analysis with a given NPS model. The NPS model examined in this thesis, AnnAGNPS, demonstrated substantial limitations with respect to scale that seem to trump potential parameter uncertainty in many applications. A narrow range of discretizations (in the 4-8.5 km<sup>2</sup> scale range) suitable for conceptual model stability was identified. Response to parameter variations within this range was also examined and appears to be minimized within the structurally stable region, near discretizations of 8 km<sup>2</sup>.

The final portion of this thesis was a holistic evaluation. Coupled hydrology and water quality models are today an important tool used in the understanding and management of surface water and watershed areas. Such problems are generally subject to substantial uncertainty in parameters, process understanding, and data. Component models, drawing on different data, different concepts, and different structures, are affected differently by each of these uncertain elements. The fourth, and final, subproject draws on the previous three sub-projects, and further proposes a framework wherein the response of component models to their respective uncertain elements can be quantified and assessed, using a hydrological model and water quality model as two exemplars. Appendix A of this thesis provides an overview of the proposed framework in the context of predictive watershed quality and quantity model construction. The resulting assessments can identify model coupling strategies that permit more appropriate use and calibration of individual models, as well as better coupled model construction and interpretation. The results of this portion showed that both QUAL2E and MIKE11 may couple well with the AnnAGNPS model uncertainty at relatively high fitness calibrations. Additionally, structural parameter uncertainty was shown to be at least as significant as parameter-based uncertainties.

The results of this work provide a reasonable, manageable, and widely applicable framework for the use of coupled deterministic models to assess uncertain systems. The suggested methodologies, with or without use of the specific codes and tools mentioned, can be

readily employed to further understanding of the uncertainty issues, and uncertainty balance, surrounding contemporary, future, and legacy models.

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## GLOSSARY

### **Abbreviations:**

|          |                                                                     |
|----------|---------------------------------------------------------------------|
| AGFLOW   | Agricultural-Flow component of AnnAGNPS (Computer Code)             |
| ANN      | Artificial Neural Network                                           |
| AnnAGNPS | Annualized Agricultural NPS Model (Computer Code)                   |
| ArcGIS   | ESRI ArcGIS (Computer Code)                                         |
| BASINS   | Better Assessment Science Integrating Point and NPS (Computer Code) |
| DEM      | Digital Elevation Model                                             |
| DMset    | Set of Delineated Models                                            |
| EPA      | Environmental Protection Agency                                     |
| GA       | Genetic Algorithm                                                   |
| GIS      | Geographical Information System                                     |
| GLUE     | Generalized Likelihood Uncertainty Estimation                       |
| HRU      | Hydrological Response Unit                                          |
| HSPF     | Hydrological Simulation Program Fortran (Computer Code)             |
| HEC      | Hydrologic Engineering Center                                       |
| HEC-1    | HEC [Program] 1 (Computer Code)                                     |
| HEC-HMS  | HEC Hydrology Modeling System (Computer Code)                       |
| WQPM     | Water Quality Prototype Model                                       |
| USGS     | US Geological Survey                                                |
| LCPM     | Land Cover Prototype Model                                          |
| LHS      | Latin Hypercube Sampling                                            |
| LU       | Land Use                                                            |
| MRLC     | Multi-Resolution Land Characteristics Consortium                    |
| NAWQA    | National Water Quality Assessment                                   |
| NED      | National Elevation Dataset                                          |
| NEXRAD   | Next Generation Radar                                               |
| NLCD     | National Land Cover Data                                            |
| NPS      | Non-Point Source(s)                                                 |
| PRMS     | Precipitation-Runoff Modeling System (Computer Code)                |
| QUAL     | Group of Computer Codes for Water Quality Modeling                  |
| REA      | Representative Elementary Area                                      |
| RORB     | Runoff Routing [Burroughs] (Computer Code)                          |

|          |                                                 |
|----------|-------------------------------------------------|
| SCE      | Shuffled Complex Evolution                      |
| SHE      | Système Hydrologique Européen (Computer Code)   |
| SODA     | Simultaneous Optimization and Data Assimilation |
| SWM      | Stanford Watershed Model                        |
| SWMM     | Storm Water Management Model (Computer Code)    |
| TIN      | Triangular, Irregular Network                   |
| TOPAZ    | Topographic Parameterization (Computer Code)    |
| TOPMODEL | Topographic Watershed Model (Computer Code)     |
| USDA     | US Department of Agriculture                    |
| USFWS    | US Fish and Wildlife Service                    |
| USGS     | US Geological Survey                            |
| WMO      | World Meteorological Organization               |
| WSR      | Weather Surveillance Radar                      |

#### **Other Terms:**

|                        |                                                                                                                                                                                                                                                            |
|------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Equifinality           | Describes the problem of a model calibration, that can be attained by many different modeling decisions (parameter sets, conceptual structure), which are equally plausible, given a calibration criteria or test of model fitness.                        |
| GLUE                   | A framework for identification of equally representative models to address the problem of structural, conceptual or parameter equifinality, as described above. (See also Abbreviations).                                                                  |
| Likelihood             | A likelihood function, describing a degree of belief in e.g. a parameter set, can be used to rank relative hypotheses based on e.g. suitability of model fit to calibration data. A group of representative models can thus be ranked by degree of belief. |
| Lossless Compression   | Lossless data compression (as opposed to lossy data compression) is a compression of information into a format that allows for the original data to be retrieved exactly. Lossy data compression implies loss of information.                              |
| Stochastic Calibration | This is the calibration of models in a manner that acknowledges and allows for exploration of the model behaviour under uncertainty.                                                                                                                       |
| Stochastic Suitability | Describes the appropriateness of (typically deterministic) assumptions and approaches for modeling decisions that are subsequently subjected to uncertainty analysis.                                                                                      |

**Symbols:**

|                     |                                                                                     |
|---------------------|-------------------------------------------------------------------------------------|
| $\bar{\phantom{x}}$ | Time Smoothed                                                                       |
| $\wedge$            | Per Unit Mass                                                                       |
| $\Delta$            | Slope of Saturation Vapor Pressure-Temperature Curve (kPa/°C)                       |
| $\gamma$            | Psychrometric Constant (kPa/°C)                                                     |
| $\rho$              | Fluid Density (M/L <sup>3</sup> )                                                   |
| $v$                 | Mass Average Velocity (L/T)                                                         |
| $t$                 | Time (T)                                                                            |
| $\tau$              | Viscous Stress Tensor (M/T <sup>2</sup> L)                                          |
| $q$                 | Energy Flux Relative to Mass Average Velocity (M/T <sup>3</sup> )                   |
| $g$                 | Gravitational Acceleration (L/T <sup>2</sup> )                                      |
| $p$                 | Fluid Pressure (M/LT <sup>2</sup> )                                                 |
| $U$                 | Internal Energy (ML <sup>2</sup> /T <sup>2</sup> )                                  |
| $W$                 | Rate of Work on Surroundings (ML <sup>2</sup> /T <sup>3</sup> )                     |
| $Ev$                | Rate of Viscous Dissipation of Mechanical Energy (ML <sup>2</sup> /T <sup>3</sup> ) |
| CN                  | SCS Curve Number (-)                                                                |
| $e_{sat}$           | Saturation vapor pressure (kPa)                                                     |
| $e$                 | Actual vapor pressure (kPa)                                                         |
| ETP                 | Potential evapotranspiration (mm)                                                   |
| $F_c$               | Cloud Factor                                                                        |
| $F_a$               | Atmospheric Correction Factor                                                       |
| $G$                 | Soil heat flux (MJ/m <sup>2</sup> )                                                 |
| $H_v$               | Latent heat of vaporization (MJ/kg)                                                 |
| $Q$                 | Surface runoff [depth] (mm)                                                         |
| $R$                 | Net radiation (MJ/m <sup>2</sup> )                                                  |
| REA                 | Representative elementary area                                                      |
| RSN                 | Net Shortwave Radiation (MJ/m <sup>2</sup> )                                        |
| RLN                 | Net Longwave Radiation (MJ/m <sup>2</sup> )                                         |
| RX                  | Extraterrestrial solar radiation (MJ/m <sup>2</sup> )                               |
| $S$                 | SCS retention variable                                                              |
| $S_1$               | Wilting point value of $S$                                                          |
| $S_2$               | Halfway point value of $S$                                                          |
| $S_3$               | Field capacity point value of $S$                                                   |
| $S_c$               | Solar Constant                                                                      |

|    |                                                    |
|----|----------------------------------------------------|
| St | Timestep value of S                                |
| uc | Uncertainty associated with conceptual model       |
| ud | Uncertainty associated with data                   |
| ui | Uncertainty associated with model inputs           |
| um | Uncertainty associated with model structure        |
| un | Uncertainty associated with model discretization   |
| up | Uncertainty associated with model parameterization |
| W  | Wind function variable (-)                         |
| WI | Water input to the field area soil (mm)            |

# CHAPTER 1

## INTRODUCTION

### 1.1 PROBLEM DEFINITION

This research project explores a novel uncertainty-based approach for modeling of watershed hydrology and the related effects of NPS pollutants on water quality. In particular, the research focuses on incorporating uncertainty algorithms and metrics at an early stage of surface hydrology model construction.

Numerical models, including those used for environmental and watershed systems, have gradually arisen from a consistent progression of tools used to complement other techniques (including fieldwork and laboratory experimentation) and to test conceptual understanding of complex systems. As the usability and sophistication of these tools have grown, so too has the complexity involved. The need for healthy skepticism of simulation results and tools to quantify result quality is as pronounced as ever.

The use of stochastic models, which attempt to quantify uncertainty in model outputs, is today an often used method that attempts to manage the factor of model quality. Unfortunately, proper deployment of such systems is non-trivial, and requires a series of Pareto-optimization problems and assumptions. Results between two systems, two locations, two timeframes or even two modelers are often incompatible. Much attention has generally been paid to construction and calibration of models as well as data processing, while the issues surrounding model validation, error propagation, and analyses of uncertainty, risk, and reliability have not been as comprehensively examined.

This thesis draws on several approaches to the watershed modeling problem, and the incorporation and quantification of uncertainty components. The framework proposed is intended to address these and related issues surrounding the use of modern numerical models over varied spatial-temporal domains. While the focus here is on the use of coupled water-quality/hydrology models, the approach has potential for use in a wide variety of fields.

### 1.2 THESIS ORGANIZATION

This thesis is organized into a presentation of the key tasks required for the study. The novel work has been subdivided into four major project components, partitioned into documents of sufficient breadth and length to be suitable for dissemination and communication, but also of

sufficient focus to be reviewed and discussed within a relatively narrower context. They are presented briefly here for the reader's reference. The major steps and objectives can be outlined as follows:

1) Review literature on topics relevant to the study

A literature review was conducted on watershed-level models, their historical and conceptual basis, and the sources and methods commonly used to handle uncertainty therein.

2) Introduce an objective test of stochastic behaviour in riverine water quality models.

Predictions of river water quality models are subject to substantial uncertainties, which depend not only on parameterization and calibration strategies but also on the structure of the conceptual model itself. To evaluate the importance of this effect and associated implications for stochastic models, investigations were conducted based on a segment of the Potomac River in the eastern US. Two commonly used conceptual representations of real-world processes were used (Mike11 and QUAL2E), and their simulation of dissolved oxygen (DO), biological oxygen demand (BOD) and ammonium ( $\text{NH}_4$ ) components scrutinized. A Generalized Likelihood Uncertainty Estimation (GLUE) approach to the inverse problem was then used to examine how uncertainty changed along the river network for each conceptual model. Differences were observed not only between deterministic instances of each conceptual model, but also between their response surfaces as a whole. Uncertainties within the river network are substantially influenced by the selection of calibration data used, as well as the primary source of the constituent examined (areal vs. point). The suggested methodology can be used to test conceptual model validity for specific applications. The results of this study will help users select and assess models for varied problems, and refine appropriate data collection and monitoring schemes. A formal analysis of the stochastic suitability (and differing nature) of two 'out-of-the-box' deterministic models is novel, and especially relevant given the increasingly common (arguably misguided) 'stochastic' analyses done in this manner for water quality and related problems. The work also provides a novel pathway to the identifiability (equifinality) issue.

3) Define procedures for stochastic calibration of riverine water quality models

Watershed-level modeling has become an essential tool in planning and managing environmental risks and the relationship between pollutant sources and water bodies. Water quality models are generally deployed in such cases to provide insight on source assessments and their impacts on water quality targets as well as the consequences of varied management scenarios (e.g., Parker et al. 2008a).

Typically, model parameters are adjusted to fit one or several years of reference data. It is well understood for deterministic models that the chosen ‘calibrated’ parameter set, and thus simulation results, depend on the reference data (often sparse) and the calibration strategy used. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

Stochastic models attempt to mitigate these issues to some degree by representing modeled phenomena as a distribution of possible outcomes. A common implementation is to perturb input parameters, through use of Monte-Carlo simulations for example, and assess likely outcomes from the results. Though commonly used, the suitability of well-accepted deterministic calibration criteria (e.g., Least Squared Error) for stochastic model calibration is not, however, clear.

The approach of this project is to illustrate the suitability, relative benefits and substantial disadvantages of these ‘deterministic-optimization’ approaches in stochastic contexts. Three alternate calibration strategies suitable for modeling water quality under uncertainty are proposed and then demonstrated.

A formal analysis of the stochastic suitability (and differing nature) of ‘deterministic’ calibration criteria for these models is novel. Like the previous project, it leads to a broader discussion of model complexity and suitability.

#### 4) Determine suitable land use scales for NPS modeling under uncertainty

In a fashion analogous to the previous two projects, the uncertainty associated with a NPS model can be attributed to both the parameterization and model structure. An interesting implication of the areal nature of NPS models is the direct relationship between model structure (i.e., subwatershed size) and sample set for the parameterization of raw input data.

The approach of this project is to find limitations in scale for use of the conceptual model, then examine the scales at which a suitable stochastic depiction of key parameter sets can be generated. The overlapping regions are optimal (and possibly the only suitable regions) for conducting meaningful stochastic analysis can be conducted with a given NPS model.

An analysis of stochastic suitability and uncertainty associated with both the conceptual model and the parameter set is quite novel. Similar work (as discussed in Chapter 2) has been done to find an optimal scale for deterministic problems (where, in fact, calibration can be adjusted to compensate for sub-optimal scale selection), but here is provided an examination of the more interesting (and more relevant) case of managing data and structure uncertainty as stochastic components. The notion of a division strategy based primarily on areas of equal uncertainty (rather than e.g., equal critical source area or minimum channel length) is novel.

#### 5) Construct a procedure for NPS and water quality model coupling under uncertainty

This project draws on the previous three and illustrates construction of coupled watershed models for several problems under uncertainty.

Most of the literature ignores either expressly or, more often, implicitly the model uncertainty associated with structure. These projects, and particularly this final one, emphasize throughout a more sound handling of both model parameter and model structure (since the two are related) components to the uncertainty problem.

In this component project, the author demonstrates how this revised paradigm can lead to improvements not only to individual component model (better model structure, better calibration) but also to better and more powerful ways of examining complex problems such as the use of coupled models. Two new model coupling techniques for stochastic investigation are presented: balanced-uncertainty or constant-uncertainty, with relative performance examined. Several metrics for stochastic watershed behaviour description are also presented, based on the new paradigm.

#### 6) Discussion and Recommendations

A summary review of the overall project and major findings is presented, along with a discussion of potential implications for current and future work. Recommendations are also made, based on the results and analyses from prior steps. The recommendations

focus on consequences of the work, as well as areas where potential improvements may be made.

### **1.3 GOALS**

The primary goal of this work is to propose a framework for a quantitative algorithmic approach to coupled model construction. The belief is, firstly, that all such applications of models are subject to substantial uncertainties, be they explicitly acknowledged or otherwise. Further, it is demonstrated that incorporation of uncertainty principles and metrics at an early phase of a typical NPS study can be beneficial on several fronts.

This study provides a stepping stone towards more efficient numerical models, and particularly more efficient interpretation and structuring of such models. From a greater perspective, local and regional studies that include the types of quantitative uncertainty metrics proposed here should lead, in turn, to better tools for management and decision support, along with reduced duplication of effort.

## **CHAPTER 2**

### **BACKGROUND KNOWLEDGE**

This study will draw on diverse approaches to the watershed modeling problem, and the incorporation of uncertainty components. Since its origins in the late nineteenth century, mathematical modeling of watershed hydrology has grown into a ubiquitous tool for addressing the gamut of environmental and water resources problems. Recent developments in the field include the emergence and incorporation of geographical information systems (GIS), remote sensing, and data acquisition, chemical tracers, topographic representation, up-scaling of hydrologic conservation equations, spatial variability of hydraulic roughness, infiltration and precipitation, spatial and temporal scaling, model calibration, and the linkage with water quality models.

#### **2.1 MATHEMATICAL MODELING OF WATERSHED HYDROLOGY**

##### ***2.1.1 INTRODUCTION***

A watershed hydrology model is a system of mathematical descriptions of the component processes of the hydrologic cycle. The first hydrological models were developed in the nineteenth century for civil engineering design applications. In the twentieth century, substantial improvements in the underlying theories and conceptual models emerged, culminating in the development of the sophisticated numerical models in common use today.

##### ***2.1.2 EARLY HISTORY/COMPONENT MODELS***

The origins of mathematical modeling for hydrological systems date back to the simple approaches developed in the nineteenth century by Mulvaney and then Imbeau. In the 1910s Green and Ampt did some early work on a theory of infiltration, and derived a simplified physically-based formula for computing the infiltration rate. The 1930s saw Sherman suggest a unit hydrograph concept, linking runoff response to excess rainfall, while Horton contributed a theory of infiltration to estimate rainfall excess and improve hydrograph separation methods, as well as a semi-empirical equation for overland flow. Horton went on to model erosion and stream-flow generation by overland flow, and presented what would become commonly known as “Horton’s (empirical) laws”. The understanding of subsurface flows increased greatly over the same period, with important work from Hursh and others noting that subsurface flows constituted a significant component of storm flow hydrographs in some regions. This was

expanded upon in subsequent years by work from Hewlett, Nielsen and Remson, amongst others, which revealed that unsaturated flow can generate stream-flow via streamside saturated zones. Together with Horton's theories, the research into subsurface flow mechanisms expanded into a more integrated picture of stream-flow generation. In these contributions, evaporation and other abstractions were treated using coefficients or indices.

More sophisticated attempts to quantify water losses emerged in the work of Richardson, and then Cummings, and their analysis of evaporation from lakes. Subsequent work by Thornthwaite and Penman focused instead on quantify evapotranspiration losses. Other work addressed abstractions such as interception, depression storage, and detention storage. In the 1950s, the US Soil Conservation Service developed its curve-number method to take abstractions into account in the computation of storm runoff. In the same period, substantial advances in the theoretical formulation of flow routing were also achieved, as Lighthill and Whitham developed the kinematic wave theory, furthering the earlier work of Keulegan.

The foundations of quantitative groundwater hydrology were investigations in the 1930s by Fair and Hatch, who derived a formula for computing the permeability of soil, and then Theis, who combined Darcy's law with the continuity equation. The following decade saw development of baseflow separation techniques, with work by Barnes and then Jacob. Work on incorporating linear system theory eventually led to the instantaneous unit hydrograph and generalized unit hydrograph theories, by Nash and Dooge, respectively.

## **2.2 NUMERICAL WATERSHED SIMULATION CODES**

### ***2.2.1 EMERGENCE OF HOLISTIC WATERSHED CODES***

The emergence of transistor-based computers made possible the combination of multiple component models, describing the entire hydrologic cycle, as in the Stanford Watershed Model developed by Crawford and Linsley in 1966. This code was perhaps the first that attempted to model most processes involved in the watershed to a significant degree, and its descendents, including the Hydrological Simulation Program Fortran (HSPF), remain in common use today. Other early systems have also survived, for instance the code that became known as HEC-1. The 1970s saw continued proliferation of codes simulating watershed hydrology, from Metcalf and Eddy's SWMM to Beven and Kirkby's TOPMODEL. Later models included the 'Système Hydrologique Européen' (SHE) by Abbott et al. in 1986. Many of the codes also remain in use today, though all have seen improvements. Development of new or revised models has continued

since, with individual organizations or agencies frequently releasing their own codes or, at least as often, variants of previously developed models.

As a diverse range of codes began to emerge, the World Meteorological Organization (WMO) sponsored several studies that compared the available alternatives. Their 1975, 1986 and 1992 studies dealt with models focused, in turn, on hydrologic forecasting, flow rate simulation and dynamic stream-flow forecasting. The majority of independent efforts since the WMO studies have been to compare a subset of watershed models, or models of a given component process. Additionally, developers of certain codes have offered comparisons of their programs with one or more other models.

Many current codes have essentially the same fundamental structure as the HSPF code of the 1970s, based largely on Freeze and Harlan's 1969 outline of a three-dimensional approach. At that time, the computational modeling of water quality drawing on hydrologic information was still just emerging, with models of dissolved oxygen in a reach of stream under continued development along with pollutant transport in streams and watersheds.

Major changes since these early models have largely been due to improvements in computer technology or data availability, along with the comparisons of newer conceptual model simulation results to experimental data. Many of the advances address better use of new or improved data sources, for instance the incorporation of digital elevation models (DEMs) and GIS. A related issue is the concept of sub-grid spatial variability and equation up-scaling. Other advances include the use of topographic indices and the ability to draw on sophisticated calibration measurements (e.g., chemical tracers.).

### ***2.2.2 CODE CLASSIFICATION***

Much is oft made of the difference between 'lumped' and 'distributed' models. This distinction stems, originally, from the fact that, though the underlying equations in conceptual models are usually continuous, analytical solutions are not feasibly obtained beyond particularly simple cases, so most codes draw instead on numerical approaches.

In rigorous terms, "distributed" models consider spatial and temporal derivatives, while "lumped" models are those that ignore the spatial derivatives. In the former, the solutions are a function of time and space, while the latter only consider changes over time. Functionally however, most watersheds have limited data available, to an extent that does not allow for a fully distributed description (where all aspects must also be distributed, including parameters,

geometry, boundary conditions, etc.). Some degree of lumping is therefore generally dictated, and most modern models comprise both distributed and lumped components. The distinction between approaches has become further blurred as modern computers and dataset handle input and simulation at ever-finer resolution. Today, many so-called ‘distributed’ models are nothing more than models lumped in a raster fashion.

Another distinction between codes is the selection of conceptual component models used to describe the hydrological cycle. The tradeoffs between empirical or physical models depend on the individual component examined and its importance for the designed purpose of the code, along with the data and numerical implications. Codes draw on a wide range of these models, and the choices are also affected by issues such as the topography and geographic region to which a code is likely to be applied.

Several attempts at formal classification of commonly available models have been made. Singh (1995, 2002) focused on hydrologic models and attempted to describe distinctions in scale and process description, while Wurbs (1998) focused on availability and the intended focus of codes available to water modelers.

## **2.3 STATE OF THE ART – DATA ACQUISITION AND MANAGEMENT**

Hornsberger and Boyer (1995) along with others have, in their reviews, noted the use of GIS, remotely sensed data, and environmental tracers to be among the most important recent advances in watershed modeling. These data-acquisition advances have shifted, in many respects, the paradigm of data scarcity, by affording the opportunity to gather abundant quantities of data regarding spatial distribution of, for instance, topographical and surface cover data.

### ***2.3.1 TOPOGRAPHICAL DATA & ELEVATION MODELS***

Prior to the 1980s, topographic data were most commonly sourced from contour maps. Modern data models, in conjunction with remote sensing techniques, have since provided the means to more accurately depict spatial changes in elevation for complex landscapes. In addition, digitized terrain and DEMs allow for rapid computation of basin and stream network geometry, slope, and flow direction.

There are several data models for treatment of DEM data in common use, ranging from triangular irregular networks (TIN) and raster schemes to vector and contour-based representations (Moore and Grayson 1991). The most widely used data structures are grid networks, or rasters. Many codes (e.g., Beasley et al. 1980, Abbott et al. 1986a, b) use a grid

network as their basic structure. Though computationally efficient and useful for planning purposes, Mark (1978) and Moore and Grayson (1991) have discussed some of the limitations of grid structures as applied to hydrologic problems. Others (Moore et al 1988a, b, O'Loughlin 1986) have used contour-based DEMs for hydrologic and ecologic applications. A third approach has used a kinematic wave model for computing overland flow, based on a DEM representation (Vieux 1988, Goodrich and Woolhiser 1991). As the integration of remotely sensed, GIS, and DEM-based data in the model structure has become more sophisticated, more models have sought to take advantage of these developments. (e.g., Julien et al. 1995, Olivera and Maidment 1999, Fortin et al. 2001).

To incorporate topographical data, models themselves can conceive of watershed area as either a grid structure, similar to the rasterized elevation data, and other numerical methods (e.g., finite-element) themselves, or as some other, non-raster, network of elemental sections (Singh 1996). Sub-areas thus discretized can then be linked together through routing elements, forming the dendritic network and the watershed model.

### ***2.3.2 CHEMICAL TRACERS***

Radiological isotopes, chlorofluorocarbons and other chemical tracers have all been used to define, or calibrate, models of water flow (Adar and Neuman 1988, Dunkle et al. 1993, Robson et al. 1992). Such direct-experiment approaches can yield a wealth of information on flow sources and paths which are otherwise difficult to evaluate, supporting analysis and interpretation of additional remotely-sensed data.

### ***2.3.3 REMOTE SENSING***

Perhaps the most significant advances have been made in data collection with the advent and mainstreaming of new technologies, especially remote sensing, satellites, and radar. Their use has consequently become much more widespread over the last 20 years and continues to receive a great deal of attention. These technologies provide the ability to gather and geo-reference data regarding topography, soil, land-use, and meteorological parameters over a large area at a given point in time. As direct observation technology continues to progress, so too do the techniques and algorithms available for indirect measurement of parameters of interest.

Radar measurements provide a much truer spatial mapping of precipitation, as opposed to point measurements from older rain gauging techniques, which are particularly suited for use in distributed models. The resolution of newer implementations promises to determine precipitation

data at high spatial and temporal resolution in real-time. The Next Generation [Weather] Radar (NEXRAD, also termed WSR-88) is a representative example of progress. Deployment for the WSR-88 Doppler systems began in 1988 (replacing the previous WSR-74 and WSR-54 deployments) and continued until 1997. Improvements to pieces of the NEXRAD network and similar systems continue, on aspects ranging from new and refined sensing technologies (Brewster et al. 2005, Scott et al. 2001) to data assimilation (Bocchiola 2007, Young et al. 2000).

Mapping and classification of land use and vegetation or snowpack cover data have also improved, due to projects (such as the Landsat Thematic Mapper, the Multispectral Scanner, and Systeme Probatoire de la Terre) that produce satellite imagery, which can be used alone or in conjunction with aerial photos and terrain data. Satellite-based remote sensing systems continue to progress in a fashion similar to land-based networks (such as NEXRAD). The Canadian Space Agency's RADAR-SAT2, launched in December 2007, began returning images in mid-January 2008, and will offer several new beam modes, with spatial resolution ranging from 3 to 100 meters and fully polarimetric C-band imagery (Kaya et al. 2004). In turn, land-cover classes can be used to obtain improved estimates of other parameters, as illustrated by Kite and Kouwen (1992) and Chen et al. (2005).

These new capabilities to observe and gather hydrologic data have stemmed entirely new applications of watershed models, which have found new uses, for instance, in real-time modeling applications. These applications, in turn, have stemmed new implications for management: Coskun (2008) has proposed an international 'Environmental Security' coalition for member states of the North Atlantic Treaty Organization (NATO). Flood and runoff forecasting, drought assessment/forecasting, mapping of groundwater potential, and management strategy assessment are but a few of the applications for which these approaches hold important potential (Coskun 2008, Goodrich et al. 1991).

#### ***2.3.4 DATA MANAGEMENT SYSTEMS: GIS AND DATA***

The augmented availability of these data types at higher resolutions, coupled with the drive to incorporate them into watershed models, has progressively led to a requirement for better data management and visualization systems. Non-raster based models, in particular, have seen a series of changes to translate a high volume of high resolution data into manageable digests for conceptual modeling tasks. This has resulted in the development of topographic parameterization and related terrain analysis techniques (e.g., Leavesley and Stannard 1990).

## 2.4 STATE OF THE ART – RESOLUTION AND SCALE ISSUES

### 2.4.1 SCALING AND VARIABILITY

Scale is usually defined as either the discretization used for computational purposes, or the spatial coarseness (length in the spatial domain, and duration in the time domain) at which observations are made (Singh 2002). Spatial variability describes the change in description of data or processes across each dimension, and is thus closely tied to the scale itself. Seyfried and Wilcox (1995) explored the effect of variability on hydrological response over a range of scales, using several field processes as examples.

Many hydrologic models employ point-scale equations based on conservation of mass, momentum, and energy. In such cases, the computations require data at a scale much finer than is readily available. This means that the point-scale equations must be up-scaled in order to conserve mass, momentum, and energy and to ensure compatibility between the scales of observed data and governing equations. It is important, however, to understand that excessive process description at one scale is effectively lost through the processes of integration in time and space and through averaging, justifying lumping and conceptual model simplification in many cases. Morel-Seytoux (1988) showed how simplifications can be made so that straightforward scaling integration is accomplished in a physically based stochastic framework. Indeed, as shown by Kavvas (1999) when a larger scale hydrological process (or parameter) itself is formed by averaging a small-scale process, the high frequency components of the smaller scale process are eliminated by averaging, and this leads to considerable simplification of the average hydrologic conservation equations.

### 2.4.2 SPATIAL RESOLUTION

With these issues outlined, it becomes clear that selection of the spatial scale to be used must also affect selection of a model. Loague (1988) and Chen (1994) have both demonstrated this, as has subsequent work.

The finest spatial scale which can acceptably characterize spatial heterogeneity in a hydrological model has been examined by Bathurst (1986), who suggested dividing the watershed into elements no larger than 1% of the total area to ensure that each element was more or less homogeneous, Wood et al. (1988), who proposed the notion of a representative elementary area (REA), and several others. Wood et al. defined the REA as the ‘smallest discernible point which is representative of the continuum’. This suggests a preferable temporal and spatial scale over which the process representations can remain simple, and distributed

catchment behaviour represented without the complexity of local heterogeneity (see Figure 2.1). The concept is analogous to the representative elemental volume concept of Hubbert (1956). Blösch et al. (1995) reasoned it is difficult, in practice, to determine the REA because it is strongly controlled by environmental characteristics.

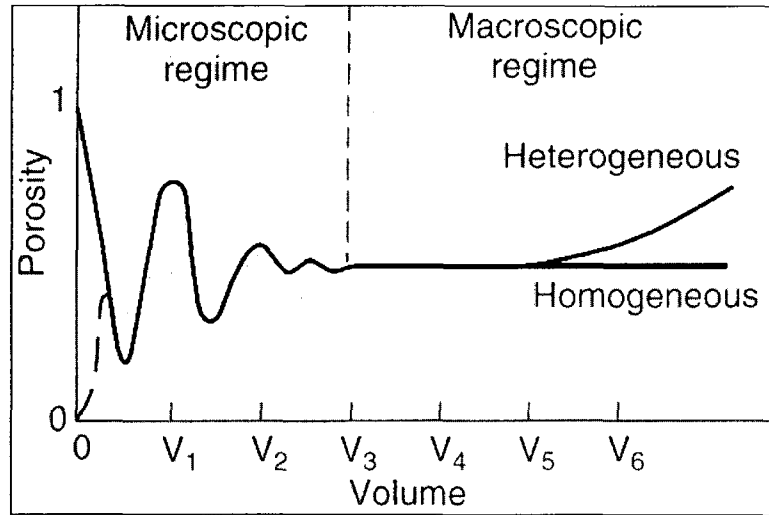


Figure 2.1: Representative Elementary Volume Determination (adapted from Hubbert 1956).

Zhang and Montgomery (1994) concluded that a grid size smaller than the hill-slope length was necessary to adequately simulate the processes controlled by land form, while Molnar and Julien (2000) found that coarser (0.835 vs. 0.016 km<sup>2</sup>) grid-cell resolutions can be used for runoff simulations as long as parameters are appropriately calibrated, and suggested the primary effect of increasing grid-cell size on simulation parameters is to require an increase in overland and channel roughness parameters. Song and James (1992) proposed a stochastic method to find an optimal scale for model application.

#### 2.4.3 TEMPORAL RESOLUTION

The issue of different timescales for individual hydrologic components remains an important issue. Common approaches generally apply conceptual models for fixed (e.g. daily) intervals, which can be viewed, in some ways, as analogous to rasterized approaches to spatial issues. Alternatively, event based (e.g., prior to, during and after precipitation events) discretization are perhaps more analogous to coarser, or hydrological lumping. Hughes (1993) suggested incorporation of variable time intervals in deterministic models. Conceptual disaggregation of rainfall into simple, constant and triangular distributions has been shown to

cause significant distortion in peak runoff rates (Woolhiser and Goodrich 1988). Additionally, the timescale of problem considered substantially influences the type of the conceptual model and data considered.

## **2.5 STATE-OF-THE-ART – CALIBRATION, SENSITIVITY AND ANALYSIS**

### **2.5.1 MODEL CALIBRATION**

With increasing model complexity and increasing calibration and input data requirements, model calibration has become an increasingly challenging step in the model construction process. Significant advances have followed, as outlined by Gupta et al. (1998). Several optimization methods have been developed for parameter estimation (both local and global), as discussed by Sorooshan and Gupta (1995). Typically, these methods are comprised of four components: the objective function, the optimization algorithm, a termination criterion, and calibration data. Clarke (1973) suggested basing the objective function on the stochastic properties of the errors in the model and the data.

Common problems with the prevalent optimization strategies today include the lack of a unique ‘best’ solution and the ability to handle ever larger data sets. Monte-Carlo membership, the prediction uncertainty method, and GLUE are some attempts to address these problems (van Staten and Keesman 1991, Klepper et al. 1991, Freer et al. 1996). More recently, Gupta et al. (1998) proposed a multi-objective paradigm that could include some handling of model error. Vrugt et al. (2005) developed a method they termed “simultaneous optimization and data assimilation” (SODA), combining aspects of Shuffled Complex Evolution (SCE) parameter search, as described in Section 2.6.5, with an ensemble Kalman filter. This combination aims to account for both parameter and non-parameter uncertainty (including input, output and structural sources) even in cases where optimal model parameters are unknown.

### **2.5.2 MACHINE LEARNING TECHNIQUES**

The use of Artificial Neural Networks (ANNs) is another alternative to parameter estimation problems, particularly suited for nonlinear systems such as rainfall-runoff forecasting [e.g., Lorrai and Sechi (1995)]. The key feature, but also reproach, was accurately identified by Hsu et al. (1995): ANNs do not require modeling the internal structure of the watershed, and can therefore be useful alternatives, but are not adequate replacements for conceptual watershed modeling. Genetic Algorithms (GAs) have also found applications in the field. Applications have ranged from calibration of conceptual models (e.g., Wang 1991) to more recent approaches

incorporating evolution of the expression or algorithm itself (e.g., Savic et al. 1999). Gashing et al. (1981) developed a knowledge-based expert system based on SWM for water resource problems, a concept which has continued to receive attention (e.g., Liu et al. 2007, Simanovic 1990), though the potential application of artificial intelligence has largely not (see, for instance, Liao 2005).

### 2.5.3 IMPACT AND WATER QUALITY ANALYSIS

The linking of hydrologic models with those of geochemistry, environmental biology, meteorology, and climatology has grown to be increasingly common since the 1980s, facilitated largely by new data technologies, coupled with an increased understanding of the issues surrounding spatial variability.

Several watershed hydrology models have moved towards direct incorporation of water-quality components into their structure. The demand for these tools is likely to continue to grow with the increasing need and applications of better, more integrated, environmental management systems.

|       |                |               |                |                |                |                |                |
|-------|----------------|---------------|----------------|----------------|----------------|----------------|----------------|
| $t=0$ | 0              | 0             | 0              | $\epsilon$     | 0              | 0              | 0              |
| $t=1$ | 0              | 0             | $\epsilon$     | $-2\epsilon$   | $\epsilon$     | 0              | 0              |
| $t=2$ | 0              | $\epsilon$    | $-4\epsilon$   | $6\epsilon$    | $-4\epsilon$   | $\epsilon$     | 0              |
| $t=3$ | $\epsilon$     | $-6\epsilon$  | $15\epsilon$   | $-20\epsilon$  | $15\epsilon$   | $-6\epsilon$   | $\epsilon$     |
| $t=4$ | $-8\epsilon$   | $28\epsilon$  | $-46\epsilon$  | $70\epsilon$   | $-46\epsilon$  | $28\epsilon$   | $-8\epsilon$   |
| $t=5$ | $45\epsilon$   | $-10\epsilon$ | $190\epsilon$  | $-232\epsilon$ | $190\epsilon$  | $-110\epsilon$ | $45\epsilon$   |
| $t=6$ | $-210\epsilon$ | $455\epsilon$ | $-722\epsilon$ | $844\epsilon$  | $-722\epsilon$ | $455\epsilon$  | $-210\epsilon$ |

Figure 2.2: Error propagation effects in a forward-difference scheme

#### **2.5.4 ERROR ANALYSIS**

One of the major limitations of current watershed models is the lack of error analysis in most applications. Indeed, it is often not clear from the user perspective what the model errors are or how errors are propagating through components and parameters. Figure 2.2 illustrates the effects of error propagation in a forward-difference scheme, where  $\epsilon$  represents an error that propagates in space (columns) and time (rows).

Even in such a relatively simple scenario, the significance of temporal and spatial propagation of error quickly becomes apparent. This adds ambiguity, and results in additional challenges for model selection and comprehension tasks.

### **2.6 STATE-OF-THE-ART - ERROR AND UNCERTAINTY IN ENVIRONMENTAL SYSTEMS**

#### **2.6.1 TERMINOLOGY OVERVIEW**

It is useful at this point to distinguish several terms, often used interchangeably. Error refers to the disagreement between a measurement and the true or accepted value. Precision refers to the tolerance or repeatability of a measurement, and is independent of the true value. Accuracy relates to the quality of a result (low error), and is distinguished from precision, which relates to the quality of the operation by which the result is obtained. Uncertainty of a measured value is an interval around that value such that any repetition of the measurement will produce a new result that lies within this interval. Uncertainty, rather than error, is the important term in most applications, and it is of particular importance to planners and modelers. The emphasis in this thesis, however, is focused in particular on the uncertainty associated with model estimates.

#### **2.6.2 ERROR**

As mentioned above, the error of a measurement is the discrepancy between the ‘true’ value and the value observed. All measurements have an inherent amount of error associated with them, and the act of observation itself affects the measured value to some degree. The task of modeling environmental processes at the catchment-scale involves varied measurement types and quality – including relatively invasive measurements that can significantly perturb the value being measured (but are generally more precise), and more non-invasive techniques which are also subject to significant error (and are generally less precise).

### 2.6.3 UNCERTAINTY

With respect to the modeling task, the impact of data error can be assessed quantitatively by considering inputs as subject to measurement uncertainty. Other sources of error and uncertainty also exist and propagate through the modeling process. Wainwright and Mulligan (2004) distinguish computational, procedural, propagation and specification error, while Zimmerman (2000) identifies lack and abundance of information, conflicting evidence, ambiguity, measurement uncertainty and belief as causes of uncertainty in model application. While both approaches are enlightening, there is much overlap in these definitions, and in complex systems such distinctions quickly become cumbersome.

For the purpose of convenience, it is often more practical to differentiate sources on a functional basis. Thus, for the task at hand three distinct levels of uncertainty that filter through to quantitative model predictions were identified.

The uncertainty associated with the raw data, termed here  $u_d$ , incorporates such factors as measurement error and bad (or missing) data. The uncertainty associated with the model parameters is defined as  $u_p$ , and reflects the uncertainty introduced during the conversion and interpretation of raw data to suitable input forms for the numerical model, as well as components surrounding calibration parameters. Together, these two sources form the uncertainty associated with model inputs, or  $u_i$ . The other component,  $u_m$ , is the uncertainty associated with the model structure itself. This part of the uncertainty evolves from inadequate conceptualization ( $u_c$ ) of processes being simulated as well as the connectivity and numerical discretization ( $u_n$ ) of model components (see Equation 2-1, where  $u_t$  is the total uncertainty of model predictions).

$$u_t = f(u_i, u_m) = f(u_d, u_p, u_c, u_n) \quad (2-1)$$

### 2.6.4 REDUCING UNCERTAINTY

With this framework defined, the question of reducing the uncertainty of the model outputs (and thus the data, parameter and model components) naturally arises. The data problem is especially prevalent in relatively uncontrolled settings with sparse record points, and thus of particular importance in environmental contexts such as watershed modeling. Coupled with this is the reduced ability to reset or remeasure conditions at a given spatial-temporal point. One approach to bettering data issues is to reduce the impact of relatively infrequent aberrations in the data model. A spatially distributed stochastic precipitation model, for instance, can be assembled from precipitation measuring stations within a given catchment. Such a strategy

further reduces the relative statistical significance of outliers (or input errors) which are less likely to occur simultaneously at several locations. A statistical description of several stations considered together may therefore help identify and/or mitigate those outliers due to data problems alone than is possible when considering a single temporal series at a given location alone.

The other source of input uncertainty, described above, involves the parameterization of the initial data model to match the model conceptualization and structure. It is thus closely tied to both the data and particular model structures, and can also be considered as the uncertainty inherent to linkage. This is the input component that typically demands the most of the user, both in terms of the inference from spatial data sources and model comprehension, and is the focus of the calibration process. Typically, models are calibrated by testing and optimizing their predictive accuracy, gauged against historical records with similar condition-spaces to the model's intended use. Specific optimization techniques range from straightforward numerical methods to procedures involving artificial intelligence and evolutionary algorithms. A detailed exploration of these procedures would be prohibitively long here, but it will suffice to say that they are plentiful and varied. It is well understood for deterministic models that the chosen 'calibrated' parameter set, and thus simulation results, depend on the reference data and calibration strategy used. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

The final uncertainty component ( $u_m$ ) is essentially a fixed component once a given model conceptualization (e.g., code, although some codes offer alternate component models) and structure (e.g., discretization) have been defined. Additionally, since the structure and component models involved are typically buried in source and technical manuals, it is something of a 'blind' term and is occasionally neglected.

The process of uncertainty reduction is not straightforward, but can be broadly conceptualized as a Pareto optimization problem. In catchments with large discretized components for example, conceptual models tend to be more reflective of processes and overall patterns at the expense of heterogeneity in parameter values. Conversely, smaller discretizations tend to reduce the range of parameter values, but conceptual models may become invalid, even for relatively simple processes such as flow routing (see Figure 2.3). Scaling (and the associated

change of parameter with scale) is thus an important consideration when addressing model uncertainty.

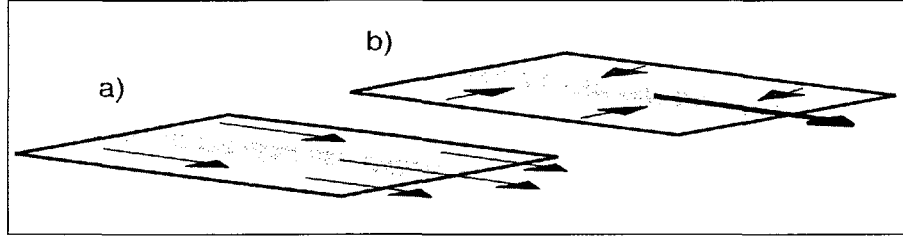


Figure 2.3: Two different conceptual models of flow within an element containing a channel (from Grayson and Blöschl 2001)

### 2.6.5 QUANTIFYING UNCERTAINTY

A variety of techniques for quantitative evaluation of uncertainty are available. Error-propagation and interval arithmetic type calculations can be used in comparatively simple models to compute the effects of input uncertainty. In more complex systems and modern codes, alternate analysis techniques are almost always required.

One of the most commonly used approaches for estimating model uncertainty is the Monte Carlo method. In this technique, multiple realizations of model input and parameter sets are generated based on distribution functions which are used to perturb the initial values. From the results of a sufficient number of realizations, probability estimates and error bands can be made to give ranges of possible outputs and confidence intervals (see, for instance De Roo et al. 1992, Håkanson 1996, and Phillips and Marks 1996). When contrasted with analytical methods, Monte Carlo analysis offers the advantage of being able to simulate variations in spatially distributed parameters, along with more complex interactions of uncertainty in component model outputs and intermediary variables. Nevertheless, implementation of the approach to large parameter sets can involve implementation of sampling designs and sensitivity analyses in addition to requiring hundreds or thousands of simulations for reliable results (see Heuvelink 1992, Klepper 1997, and Parysow et al. 2000).

In the random sampling case of parameter distributions, Monte Carlo analysis necessitates large numbers of simulations in order to accurately portray the parameter space. In many cases this approach becomes unwieldy, but this can be mitigated through use of strategic sampling techniques. One such approach is the Latin-Hypercube Sampling strategy (LHS) which is a stratified sampling method commonly used to reduce the number of Monte Carlo runs required.

Individual model parameters are sampled evenly from the cumulative distribution into groups (or bins). By selecting parameters for a run from each bin, the variable space can be sampled with significantly fewer runs.

In the SCE algorithm, developed in 1992 at the University of Arizona (hence the ‘-UA’ suffix that is often attached), the parameter space is sampled into a ‘population’ of several points representing parameter sets (see Figure 2.4). These points are then partitioned into a number of ‘complexes’. Essentially, the optimization algorithm is analogous to those found in classical genetic or evolutionary algorithms. The complexes are made to evolve in the direction of global improvement, using competitive evolution techniques. At periodic stages in the evolution, the entire set of points is shuffled and reassigned to new complexes to enable information sharing. Duan et al. (1992) outlined the specific fitness functions associated with the method in some detail. Improvements to the original algorithm have also been suggested and may be of particular value in certain applications (see for instance, SCEM-UA 2001). Other methods, such as SODA (discussed in Section 2.5.1) rely on a combination of approaches.

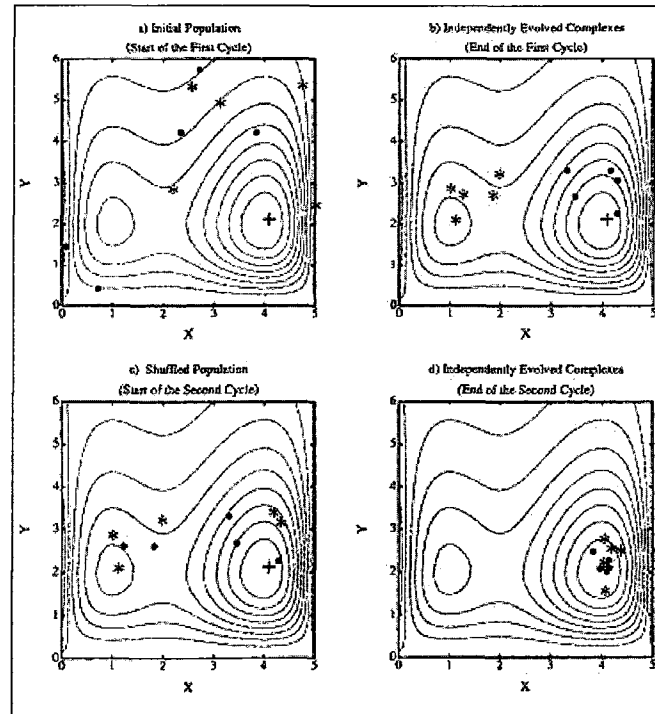


Figure 2.4: Sampling in the Shuffled Complex Evolution (SCE) method (from Duan et al. 1992)

In contrast to a search for an optimal parameter set, the GLUE procedure acknowledges the uncertainty associated with any representative set, and aims only to make an assessment of the likelihood of a set being an acceptable simulator of the watershed behaviour. In the GLUE algorithm, as developed by Beven and Binley (1992), many different model parameter sets are chosen for simulation. Evaluation measures are then used to reject some models (model structure/parameter set combinations) as nonbehavioural while all those considered as behavioural are retained in prediction. The predictions of the behavioural models are weighted by a likelihood measure based on past performance to form a cumulative weighted distribution of any predicted variable of interest.

The measures of likelihood are termed Bayesian estimators, and the parameter sets can be generated using a random (Monte Carlo) approach or subjectively based on, for instance, user experience. While LHS or similar techniques can also be used, one advantage of the GLUE algorithm is that it requires no assumptions to be made about the distribution function (see Beven 1993). The objective function chosen for the simulation is another significant factor in obtaining reliable results with the GLUE methodology (Legates and McCabe 1999, Wagener et al. 2003).

#### **2.6.6 QUALITATIVE APPROACHES**

It should also be noted that there is a school of thought that holds such error-estimation techniques as inherently untenable in numerous instances. Hall and Anderson (2002) criticize objective-based error estimation techniques, noting the lack of sufficient data and detailed measurements in many cases. This argument frequently rejects the validity of probabilistic terms and favors instead discussion of possibilities.

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## CHAPTER 3

### AN OBJECTIVE TEST OF STOCHASTIC BEHAVIOR IN RIVERINE WATER QUALITY MODELS

#### 3.0 CHAPTER OVERVIEW

This chapter was accepted for presentation at the IWA 2008 World Water Congress in Vienna, Austria, and was published in the *Water Science and Technology* 59(1) pp.159-165 (2009).

#### **ABSTRACT**

Predictions of river water quality models are subject to substantial uncertainties, which depend not only on parameterization and calibration strategies but also on the structure of the conceptual model itself. To evaluate the importance of this effect and associated implications for stochastic models, investigations were conducted based on a segment of the Potomac River in the eastern US. Two commonly used conceptual representations of real-world processes were used (MIKE11 and QUAL2E), and their simulation of DO, BOD and  $\text{NH}_4$  components scrutinized. A GLUE approach to the inverse problem was then used to examine how uncertainty changed along the river network for each conceptual model. Differences were observed not only between deterministic instances of each conceptual model, but also between their response surfaces as a whole. Uncertainties within the river network are substantially influenced by the selection of calibration data used, as well as the primary source of the constituent examined. The suggested methodology can be used to test conceptual model validity for specific applications. The results of this study will help users select and assess models for varied problems, and refine appropriate data collection and monitoring schemes.

Listed keywords were: Water Quality, Numerical Models, Uncertainty, Watershed, MIKE11, and QUAL2E.

#### 3.1 INTRODUCTION

##### **3.1.1 BACKGROUND**

Watershed-level modeling has become an essential tool in planning and managing environmental risks and the relationship between pollutant sources and water bodies, and an approved Total Maximum Daily Loading (TMDL) evaluation has become a de facto requisite for

assistance funding. Water quality models are generally deployed in such cases to provide insight on source assessments and their impacts on water quality targets as well as the consequences of varied management scenarios (e.g., Parker et al. 2008)

Model parameters are adjusted to fit one or several years of reference data. It is well understood for deterministic models that the chosen ‘calibrated’ parameter set, and thus simulation results, depend on the reference data and calibration strategy used. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

Stochastic models attempt to mitigate these issues to some degree by representing modeled phenomena as a distribution of possible outcomes. A common implementation is to perturb input parameters, through use of Monte-Carlo simulations, for example, and assess likely outcomes from the results.

Equally important to the stochastic model response, however, is the underlying conceptual model structure itself. In practice, this issue is rarely explicitly considered, as a handful of codes, primarily designed for deterministic simulation, are in wide use. The approach of this paper is to examine and illustrate the stochastic response of two competitive conceptual models for water quality simulation in riverine systems.

### ***3.1.2 WATER QUALITY MODELS***

The earliest formal water quality conceptual models, from Streeter and Phelps (1925), as well as others, included a dissolved oxygen (DO) supply and biochemical oxygen demand (BOD) balance. Since that time, as knowledge has progressed, revised conceptual models have been proposed for these and other major processes in river systems (cf. Thomas, 1948; Bowie et al., 1985). Many of these models have in turn found one or more incarnations in a variety of computer codes such as QUAL2E, MIKE11 and others (Brown and Barnwell, 1987; McCutcheon, 1989) to support analyses of problems such as pollution control and land-use and waste-loading planning.

While some models have been expressly developed for stochastic use, such models tend to be more narrowly applicable, and the vast majority of models in regular use remain deterministic models. The EPA, for instance, recommends use of QUAL2E (and the derivative QUAL2EK) in their Better Assessment Science Integrating Point & Nonpoint Sources (BASINS) framework, designed for use by regional, state, and local agencies in examining management alternatives for

watersheds (Duda et al., 2003). Sampling methods such as Monte-Carlo simulation are often used to account for (parameter) uncertainties in such deterministic-based models.

## 3.2 METHODOLOGY

### 3.2.1 STUDY AREA AND DATA

The Potomac Watershed stretches across approximately 38 000 km<sup>2</sup>, of the Eastern US. The Potomac River itself covers roughly 620 km from Fairfax Stone in West Virginia to Point Lookout in Maryland. The average river flow at the Washington, DC location is about 310 m<sup>3</sup>/s, with minimum and maximum recorded flows of 17 m<sup>3</sup>/s (September, 1966) and 12000 m<sup>3</sup>/s (March 1936), respectively. The watershed flows into Chesapeake Bay, becoming tidal where the river crosses the Fall Line into the Coastal Plain province. Downstream from here, the water becomes increasingly brackish with a gradual increase in salinity. This study limits itself to the purely freshwater and non-tidal portion of the Potomac (Figure 3.1).

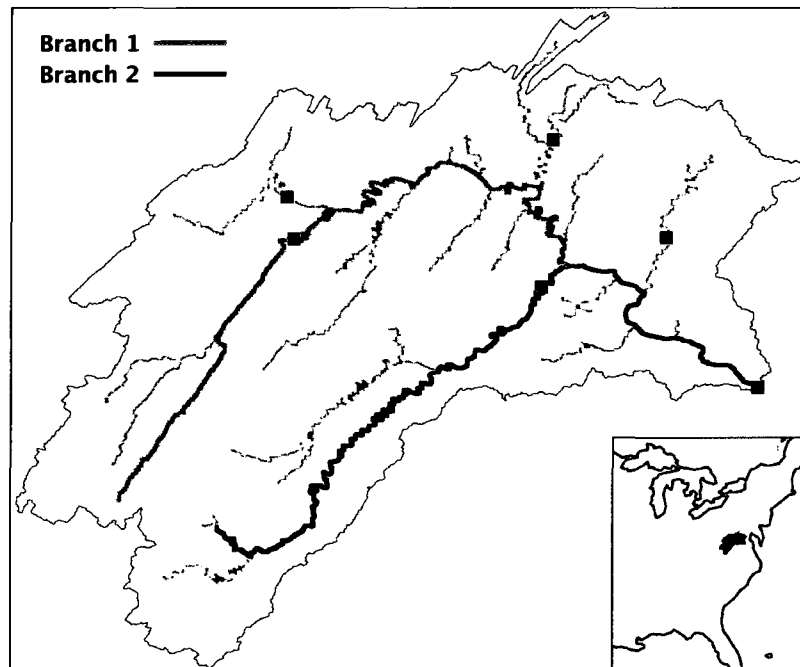


Figure 3.1: Non-tidal Potomac Watershed (location shown in inset). River network as modeled shown in dark grey, with two branches highlighted in orange and blue (green indicates overlapping reaches). Red squares indicate water quality calibration points.

From 1991 to 1996, the US Geological Survey's (USGS) National Water Quality Assessment (NAWQA) program began extensive work in the basin to monitor surface and

ground water quality and ecology. That dataset is used here, and draws on over 50 USGS stations to provide information on stream flow quantity for the year 1993. These data are available at up to daily timesteps for individual stations. Water quality data are available at 5 ‘integrator’ and 5 ‘indicator’ stations on a monthly basis. Point Sources loading the river system were identified from US EPA (2007).

### ***3.2.2 WATER QUALITY SIMULATION***

Typical constituents of interest in water quality models include DO, nutrients (e.g., nitrogen, phosphorus), and toxics (e.g., pesticides). For this paper a conversion kinetics model based on the widely used QUAL2E code (see Brown and Barnell, 1987) was compared with the formulation of the MIKE11 code (see DHI, 1992). An extensive review of water quality modeling approaches in beyond the scope of this outline, (but can be found in e.g., Rauch et al., 1998 or Bowie et al., 1985). Appendix G lists representative equations and processes found in a water quality model.

Although similar in overall structure and application, the two kinetic models tested here differ in several important respects. Rapidly biodegradable organic matter demand (BOD) is treated as a single state variable in the QUAL2E models, and as three fractions (dissolved, suspended and sedimented) in the MIKE11 model. In addition, while the base MIKE11 model limits itself to also considering DO and nitrogen species, QUAL2E considers algal biomass, organic nutrient components, as well as a more complex representation of nitrification (where nitrite is tracked).

Output of the two models was compared for stochastic simulation of DO, BOD and ammonia-N ( $\text{NH}_4$ ). Initial ranges for water quality model parameters are estimated from literature values (Bowie et al., 1985). Spatial-varied inputs (e.g., water loadings) for the river system were extracted from the flow gauging station and point source data sets. Flow differences between two sequential stations not explained by one or several point sources were considered to be attributable to baseflow and surface runoff components, distributed evenly over the river length between the two stations. Representative constituent concentrations for these flow components were considered as a further set of parameters to be varied across runs. The candidate range of these model parameters was based on seasonal averages at indicator stations. The addition of this component, essentially a weak NPS model, is useful but may lead to additional challenges (not the least of which is computational requirements), which is likely why others (e.g., Rode, 2007) have preferred to use a point-source only description. Such an approach can also be considered a

special case of that applied here, with the constituent contribution parameter set to a fixed value (0).

### 3.2.3 MODEL RESPONSE EVALUATION

For each conceptual model, the representative model set was then derived. The problem can be viewed as an inverse modeling exercise. It is usual to pose such problems in terms of the observation equation.

$$y_t = g(u_0, \dots, u_1, \xi_0, \dots, \xi_t, \zeta_t, \theta, t) \quad (3-2)$$

In Equation 3-2 terms include the model output ( $y_t$ ) the model inputs ( $u_t$ ), errors associated with model inputs ( $\xi_t$ ), measurement error ( $\zeta_t$ ), and a vector of model parameters ( $\theta$ ) for each point  $t$ . The problem to be solved is the retrieval of the parameter set  $\theta = \{\pi_i\}_{i=1, \dots, N}$  and particularly the associated posterior distribution  $p(\theta | y)$ , given  $N$  stream data observations  $y = \{y_i\}_{i=1, \dots, N}$ . When  $p(\theta)$  is defined, Bayesian approaches such as forward (likelihood) models (e.g., the sequential Bayes algorithm) or direct local inverse models are well-suited for the inference of  $p(\theta | y)$ . In more complex cases there may not always be a well-defined posterior parameter distribution [i.e.,  $p(\theta)$ ], which is the set of parameters that produce representative models.

A Generalized Likelihood Uncertainty Estimation (GLUE) algorithm, as outlined by Beven and Binley (1992), was used to identify which parameter sets provide an adequate representation of the river system water chemistry. The GLUE framework offers several advantages for these types of problems, as it allows for the very complex likelihood surfaces expected with such parameter interactions. In this technique, the focus is on estimating posterior distributions for predicted variables directly from the outputs of a set of representative models, rather than from a model and an additive residual model. The resulting set of models is further constrained by the calibration data and criteria (cf. Beven, 2001 and Rode et al., 2007), and contains information on the simulation output variability for all representative input sets. The representative set can be viewed as the range of water quality models that conform to the calibration criteria, which in turn are constrained by the specific dataset used. Stated another way, this set contains information on the water quality model output variability for all representative input parameter sets. Furthermore, individual representative models can be weighted according to the degree of belief (or likelihood) in each model. Thus, by making an assumption on the model output distribution structure, a measure of output ‘uncertainty’ at each location in the riverine system is obtained.

Results from the GLUE examination are presented in several ways. The important concept is that of surface response, which is the range of simulation results at a given point (in space, or time) from those models which are considered representative. A ‘narrow’ surface response at a given location indicates many models predicting very similar values there, while a ‘wider’ response suggest a greater variation in predicted outputs among representative models.

### ***3.2.4 STOCHASTIC RESPONSE MODEL TOOLKIT***

With the base models and simulation strategy decided upon, a toolset was developed to facilitate the model response evaluation methodology. A FORTRAN script implementation of the strategy detailed above was developed into a water quality inverse modeling toolkit (dubbed ‘qualIT’ for reference). The toolkit consists of three major components. The first of these is the run manager, which is responsible for tracking seed numbers and conditions at each run number and generating suitable parameter sets for the subsequent modules. The simulation manager calls the base water quality models, and passes the generated parameter sets for execution. The output processor produces a manageable digest (output fitness at user-specified locations) of run results returned by the conceptual model.

This modular structure is advantageous in that it allows for complete reproducibility of conditions at a given run number. This, in turn, permits efficient use of processing resources for both serial (e.g., calibration at new data locations) and parallel (e.g., base run generation) simulations tasks. Processing was done on an ad hoc ‘CONDOR’ cluster (cf. Tannenbaum et al., 2002), consisting of up to 5 modern desktop computers (subject to availability) totaling 8 processors at an approximate total of 16 billion cycles per second, and managed by a custom built ‘HPC\_monitor’ package.

### ***3.2.5 SIMULATION MATRIX AND METRICS***

A base set of runs was conducted for each conceptual model, consisting of 2 million randomized parameter sets from the selected sample space. These initial runs were divided into parallel jobs across several processors, and then reassembled for further processing. Subsequent processing included a sequentially implemented ‘base calibration’ (representative set selection) based on fitness at each data point. This fitness was based on the absolute relative error (ARE), when compared with annual averages, using the simple relation found in Equation 3-3

$$\text{fitness} = \frac{1}{\text{ARE}} = \left| \frac{C_{\text{observed}}}{C_{\text{approximated}} - C_{\text{observed}}} \right| \quad (3-3)$$

The ‘base calibration’ selection was designed to capture essentially all runs that could be considered representative at all points. In addition, a narrower ‘highest likelihood’ surface was also selected, based on fitness of outlet prediction (Eq. 3-3), resulting in a final data set of the 200 highest fitness runs, or 0.01% of the initial runs (see Table 3.1). The resulting run sets share similar characteristics and sample size, suggesting that the selection criteria and initial run size were sufficient to avoid some potential sampling issues.

Table 3.1 Run Calibration and Subset Selection

|                  | Absolute Relative Error at<br>Outlet (%) |       |                 | Number of<br>Runs | Percent of<br>all Runs |
|------------------|------------------------------------------|-------|-----------------|-------------------|------------------------|
|                  | DO                                       | BOD   | NH <sub>4</sub> |                   |                        |
| MIKE11           |                                          |       |                 |                   |                        |
| Base Calibration | 23.22                                    | 64.11 | 37.80           | 17358             | 0.86                   |
| High-Likelihood  | 5.32                                     | 37.38 | 6.20            | 200               | 0.01                   |
| QUAL2E           |                                          |       |                 |                   |                        |
| Base Calibration | 23.19                                    | 65.24 | 41.28           | 17254             | 0.86                   |
| High-Likelihood  | 5.32                                     | 36.76 | 6.14            | 200               | 0.01                   |

### 3.2.6 SURFACE RESPONSE METRICS

The basic statistical measure used to describe the response surface in this paper is the coefficient of variation (sometimes termed relative variability), which expresses the dispersion (the standard deviation,  $\sigma$ ) of a data set around its mean ( $\mu$ ) (cf. Equation 3-4).

$$c_v = \frac{\sigma}{\mu} \quad (3-4)$$

In this case the data set is the set of output parameter values within the set of representative models. The coefficient of variation,  $c_v$ , is useful because it allows the degree of

variation in several series of data to be compared, and is therefore often used to assess relative volatility or risk. In addition, an aggregate metric is also used to help summarize and present results:

$$C_{V_{agg}} = \frac{C_{v_{DO}}}{3} + \frac{C_{v_{BOD}}}{3} + \frac{C_{v_{NH4}}}{3} \quad (3-5)$$

This metric can be thought of as an average equivalent to the coefficient of variation of the three constituents of interest considered here.

### 3.3 RESULTS AND CONCLUSIONS

#### 3.3.1 RESULTS

The study area was divided into two main branches for discussion here, with an overlapping length of reach near the outlet (see Figure 3.1). As mentioned in the discussion of Equations 3-4 and 3-5, the aggregate coefficient of variation (ACV) metric is useful in comparing surface responses of each model. The ACVs for each conceptual model are presented in Figure 3.4 for both the main and secondary branch.

Figure 3.2 portrays the change in response surface throughout the reach network for each conceptual model. In this way, information on the spatial change of the uncertainty ‘cloud’ of modeled water quality constituents is presented. Several interesting characteristics are suggested from this initial plot. Firstly, although the MIKE11 response surface is marginally narrower (suggesting lower uncertainty in simulation results), both models appear to behave very similarly near the outlet. Conversely, the models differ significantly in their surface responses over the tributary branches regions.

To some extent this change is to be expected. The water quality calibration points shown in Figure 3.1 are not distributed evenly throughout the watershed. Information from calibration points constrain the model set deemed to be representative and therefore tends to narrow the uncertainty cloud in the region. Though both highlighted branches have a calibration point directly in their lengths, several tributaries of the primary branch (in the north) also pass through calibration points. In this way, additional information is ‘flowing’ (with the literal water flow) from these tributary reaches into the principal branch. This concept of information (or data) ‘flow’ is important in interpreting the subsequent model response.

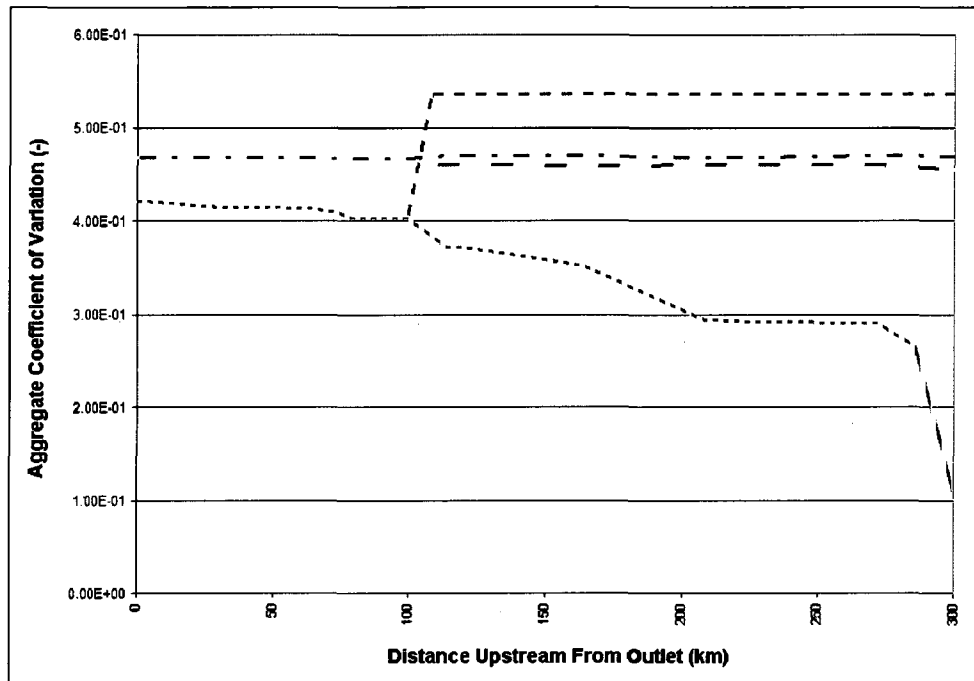


Figure 3.2: Base Calibration Surface Response of MIKE11 (in Orange) and QUAL2E (in Green) conceptual models. Darker lines indicate secondary branches for both models, as defined in Figure 3.1.

Both branches in the QUAL2E model appear to have similar responses to the outlet region, with a relatively similar, steady ACV in each branch. In this base calibration response surface the first branch appears to have a marginally smaller 'spread' than the second one, with a slight rise in uncertainty in each branch as the model moves upstream (away from data inflows). As the two branches mix (near the 100 km mark), the ACV narrows marginally further, suggesting that both branches are contributing to reducing the combined uncertainty, with data and simulation result flows from the second branch supporting the first.

The MIKE11 model appears to respond quite differently in several respects. Firstly, while the ACV near the outlet is similar (in magnitude and stability) to that of the QUAL2E model, there is a considerable difference in the ACV of each main branch upstream of the mixing point. The main branch, with relatively more information, has a much lower ACV than is found at the outlet, and also a much larger variation within the branch itself than was noted in the QUAL2E simulation results. Conversely, the second branch has a larger ACV than is found at the outlet or in the first branch. Also interesting is the comparison in the mixing: though the primary branch accounts for only about 30% more literal water flow than the secondary, the mixed ACV tends

decidedly towards the main branch (containing a larger majority of ‘data flow’). Unlike the QUAL2E simulation however, the complementary information in the secondary branch does not appear to be contributing to a reduction of the main branch ACV near the outlet.

These differences between conceptual models are a product of several factors. As mentioned earlier, while the calibration and results presented are limited to considering the BOD, DO and  $\text{NH}_4$  modeled by the MIKE11 model, the QUAL2E model is also tracking several additional state variables (e.g., phosphorus, algal biomass), and is more parameterized. These ‘hidden’ conceptual model components can act somewhat as constraining buffers to rapid change, adding some measure of uncertainty-inertia to the QUAL2E simulation results.

A second response surface was also examined, and is shown in Figure 3.3. This reflects a subset of the previous base calibration result set, selected at the outlet from those runs with the highest fitness. This high-likelihood set would perhaps be suitable for management decision making tasks.

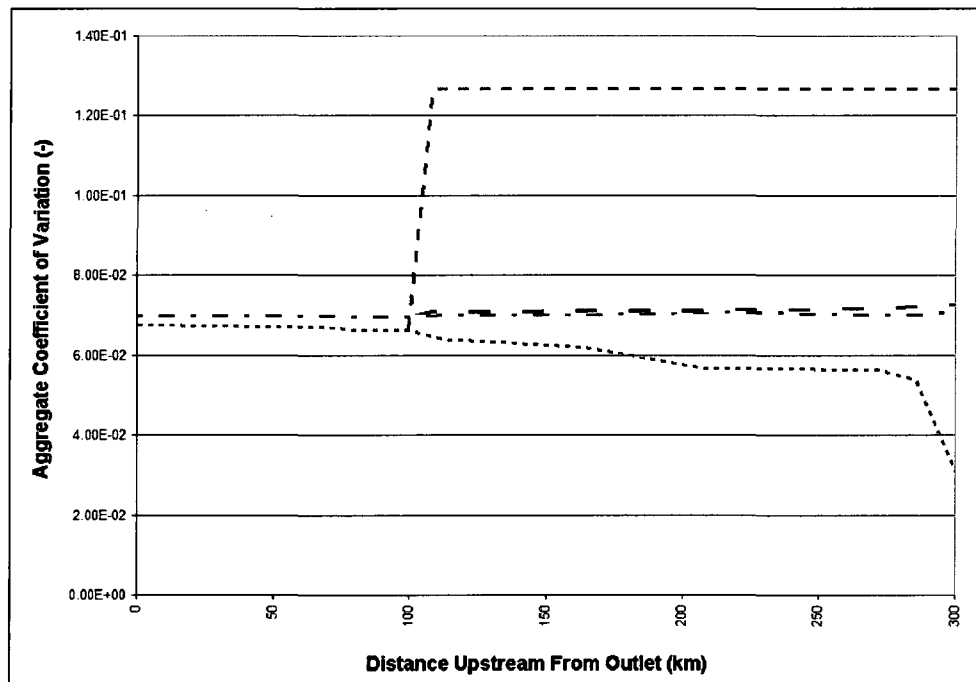


Figure 3.3: High-Likelihood Surface Response of MIKE11 (in Orange) and QUAL2E (in Green) conceptual models. Darker lines indicate secondary branches for both models, as defined in Figure 3.1.

An examination of these results shows essentially the same overall trends as the base calibration uncertainty analysis. Indeed, while the uncertainty cloud spread, as measured by the

ACV, is more narrow for the high likelihood subset (note the change in y-axis scale), both conceptual models still behave similarly towards the outlet and quite differently in the main branches. However, two significant differences are still apparent. The MIKE11 secondary branch surface analysis still leads to a larger ACV than the primary branch, however the difference between the two has been substantially narrowed, and the maximum MIKE11 ACV is now much closer to the maximum QUAL2E ACV in the main branch. The QUAL2E secondary branch has also gained in confidence, and both primary and secondary branches now show roughly equal performance at all locations (cf. Figure 3.2). Taken together, these behaviours help the modeler (and decision maker) to understand how the high-likelihood condition is altering the surface response. In this case the subset is being selected primarily from runs with a narrower range of water quality constituent results in the secondary branch.

The question of relative predictive performance of each base calibration set arises naturally. Indeed, of what use is a narrower response surface in a model if the ARE is noticeably higher? The run summary presented in Table 3.1 addresses this concern and shows that the difference lies not so much in the prediction quality as in the uncertainty surface itself.

In addition to spatial response, the temporal surface response was also examined. This was accomplished by comparing water quality model simulation results from the high-likelihood set (calibrated on an annual basis at the outlet) on a month-by-month basis with observed data. Results are shown as response extents, consisting of the upper and lower 95% bounds of representative model simulation outputs, and means in Figure 3.4.

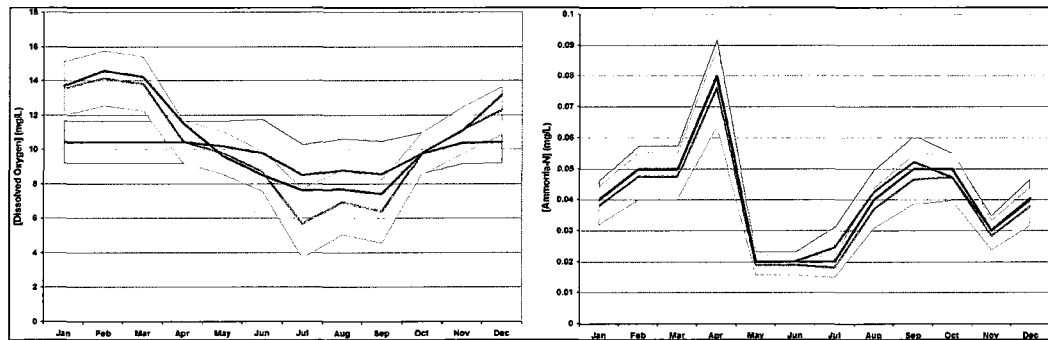


Figure 3.4: High-likelihood surface response (95% bounds) at outlet of MIKE11 (in Orange) and QUAL2E (in Green) conceptual models calibrated on an annual basis. Blue line indicates observed data. Solid lines show mean of representative models.

It should once again be emphasized that the calibration (and selection) was done on an annual basis, so that these plots in fact show data response under 12 flow regimes different to those in the calibration/selection set.

The analogy to the spatial results is striking, particularly in the DO plot. While the ACV of the MIKE11 tends to be much better in flow regimes similar to the annual calibration conditions (i.e. high flows), the width of cloud varies greatly from month to month. Summer conditions contribute substantially less to the ‘average’ conditions, and are less well represented. The MIKE11 cloud as a whole also appears to track the seasonal changes in the data quite well, as can be seen by following the cloud mean. Conversely, the QUAL2E once again shows signs of model inertia – it tends to reflect the average conditions rather than move to match the changing data. The ACV (cloud width) is again steadier in the QUAL2E model than in the MIKE11 representation.

### **3.3.2 CONCLUSIONS**

The suggested methodology can be used to test conceptual model validity for specific applications. The results of this study will help users select and assess models for varied problems, and refine appropriate data collection and monitoring schemes. A common theme that emerges from the observed results is the importance in understanding the response characteristics. As an example, in our chosen case study, an annually calibrated stochastic MIKE11 model might be deemed useful for monthly simulation. The results here suggest that a similarly calibrated QUAL2E model could be decidedly less suitable, depending on the type of problem addressed. Additionally, while both models appear to have approximately the same predictive ability for a given set of calibration criteria, the MIKE11 model appears far more sensitive to data availability. At least in this study, the MIKE11 model response changed greatly depending on the proximity to calibration points, while the QUAL2E model tended to improve less rapidly near high data locations, but also to degrade less away from such locations. This finding has important ramifications for the development of data sampling schemes and model selection in sparse vs. dense data situations. The proposed use of GLUE for selection of a preferred conceptual model structure is a novel addition to the field of water quality modeling.

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## **CHAPTER 4**

# **STOCHASTIC CALIBRATION OF RIVERINE WATER QUALITY MODELS**

### **4.0 CHAPTER OVERVIEW**

This chapter was accepted for presentation at the Water Environment Federation's 81<sup>st</sup> Annual Technical Exhibition and publication in the proceedings thereof. It is also under consideration for publication in *Water Environment Research*.

#### ***ABSTRACT***

Though commonly used, the suitability of deterministic calibration criteria for stochastic model calibration and uncertainty analysis is unclear. The approach of this paper is to examine the suitability, relative benefits and substantial disadvantages of 'deterministic-optimization' approaches in stochastic contexts. Three alternate calibration strategies suitable for modeling water quality under uncertainty are proposed and then demonstrated. The findings suggest potential improvements be made to current calibration paradigms.

Absolute relative error (ARE) calibration strategies, and several special applications thereof, were found to match or exceed root mean square error (RMSE) calibration strategies in terms of overall performance, with the enhancement of superior model surface response characteristics. Additionally, applying more stringent ARE criteria were found to improve stochastic calibration response when contrasted with increasing RMSE threshold criteria. Several qualitative benefits of ARE and related metrics were also shown. Since many environmental systems, and almost all water quality models, are subject to substantial uncertainty, approaches such as those proposed hold substantial, widely applicable, benefits.

Listed keywords were: Water Quality, Model, Uncertainty, Calibration, Stochastic.

### **4.1 INTRODUCTION**

#### ***4.1.1 BACKGROUND***

Watershed-level modeling has become an essential tool in planning and managing environmental risks and the relationship between pollutant sources and water bodies, and an approved Total Maximum Daily Loading (TMDL) evaluation has become a de facto requisite for assistance funding. Water quality models are generally deployed in such cases to provide insight

on source assessments and their impacts on water quality targets as well as the consequences of varied management scenarios (e.g., Parker et al., 2008a).

Model parameters are adjusted to fit one or several years of reference data. It is well understood for deterministic models that the chosen ‘calibrated’ parameter set, and thus simulation results, depends on the reference data and calibration strategy used. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

Stochastic models attempt to mitigate these issues to some degree by representing modeled phenomena as a distribution of possible outcomes. A common implementation is to perturb input parameters, through use of Monte-Carlo simulations for example, and assess likely outcomes from the results.

#### ***4.1.2 WATER QUALITY MODELING***

Water quality models have evolved from the early dissolved oxygen (DO) supply and biochemical oxygen demand (BOD) considerations of Streeter and Phelps (1925), to modern incarnations in a variety of computer codes which are used to support analysis of problems such as pollution control and land-use and waste-loading planning. Modern codes such as QUAL2E (Brown and Barnwell, 1987) go beyond the oxygen balance and can consider nitrogen, phosphorus and other cycles. As models become more sophisticated, the parameter sets required to calibrate a code for a given application become larger and more complex (Bowie, 1985). The resulting (parameter) uncertainty is a major consideration for the use of modeling results.

While some models have been expressly developed for stochastic use, such models tend to be more narrowly applicable, and the vast majority of models in regular use remain deterministic models. The EPA, for instance, recommends use of QUAL2E (and the derivative QUAL2K) in their Better Assessment Science Integrating Point & Nonpoint Sources (BASINS) framework, designed for use by regional, state, and local agencies in examining management alternatives for watersheds (Duda et al., 2003). Sampling methods such as Monte-Carlo simulation are often used to account for (parameter) uncertainties in such deterministic-based models.

#### ***4.1.3 MODEL CALIBRATION***

The Root Mean Square Error (RMSE) is commonly used (along with related metrics) for deterministic model optimization. The advantages of RMSE for this type of problem are several-fold. It is an easily computed and interpreted statistic with the same units as the modeled

parameter. Two or more statistical models can be readily compared using the RMSE as a measure of goodness of fit, where the smallest RMSE is interpreted as the ‘better’ model. A readily identifiable disadvantage to the RMSE for deterministic applications is the effect of localized large errors (even in small spatial, temporal or parameter regions).

The wide use and acceptance of RMSE for these types of problems has led to frequent use of the same methods for stochastic evaluations - either explicitly, or implicitly via post-calibration Monte-Carlo analysis (e.g., Marsili-Libelli and Giuseppi, 2008; Rode et al., 2007; van Grievsen and Meixner, 2007). More formally, RMSE and related measures have found ample applications (and justification) in Bayesian approaches, although they may not always be the superior alternative or, indeed, appropriate (see e.g., Romanowicz and Beven, 2006; Ojeda et al., 2007).

## **4.2 METHODOLOGY**

### **4.2.1 STUDY AREA AND DATA**

The Potomac Watershed stretches across approximately 38 000 km<sup>2</sup>, of the Eastern US. The Potomac River itself covers roughly 620 km from Fairfax Stone in West Virginia to Point Lookout in Maryland. The average river flow at the Washington, DC location is about 310 m<sup>3</sup>/s, with minimum and maximum recorded flows of 17 m<sup>3</sup>/s (September 1966) and 12000 m<sup>3</sup>/s (March, 1936), respectively. The watershed flows into Chesapeake Bay, becoming tidal where the river crosses the Fall Line into the Coastal Plain province. Downstream from here, the water becomes increasingly brackish with a gradual increase in salinity. This study limits itself to the purely freshwater and non-tidal portion of the Potomac (shown in Figure 4.1).

From 1991 to 1996, the US Geological Survey’s (USGS) National Water Quality Assessment (NAWQA) program began extensive work in the basin to monitor surface and ground water quality and ecology. That dataset is used here, and draws on over 50 USGS stations to provide information on stream flow quantity for the year 1993. These data are available at up to daily timesteps for individual stations. Water quality data are available at 5 ‘integrator’ and 5 ‘indicator’ stations on a monthly basis. Point Sources loading the river system were identified from US EPA (2007).

### **4.2.2 WATER QUALITY SIMULATION**

Typical constituents of interest in water quality models include DO, nutrients (e.g., nitrogen, phosphorus), and toxics (e.g., pesticides). For this paper a conversion kinetics model

based on the widely used QUAL2E code (see Brown and Barnell, 1987) was used. An extensive review of water quality modeling approaches is beyond the scope of this outline, (but can be found in e.g., Rauch et al., 1998 or Bowie et al., 1985).

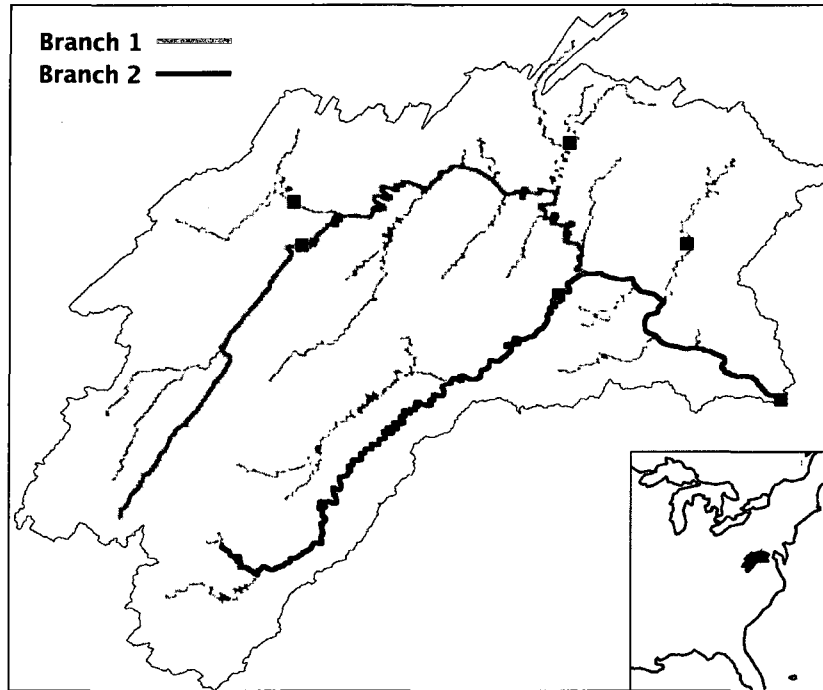


Figure 4.1: Non-tidal Potomac River Watershed (location shown in inset). Red squares indicate water quality calibration points.

Output of the model was compared for stochastic simulation of DO, BOD and ammonia-N ( $\text{NH}_4$ ). Initial ranges for water quality model parameters are estimated from literature values (Bowie et al., 1985). Spatial-varied inputs (e.g., water loadings) for the river system were extracted from the flow gauging station and point source data sets. Flow differences between two sequential stations not explained by one or several point sources were considered to be attributable to baseflow and surface runoff components, distributed evenly over the river length between the two stations. Representative constituent concentrations for these flow components were considered as a further set of parameters to be varied across runs. The candidate range of these model parameters was based on seasonal averages at indicator stations. The addition of this component, essentially a weak NPS model, is useful but may lead to additional challenges (not the least of which is computational), which is likely why others (e.g., Rode, 2007) have preferred to use a point-source only description. Such an approach can also be considered a special case of that applied here, with the constituent contribution parameter set to a fixed value (0).

### 4.2.3 MODEL RESPONSE EVALUATION

For each conceptual model, the representative model set was then derived. The problem can be viewed as an inverse modeling exercise. It is usual to pose such problems in terms of the observation equation:

$$y_t = g(u_0, \dots, u_1, \xi_0, \dots, \xi_t, \zeta_t, \theta, t) \quad (4-1)$$

In Equation 4-1 terms include the model output ( $y_t$ ) the model inputs ( $u_t$ ), errors associated with model inputs ( $\xi_t$ ), measurement error ( $\zeta_t$ ), and a vector of model parameters ( $\theta$ ) for each point  $t$ . The problem to be solved is the retrieval of the parameter set  $\theta = \{\theta_i\}_{i=1, \dots, N}$  and particularly the associated posterior distribution  $p(\theta | y)$ , given  $N$  stream data observations  $y = \{y_i\}_{i=1, \dots, N}$ . When  $p(\theta)$  is defined, Bayesian approaches such as forward (likelihood) models (e.g., the sequential Bayes algorithm) or direct local inverse models are well-suited for the inference of  $p(\theta | y)$ . In more complex cases there may not always be a well-defined posterior parameter distribution [i.e.,  $p(\theta)$ ], which is the set of parameters that produce representative models.

A Generalized Likelihood Uncertainty Estimation (GLUE) algorithm, as outlined by Beven and Binley (1992), was used to identify which parameter sets provide an adequate representation of the river system water chemistry. The GLUE framework offers several advantages for these types of problems, as it allows for the very complex likelihood surfaces expected with such parameter interactions. In this technique, the focus is on estimating posterior distributions for predicted variables directly from the outputs of a set of representative models, rather than from a model and an additive residual model. The resulting set of models is further constrained by the calibration data and criteria (cf. Beven, 2001 and Rode et al., 2007), and contains information on the simulation output variability for all representative input sets. The representative set can be viewed as the range of water quality models that conform to the calibration criteria, which in turn are constrained by the specific dataset used. Stated another way, this set contains information on the water quality model output variability for all representative input parameter sets. Furthermore, individual representative models can be weighted according to the degree of belief (or likelihood) in each model. Thus, by making an assumption on the model output distribution structure, a measure of output ‘uncertainty’ at each location in the riverine system is obtained.

#### ***4.2.4 STOCHASTIC RESPONSE MODEL TOOLKIT***

With the base models and simulation strategy decided upon, a toolset was developed to facilitate the model response evaluation methodology. A FORTRAN and script implementation of the strategy detailed above was developed into a water quality inverse modeling toolkit (dubbed 'qualIT' for reference). The toolkit consists of 3 major components. The first of these is the run manager, which is responsible for tracking seed numbers and conditions at each run number and generating suitable parameter sets for the subsequent modules. The simulation manager calls the base water quality model, and passes the generated parameter sets for execution. The output processor produces a manageable digest of run results returned by the conceptual model.

This modular structure is advantageous in that it allows for complete reproducibility of conditions at a given run number. This, in turn, permits efficient use of processing resources for both serial (e.g., calibration at new data locations) and parallel (e.g., base run generation) simulations tasks. Processing was done on an ad hoc 'CONDOR' cluster (cf. Tannenbaum et al., 2002), consisting of up to 5 modern desktop computers (subject to availability) totaling 8 processors at an approximate total of 16 billion cycles per second, and managed by the custom built 'HPC\_monitor' package.

#### ***4.2.5 SIMULATION MATRIX AND METRICS***

A base set of runs was conducted for each conceptual model, consisting of 2 million randomized parameter sets from the selected sample space. These initial runs were divided into parallel jobs across several processors, and then reassembled for further processing. Subsequent processing included calibration based on fitness at each data point.

Four calibration strategies were defined then tested for stochastic performance in the sparse-data water quality problem (Table 4.1). The first criterion is based on a 'deterministic-optimization' approach, while the remaining criteria used metrics designed to be advantageous in stochastic calibration. Simulations were compared on both a seasonal and annual basis at locations throughout the watershed.

As described in the next section, two calibration levels were considered in the run matrix. The first, 'base calibration' level (ARE and RMSEa) was designed to capture essentially all runs that could be considered representative at all points. A narrower surface response, more in line with typical predictive applications, was also examined (in the WRE and RMSEb calibrations).

Table 4.1. Calibration Criteria Examined

| <i>Descriptive Title</i>                          | <i>Abbreviated Title</i> |
|---------------------------------------------------|--------------------------|
| <i>Root Mean Squared Error Method</i>             | <i>(RMSE)</i>            |
| <i>Absolute Relative Error Method</i>             | <i>(ARE)</i>             |
| <i>Weighted Relative Error Method</i>             | <i>(WRE)</i>             |
| <i>Stochastic Exceedance Calibration Strategy</i> | <i>(SECS)</i>            |

#### 4.2.6 RMSE

The RMSE is calculated according to the following equation:

$$RMSE = \sqrt{\frac{\sum_{i=1}^n (c_{model_n} - c_{data_n})^2}{n}} \quad (4-2)$$

where  $c_{data_n}$  and  $c_{model_n}$  are the  $n$ th observed and simulated constituent concentration, respectively. It should be emphasized that the output for a given model run must be in hand at all space-time locations for which calibration data are available in order to calculate the RMSE.

Problems with actual use of RMSE for surface response evaluation quickly become apparent in the development of multi-objective calibration. It is well understood in a deterministic context that the RMSE is very sensitive to large values and outliers. The same problem manifests itself differently in stochastic contexts, where the inverse of the RMSE is often used as a likelihood measure to weigh model significance. In such instances, even very non-representative models may continue to influence the aggregate surface response. This issue has been raised in the literature (e.g., Beven, 2005), and was supported by preparatory analysis in this study.

In an evaluation of calibration criteria, this issue becomes particularly important, as the problem centers around identifying the surface response of multiple representative models. Therefore, in this context, the approach was to use a binary likelihood function that considers models as either acceptable (representative) or non-acceptable. Therefore, all realizations were passed through a filter that excluded all data with an ARE larger than 2.0 at any location or timeframe (considered ‘unreasonable’) prior to being considered in the RMSE analysis. The

surface response was then analyzed for the 10% of models with the lowest calculated RMSE (base calibration RMSEa) and then again for the ‘best’ 5% of all eligible models (RMSEb).

While the exclusion of models failing a basic reasonableness test may arguably make for a less pure RMSE surface examined in this analysis, the majority of excluded models will of course have RMSE values higher than the top 10% (itself a somewhat arbitrary distinction) of models in the selected region. It is the belief of the author that this decision is in line with the reasonable application of RMSE as a calibration criterion, since these extreme outliers are (and indeed, should be) in practice excluded from consideration anyways, in quite varied ways.

#### 4.2.7 ABSOLUTE RELATIVE ERROR (ARE)

The ARE calibrations was based on the absolute error relative to data, when compared with annual and seasonal averages, using the simple relation found in Equation 4-3.

$$ARE = \left| \frac{(c_{model} - c_{data})}{c_{data}} \right| \quad (4-3)$$

One challenge with specifying ARE criteria is specifying conditions that are sufficient to suggest model suitability everywhere without excluding models that may perform very well in significant locations but only moderately well in less significant locations. The structure of the ARE allows us to readily handle such constraints however. The ARE base calibration considered all models with an ARE below 0.5 for both DO and NH<sub>4</sub>, but a lesser condition of 1.0 for BOD.

#### 4.2.7 WEIGHTED RELATIVE ERROR (WRE)

The WRE criterion seeks to improve upon the ARE, and is really a special case thereof. In this calibration set, the goal was to generate a surface that may be useful for predictive modeling. As noted, a disadvantage of the ARE is that it may exclude ‘good’ models because of relatively poor performance in relatively unimportant areas. To address this, the ARE criteria can be adjusted in accordance to a desired degree of tolerance of model performance in a spatial-temporal calibration. The WRE implementation used in this analysis considered all runs that had an ARE at the outlet of 0.25 for DO and NH<sub>4</sub> and 0.5 for BOD, requirements roughly twice as stringent as those in the ‘base’ calibration. Relative error thresholds at other locations were derived in inverse relation to flow:

$$WRE_{x,y,t} = ARE_{outlet,t} \cdot \frac{Q_{outlet,t}}{Q_{x,y,t}} \quad (4-4)$$

This strategy permits model candidates that perform well at high flow ( $Q$ ) locations ( $x, y$  closer to the outlet) or periods ( $t$ ) to be deemed acceptable even with lesser performance at low flow locations.

#### 4.2.8 STOCHASTIC EXCEEDANCE CALIBRATION STRATEGY (SECS)

The SECS was conceived as an additional potential improvement on the ARE/WRE calibrations. In several applications, it is useful to be able to provide conservative calibrations that accurately predict constituents when water quality conditions become ‘poor’, at the expense of some confidence in model endpoints under ‘good’ conditions. The SECS, therefore, is a contextual calibration strategy. This type of simulation can be very useful for a variety of management issues, as well as problems considering, for example, environmental stressors on aquatic life (as in Parker, 2004). In the analysis presented here, the SECS calibration was conducted as a version of the WRE calibration that further treated parameter sets which overestimated DO (favorable to aquatic life) or underestimated  $NH_4$  (a potential stressor) as non-representative.

#### 4.2.9 SURFACE RESPONSE METRICS

The basic statistical measure used to describe the response surface in this paper is the coefficient of variation (sometimes termed relative variability), which expresses the dispersion of a data set around its mean (cf. Equation 4-5).

$$c_v = \frac{\sigma}{\mu} \quad (4-5)$$

The coefficient of variation is useful because it allows the degree of variation in several series of data to be compared, and is therefore often used to assess relative volatility or risk. In addition, an aggregate metric is also used to help summarize and present results:

$$c_{v_{agg}} = \frac{c_{v_{DO}}}{3} + \frac{c_{v_{BOD}}}{3} + \frac{c_{v_{NH_4}}}{3} \quad (4-6)$$

This metric can be thought of as an average equivalent to the coefficient of variation of the three constituents of interest considered here.

### 4.3 RESULTS

#### 4.3.1 BASE CALIBRATIONS

The study area was divided into two main branches for discussion here, with an overlapping length of reach near the outlet (as shown in Figure 4.1). As mentioned in the discussion of Equations 4-5 and 4-6, the aggregate coefficient of variation (ACV) metric is useful in comparing surface responses of each model. The ACV for the RMSEa and ARE base calibrations is presented in Figure 4.2 for both the main and secondary branch.

This plot can be seen as portraying the change in surface response throughout the reach network for each remaining set of representative models. In this way, information on the spatial change of the uncertainty ‘cloud’ of modeled water quality constituents is presented. Several interesting characteristics are suggested from this initial plot.

Both ARE and RMSEa calibrations appear to have similar responses, with a relatively steady ACV near the outlet region. Upstream of the mixing point, the simulation results in each branch diverge as the inflow of calibration data in one branch lessens, and the variation in surface response therefore ‘spreads’. The major observable difference between the two strategies in this plot is that in the RMSEa case, the main branch (with approximately 30% more flow than the secondary branch) comprises the majority of the variation upstream of the mixing point, while for the ARE calibration the opposite is true. As the two branches mix (near the 100 km mark), information (data and calibration results) flows from each upstream branch into the downstream reach. It also evident that, for these base calibrations, the RMSEa model has a smaller ACV in all locations than the ARE scenario.

The ACV is, as detailed in Equation 4-6, an aggregate metric. While useful for examining broad changes across spatial or temporal dimensions, it is also instructive to examine individual coefficients of variation at a few locations, as in Figure 4.3.

These results inform the observer of several behaviours in the calibrated model response, and illustrate some greater underlying differences between approaches. Both models have similar coefficients of variation for DO, but handle the other constituents quite differently. A predictable behaviour is the emphasis placed on large values (and the associated constituents) by the RMSEa calibration, which appears to be optimizing BOD, DO and  $\text{NH}_4$  in turn. This is seen by the fact that the  $c_v$  is lower for BOD, which suggests that all representative models are similar with respect to BOD. The ARE scenario is able to place less emphasis on the BOD parameter and seeks instead to improve DO and  $\text{NH}_4$  components. Additionally, the extremely narrow variation

in the  $\text{NH}_4$  constituents suggests the ARE model is being limited by this calibration condition, at both outlet and headwaters locations. This sort of information is useful in identifying, for example, poor data conditions, or inadequate calibration requirements for a given conceptual model.

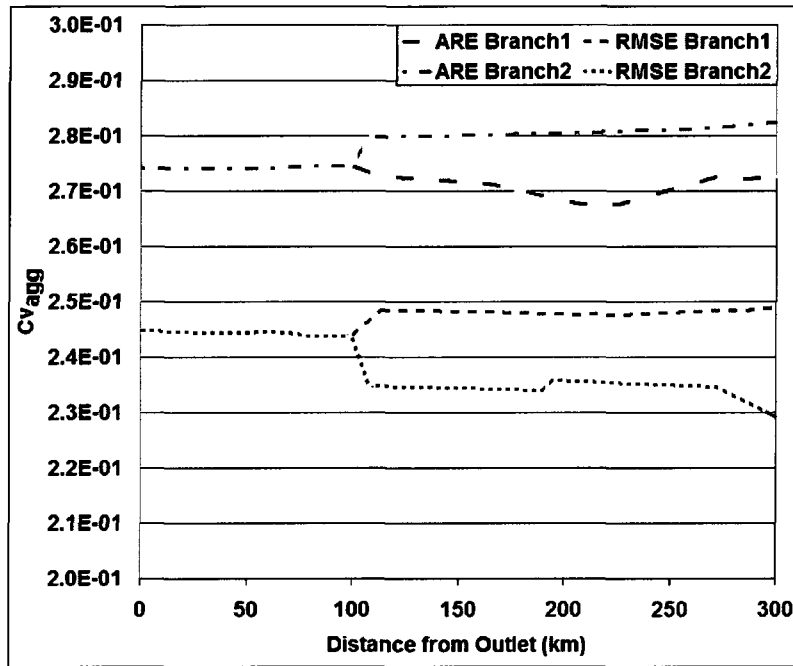


Figure 4.2: ARE and RMSEa calibration scenario ACVs versus position

The effect of the difference in emphasis on BOD can also be examined in a spatial sense, as in Figure 4.4, where the BOD component has been removed from the ACV calculation. The situation in Figure 4.2 is dramatically reversed (note the difference in scale), with the aggregate surface response for DO and  $\text{NH}_4$  comparison now performing much better in the ARE scenario.

#### 4.3.2 IMPROVED CALIBRATIONS

Secondary, tighter response surfaces were also examined, as derived from the base calibration strategies. These were the WRE and RMSEb simulations shown in Figure 4.5.

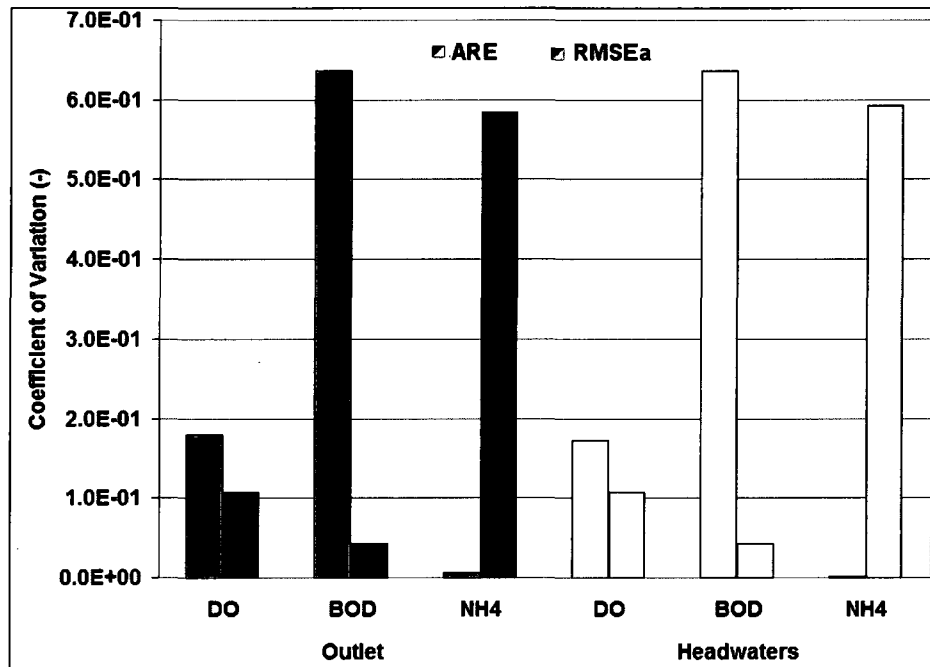


Figure 4.3: Separate CVs in ARE and RMSEa surface response

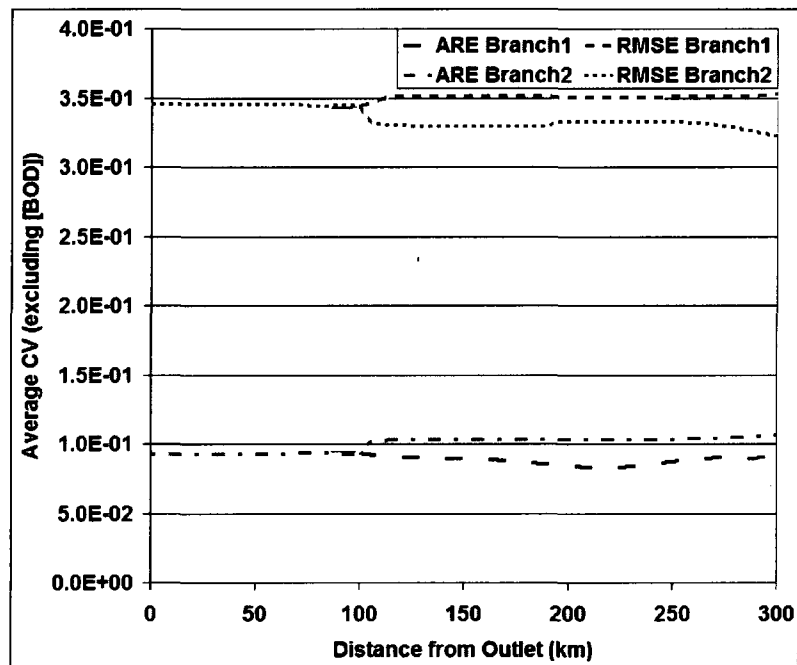


Figure 4.4: ARE and RMSEa (base) calibrated model ACVs (excluding BOD) versus position

Each result reflects a subset of the previous base calibration result sets (the ARE and RMSEa, respectively) which seeks to find a ‘high-likelihood’ calibrated parameter set yielding improved coefficients of variation. This set is illustrative of the types of calibration improvements that may be useful for management or decision making tasks, given a suitable conceptual model. The ACV change with position for the RMSEb is very similar to that of the base, RMSEa, calibration. The WRE ACV substantially outperforms not only the base ARE scenario, but also when compared to either RMSE calibration. Additionally, both branches perform approximately equally in the WRE scenario.

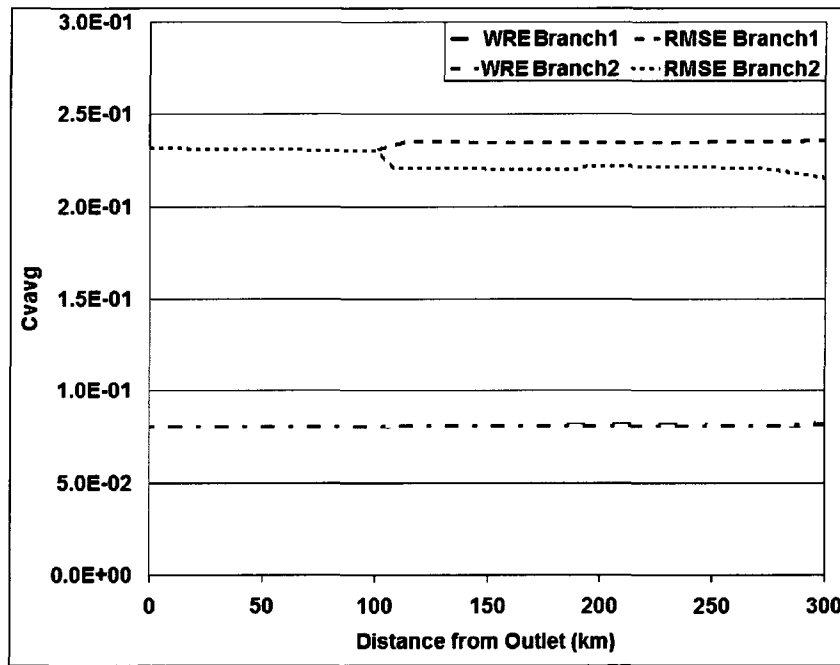


Figure 4.5: WRE and RMSE (high-fitness) calibrated model ACVs (excluding BOD) versus position

In addition to spatial response, the temporal surface response was also examined. This was accomplished by comparing water quality model simulation results from the high-likelihood set on a month-by-month basis with observed data. Results are shown as response ‘cloud’ extents and means in Figure 4.6.

While the WRE condition has indeed narrowed the model response surface dramatically, and in fact shifted the cloud considerably, the RMSEb shows little improvement over the base calibration, with only a slight narrowing. The difference in cloud shape between the ARE and WRE models, in contrast to the two RMSE cases, belie the predominant selection regions for the

added constraints. The surface from the WRE calibration matches expected behaviour, and shows higher variation in low flow regions (e.g., summer) than during high flow periods. The seasonal change in coefficient of variation components was also examined, as shown in Figure 4.7. Examination of these results reinforces the conclusion that the RMSE model has changed little, as it continues to suffer from a high  $\text{NH}_4$  component in the ACV as identified in the discussion of Figure 4.3. As before, simultaneous calibration of the relatively large DO and BOD constituents is effectively reducing the importance of the  $\text{NH}_4$  simulation. Only as the CV of the BOD increases important do improvements in the  $\text{NH}_4$  surface become apparent, indicating possible representative model selection based on  $\text{NH}_4$  simulation fitness. Conversely, the WRE model has improved considerably.

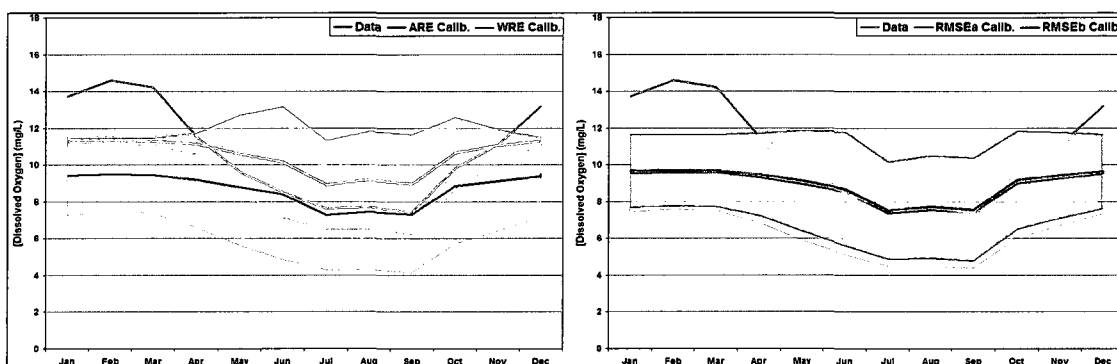


Figure 4.6: DO surface response (95%) for ARE, WRE, RMSEa and RMSEb calibrations. Solid lines indicate means of representative models.

#### 4.3.3 SECS RESULTS

The SECS calibration is a further refinement on the ARE/WRE calibrations that excludes parameters sets leading to overestimates of favorable conditions (e.g., DO) or underestimation of poor conditions (e.g.,  $\text{NH}_4$ ). Results for the latter are illustrative, and are shown in Figure 4.8.

As designed, the highlighted results in Figure 4.8 show a reduced subset of the WRE calibration which eliminates non-conservative predictions of  $\text{NH}_4$  concentrations. Perhaps more interestingly, the SECS set also excludes models from the WRE criteria that are more conservative than itself in some locations (but non-conservative in others). The resulting surface response is narrowed, near many calibration points, on both the upper and lower bounds.

#### 4.4 DISCUSSION AND CONCLUSION

The suggested methodology can be employed to examine the performance of a calibration strategy for a given conceptual model (or code). It should be emphasized that the calibration set

and resulting surface response is also a function of the conceptual model structure itself (as examined in Parker et al., 2008b), as well as the data used for calibration. Some limitations and surface characteristics (e.g., DO under-prediction in Figure 4.6) may result from the conceptual model and data conditions themselves, and be common to all valid parameter sets.

Nevertheless, several important themes and concepts are illustrated in the results presented above.

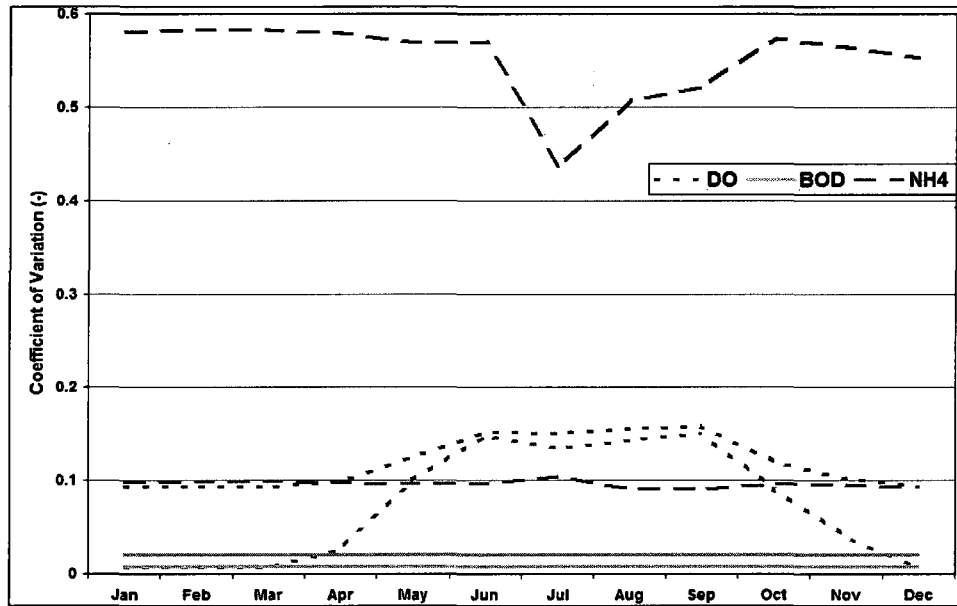


Figure 4.7: Coefficient of variation of DO, BOD and  $\text{NH}_4$  response for WRE (green) and RMSEb (blue) calibrations

#### 4.4.1 INTERPRETATION AND IMPLICATIONS

The difference in ACV between the two branches, shown in Figure 4.2, could be expected. Indeed, the water quality calibration points shown in Figure 4.1 are not distributed evenly throughout the watershed. Information from calibration points constrains the representative model set and therefore tends to narrow the uncertainty cloud in the region. Though both highlighted branches have a calibration point directly in their lengths, several tributaries of the primary branch (in the north) also pass through calibration points. In this way, additional information is ‘flowing’ (with the literal water flow) from these tributary reaches into the principal branch. This concept of information (or data) ‘flow’ is important in interpreting the subsequent model response. Interestingly, in the RMSEa calibration shown in Figure 4.2, the data-rich primary branch is contributing more uncertainty than the secondary branch for which

less data are available. This is the opposite of the behaviour observed in the ARE case, and may indicate that the RMSEa is not making as efficient use of the available data. Instead, as shown in Figure 4.4, the RMSEa appears to be focused on optimizing the largest constituents.

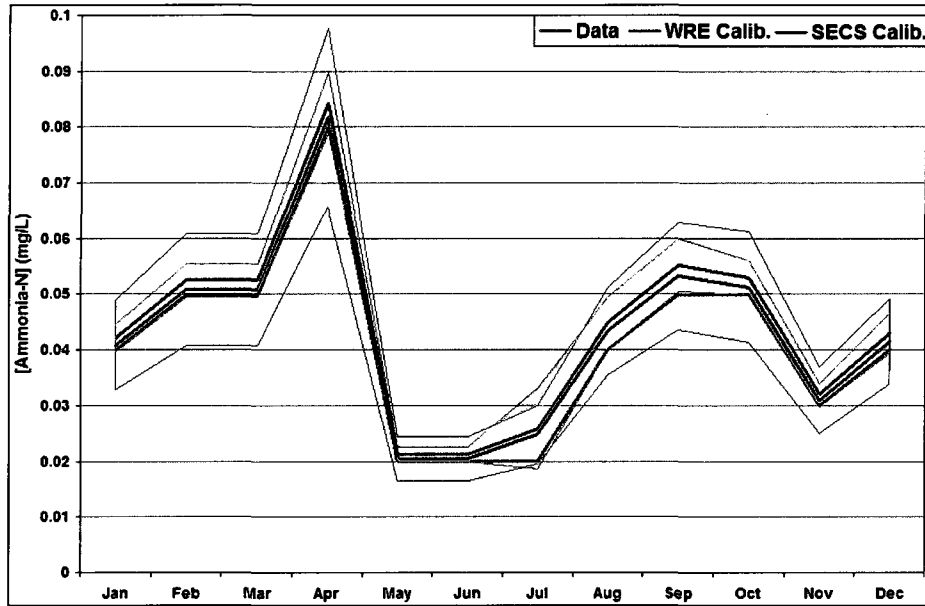


Figure 4.8: Seasonal  $\text{NH}_4$  surface response (95%) for SECS and WRE calibrations. Solid lines show mean of representative models.

This highlights one advantage of the ARE approach, which can expressly allow for a lesser confidence requirement in some variables than others. Similar results could potentially be obtained with the RMSE approach through either assigning lesser weights to such variables in the mean calculation or normalizing values. The challenge then becomes assessing the suitability of weights (or normalization strategy), and accounting for these in subsequent model interpretation.

The comparison of WRE and RMSEb results is also significant, and illustrate one disadvantage of using a metric that effectively compresses information irreversibly, such as RMSE, for stochastic calibration in several dimensions, including time, space and also constituent nature. Indeed, while the parameter set for an ARE calibration criterion of 20% will, by definition, consist of individuals that are within 20% of observed data for calibrated conditions, it is difficult, perhaps impossible, to estimate what degree of confidence can be expected in a given RMSE-calibrated parameter space at any particular location or time, or for

any constituent. This has important potential implication in predictive contexts, where it may be reasonable to assume a minimum local performance of ARE but not RMSE.

Additionally, optimization with RMSE consists of selecting candidates with a better aggregate measure. This in effect selects a subset of the previous parameter space, but this subset may not offer improvements in any tangible sense, and may be essentially identical. Additionally, the definition of ‘better’ is poorly defined in such cases, in contrast to the ARE/WRE definitions which explicitly state, and require, minimum performance at each data point. This limitation is evident even in the RMSE setup process, as some filter was needed to limit the effect of very non-representative models. If such models were not excluded, candidates with good fit to outlier or ‘highly’ weighted values (e.g., BOD) would further degrade results.

By contrast, the ARE performance can be progressively improved by refining the exclusion condition until the exclusion condition is so limiting that the number of representative candidates becomes effectively nil. This inability of the ARE to find satisfactory representative candidates is an important difference (an advantage!) when compared to the RMSE (even exceedingly poor models can be ranked based on RMSE), as it can identify conditions where available information and model structure are unsuitable to a desired confidence in prediction results, and should be revised.

The WRE is a further improvement that can be made to the ARE to address such failures, and the example deployment presented in this paper considers error weighted relative to flow as an optimization strategy for the watershed calibration, permitting relatively high prediction error in regions of low flow. This flow-based calibration is advantageous in that it still allows the calibrated model predictive requirements to be retrieved at any location and flow condition. Alternative potential weighting schemes could include precisely the inverse scheme (in some contexts, conditions during low flow may be most important), or a weight derived from data confidence (based perhaps on time-series variation, equipment or even observer records).

As discussed above (and shown in Figure 4.6), the ability of WRE optimization to select a subset based on additional requirements can lead to substantial changes in surface response when compared to the base calibration, and associated improvements in model performance. Additionally, contextual calibrations can be devised, such as that presented for the SECS scenario (Figure 4.8).

#### **4.4.2 FURTHER CONSIDERATIONS**

Several additional, practical issues in the implementation of RMSE and ARE (and related) deserve additional comment, not only in view of model construction and setup, but also in terms of model maintenance and the injection of new data points into previously calibrated models.

An important difference between the proposed calibration criteria methods is that the non-RMSE methods can be applied sequentially. As an example, for the GLUE methodology as applied here, the RMSE calibration must consider every potential ‘representative’ (i.e., the entire inverse run set) model at each location and timeframe considered. This is because the best 10 or 20% (with lowest RMSE) of the model runs are considered representative, thus all runs must be stored prior to selecting the representative set. Practically, this means that an extremely large number of runs must be conducted (although they can be done in parallel), and addition of new data or calibration conditions will always require consideration of the entire inverse run set. This, in turn, may make previously non-representative models representative.

Conversely, the ARE and related methods are applied sequentially, and progressively eliminate non-representative candidates at each calibration point and condition, based on a fixed calibration criterion. Candidates, once eliminated, are no longer considered, so the set of potential representative runs decreases as the calibration progresses. New data points need only consider the remaining candidates and can further eliminate non-representative models. In contrast to the RMSE method, the calibration process therefore accelerates as it progresses.

The ARE type methods therefore do not allow for rejected models to be redeemed by additional calibration points (though still by revised calibration points) in the same fashion as the RMSE can. As discussed previously, this allows the conditions where inadequate thresholds (too stringent or too lax) have been applied to be readily identified, which can be used to improve subsequent calibrations or identify data points which may be outliers.

#### **4.4.3 CONCLUSION**

It should be noted that the authors, despite a general belief that distinguishing between ‘good’ and ‘bad’ representative models is tenuous ground, recognize that RMSE can be appropriately used to weigh degrees of belief within a calibrated (representative) region. The key contention, illustrated by example herein, is that the RMSE is in several respects disadvantageous as the calibration criterion itself in stochastic analysis, and particularly uncertainty analysis of deterministic models through Monte Carlo simulation.

The disadvantages of the RMSE when compared with the alternatives are several-fold. First, it does not explicitly require minimum performance of candidate models with respect to any individual constituent or data point. All three of the suggested alternative calibration strategies do. Secondly, use of higher RMSE as a optimization criteria does relatively little to alter the surface response of candidate models, particularly when compared with strategies such as the WRE (or SECS) which can shape the relative model performance around points (or for applications) of particular interest as needed. Both the base and high fitness RMSE surfaces yielded predictive surfaces with very little improvement over the base ARE surface.

Further problems are involved in model use and interpretation. RMSE does not explicitly models, and can redeem even very bad ones. In contrast, the alternative strategies require the modeler to define minimum performance levels for representative models. RMSE also poses substantial limitations for simulation result interpretation in space and time, due to its compression of data series into a single metric.

A common theme that emerges from the discussion here is the importance in understanding the interaction of data, model structure and calibration criteria in determining suitable parameter sets and associated response characteristics for a given problem. Defining the surface response of calibrated models can yield important information on stochastic model performance in time and space. The findings and type of analysis illustrated have ramifications for the development of data sampling schemes and interpretation as well as calibration itself.

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## CHAPTER 5

### MODEL STRUCTURE AND UNCERTAINTY FOR STOCHASTIC NON-POINT SOURCE MODELING APPLICATIONS

#### 5.0 CHAPTER OVERVIEW

This chapter has been submitted for publication in the *Journal of Hydrology*.

#### ***ABSTRACT***

The uncertainty associated with a rainfall runoff and non-point source loading (NPS) model can be attributed to both the parameterization and model structure. An interesting implication of the areal nature of NPS models is the direct relationship between model structure (i.e., subwatershed size) and sample size for the parameterization of spatial data.

The approach of this research is to find structural limitations in scale for the use of the conceptual NPS model, then examine the scales at which suitable stochastic depictions of key parameter sets can be generated. The overlapping regions are optimal (and possibly the only suitable regions) for conducting meaningful stochastic analysis with a given NPS model.

Previous work has sought to find optimal scales for deterministic analysis (where, in fact, calibration can be adjusted to compensate for sub-optimal scale selection); however, analysis of stochastic suitability and uncertainty associated with both the conceptual model and the parameter set, as presented here, is novel; as is the strategy of delineating a watershed based on the uncertainty distribution

The results of this paper demonstrate a narrow range of acceptable model structure for stochastic analysis in the chosen NPS model. In the case examined, the uncertainties associated with parameterization and parameter sensitivity are shown to be outweighed in significance by those resulting from structural and conceptual decisions.

Listed index terms were: Hydrology, Modeling, Model calibration, Stochastic Hydrology, Watershed. Listed keywords were: Runoff, Model, Non-Point Source, Stochastic, Uncertainty, and TMDL.

## 5.1 INTRODUCTION

### 5.1.1 BACKGROUND

Watershed-level modeling has become an essential tool in understanding and managing environmental risks and the relationship between pollutant sources and water bodies. An approved Total Maximum Daily Loading (TMDL) evaluation, for instance, has become a de facto requisite for assistance funding in many locales. Particularly in recent years, an increased focus has been placed upon the issues of both point and non-point pollutant sources at the watershed level. Pollutant loading and hydrology models are deployed in such cases to provide insight on source assessments and their impacts on water quality targets, as well as the consequences of varied management scenarios (e.g., Parker et al., 2008).

These types of assessments have proven to be challenging, particularly in moderately complex to complex systems, where model parameters are adjusted to fit one or several years of reference data. It is well understood for deterministic models that the chosen ‘calibrated’ parameter set, and thus simulation results, depend on some combination of the reference data and calibration strategy (criteria) chosen. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

Stochastic models attempt to mitigate such issues to some degree by representing modeled phenomena as a distribution of possible outcomes. A common implementation is to perturb input parameters, through use of Monte-Carlo simulations for example, and assess likely outcomes from the results. One advantage of such approaches is that they are readily implemented late in the (otherwise deterministic) model construction timeline, as an added tool for result interpretation.

Equally important to the stochastic model response, however, is the underlying conceptual model structure itself. In practice, this issue is rarely explicitly considered, as a handful of codes, primarily designed for deterministic simulation, are in widespread use.

This paper outlines a method to find limitations in scale for use of a given conceptual model, and then examine the scales at which a suitable stochastic representation of key parameter sets can be obtained. The overlapping regions are optimal, and possibly the only suitable regions, for meaningful stochastic analysis given a non-point source pollutant loading (NPS) model.

### 5.1.2 REVIEW OF UNCERTAINTY AND SCALE

Most hydrologic models employ point-scale equations based on conservation of mass, momentum, and energy. Often, such computations require data at a scale much finer than is readily available. In such cases, the point-scale equations must be up-scaled in order to conserve mass, momentum, and energy, ensuring compatibility between scales of observed data and governing equations. Therefore, the spatial scale must greatly influence the choice of a model (and vice-versa).

Seyfried and Wilcox (1995) analyzed how the nature of spatial variability affects the hydrological response of a catchment over a range of scales, using several field processes as examples. Kavvas (1999) showed that when larger scale processes are formed by the averaging of small-scale processes, high frequency components of the smaller scale are effectively eliminated, leading to considerable simplification of hydrologic conservation equations. This up-scaling also plays an important role in dealing with those parameters which also vary spatially (e.g., Chen et al. 1994, Kavvas, 1998). Model parameters are usually based on spatial variation of point-scale data (or parameters mapped to such data) obtained using GIS, remote sensing and other tools.

Previous work, focused on identifying the finest scale that can be used to adequately represent spatial variation in a hydrological model. Bathurst (1986) suggested dividing the watershed into elements no larger than 1% of the total area, to ensure that each element was more or less homogeneous; Wood et al. (1988) proposed the notion of a representative elementary area (REA); and several others have examined this issue. Wood et al. (1988) defined the REA as the 'smallest discernible point which is representative of the continuum'. This suggests preferable temporal and spatial scales over which process representation can remain simple, and distributed catchment behaviour represented without the complexity of local heterogeneity. The concept is analogous to the representative elemental volume concept of Hubbert (1956). Blösch et al. (1995) reasoned it is difficult, in practice, to determine the REA because it is strongly controlled by environmental characteristics. Zhang and Montgomery (1994) concluded that grid sizes smaller than the hill-slope length are necessary to adequately simulate the processes controlled by land forms, while Molnar and Julien (2000) found that coarser (0.835 vs. 0.016 km<sup>2</sup>) grid-cell resolutions can be used for runoff simulations so long as parameters are appropriately calibrated, and they suggested the primary effect of increasing grid-cell size on simulation parameters is to require an increase in overland and channel roughness parameters.

The methodology presented here aims to assess the relative importance of the uncertainty associated with both scale and parameter issues in hydrological models used for non-point source pollutant loading applications.

## 5.2 METHODOLOGY

### 5.2.1 CASE STUDY AREA & DATA

The Potomac Watershed stretches across approximately 38 000 km<sup>2</sup>, of the Eastern US. The Potomac River itself covers roughly 620 km from Fairfax Stone in West Virginia to Point Lookout in Maryland. The average river flow at the Washington, D.C location is about 310 m<sup>3</sup>/s, with minimum and maximum recorded flows of 17 m<sup>3</sup>/s (September 1966) and 12000 m<sup>3</sup>/s (March 1936), respectively. The watershed flows into Chesapeake Bay, becoming tidal near Washington DC where the river crosses the fall line into the Coastal Plain province. This study limits itself to the purely freshwater and non-tidal portion of the Potomac River.

From 1991 to 1996, the US Geological Survey's (USGS) National Water Quality Assessment (NAWQA) program began extensive work in the basin to monitor surface and ground water quality and ecology. That dataset is used here, drawing on over 50 USGS stations to provide information on stream flow quantity for the year 1993. These data were available at temporal resolutions up to daily timesteps for individual stations. Water quality data are available at 5 'integrator' and 5 'indicator' stations on a monthly basis. Point sources loading the river system were identified from US EPA (2007).

Simulations in this paper were conducted using the continuous-simulation Annualized Agricultural NPS pollutant loading model, developed by the US Department of Agriculture (USDA). AnnAGNPS is a comprehensive package, particularly suited for analyzing non-point source pollutant loading issues at the watershed level. Conceptually, the model subdivides a watershed into homogeneous drainage areas, which are in turn connected by a dendritic reach system. Water and pollutant loadings from individual fields are simulated as runoff events from rainfall, snowmelt, and irrigation data (NPS modeling). Soil loss is calculated based on the Revised Universal Soil Loss Equation (RUSLE). The model also includes a substantial database with values of parameters for agricultural applications and management scenarios (cf. Bosh et al., 1998).

### 5.2.2 MODEL STRUCTURE SCALING

The initial step in the proposed approach is the determination of scales at which the hydrological and NPS model behave adequately for stochastic analysis. The goal of this stage is to identify a range of model delineation (lumped area and reach networks) which will permit Monte Carlo analysis around a given conceptual model and related parameter set.

The approach used in this paper was to conduct a sensitivity analysis of conceptual model stability at scales between 0.25-15.5 km<sup>2</sup>. As the model delineation is also governed by the site topography, the analysis was performed on three sub-watersheds, described in Table 5.1, to isolate conceptual model issues over a plausible range of model structures.

Table 5.1 Subarea Characteristics

| <i>Watershed Case</i> | <i>Drainage Area<br/>(km<sup>2</sup>)</i> | <i>Scales Examined<br/>(avg. area, in km<sup>2</sup>)</i> | <i>Subdivision<br/>Count</i> | <i>Run<br/>Count</i> |
|-----------------------|-------------------------------------------|-----------------------------------------------------------|------------------------------|----------------------|
| 1                     | 1210                                      | 0.3-15.5                                                  | 78-4727                      | 12                   |
| 2                     | 525                                       | 0.3-10.9                                                  | 48-1992                      | 13                   |
| 3                     | 312                                       | 0.3-13.6                                                  | 23-1191                      | 16                   |

The model runs were populated with identical, grossly averaged, soil and land-use conditions in each case and the results were examined for changes in runoff volume and sediment transport. Any differences between model outputs, therefore, are products of the union between the discretization and conceptual structure of the model.

### 5.2.3 MODEL PARAMETER SCALING

With a range of suitable scales for the conceptual model determined, the task now becomes to find the discretization that leads to suitable parameter representation in the same range. In deterministic analysis, parameters (reflecting, for example, land use) are represented as single values. The discretization problem in such instances therefore often seeks to find the degree of 'lumping' (scale) at which a single value, often a weighted average, can be considered representative.

In a stochastic setting, the problem is slightly different. Parameters, in this context, must be considered as distributions of plausible values rather than point values. Therefore, in such cases, we are most interested in determining the scale which allows for a suitable distribution to be fitted to spatial data. In these instances, issues of sampling size and delineation are of increased importance.

A simple conceptual model for examining the effect of spatial parameters on model runoff-related outputs is the rational equation, which can be used to compute the amount of runoff expected for a given area and precipitation. The equation can be formulated as follows:

$$Q = C' \cdot I \cdot A \quad (5-1)$$

Where  $Q$  is the peak runoff rate in ( $\text{m}^3/\text{s}$ ),  $I$  is the rainfall intensity ( $\text{mm/hr}$ ) and  $A$  is the drainage area in  $\text{km}^2$ .  $C$  is a parameter reflecting the runoff coefficient, based on a weighted average of recommended values for soil type and land use conditions, in a discrete region. In Equation 1,  $C'$  is the modified runoff coefficient for use with these units, which is the nominal runoff coefficient multiplied by a factor of 0.28. Nominal runoff coefficients are estimated from literature values (e.g., McCuen, 2004).

Another simple and widely used equation is the Soil Conservation Service (SCS) Curve Number (CN) method. In this formulation, the runoff is a function of both the CN (which is related to the potential maximum retention after runoff begins), the initial abstractions (which is often taken as function of CN), and the rainfall itself. Practically, this can be considered a special case of the rational equation where  $C$  is variable with precipitation for a given CN.

Despite the prevalence of CN methods in parametric models, there are several advantages of using a constant runoff coefficient at a given location (raster pixels) for statistical description and aggregation of runoff characteristics within a given subcatchment. Such an approach approximates, from a single spatial variable, an expected hydrological behaviour useful for a range of climate conditions over the course of a year. Table 5.2 lists the runoff coefficients mapping to Landsat land class used in the analysis below. The approach used here was to examine the spatial variation of these mapped runoff coefficient values and the effect of scale and structure changes on distribution and sampling issues.

Several statistics were calculated via a geospatial information system (GIS) for each discretized area. Primary statistics considered were raster cell count ( $n$ ), mean of  $C$  ( $\mu$ ), standard deviation of  $C$  ( $\sigma$ ), minimum and maximum values of  $C$  (along with range), area and length. Based on these primary statistics, tabular calculations for each cell were conducted to generate descriptive statistics for comparison. Two of these are discussed here, the confidence interval ( $CI$ ) and the fractional uncertainty ( $Uf$ ). These descriptive statistics are defined in Equations (5-2) and (5-3).

Where  $\alpha$  is the level of significance,  $Z_{0.5\alpha}$  is the abscissa under the standard normal curve that contains  $0.5\alpha$  area on either side, (2.58 for an  $\alpha$  of 0.01), and  $CI_\alpha$  is the value such that the confidence interval is  $\mu \pm CI_\alpha$ . Several levels of significance were examined, with similar patterns observed. For clarity, the remainder of this paper discusses a value of  $\alpha$  of 0.01 when discussing confidence intervals and fractional uncertainties

Table 5.2 Landsat Description and Assigned Runoff Coefficient

| Land | Land Class Description               | Runoff |
|------|--------------------------------------|--------|
| 11   | Open Water                           | 100    |
| 12   | Perennial Ice Snow                   | 100    |
| 22   | High Intensity Residential           | 60     |
| 23   | Commercial/Industrial/Transportation | 60     |
| 82   | Row Crops                            | 60     |
| 31   | Barren Rock/Sand/Clay                | 50     |
| 32   | Quarries/Strip Mines/Gravel Pits     | 50     |
| 21   | Low Intensity Residential            | 40     |
| 71   | Grasslands/Herbaceous                | 35     |
| 84   | Fallow                               | 35     |
| 83   | Small Grains                         | 31     |
| 33   | Transitional                         | 30     |
| 51   | Shrubland                            | 30     |
| 91   | Woody Wetlands                       | 30     |
| 92   | Emergent Herbaceous Wetlands         | 30     |
| 81   | Pasture/Hay                          | 20     |
| 85   | Urban/Recreational Grasses           | 20     |
| 41   | Deciduous Forest                     | 13     |
| 42   | Evergreen Forest                     | 13     |
| 43   | Mixed Forest                         | 13     |
| 61   | Orchards/Vineyards/Other             | 13     |

$$CI_{\alpha} = \frac{Z_{\alpha/2} \sigma}{\sqrt{n}} \quad (5-2)$$

(confidence interval is  $\mu \pm CI_{\alpha}$ ; for  $\alpha = 0.01$ ,  $Z = 2.58$ )

$$U_f = \frac{CI_{\alpha}}{\mu} \quad (5-3)$$

### 5.3 RESULTS

#### 5.3.1 CONCEPTUAL MODEL AND STRUCTURE SCALING

The tests for conceptual and structural model issues of the AnnAGNPS representation were conducted in three subwatersheds by varying critical source area and minimum source channel length parameters in the topographic parameterization process. Figure 5.1 shows the annual average sediment yield for the tested regions in a range of scale discretizations. Sediment yield was selected as the important model output as it is related to both overall flow volume and erosion of particulate matter into the riverine system. For NPS pollutant modeling application, of the type frequently studied using AnnAGNPS, it is precisely these mechanisms of particular interest when considering transport of dissolved and attached chemicals (nutrients).

As expected, it is apparent that there is noticeable sensitivity to scale in the watershed sediment yield response. In the lower range of average cell area (more discretized structure), the model response appears to be as significantly altered by structure as by the explicit ‘parameter’ set or topography itself, with nearly a 500% increase in the 0.25-4 km<sup>2</sup> range for all cases. The results were normalized to the 4 km<sup>2</sup> value from Figure 5.1 for additional analysis, as shown in Figure 5.2.

Figure 5.2 shows a region of model stability for a range of discretizations for the considered subwatersheds throughout the study area, bordered on either extreme by regions of greater divergence. To characterize the behaviour of the watershed (and subwatersheds) as a whole, the information can also be presented as a single ‘stability’ curve, as shown in Figure 5.3.

Figure 5.3 provides a measure of the conceptual model sensitivity to model discretization (structure) in the study area (and subregions thereof).

Results from the parameter scaling tests were derived primarily from spatial distributions of input data, as outlined in the methodology section.

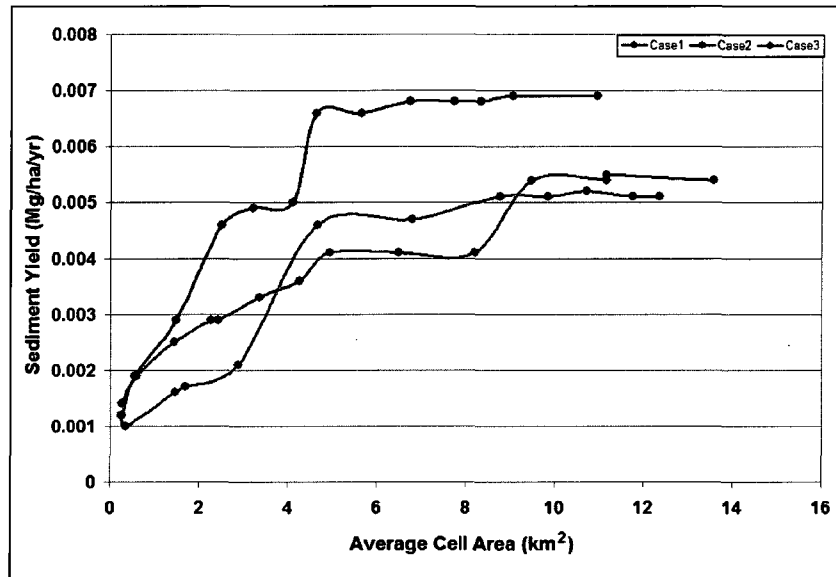


Figure 5.1: Average annual sediment yield variation with scale.

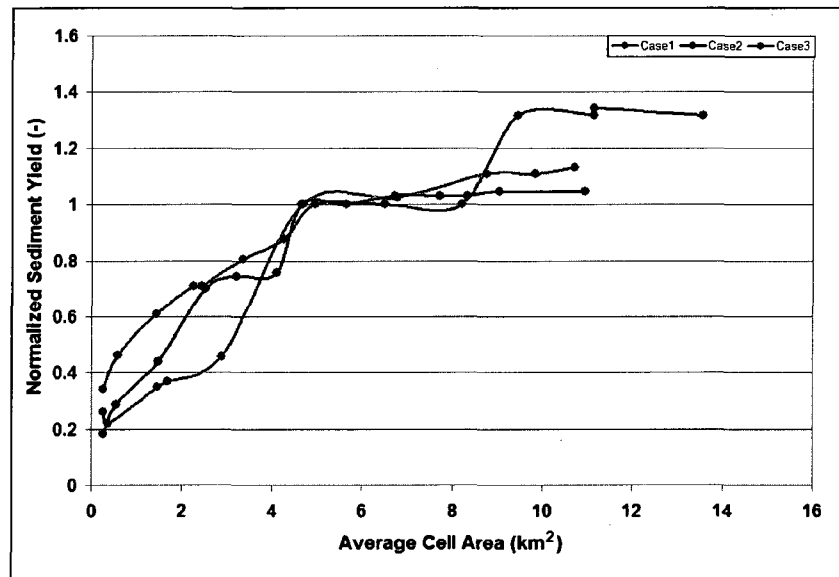


Figure 5.2: Normalized average annual sediment yield variation with scale.

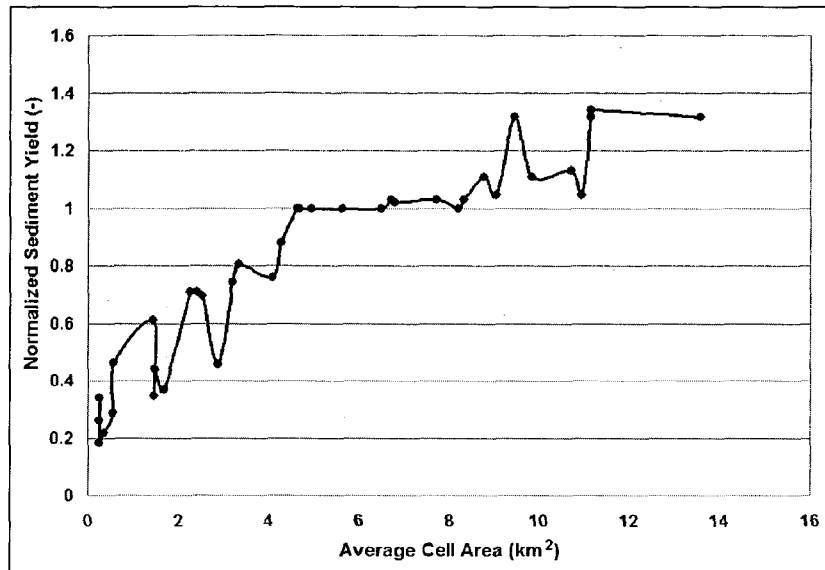


Figure 5.3: Sediment stability curve generated from normalized data in Figure 5.3.

Table 5.3 lists the results of the parameter scaling for 9 different discretizations (one per row) of the entire study area across 6 columns containing descriptive summary statistics. The first column lists the average cell area for each discretization, which is fairly straightforward. The second column lists the percentage of the total study area that is contained in cells with a raster count lower than 30 (and may be under sampled). As the average cell size increases, the number of relatively small cells becomes smaller. The third column shows the average of  $CI_{0.01}$  as defined in Equation 5-2. The fourth column shows the same value, corrected this time for the added uncertainty of increasing borders between individual subareas. As the number of cells increases, so do the relative contribution of border cells (which may be split). This was also considered with a conservative calculation based on adjacent cell means. The fifth column, like the second, provides a measure of problematic subregions, by counting the number of cells with a  $CI_{0.01}$  greater than an arbitrary cutoff value of 5. The final two columns list the percentage of overall watershed area in high  $CI_{0.01}$  regions, relative to the average listed. As shown in Figure 5.5 these cells are, for the most part, high uncertainty areas constrained by topography and network connectivity.

Table 5.3 Descriptive Statistics of Parametric Variation in Study Area

| Avg. Cell Size (km <sup>2</sup> ) | Percent Area with $n < 30$ | Avg $CI_{0.01}$ | Avg. $CI_{0.01}$ Corrected | $CI_{0.01} > 5$ | $CI_{0.01} > \text{Avg } CI_{0.01}$ (Corrected) | $CI_{0.01} > \text{Avg } CI_{0.01}^2$ (Corrected) |
|-----------------------------------|----------------------------|-----------------|----------------------------|-----------------|-------------------------------------------------|---------------------------------------------------|
| 2.25                              | 0.471%                     | 2.30            | 2.41                       | 1580            | 6.18%                                           | 0.93%                                             |
| 3.03                              | 0.259%                     | 2.10            | 2.19                       | 986             | 10.37%                                          | 1.65%                                             |
| 3.81                              | 0.178%                     | 1.97            | 2.06                       | 697             | 8.68%                                           | 1.41%                                             |
| 4.66                              | 0.120%                     | 1.86            | 1.94                       | 516             | 7.62%                                           | 1.32%                                             |
| 6.53                              | 0.071%                     | 1.69            | 1.76                       | 313             | 6.52%                                           | 1.13%                                             |
| 8.29                              | 0.041%                     | 1.60            | 1.67                       | 235             | 5.46%                                           | 0.99%                                             |
| 10.2                              | 0.030%                     | 1.50            | 1.55                       | 174             | 5.26%                                           | 0.88%                                             |
| 15                                | 0.027%                     | 1.43            | 1.48                       | 121             | 3.50%                                           | 0.57%                                             |
| 42                                | 0.001%                     | 0.85            | 0.89                       | 15              | 3.94%                                           | 0.79%                                             |

Figure 5.4 is related to Table 5.3, and shows the change in fractional parameter uncertainty for the examined discretization scenarios., as described in Equation 5-3, based on a calculation of the  $CI_{0.01}$  and the mean for each cell area. The ‘no correction’ and ‘corrected’ values are straightforward calculations based on the results of Table 5.3 across individual cells. The ‘theoretical’ plot is a similar calculation, done based on a  $CI_{0.01}$  value calculated from average  $n$ ,  $\mu$  and  $\sigma$  for a given discretization.,

## 5.4 CASE STUDY

### 5.4.1 SCALE SELECTION

Based on the parameter and conceptual/structural uncertainty tests, a scale in the range of no less than 4 km<sup>2</sup> and not more than 8.5 km<sup>2</sup> average cell area was selected. While it may be argued that a greater average cell area would allow for lesser purely input parameter-related error, the structural uncertainty issues were identified as particularly important outside this range (see Figure 5.3). Additionally, although input parameter uncertainty does decrease at higher scales, the region between about 5-15 km<sup>2</sup> ( $CI_{0.01}$  change of 0.43 over ~10 km<sup>2</sup>) is considerably flatter than at scales in the 0-5 km<sup>2</sup> ( $CI_{0.01}$  change of 0.44 over just ~2.5km<sup>2</sup>). Ideally of course, the optimal structural region should overlap a range of scales where optimal parameterization

may occur, but as discussed previously, the selected model showed only a relatively narrow region of structural stability. Several alternatives for discretization within this range were considered and tested for parameter uncertainty using descriptive statistics such as CI, including several attempts at zonal discretization based on regional variations in fractional uncertainty. Discretization is based on two principal variables: the minimum source channel length (MSCL) and the critical source area (CSA). The CSA is defined as the minimum area required to support a permanent channel, while the MSCL is a threshold below which first-order channels are not generated in the delineation process. Figure 5.5 shows some of the parametric uncertainty 'hotspots' for a representative discretization.

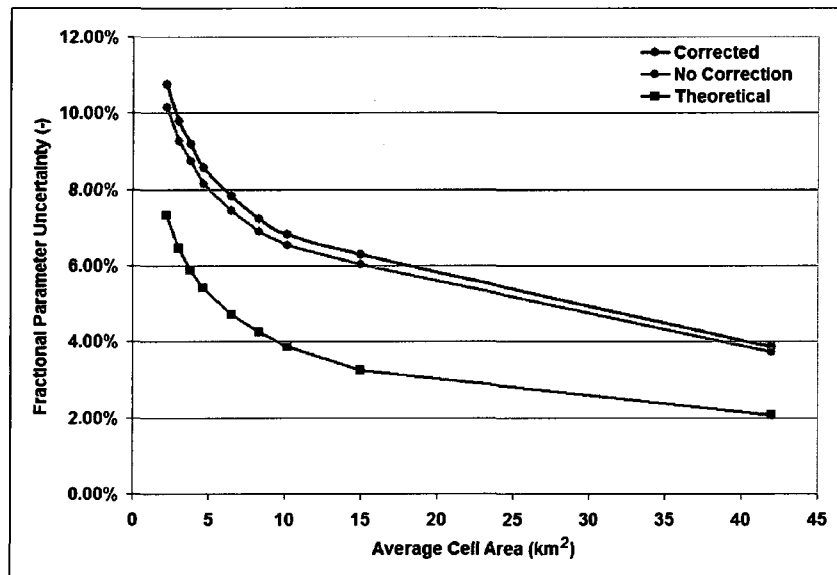


Figure 5.4: Fractional Parameter Uncertainty Change with respect to Discretization.

Spatial varied MSCL and CSA (first larger, then lower by a factor of 2) were tested in these regions in an attempt to force the discretization into larger aggregates (potentially reducing, or outright eliminating, areas of high parameter uncertainty). No substantial difference was found from the spatially varying MSCL or CSA in these high uncertainty areas, even when adding sizeable buffer zones (of up to 10 km). This was interpreted as confirming physical (topographic) limitations forcing the D8 (delineation) and subsequent parameterization algorithms into high uncertainty conditions around certain reach network junctures and edges. In other cases, where topography may not be limiting, this approach could be used to find further improvements to the parameter discretization strategy.

The final run selected had an average area of 8.3 km<sup>2</sup>, based on a constant MSCL of 1000 m and a CSA of 1000 hectares.

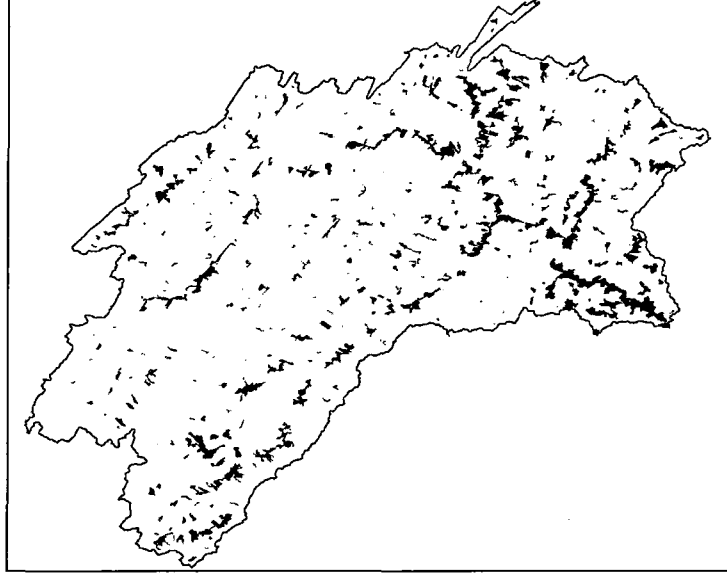


Figure 5.5: High parameter-uncertainty areas in the 6.5 km<sup>2</sup> delineation case. Areas shown in orange are areas with 99% CI greater than average.

#### 5.4.2 BASEFLOW SEPARATION

Data for flows were taken from the USGS Surface-Water Daily Data Set for the study period (USGS, 2007). Hydrograph separation was done using the Chapman filter equation, as implemented in the ABSCAN software (Parker, 2006). Digital filter techniques, originally used in signal analysis, were employed in a water resources context by Lyne and Hollick (1979) to separate high frequency (direct runoff) and low frequency (baseflow) components from the streamflow ‘signal’. Chapman (1991) noted that the Lyne–Hollick algorithm incorrectly provides a constant streamflow  $Q$ , or baseflow  $b$ , when direct runoff has ceased and therefore developed the new equation:

$$b_t = \frac{3\alpha - 1}{3 - \alpha} \cdot b_{t-1} + \frac{1 - \alpha}{3 - \alpha} \cdot (Q_t + Q_{t-1}) \quad (5-4)$$

which can calculate  $b$  at each timestep  $t$  given the associated  $Q$ . When the quick runoff component has ceased, the filter parameter  $\alpha$  becomes the hydrological recession constant  $a$  in equation (5-5), commonly used to describe baseflow recession during dry weather periods without groundwater recharge:

$$b_k = ab_k - 1 \quad (5-5)$$

The Chapman method was selected as it offered good performance with a single conceptually-based parameter,  $\alpha$ . Values for  $\alpha$  were estimated from historical records near the outlet of the study area, taken from Sinclair and Pitz (1999). A value of  $\alpha=0.5$  was used in the model separation.

#### 5.4.3 CALIBRATION

Given the nature of hydrological models, particularly for a watershed of this size and scope, additional adjustments are often necessary on a regional scale to reproduce individual events and/or patterns. Nonetheless, since the object here was to demonstrate the stochastic behaviour of a given calibration, a gross calibration with a higher degree of reproducibility across delineation cases was deemed preferable to a more stringent calibration with lower reproducibility. Therefore, the calibration task was simplified to the adjustment of two key hydrological parameters, specifically the runoff CN and storm distribution type, as well as two erosive parameters: the long term random roughness coefficient along with the sheet and concentrated flow roughness coefficient. Calibrated values for CN are shown in Table 4. The calibrated storm distribution type was adjusted to type III, the random roughness coefficient was held at 64 mm, and the sheet/concentrated flow roughness coefficient was set to  $0.13 \text{ m}^{-1/3}\cdot\text{s}$ .

Table 5.4: Calibrated CN Values for AnnAGNPS

| <i>Landuse Class</i> | <i>Hydrological Soil Group</i> |          |          |          |
|----------------------|--------------------------------|----------|----------|----------|
|                      | <i>A</i>                       | <i>B</i> | <i>C</i> | <i>D</i> |
| <i>Forest</i>        | 68                             | 70       | 72       | 73       |
| <i>Pasture</i>       | 74                             | 78       | 81       | 83       |
| <i>Rangeland</i>     | 74                             | 78       | 81       | 83       |
| <i>Crop</i>          | 79                             | 88       | 88       | 96       |
| <i>Urban</i>         | 89                             | 95       | 96       | 99       |

This simplified calibration strategy yielded nearly identical outlet discharge values in the stable structural model range examined. The 10 and 8 km<sup>2</sup> model structures had flow correlation coefficients greater than 99.99% and a RMSE of 3.12 m<sup>3</sup>/s. The corresponding sediment correlation coefficient was virtually identical, though with a higher RMSE of 169 Mg. Dynamic sediment yields at the watershed outlet were not computable using higher resolutions than 8 km<sup>2</sup>, due to array errors. Figure 5.6 shows the calibrated model values when compared with observed data for 1993.

Though the calibrated simulation results shown in Figure 5.6 do reproduce overall seasonal patterns reasonably well, it has some less-than-ideal properties as well. The model slightly under- and over-predicts observed values in many places, but perhaps more importantly appears somewhat jumpy. This may be attributable to one of several factors, ranging from choice of baseflow model to very localized precipitation events or hydrology that are misrepresented in the climate records or landuse data, respectively. Normally such characteristics could be improved upon by further calibration by e.g., localized adjustment of parameters; however, the requirement for the analysis here is not so much for a perfect calibration as for a highly reproducible, relatively stable one.

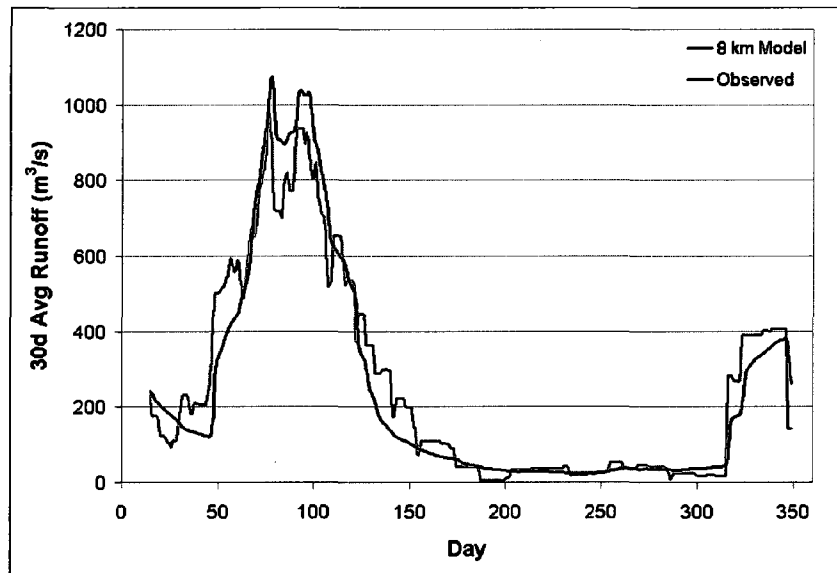


Figure 5.6: Model Calibration results. Plot indicates discharge at outlet.

#### 5.4.4 SIMULATION RESULTS AND COMPARISON

Given that model structures outside the 'stable' region identified in Figure 5.3 had previously shown heightened sensitivity to changes in cell area, a sub-region of the initial calibrated watershed (corresponding to the Shenandoah River branch) was examined for each scale. Figure 5.7 shows the annual distribution of sediment loadings for the watershed examined. In this Figure, annual total sediment yield increases (along the y-axis) as time progresses (along the x-axis). The sediment yield of large discretizations is consistently higher than lower ones, though structures in the 4-10 km<sup>2</sup>, and particularly the 6-10 km<sup>2</sup> ranges seem to yield largely similar total annual loads.

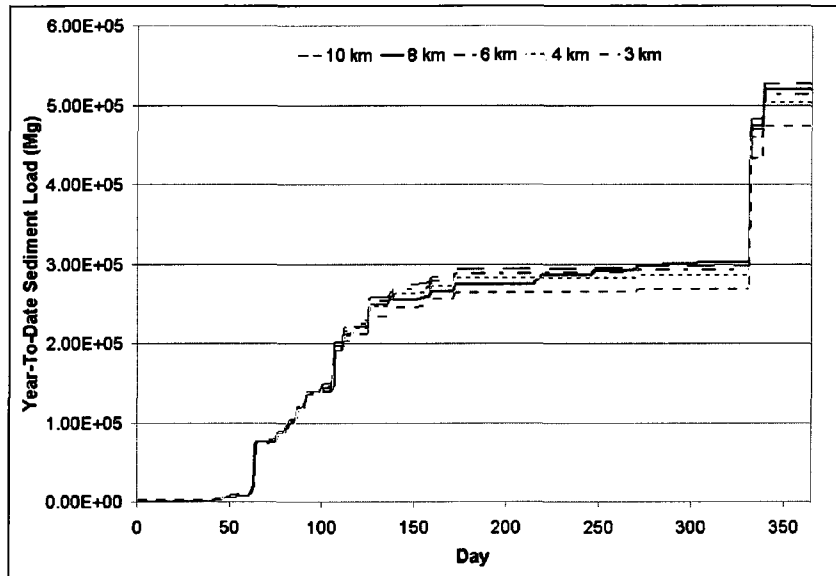


Figure 5.7: Simulated Sediment loadings at Shenandoah Sub-Basin Outlet

The 3 km<sup>2</sup> discretization (outside the stable range), in contrast, shows a more significant decrease in annual sediment yield when compared with the others. This result illustrates one implication of the findings from Figure 5.3. Models calibrated at the outlet will show increased changes in subwatersheds outside the stable model structure scales.

In addition, a sensitivity test was conducted on one of the erosive parameters (relative roughness), which does not directly affect cell area, by testing 'random roughness' parameter values of 32 and 96 mm (50 and 150% of base, respectively). The resulting response areas were compared for each model scale. Figure 5.8 shows the surface response area of the 8 km<sup>2</sup> model, along with the upper and lower limits of the 10 and 3 km<sup>2</sup> models. The 8 km<sup>2</sup> surface is clearly narrower (lower difference between upper and lower limits) than either the 10 or 3 km<sup>2</sup> model, which both show higher sensitivities to changes in the random roughness parameter.

## 5.5 DISCUSSION

The proposed method was able to identify structural characteristics important in understanding model performance. A range of optimal scales for model construction was determined, and the case study illustrated that discretization at those optimal scales performed in a more robust manner. The predictions of optimally-structured models were less sensitive to structural (e.g., subarea) variations important in model calibration over large areas. Equally, the optimal model showed reduced sensitivity to changes in non-structural parameters. In the context

of a Monte-Carlo type approach to uncertainty analysis, the resulting differences (dispersion) in model outputs appear to have been minimized.

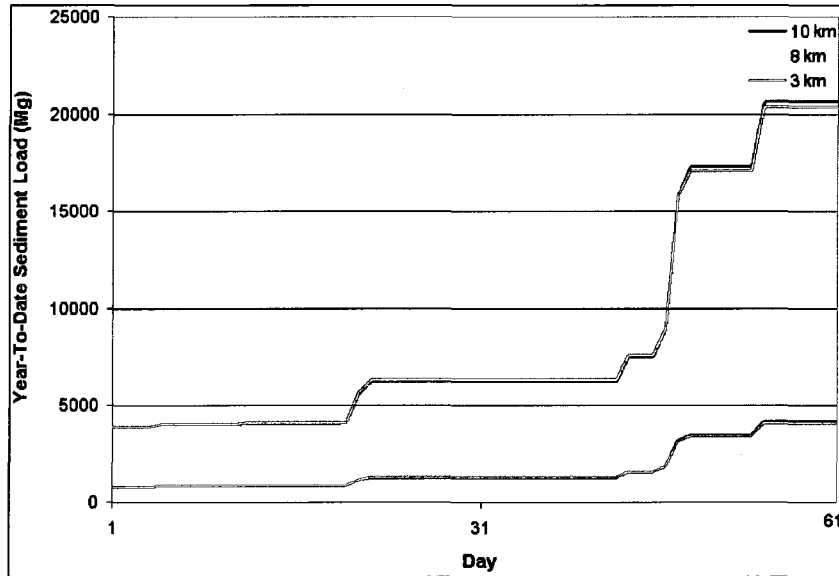


Figure 5.8: Influence of model scale on sediment loading at Shenandoah Sub-Basin Outlet surface response for variation in random roughness parameter between 32 and 96 mm.

The proposed analysis also proved generally useful for interpretation of a given conceptual model. It seems clear from the results presented that scale selection in the AnnAGNPS model is limited by conceptual model uncertainty and stability issues rather than parameter uncertainty, which is more commonly used. To further examine this issue, Figure 5.9 presents an analysis of parameter and scale uncertainty components as observed during the case study.

To generate Figure 5.9, the calibrated model was allowed to vary a sensitive parameter (random roughness) and scale by 25% around the 'optimal' 8 km<sup>2</sup> model, resulting in a case matrix of 9 runs (3 different parameter values at 3 different scales). Absolute relative error (ARE) was examined between minima and maxima at each timestep. It is evident in this plot that the analysis of parameter sensitivity alone is capturing only about half of the variation in simulation results. A related issue is how parameter uncertainty is affected by scale itself. Results from the case study, such as those shown in Figure 5.8 indicate that the 8 km<sup>2</sup> model is minimizing model sensitivity to both structural and parameter changes when compared with values outside the optimal range.

## 5.6 CONCLUSION

The methodology presented here allows for a reasonable stochastic analysis of pollutant loading problems given a deterministic-based code. The proposed methodology involves testing of conceptual model scale issues, followed by testing of parameter-related scaling issues, and subsequent determination of suitable (optimal) overlapping ranges of scale for stochastic model construction. It should be noted that the authors do not suggest that the application of such codes are without problems associated with the deterministic construction of the model itself. However, the inherent problems of such approaches notwithstanding, they remain by far the most commonly used tools for many important problems (e.g. TMDL), and a need to conduct reasonable analysis of the uncertainty characteristic of new and old models is evident.

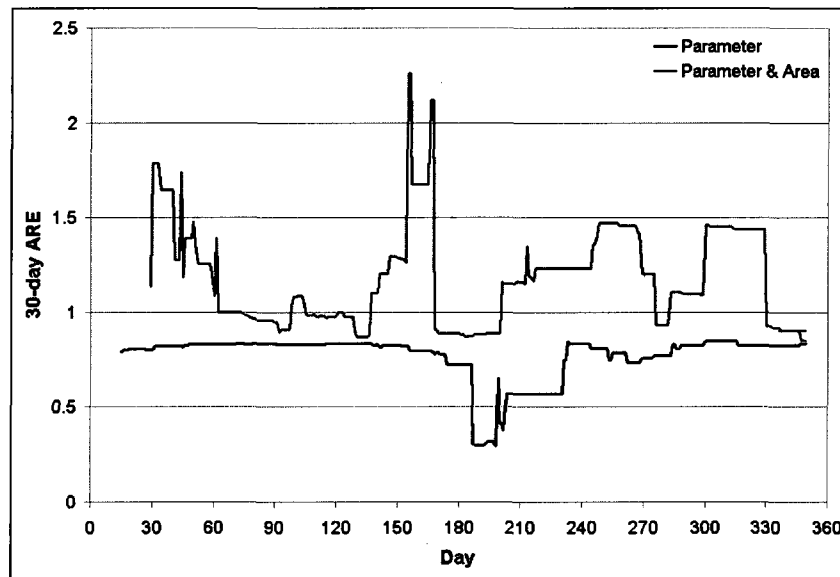


Figure 5.9: Moving Average Relative Error of Parameter and Scale Uncertainty Components in Simulation Results at Shenandoah Outlet for 1993.

Given this caveat, if models are to be constructed using somewhat complex deterministic structures, the type of analysis presented here is invaluable in assessing how a model can be reasonably applied (and then perturbed via e.g. Monte-Carlo analysis), as well as how structural decisions affect the uncertainty associated with the parameterization and the simulation results itself.

In the case presented here (and, it is suggested, most others with comparable models), the uncertainties associated with parameterization and parameter sensitivity are outweighed in significance by those resulting from structural and conceptual decisions. The optimal scale for

structural use of the AnnAGNPS model in this watershed was found to be between approximately 4-8.5 km<sup>2</sup>. When considering parameter issues within this stable structural scale range, a preferred discretization of 8 km<sup>2</sup> was found. It is hoped that these techniques may shed some light on the relative importance of (parameter) calibration and uncertainty analysis as they are generally performed.

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## CHAPTER 6

### COUPLING MODEL UNCERTAINTY FOR COUPLED RAINFALL/RUNOFF AND SURFACE WATER QUALITY MODELS

#### 6.0 CHAPTER OVERVIEW

This chapter has been submitted for publication in *Water Research*.

#### **ABSTRACT**

Coupled hydrology and water quality models are today an important tool, used in the understanding and management of surface water and watershed areas. Such problems are generally subject to substantial uncertainty in parameters, process understanding, and data. Component models, drawing on different data, different concepts, and different structures, are affected differently by each of these uncertain elements.

This paper proposes a framework wherein the response of component models to their respective uncertain elements can be quantified and assessed, using a hydrological model and water quality model as two exemplars. The resulting assessments can be used to identify model coupling strategies that permit more appropriate use and calibration of individual models, and a better overall coupled model response.

One key finding was that an approximate balance of water quality and hydrological model responses can be obtained using both the QUAL2E and Mike11 water quality models. The balance point, however, does not support a particularly narrow surface response (or stringent calibration criteria) with respect to the water quality calibration data, at least in the case examined here. Additionally, it is clear from the results presented that the structural source of uncertainty is at least as significant as parameter-based uncertainties in areal models.

Listed keywords were: Water Quality, Hydrology, Uncertainty, Watershed, Coupled, Model

#### 6.1 INTRODUCTION

Watershed-level modeling has become an essential tool in planning and managing environmental risks and the relationship between pollutant sources and water bodies, and an approved Total Maximum Daily Loading (TMDL) evaluation has become a de facto requisite for assistance funding. Particularly in recent years, an increasing focus has been made on the issues

of both point and non-point pollutant sources at the watershed level, and their associated effects on water quality. Pollutant loading and hydrology models are generally deployed in such cases to provide insight on source assessments and their impacts on water quality targets as well as the consequences of varied management scenarios (e.g., Parker et al., 2008a). Water chemistry is often modeled using a dedicated water quality package, drawing on hydrological model outputs to assess in-stream condition.

These types of assessments have proven to be challenging, particularly in moderately to highly complex systems. Model parameters are adjusted to fit one or several years of reference data. It is well understood for deterministic models that the chosen ‘calibrated’ parameter set, and thus simulation results, depend on the reference data and the calibration strategy used. Since similar results are often achieved with different approaches, the issue of which parameter set should be used frequently arises. This phenomenon is known as model equifinality.

Stochastic models attempt to mitigate these issues to some degree by representing modeled phenomena as a distribution of possible outcomes. A common implementation is to perturb input parameters, through use of Monte-Carlo simulations for example, and assess likely outcomes from the results. One advantage of this approach is that it is readily implemented late in the (otherwise deterministic) model construction timeline, as an added tool for result interpretation. Much of the literature ignores either expressly or, more often implicitly, the model uncertainty associated with model structure. This omission is particularly problematic in cases where two models are, in effect, joined into a super-structure.

This project emphasizes the formal quantification and handling of both model parameter and model structure components of the uncertainty problem throughout the model construction process. This is in stark contrast to approaches that attempt to qualify such issues during model interpretation phases. Through use of examples, this paper demonstrates how a revised approach can lead to improvements not only to individual component models (better model structure, better calibration) but also to more quantitative ways of balancing component models, and examining problems of sufficient complexity to require the use of coupled models.

## **6.2 METHODOLOGY**

### **6.2.1 OVERVIEW**

This paper proposes a revised methodology for coupling of a hydrological model with a water quality model, in an attempt, for instance, to depict the dynamics of riverine water quality

throughout a watershed. Particular emphasis is placed on understanding the issue of equifinality and parameter sensitivity, important in understanding how component and coupled models behave under uncertainty. A case study is also presented.

### **6.2.2 CASE STUDY REGION**

The Potomac Watershed stretches across approximately 38 000 km<sup>2</sup>, of the Eastern US. The Potomac River itself covers roughly 620 km from Fairfax Stone in West Virginia to Point Lookout in Maryland. The average river flow at the Washington, DC location is about 310 m<sup>3</sup>/s, with minimum and maximum recorded flows of 17 m<sup>3</sup>/s (September, 1966) and 12000 m<sup>3</sup>/s (March, 1936), respectively. The watershed flows into Chesapeake Bay, becoming tidal near Washington DC where the river crosses the Fall Line into the Coastal Plain province. Downstream from here, the water becomes increasingly brackish with a gradual increase in salinity. This study limits itself to the purely freshwater and non-tidal portion of the Potomac River.

From 1991 to 1996, the US Geological Survey's (USGS) National Water Quality Assessment (NAWQA) program began extensive work in the basin to monitor surface and ground water quality and ecology. That dataset is used here, and draws on over 50 USGS stations to provide information on stream flow quantity. These data are available at temporal resolutions up to daily time steps for individual stations. Water quality data are available at 5 'integrator' and 5 'indicator' stations on a monthly basis. Point Sources loading the river system were identified from US EPA (2008). Model calibration was based on the 1993-1994 calendar year. The case study simulation also examines predictive results over the 1994-1995 calendar year.

Simulations in this paper were conducted using the continuous-simulation Annualized Agricultural Non Point Source (AnnAGNPS) pollutant loading model, which was developed by the US Department of Agriculture (USDA). AnnAGNPS is a comprehensive package, particularly suited for analyzing non-point source issues at the watershed level. The watershed is divided into homogeneous drainage areas which are in turn connected by a dendritic reach system. Water and pollutant loadings from individual fields are simulated as runoff events from rainfall, snowmelt, and irrigation data. Soil loss is calculated based on the Revised Universal Soil Loss Equation (RUSLE). The model also includes a substantial database with values of parameters for agricultural applications and management scenarios (cf. Bosh et al., 1998).

Water quality simulations were conducted using the conversion kinetics model of the widely used QUAL2E code (see Brown and Barnell, 1987). Typical constituents of interest in

water quality models include dissolved oxygen, nutrients (e.g., nitrogen, phosphorus), and toxics (e.g., pesticides). An extensive review of water quality modeling approaches is beyond the scope of this paper, (but can be found in e.g., Rauch et al., 1998 or Bowie et al., 1985). In addition to dissolved oxygen, nitrogen (including nitrite tracking) and biodegradable organic matter demand, QUAL2E considers algal biomass, organic nutrient and phosphorus components.

### 6.2.3 BASEFLOW SEPARATION

Data for flows were taken from the USGS Surface-Water Daily Data Set for the study period (USGS, 2007). Hydrograph separation was done using the Chapman filter equation, as implemented in the ABSCAN software (Parker, 2006). Digital filter techniques, originally used in signal analysis, were employed in a water resources context by Lyne and Hollick (1979) to separate high frequency (direct runoff) and low frequency (baseflow) components from the streamflow ‘signal’. Chapman (1991) noted that the Lyne–Hollick algorithm incorrectly provides a constant streamflow  $Q$ , or baseflow  $b$ , when direct runoff has ceased and therefore developed the new equation:

$$b_t = \frac{3\alpha - 1}{3 - \alpha} \cdot b_{t-1} + \frac{1 - \alpha}{3 - \alpha} \cdot (Q_t + Q_{t-1}) \quad (5-4)$$

This equation calculates  $b$  at each timestep  $t$  given the associated  $Q$ . When the quick runoff component has ceased, the filter parameter  $\alpha$  becomes the hydrological recession constant  $a$  in equation (5-5), commonly used to describe baseflow recession during dry weather periods without groundwater recharge:

$$b_k = ab_k - 1 \quad (5-5)$$

The Chapman method was selected as it offered good performance with a single conceptually-based parameter,  $\alpha$ . Values for  $\alpha$  were estimated from historical records near the outlet of the study area, taken from Sinclair and Pitz (1999). Table 6.1 shows parameterization results of the Chapman filter, with values for  $\alpha$  in each column and relative importance of baseflow to streamflow considered in the rows for 4 years (1992-1995). A final value of 0.5 was used in the model separation (cf. Table 6.1).

#### 6.2.4 NPS MODEL EVALUATION

An analysis of uncertainty in the non-point source and hydrological loading component used here (i.e., AnnAGNPS) was conducted using the methodology outlined in Parker et al. (2008d).

Table 6.1: Baseflow Separation Parameterization Test Results for Station 1646500 (Outlet).  $\tilde{x}$  indicates median Flow values.

|                                     | Chapman Parameter Value |         |         |         |         |
|-------------------------------------|-------------------------|---------|---------|---------|---------|
|                                     | 0.40                    | 0.45    | 0.50    | 0.55    | 0.60    |
| <b>1992</b>                         |                         |         |         |         |         |
| Qbase:Qtotal                        | 0.49925                 | 0.49915 | 0.49902 | 0.49886 | 0.49866 |
| $\tilde{x}$ base: $\tilde{x}$ total | 0.50378                 | 0.51131 | 0.52648 | 0.52851 | 0.52776 |
| $\tilde{x}$ base                    | 81.408                  | 82.624  | 85.077  | 85.404  | 85.282  |
| <b>1993</b>                         |                         |         |         |         |         |
| Qbase:Qtotal                        | 0.50046                 | 0.50052 | 0.50059 | 0.50069 | 0.50080 |
| $\tilde{x}$ base: $\tilde{x}$ total | 0.52458                 | 0.52057 | 0.52293 | 0.52316 | 0.52564 |
| $\tilde{x}$ base                    | 92.043                  | 91.340  | 91.754  | 91.794  | 92.229  |
| <b>1994</b>                         |                         |         |         |         |         |
| Qbase:Qtotal                        | 0.50005                 | 0.50006 | 0.50007 | 0.50008 | 0.50010 |
| $\tilde{x}$ base: $\tilde{x}$ total | 0.52021                 | 0.51903 | 0.51771 | 0.52442 | 0.53327 |
| $\tilde{x}$ base                    | 90.247                  | 90.042  | 89.813  | 90.976  | 92.511  |
| <b>1995</b>                         |                         |         |         |         |         |
| Qbase:Qtotal                        | 0.49972                 | 0.49968 | 0.49964 | 0.49958 | 0.49950 |
| $\tilde{x}$ base: $\tilde{x}$ total | 0.49494                 | 0.49222 | 0.49471 | 0.49748 | 0.49700 |
| $\tilde{x}$ base                    | 94.827                  | 94.305  | 94.782  | 95.314  | 95.221  |
| <b>Average</b>                      |                         |         |         |         |         |
| Qbase:Qtotal                        | 0.49987                 | 0.49985 | 0.49983 | 0.49980 | 0.49977 |
| $\tilde{x}$ base: $\tilde{x}$ total | 0.51088                 | 0.51078 | 0.51546 | 0.51839 | 0.52091 |
| $\tilde{x}$ base                    | 89.631                  | 89.578  | 90.356  | 90.872  | 91.311  |

The first step in the approach was to determine the scales at which the NPS model behaves adequately for stochastic analysis. The goal of this stage was to identify a range of model delineation (lumped area and reach networks) which could permit Monte Carlo analysis around a given conceptual model and related parameter set. As the model delineation is also governed by the site topography, the analysis was performed on three sub-watersheds to isolate conceptual model issues over a plausible range of model structures. The model runs were populated with

identical, grossly averaged, soil and land-use conditions in each case and the results were examined for changes in runoff volume and sediment transport. Any differences between model outputs, therefore, are products of the union between the discretization and conceptual structure of the model.

With a range of suitable scales for the conceptual model determined, the task now becomes to find the discretization that leads to suitable parameter representation in the same range. In a stochastic setting, parameters can be considered as distributions of plausible values rather than point values. Therefore, in such cases, it is most important to determine the scale which allows for a suitable distribution to be fitted to spatial data. The approach used here was to examine the spatial variation of these mapped runoff coefficient values and the effect of scale and structure changes on distribution and sampling issues. Several statistics were calculated via a geospatial information system (GIS) for each discretized area.

Results of the analysis in Parker et al. (2008d) suggest that scale selection in the AnnAGNPS model is limited by conceptual model uncertainty and stability issues rather than parameter uncertainty, which is more commonly used. The appropriate scale appears to be in a relatively narrow range of between 5-10 km<sup>2</sup> average cell area. Additionally, result sensitivity to parameter uncertainty seems to be minimized at near-optimal scales. Figures 6.1 and 6.2 present a summary of the findings in Parker et al. (2008d).

### **6.2.5 WATER QUALITY MODEL EVALUATION**

An analysis of uncertainty associated with the data, calibration and conceptual model of the water quality model used here (i.e., the QUAL2E formulation) was conducted using the GLUE methodology as outlined in Parker et al. (2008b). Output of the model was compared for stochastic simulation of DO, BOD, and ammonia-N (NH<sub>4</sub>). Initial ranges for water quality model parameters were estimated from literature values (Bowie et al., 1985).

The representative model set was then derived. The problem can be viewed as an inverse modeling exercise. A Generalized Likelihood Uncertainty Estimation (GLUE) algorithm, as outlined by Beven and Binley (1992), was used to identify which parameter sets provide an adequate representation of the river system water chemistry. In this technique, the focus is on estimating posterior distributions for predicted variables directly from the outputs of a set of representative models, rather than from a model and an additive residual model. The resulting set of models is further constrained by the calibration data and criteria (cf. Beven, 2001 and Rode et al., 2007), and contains information on the simulation output variability for all representative

input sets. The representative set can be viewed as the range of water quality model realizations that conform to the calibration criteria, which in turn are constrained by the specific dataset used.

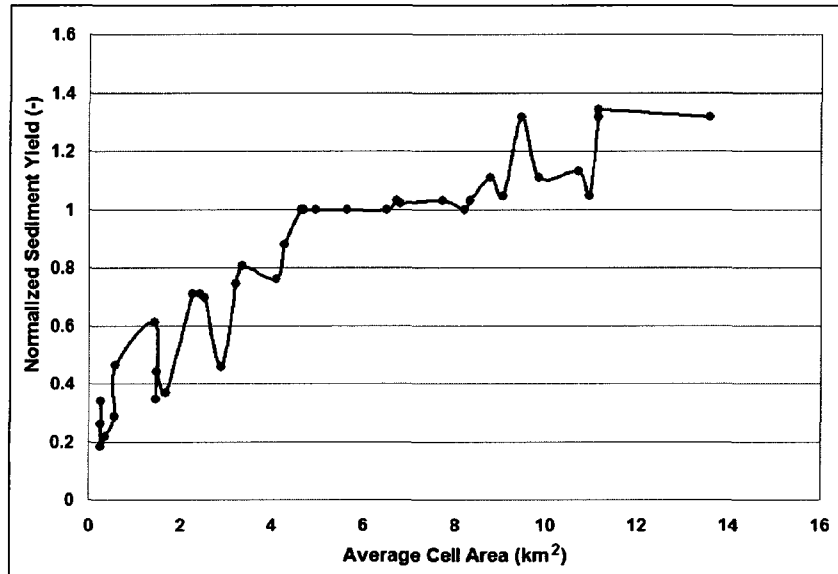


Figure 6.1: Sediment stability curve generated from normalized data for NPS model

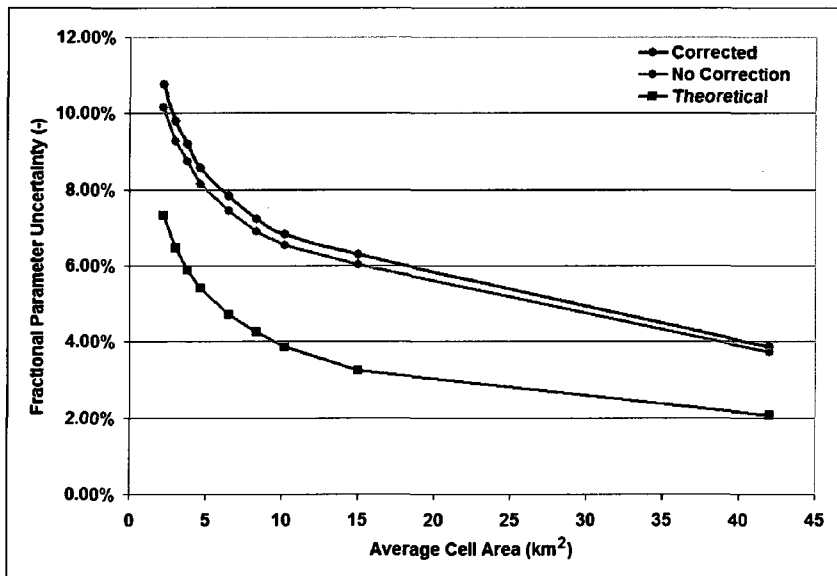


Figure 6.2: Fractional Parameter Uncertainty Change with respect to Discretization for NPS model.

The results in Parker et al. (2008b) quantified the response surface dispersion of the set of representative parameters for the QUAL2E conceptual model in the study region, for several

calibration scenarios. It was noted that the calibration set and resulting surface response are also a function of the conceptual model structure itself (as examined in Parker et al., 2008c), as well as the data used for calibration. A representative plot of the analysis conducted is shown in Figure 6.3.

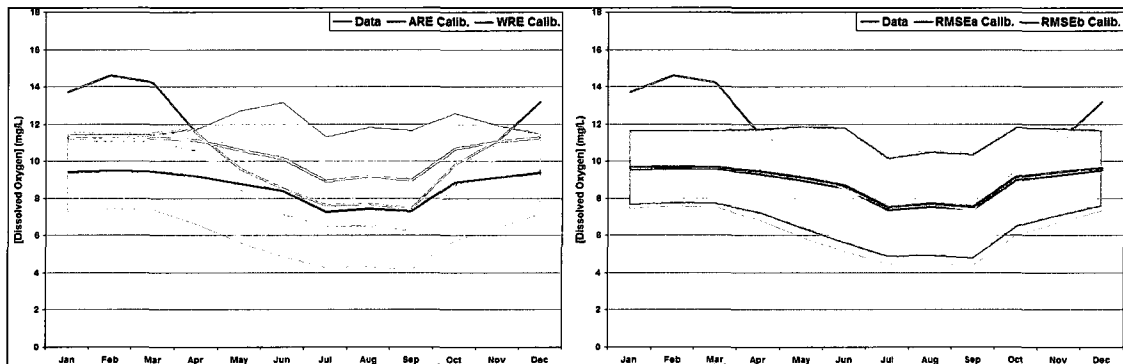


Figure 6.3. DO surface response (95%) for ARE, WRE, RMSEa and RMSEb calibrations. Solid lines are mean of representative models.

#### 6.2.6 MODEL RECONCILIATION

The original strategy proposed for this work called for the watershed model discretization to be altered across the space domain based on insights gained from the water quality inverse modeling exercise, and ultimately, by the combination of uncertainty structure of the model for a given water quality calibration criteria and dataset. In such an application, two discretization schemes in particular were proposed. The first, termed the ‘balanced’ strategy, called for the NPS model discretization to be adjusted to match the dispersion of water quality (WQ) models identified in the inverse modeling problem at points along each major reach. The second scenario which was proposed was the ‘equal’ strategy, which called for the dispersion of the NPS model to be added to that of the WQ model, and for this sum to be held as a constant throughout the watershed. The first scenario favours consistency of relative contribution to overall uncertainty across models, the second favours consistency of the coupled model uncertainty across the spatial domain.

However, results in Parker et al. (2008d) showed that the NPS model’s structural uncertainty is very important at all scales, outside of a relatively narrow range of ‘stable’ discretization scales (consisting of cell areas from approximately 5-10 km<sup>2</sup>). This sensitivity to scale dominates issues of parameter and water quality uncertainty to the extent that it effectively prohibits the use of the model in any reasonable stochastic sense outside that range. These results

also call into question the validity of any model using Monte Carlo analysis on this particular code outside the stable region.

Given such a narrow range of suitable behaviour in the rainfall/runoff model, adjustments in model construction to ensure the relative balance of structural, conceptual, and parameter uncertainty conditions must be sought elsewhere. The water quality model response surface derived from the inverse approach is, as discussed in Parker et al. (2008c), a function of the calibration data set itself, the conceptual model, and the calibration criteria. Of these three, the calibration criteria are the most subject to modeler discretion, and also the most readily adjusted. An examination of the suitability of the calibration criteria, when compared with the NPS model response, was conducted.

In discussing model linkages and relative contribution to uncertainty, a common metric across models is needed. This paper focuses on the coefficient of variation (CV) for such purposes. The rationale for this is several-fold. First, the CV is a measure of distribution dispersion that is normalized to the mean value. As this is a dimensionless number, model CVs for, e.g., flows can be reasonably compared to values such as concentration. Equally, use of the CV for reporting and even statistical inference need not make an assumption about the population distribution in question (see, e.g., Sharma, 1994)

#### **6.2.7 SIMULATION**

A simulation was conducted with the coupled land-use and water quality models for the case study dataset. Calibration, as for Parker et al. (2008d), was conducted using the 365 days of 1993, and simulation results for 1994 conditions were compared with the corresponding data points. This simulation is not intended to be considered authoritative in any particular respect; however, it does provide the opportunity to illustrate the process and the resulting coupled model surface response as a forward product (in contrast, for instance, to the inverse response from Parker et al. 2008c).

### **6.3 RESULTS**

#### **6.3.1 MODEL RECONCILIATION**

The NPS model was tested for output response (parameter sensitivity) at scales where structural uncertainty effect were minimized, pursuant to the work presented in Parker et al. (2008d), and confirms some of the results found therein. Estimates of the parameter-related coefficient of variation observed in the NPS model response are shown in Figure 6.4. The

parameter input fractional uncertainty (as derived in Parker 2008d) is shown on the plot, based on sampling of spatial variability (determined by land use data). The 6, 8 and 10 km models were then tested for parameter sensitivity alone, with the corresponding CV computed (points in Figure 6.4). The lines show estimates of these parameter-related CV points relative to changes in the fractional input parameter uncertainty.

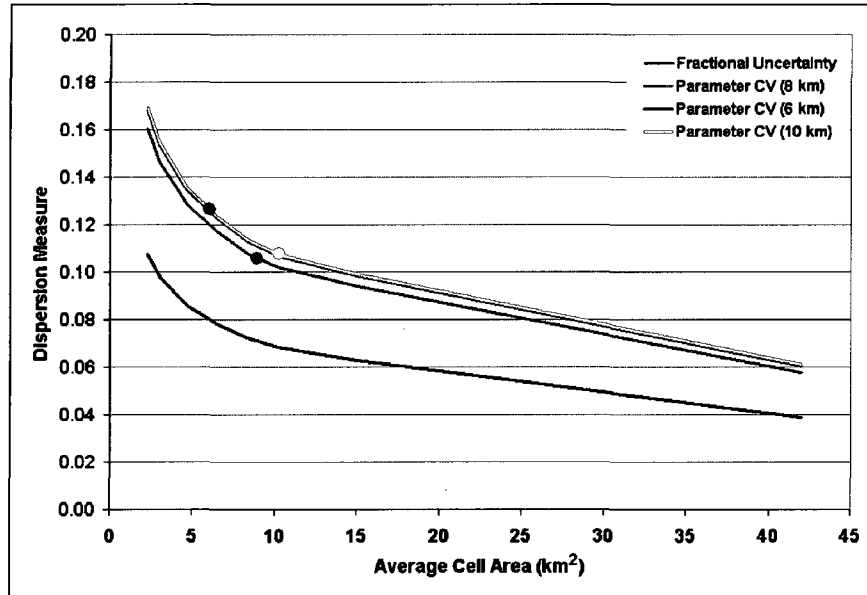


Figure 6.4: Parameter-Related Output Uncertainty for NPS model.

Notably, the parameter sensitivity is minimized in the middle region of the suitable model discretization scales (8 km<sup>2</sup>) when compared with regions on the edges (6 and 10 km<sup>2</sup> cases). Though parameter-related uncertainties are also computed (as functions of fractional parameter uncertainty) for scales outside that range in Figure 6.4, in these cases the structural uncertainty dominates. This precludes optimization, and perhaps even reasonable consideration, of uncertainties associated with parameter sensitivity in these cases (see also Parker, 2008d).

With the surface response characteristics of the NPS model characterized, the corresponding responses of the water quality model can now be quantified relative to the first model. As previously discussed, in Parker (2008b,c) for instance, the quality model response is a function of the output data itself, the calibration criteria used to determine representative parameter sets, and of course the conceptual model itself Figure 6.5 shows the surface response, measured using the ACV metric, of two different conceptual models with two different calibration thresholds, as normalized to the response of the NPS model.

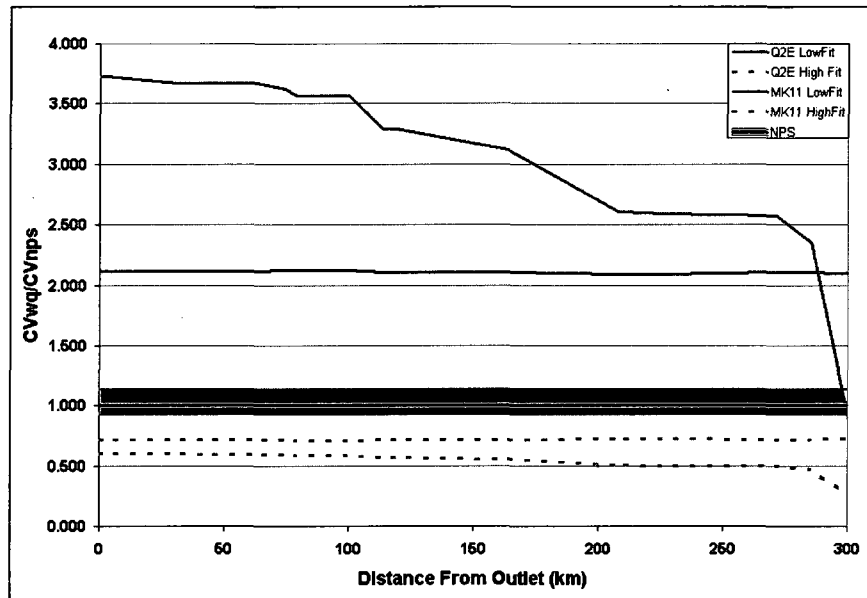


Figure 6.5: Surface Response of water quality models predictions normalized to rainfall/runoff model.  $CV_{wq}$  and  $CV_{nps}$  are the coefficient of variation associated with the WQ and NPS models, respectively.

As mentioned, each conceptual was subject to two calibration levels, a low fitness one, intended to include most model that could reasonably be considered representative, and a higher fitness one with better overall predictive ability. These strategies are discussed in further detail in Parker (2008c). Figure 6.5 is helpful in predicting how the joint response of the coupled rainfall/runoff and quality models will be affected by the individual responses at locations throughout the stream and cell network. The NPS model response is shown as a (narrow) range of parameter uncertainties (shaded region), corresponding to acceptable discretizations.

Generally, when the CV associated with the water quality model is much larger than this range, the quality model can be interpreted as under constrained when compared with the hydrological model, and contributes disproportionately to uncertainty in the coupled model output. The water quality data are then being under used. Conversely, when the water quality CV is too low, the data and calibration are constraining the parameter set to such an extent that the NPS model is not contributing much information (or not reducing the range of plausible values), and the quality is essentially over calibrated.

As can be seen in Figure 6.5, the Mikel1 conceptual model response can change significantly depending on the proximity to data points, whereas the QUAL2E model tends to be relatively more even throughout the watershed. While this, as discussed in Parker et al. (2008b),

may pose a disadvantage for QUAL2E in many applications (for instance, scenarios where a wider range of structurally stable rainfall/runoff discretizations could be explored), in this particular case, it means that both the approximately ‘balanced’ and ‘equal’ uncertainty coupling strategies proposed are likely to be best met by the QUAL2E conceptual model. Indeed, both conditions can be approximately met with the same discretization. In this case, the QUAL2E high fit calibration criteria provided the best match of water quality parameter uncertainty to NPS model structural uncertainty.

The model response can be further defined by examination of the relative contribution of CV for individual calibration criteria (e.g., for BOD, as in Figure 6.6).

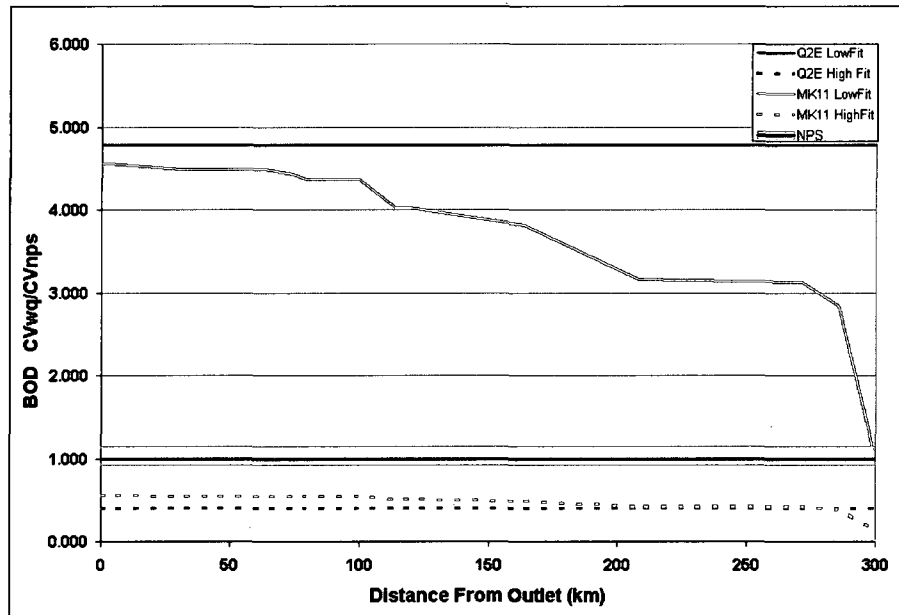


Figure 6.6: Surface Response of BOD predictions normalized to rainfall/runoff model.

Such information can potentially identify circumstances when adjustment of calibration criteria for individual components may be advantageous.

### 6.3.2 CASE STUDY SIMULATION

As discussed in the methodology section, and in more detail in previous papers, the case study run set was calibrated using the 1993 dataset. Figure 6.7 shows the rainfall/runoff modeled and observed streamflow values for that period in the first 365 points, followed by the 1994 simulation results and data. Precipitation data are shown on the second axis.

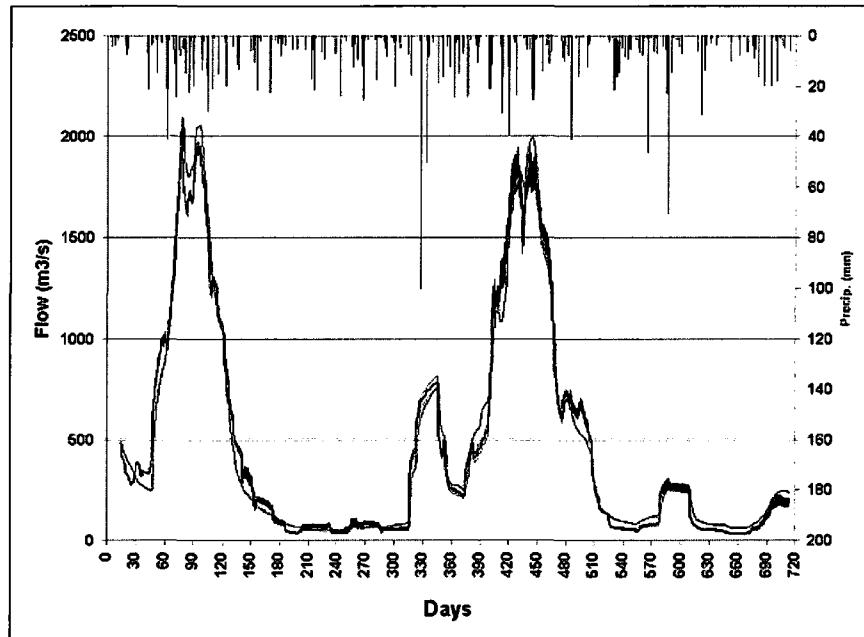


Figure 6.7: Simulated (in blue) and Observed (in Orange) Catchment Response, plotted as 30 d average flows vs. precipitation.

The modeled values in Figure 6.7 are displayed as ranges, derived from a Monte Carlo sensitivity analysis around the calibrated conditions of the 8 km<sup>2</sup> discretization case. The range of values tested was derived from the corresponding parameter uncertainty at that scale, as derived from spatial statistics (see Parker, 2008d). Overall, the fit to data is quite good, though the model appears to somewhat under predict flows during relatively dry periods. This may be due to baseflow separation, climate information, or issues related to the particular calibration methodology used, as discussed in Parker 2008d.

Water and nutrient loading results from the NPS model were then used to feed a series of water quality simulations, based on the QUAL2E conceptual model. Parameter ranges for kinetics were derived from the 'high-fitness' calibration. Defined in Parker et al. (2008c), this calibration is weighted to station data based on flow at that station, and considers all parameter sets that predict DO and NH<sub>4</sub> species concentrations within 25% of observed values and BOD concentration within 50% of observed data at the outlet. As shown in Figure 6.5, and discussed previously, this particular calibration leads to an approximately balanced model construction, with a relatively constant combined uncertainty as an additional benefit. A slightly less stringent calibration criterion could also have been used had the balance between the two models not been deemed acceptable, as it was in this case.

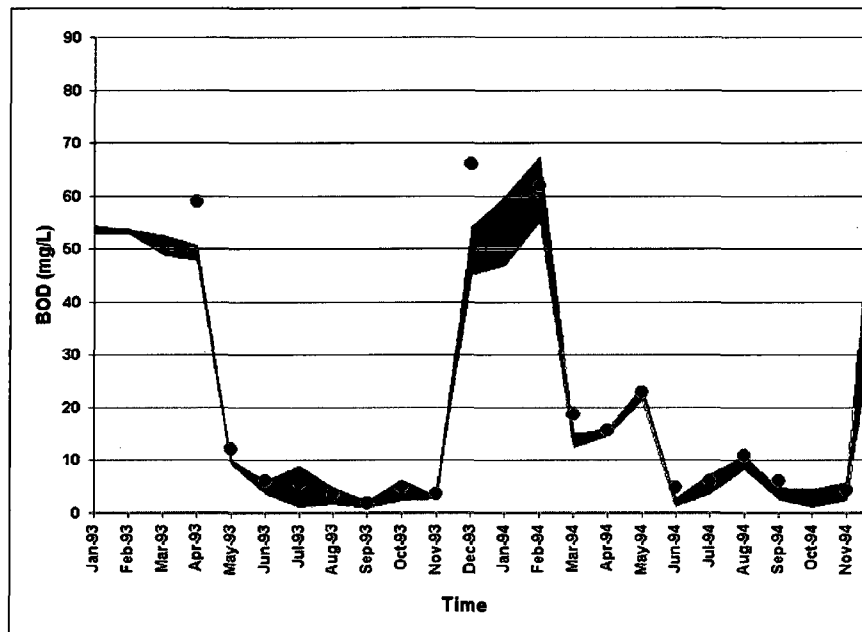


Figure 6.8: Simulated vs. Observed in-stream BOD concentration at outlet, for the 1993-1994 period.

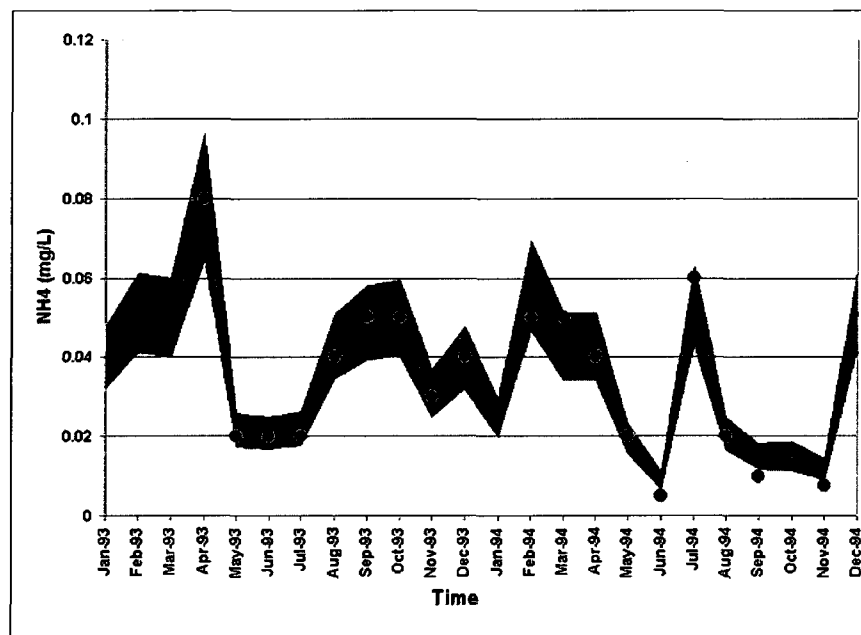


Figure 6.9: Simulated vs. Observed in-stream NH<sub>4</sub>-species concentration at outlet, for the 1993-1994 period.

Figures 6.8 and 6.9 show coupled simulation results (in blue) for water quality constituents at the outlet, with available data points shown in orange.

Overall the simulation results are quite good. The inverse model suggested in-stream constituents such as the ammonia species could be well predicted, and the results depicted in Figure 6.9 appear to confirm this. More interestingly, perhaps, is the improvement that can be seen in Figure 6.8 for BOD, which is one of the constituents more closely associated with areal sources and runoff events. It is clear, in this plot, that the inflow of a relatively large amount of data on landuse, management, climate and topography, as interpreted by the NPS model, has greatly improved the predictive ability of the coupled model. This, of course, is precisely why the use of coupled models is often necessary, and particularly valuable in dynamic simulation.

#### **6.4 DISCUSSION AND CONCLUSIONS**

The approach proposed here allowed for a detailed examination of coupled watershed hydrology and water quality model construction, particularly in view of stochastic problems.

One key finding was that an approximate balance of water quality and hydrological model response can be obtained using both the QUAL2E and Mike11 water quality models. The balance point, however, does not support a particularly narrow surface response (or stringent calibration criteria) with respect to the water quality calibration data, at least in the case examined here. Additionally, the QUAL2E model structure may be advantageous for problems where a constant or balanced uncertainty condition is desired. This may be counterintuitive, given, for instance, the relatively good performance of the Mike11 in calibration tests (as shown in Parker, 2008b). It is due, however, not only to QUAL2E's relative surface response inertia, but just as importantly to the narrow range of suitable discretizations in the NPS model used here.

Improvements in the balance point can potentially be sought in several ways. First, additional data for use in the landuse model can help to narrow the reasonable range of model responses after calibration. As that response narrows, additional riverine water quality data (and/or more stringent calibration criteria) can improve spatial and temporal calibration stringency by minimizing, for instance, the relative weight of data and sampling uncertainty in the calibration set.

Just as importantly however, are the structural limitations evident in Parker et al. (2008d), that are restated here. Indeed, the effect of structural/conceptual uncertainty outside a narrow range dwarfs that of parameter uncertainty, where, it is fair to say, a disproportionate amount of

effort has, and continues to be, spent. Improvements in coupled model construction can be sought here, by judicious selection of model structure (and discretization), as well perhaps as use of conceptual models more stable with respect to scale variations.

Some of these issues, such as the suitability of a water quality conceptual model, the suitability of calibration criteria, and the specific response associated with a sparse dataset, are no doubt associated with the particular topography, topology and other characteristics of the study region examined here. Others, such as conceptual model stability with respect to scale, model inertia or parameter sensitivity, are more likely tied to the specific tools used in this study. The approach proposed, however, can be readily applied to a wide variety of deterministic codes that are currently in regular use for coupled model applications under uncertainty. Such an analysis, as demonstrated here, can yield valuable information on model behaviour, and readily suggests opportunities for improvement in coupled model use and interpretation.

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## CHAPTER 7

### CONCLUSIONS

#### 7.1 SUMMARY OF RESULTS

##### 7.1.1 WATER QUALITY MODELING ISSUES

The suggested use of GLUE methodologies can be used to test conceptual model structure and model calibration criteria suitability for specific applications.

A common theme that emerged from the conceptual model comparison was the importance of understanding the response characteristics. As an example, in the chosen case study, an annually calibrated stochastic MIKE11 model might be deemed useful for monthly simulation. The results suggest that a similarly calibrated QUAL2E model could be decidedly less suitable, depending on the type of problem addressed. Additionally, while both models appear to have approximately the same predictive ability for given set of calibration criteria, the MIKE11 model appears far more sensitive to data availability. At least in this study, the MIKE11 model response changed greatly depending on the proximity to calibration points, while the QUAL2E model tended to improve less rapidly near high data locations, but also to degrade less when it was away from such locations. This finding, and type of analysis, has important ramifications for the development of data sampling schemes and model selection in sparse vs. dense data situations.

The calibration tests reiterate the importance of model structure and data flow issues in determining appropriate use of a model. The key contention of the calibration study, illustrated by example, was that the RMSE, though in wide use, is in several respects disadvantageous as the calibration criteria itself in stochastic analysis, and particularly uncertainty analysis. Instead, the use of lossless criteria, spatially weighed criteria, and/or exceedance criteria may be preferable for many real-world applications. One distinct feature of any such calibration criterion is the ability for calibration to fail (no suitable parameter set found) given an unsuitable criteria or dataset.

The results of these studies will help users select and assess models for varied problems, and refine appropriate data collection and monitoring schemes. The findings and type of analysis illustrated have ramifications for the development of data sampling schemes and interpretation as well as calibration and conceptual model selection (or construction) themselves.

### ***7.1.2 NPS MODELING ISSUES***

The rainfall/runoff assessment methodology presented is for a reasonable stochastic analysis of pollutant loading problems given a deterministic-based code. The inherent problems of such approaches notwithstanding, such models remain by far the most commonly used tools for many important problems (e.g., TMDL), and a need to conduct reasonable analysis of uncertainty of new and old models is evident. The type of analysis presented can assess how such models may be reasonably applied (and then perturbed via, e.g., Monte-Carlo analysis), and how structural decisions affect the uncertainty associated with the parameterization and the simulation results itself.

In the case presented here (and, it is suggested, most others with comparable models), the uncertainties associated with parameterization and parameter sensitivity are outweighed in significance with those resulting from structural and conceptual decisions. It is hoped that this may shed some light on the relative importance of (parameter) calibration and uncertainty analysis as they are generally used.

### ***7.1.3 COUPLED MODEL ISSUES***

The final paper presented a detailed examination of coupled watershed hydrology and water quality model construction, particularly in view of stochastic problems. One key finding was that an approximate balance of water quality and hydrological model response can be obtained using both the QUAL2E and Mike11 water quality models.

Improvements in the balance point can potentially be sought in several ways. First, additional data for use in the landuse model can help to narrow the reasonable range of model responses after calibration. As that response narrows, additional riverine water quality data (and/or more stringent calibration criteria) can improve spatial and temporal calibration stringency by minimizing, for instance, the relative weight of data and sampling uncertainty in the calibration set.

Just as important however, are the structural limitations. Indeed, the effect of structural/conceptual uncertainty outside a narrow range dwarfs that of parameter uncertainty, where, it is fair to say, a disproportionate amount of effort has, and continues to be, spent. Improvements in coupled model construction can be sought here, by judicious selection of model structure (and discretization), as well perhaps as use of conceptual models more stable with respect to scale variations.

Some of these issues, such as the suitability of a water quality conceptual model, the suitability of calibration criteria, and the specific response associated with a sparse dataset, are no doubt associated with the particular topography, topology and other characteristics of the study region examined here. Others, such as conceptual model stability with respect to scale, model inertia or parameter sensitivity, are more likely tied to the specific tools used in this study. The approach proposed, however, can be readily applied to a wide variety of deterministic codes that are currently in regular use for coupled modeled applications under uncertainty; such an analysis, as demonstrated here, can yield valuable information on model behaviour, and readily suggests opportunities for improvement in coupled model use and interpretation.

## 7.2 CONCLUSIONS

This study proposed a fundamental rethink of the overall algorithmic approach to coupled modeling of watershed and the associated riverine systems therein. The implementation of specific numerical techniques for a given modeling task almost always involves a series of uncertain decisions with several contrasting candidate approaches. A word of note on the guiding principles of the decision-tree associated with this particular realization follows.

In an attempt to characterize the processes stochastically, the proposed methodology includes the generation at several steps of many Monte-Carlo type simulations. The objective each time this technique is used is a set of parameter and model realizations that are as self-consistent and consistent with available data as possible. The advantages of a fairly simple, broadly applied sampling method that allows for complex parameter interaction, equifinality, and many different types of performance measures are deemed to outweigh the associated disadvantages, chiefly the increased requirement for high performance and/or parallel computing resources.

Emphasis has also been placed on using broadly reproducible methods, not only in terms of code design (e.g., robust pseudo-random number generation with seed values), but also with respect to data and conceptual model requirements. The methodology proposed is based, whenever possible, on choosing data sources and processing methods that minimize the need for qualitative assessments. While the approach does not preclude adjustments based on user expertise, it minimizes the need for extensive interpretation between data processing steps, a feature which not only simplifies user input, but also facilitates future use and interpretation of the model, due to the high reproducibility of each step. Additionally, this approach enables two

models, distinct in time and location, to be compared for additional insights or planning at higher scales.

While attempts to identify uncertainty issues are nothing new (see the above Literature Review section for an overview), the approach specified in this proposal does have some distinguishing features, particularly with respect to water quality applications. As noted by Gupta et al. (1998):

‘We disagree with the seemingly widespread conviction that the model calibration problem will simply disappear with the availability of more and better field measurements. This paper suggests that the emergence of a new and more powerful model calibration paradigm must include recognition of the inherent multiobjective nature of the problem and must explicitly recognize the role of model [structure] error.’

Previous work (e.g., Vrugt et al., 2005) has focused extensively on finding analytical solutions to these types of errors, based either on relatively simple conceptual models themselves, or on relatively simple characterization of model response. As a result, these approaches have found limited applications in real world problems, where relatively complex models, generally designed for deterministic problems, are used to answer relatively complex questions.

The state-of-the-art, in this respect, is not unlike that of a common game, chess. In stark contrast to watershed systems, comprised of thousands of state variables, unclear land, soil and hydrological boundaries, and imperfect conceptual models, chess is a relatively simple problem. The coordinate system is two-dimensional, with each subdivision falling into one of two classes. There are 7 types of components, with well defined rules governing movement through time and space. Initial conditions are absolute and known, and the entire system can, at any time, be described with 32 state variables or less. Despite the relative simplicity of the chess system, no analytical solution has ever been found. But programs and computers that play chess far better than most humans are able to can still be built. This is accomplished largely through the use of quantitative metrics, values based on both objective and heuristic concepts (such as ‘pawn structure’, ‘material’, and ‘king safety’) that can be used to evaluate the relative strength or importance of one set of positions when compared to another. This is the space that the work proposed here hopes to occupy.

It is believed that the methodology outlined here is consistent with this ideology, and does begin to explicitly address the uncertainty and error associated with model structural features, at

both the component model and coupled model level. The methodology used can be readily applied to a wide variety of computer codes and conceptual models, without extensive modification thereof, and offers the ability to generate and observe quantitative metrics at several stages. These metrics have applications beyond the construction of new models and can be used to qualify and reconcile results from third-party models.

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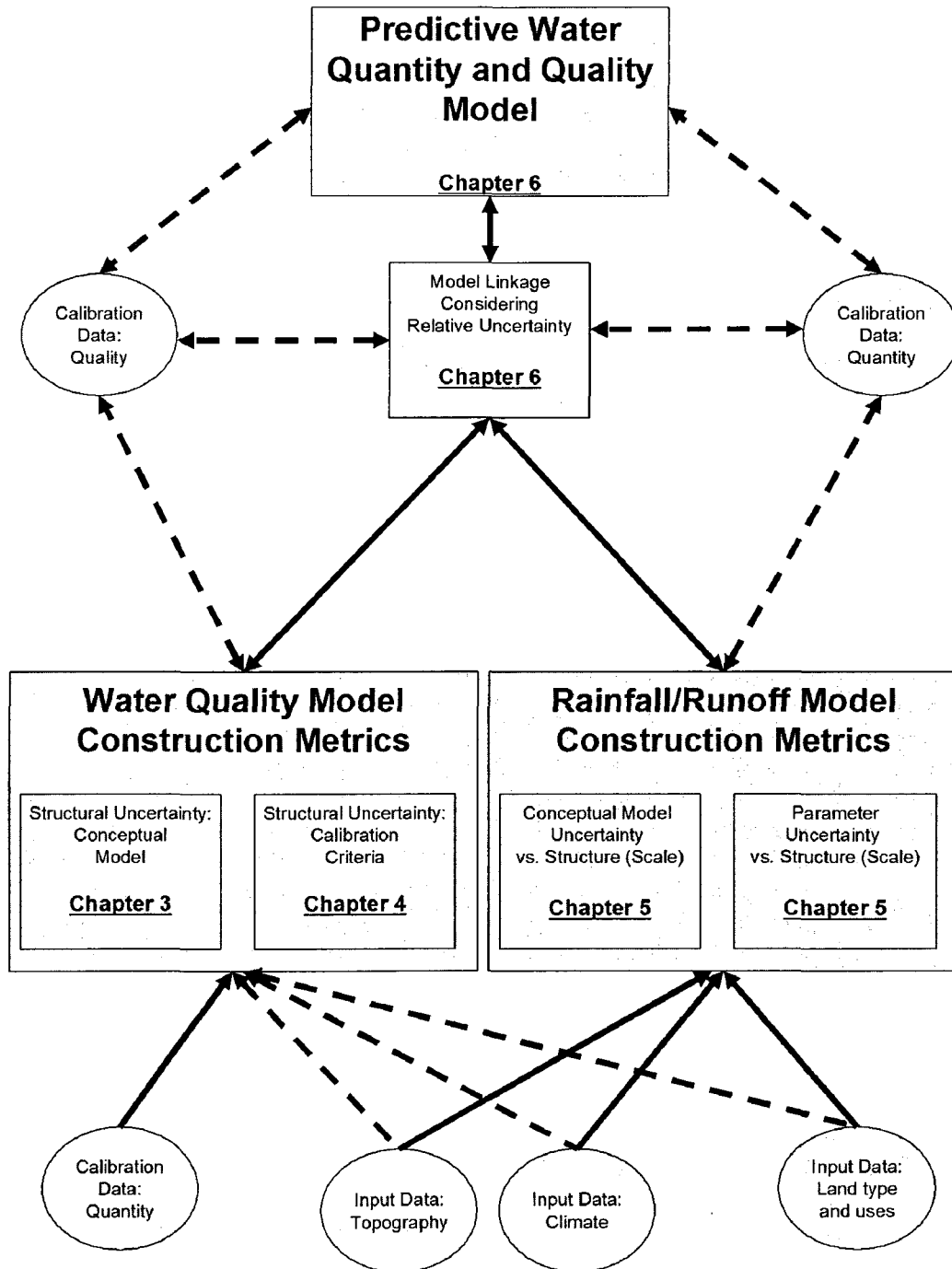
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## **APPENDICES**

# APPENDIX A: CHAPTER FLOWCHART FOR PREDICTIVE MODEL CONSTRUCTION



## **APPENDIX B: CONFIGURATION & CONTROL PROCEDURES**

### ***B.1. PURPOSE***

The policies and practice listed here are designed to minimize the risks of errors in calculation and data manipulation tasks, to ensure that the solution and results are of the highest quality and that the methodologies are consistent.

Analyses performed by hand or with custom tools are not exempt from the quality requirements specified here. However, for those cases, the analyst often has a better grasp and control over the limitations, assumptions and methodology than when using complex computer codes. Calculations and tasks routinely performed with well-established or previously developed computer codes present a particular challenge because these codes are highly complex, may be supplied by an external source, and are designed to work for a specific range of problems. Complacency and over-confidence in the codes may lead to erroneous results. The policies and practices here should help to ensure that the results are consistently of the highest quality.

### ***B.2. SOURCE CODE QUALITY ASSURANCE REQUIREMENTS***

A configuration control system must be in place to track version changes in the source code. Each version of the source code must be assigned a unique version number. Previously tested and “known-good” versions of source are to be archived and retrievable. The changes between two versions of the code must be documented.

If the source of the program, the compiler, or the operating system is modified or upgraded, the quality assurance (QA) qualification process must be repeated to verify the validity of the program. Additionally, programs acquired through third parties must be verified ‘in-house’ before being QA qualified.

### ***B.3. PROGRAM TESTING***

In order for a program to pass the QA qualification process, it must pass a series of test problems. The test problems are conducted, and must be run to completion without crashing. The results of the test problems are then extensively compared to a previously known good solution, if available. Any discrepancies or anomalies (precision or round-off errors, for example) must be documented and explained. Upon passing qualification, the date, size and version of the source code and executable files must be recorded.

The AnnAGNPS 2.01c package used was obtained from the USDA website at <http://www.sedlab.olemiss.edu/agnps.html>. The code was then verified by running the example cases provided, the “Beaver Creek” and “Mission Creek” data files, and comparing the outputs with the shipped results. The output files were identical to the reference results for both cases, and so the system was deemed tested and known-good.

The utilities constructed were tested extensively against data entered and processed manually, so as to ensure proper behaviour. Additionally, diagnostic runs were conducted with variable tracking (‘debugging’) tools to ensure that data were being loaded, handled, and outputted as desired. Backups of all ‘good’ versions were made, and any new features or modifications from a tested version were handled according to the configuration control procedure (described under Section A.4).

#### ***B.4. CONFIGURATION CONTROL***

The latest QA qualified version of a given program should be under the “\ProgramName\current\” directory. Previously known good versions are archived under “\ProgramName\Old versions\” as zip files bearing the version name. Versions pending QA qualification are placed under the “\ProgramName\pending\versionanme\” folder. All files should be regularly backed up to a writable CD or similar “read-only” storage.

**APPENDIX C: METADATA**

This section contains some representative metadata files for important datasets used in this study. Complete metadata information is available in electronic form on the companion disc to this thesis.

*C.1. TOPOGRAPHIC METADATA (SRTM)*

# Shuttle Radar Topography Mission (SRTM) Elevation Data Set

## Part 1: Set-Specific Metadata

---

*Identification\_Information:*
*Citation:**Citation\_Information:**Originator:* National Aeronautics and Space Administration (NASA)*Originator:* National Geospatial-Intelligence Agency (NGA)*Originator:* German Aerospace Center (DLR)*Originator:* Italian Space Agency (ASI)*Publication\_Date:* 2002*Title:* Shuttle Radar Topography Mission (SRTM) Elevation Data Set*Geospatial\_Data\_Presentation\_Form:* SDE raster digital data*Publication\_Information:**Publication\_Place:* Sioux Falls, SD*Publisher:* U.S. Geological Survey*Online\_Linkage:* <<http://seamless.usgs.gov>>*Description:**Abstract:*

The Shuttle Radar Topography Mission (SRTM) aboard the Space Shuttle Endeavour, launched on Feb. 11, 2000. SRTM used the same radar instrument that comprised the Spaceborne Imaging Radar-C/X-Band Synthetic Aperture Radar (SIR-C/X-SAR) that flew twice on the Space Shuttle Endeavour in 1994. SRTM was assigned to collect 3-D measurements of the Earth's surface. To collect the 3-D data, engineers added a 60-meter (approximately 200-foot) mast, installed additional C-band and X-band antennas, and improved tracking and navigation devices. The mission is a cooperative project between NASA, the National Geospatial-Intelligence Agency (NGA) of the U.S. Department of Defense and the German and Italian space agencies. It is managed by NASA's Jet Propulsion Laboratory (JPL), Pasadena, CA, for NASA's Earth Science Enterprise, Washington, D.C.

*Purpose:*

The objective of the SRTM mission is to obtain elevation radar data on a near-global scale and generate the most complete high-resolution digital topographic database of the Earth. The information collected by SRTM will be used to provide a tool to enhance the activities of scientists, the military, commercial, and civilian users.

*Supplemental\_Information:**Additional Reference:* <<http://www.jpl.nasa.gov/srtm/index.html>>

Processing Information:Program Name: SRTM2DSM\_DTED\_3.AMLObjective: Process srtm data to a digital surface model in grid format.Procedure:Copy filesRename to latlon.dtl formatCreate GRIDDefine projection as geographic with WGS84 datumProject grid from decimal seconds to decimal degreesConvert to real data type

*Environment:*

[Ed: See Part 2]

*Time\_Period\_of\_Content:*

*Time\_Period\_Information:**Range\_of\_Dates/Times:**Beginning\_Date:* 20000211*Ending\_Date:* 20000222*Currentness\_Reference:* publication date*Status:**Progress:* In work*Maintenance\_and\_Update\_Frequency:* As needed*Spatial\_Domain:*

[Ed: See Part 2]

*Keywords:**Theme:**Theme\_Keyword\_Thesaurus:* GCMD Parameter Keywords*Theme\_Keyword:* EARTH SCIENCE*Theme\_Keyword:* LAND SURFACE*Theme\_Keyword:* TOPOGRAPHY*Theme\_Keyword:* LANDFORMS*Theme\_Keyword:* TERRAIN ELEVATION*Theme\_Keyword:* 3-ARC-SECOND DEM*Theme\_Keyword:* CARTOGRAPHY*Theme\_Keyword:* DEM*Theme\_Keyword:* DIGITAL ELEVATION MODEL*Theme\_Keyword:* DIGITAL SURFACE MODEL*Theme\_Keyword:* DIGITAL MAPPING*Theme\_Keyword:* EDC*Theme\_Keyword:* EROS*Theme\_Keyword:* GEODATA*Theme\_Keyword:* GIS*Theme\_Keyword:* MAPPING*Theme\_Keyword:* RASTER*Theme\_Keyword:* USGS*Place:**Place\_Keyword\_Thesaurus:* GCMD Location Keywords*Place\_Keyword:* NORTH AMERICA*Place\_Keyword:* AFRICA*Place\_Keyword:* EUROPE*Place\_Keyword:* ASIA*Place\_Keyword:* GLOBAL*Access\_Constraints:* None*Use\_Constraints:*

None. Acknowledgement of the originating agencies would be appreciated in products derived from these data.

*Point\_of\_Contact:**Contact\_Information:**Contact\_Person\_Primary:**Contact\_Person:* Customer Services Representative*Contact\_Organization:*

The National Center for Earth Resources Observation and Science (EROS)

*Contact\_Address:**Address\_Type:* mailing and physical address

*Address:*

U.S. Geological Survey, The National Center for Earth Resources Observation and Science (EROS)

City: Sioux Falls

State\_or\_Province: SD

Postal\_Code: 57198

Country: USA

Contact\_Voice\_Telephone: 605-594-6151

Contact\_Facsimile\_Telephone: 605-594-6589

Contact\_Electronic\_Mail\_Address: custserv@usgs.gov

*Native\_Data\_Set\_Environment:*

Microsoft Windows XP Version 5.1 (Build 2600) Service Pack 1; ESRI ArcCatalog 9.0.0.535

*Data\_Quality\_Information:**Logical\_Consistency\_Report:*

To collect the 3-D data, engineers added a 60-meter (approximately 200-foot) mast, installed additional C-band and X-band antennas, and improved tracking and navigation devices

*Completeness\_Report:* Shuttle Radar Topography Mission (SRTM) Elevation Data Set

*Positional\_Accuracy:**Horizontal\_Positional\_Accuracy:**Horizontal\_Positional\_Accuracy\_Report:*

The mission objective is to produce digital topographic map products with  $\leq 20$  m absolute horizontal circular accuracy. All accuracies are quoted at the 90% level, consistent with National Map Accuracy Standards.

*Vertical\_Positional\_Accuracy:**Vertical\_Positional\_Accuracy\_Report:*

The mission objective is to produce digital topographic map products with  $\leq 16$  m absolute vertical height accuracy and  $\leq 10$  m relative vertical height accuracy. All accuracies are quoted at the 90% level, consistent with National Map Accuracy Standards.

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*Publication\_Date:* 2002

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*Originator:* Jet Propulsion Laboratory

*Publication\_Date:* 2002

*Title:* JPL Processing

*Online\_Linkage:* <ftp://edcsgs9.cr.usgs.gov/pub/srtm>

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*Process\_Description:*  
 SRTM data is being processed in a systematic fashion using the SRTM Ground Data Processing System (GDPS) supercomputer system at the Jet Propulsion Laboratory. Data are being mosaicked into approximately 14,000 one degree by one degree cells and formatted according to the Digital Terrain Elevation Data (DTED) specification for delivery to NGA, who will use it to update and extend their DTED products. Data are being processed on a continent-by-continent basis beginning with North America. NGA will apply several post-processing steps to these data including editing, spike and well removal, water body leveling and coastline definition. Following these "finishing" steps data will be returned to NASA for distribution to the scientific and civil user communities, as well as the public.

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*Ending\_Date:* 20020222

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*Publication\_Date:* 2002

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*Source\_Citation:*

*Citation\_Information:*

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U.S. Geological Survey, The National Center for Earth Resources Observation and Science (EROS)

*Publication\_Date:* 2004

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*Process\_Step:*

*Process\_Description:*

SRTM data is being processed in a systematic fashion using the SRTM Ground Data Processing System (GDPS) supercomputer system at the Jet Propulsion Laboratory. Data are being mosaicked into approximately 14,000 one degree by one degree cells and formatted according to the Digital Terrain Elevation Data (DTED) specification for delivery to NGA, who will use it to update and extend their DTED products. Data are being processed on a continent-by-continent basis beginning with North America. NGA will apply several post-processing steps to these data including editing, spike and well removal, water body leveling and coastline definition. Following these "finishing" steps data will be returned to NASA for distribution to the scientific and civil user communities, as well as the public.

one degree "cells". The edges of each cell are matched with the edges of adjacent cells to assure continuity.

*Source\_Used\_Citation\_Abbreviation:* JPL 2002

*Process\_Date:* 2002

*Source\_Produced\_Citation\_Abbreviation:* NGA 2003

*Process\_Contact:*

*Contact\_Information:*

*Contact\_Organization\_Primary:*

*Contact\_Organization:*

National Aeronautics and Space Administration (NASA) Jet Propulsion Lab (JPL)

*Contact\_Position:* N/A

*Contact\_Address:*

*Address\_Type:* mailing address

*Address:* 4800 Oak Grove Drive

*City:* Pasadena

*State\_or\_Province:* CA

*Postal\_Code:* 91009

*Country:* USA

*Contact\_Voice\_Telephone:* (818) 354-4321

*Contact\_Facsimile\_Telephone:* n/a

*Contact\_Electronic\_Mail\_Address:* n/a

*Contact\_Instructions:* <[http://www.jpl.nasa.gov/about\\_JPL/](http://www.jpl.nasa.gov/about_JPL/)>

*Process\_Step:*

*Process\_Description:*

Process SRTM data to a digital surface model in grid format. To complete this step run SRTM2DSM\_3\_DTED.AML which renames the data files, creates a GRID, defines projection as geographic with WGS84 datum, project grid from decimal seconds to decimal degrees, and converts to real data type.

*Source\_Used\_Citation\_Abbreviation:* NGA 2003

*Process\_Date:* 2002

*Source\_Produced\_Citation\_Abbreviation:* EROS 2003

*Process\_Contact:*

*Contact\_Information:*

*Contact\_Organization\_Primary:*

*Contact\_Organization:* National Geospatial-Intelligence Agency

*Contact\_Position:* n/a

*Contact\_Address:*

*Address\_Type:* mailing address

*Address:* n/a

*City:* Bethesda

*State\_or\_Province:* MD

*Postal\_Code:* 20816-5003

*Contact\_Voice\_Telephone:* (818) 354-4321

*Contact\_Facsimile\_Telephone:* n/a

*Contact\_Electronic\_Mail\_Address:* n/a

*Contact\_Instructions:* <<http://www.nga.mil/>>

*Process\_Step:*

*Process\_Description:*

The metadata was imported and updated for display through the Seamless Data Distribution System.

*Process\_Date:* 2004

*Process\_Contact:*

*Contact\_Information:*

*Contact\_Organization\_Primary:**Contact\_Organization:* National Center for Earth Resources Observation and Science*Contact\_Position:* Customer Service Representative*Contact\_Address:**Address\_Type:* mailing and physical address*Address:* National Center for Earth Resources Observation and Science*City:* Sioux Falls*State\_or\_Province:* SD*Postal\_Code:* 57198*Country:* USA*Contact\_Voice\_Telephone:* 605-594-6151*Contact\_TDD/TTY\_Telephone:* 605-594-6933*Contact\_Facsimile\_Telephone:* 605-594-6589*Contact\_Electronic\_Mail\_Address:* custserv@usgs.gov*Hours\_of\_Service:* 8-4 CT, M-F*Spatial\_Data\_Organization\_Information:**Direct\_Spatial\_Reference\_Method:* Raster*Raster\_Object\_Information:**Raster\_Object\_Type:* Pixel*Row\_Count:* 270000*Column\_Count:* 1296000*Vertical\_Count:* 1*Spatial\_Reference\_Information:**Horizontal\_Coordinate\_System\_Definition:**Geographic:**Latitude\_Resolution:* 1.000000*Longitude\_Resolution:* 1.000000*Geographic\_Coordinate\_Units:* Decimal degrees*Geodetic\_Model:**Horizontal\_Datum\_Name:* D\_WGS\_1984*Ellipsoid\_Name:* WGS\_1984*Semi-major\_Axis:* 6378137.000000*Denominator\_of\_Flattening\_Ratio:* 298.257224*Vertical\_Coordinate\_System\_Definition:**Altitude\_System\_Definition:**Altitude\_Datum\_Name:* N/A*Altitude\_Resolution:* 1.000000*Altitude\_Distance\_Units:* meters*Altitude\_Encoding\_Method:*

Explicit elevation coordinate included with horizontal coordinates

*Entity\_and\_Attribute\_Information:**Overview\_Description:**Entity\_and\_Attribute\_Overview:* N/A*Entity\_and\_Attribute\_Detail\_Citation:* N/A*Distribution\_Information:**Distributor:**Contact\_Information:**Contact\_Organization\_Primary:*

*Contact\_Organization:*

The National Center for Earth Resources Observation and Science (EROS)

*Contact\_Position:* Customer Services Representative

*Contact\_Address:*

*Address\_Type:* mailing and physical address

*Address:*

U.S. Geological Survey, The National Center for Earth Resources Observation and Science (EROS)

*City:* Sioux Falls

*State\_or\_Province:* SD

*Postal\_Code:* 57198

*Country:* USA

*Contact\_Voice\_Telephone:* 605-594-6151

*Contact\_TDD/TTY\_Telephone:* 605-594-6933

*Contact\_Facsimile\_Telephone:* 605-594-6589

*Contact\_Electronic\_Mail\_Address:* custserv@usgs.gov

*Hours\_of\_Service:* 8-4 CT, M-F

*Resource\_Description:* Downloadable Data

*Distribution\_Liability:*

Although these data have been processed successfully on a computer system at the U.S. Geological Survey, The National Center for Earth Resources Observation and Science (EROS), no warranty expressed or implied is made by either regarding the utility of the data on any system, nor shall the act of distribution constitute any such warranty. The USGS will warrant the delivery of this product in computer-readable format and will offer appropriate adjustment of credit when the product is determined unreadable by correctly adjusted computer peripherals, or when the physical medium is delivered in damaged condition. Requests for adjustments of credit must be made within 90 days from the date of this shipment from the ordering site.

*Standard\_Order\_Process:*

*Digital\_Form:*

*Digital\_Transfer\_Information:*

*Format\_Name:* ARCE

*Transfer\_Size:* 1.000

*Digital\_Transfer\_Option:*

*Online\_Option:*

*Computer\_Contact\_Information:*

*Network\_Address:*

*Network\_Resource\_Name:* <<http://seamless.usgs.gov>>

*Fees:* None

*Metadata\_Reference\_Information:*

*Metadata\_Date:* 20050330

*Metadata\_Contact:*

*Contact\_Information:*

*Contact\_Organization\_Primary:*

*Contact\_Organization:*

The National Center for Earth Resources Observation and Science (EROS)

*Contact\_Position:* Customer Services Representative

*Contact\_Address:*

*Address\_Type:* mailing and physical address

*Address:*

U.S. Geological Survey, The National Center for Earth Resources Observation and Science (EROS)

*City:* Sioux Falls

*State\_or\_Province:* SD

Postal\_Code: 57198  
 Country: USA  
 Contact\_Voice\_Telephone: 605-594-6151  
 Contact\_TDD/TTY\_Telephone: 605-594-6933  
 Contact\_Facsimile\_Telephone: 605-594-6589  
 Contact\_Electronic\_Mail\_Address: custserv@usgs.gov  
 Hours\_of\_Service: 8-4 CT, M-F  
 Metadata\_Standard\_Name: FGDC Content Standards for Digital Geospatial Metadata  
 Metadata\_Standard\_Version: FGDC-STD-001-1998  
 Metadata\_Time\_Convention: local time  
 Metadata\_Access\_Constraints: None  
 Metadata\_Use\_Constraints: None  
 Metadata\_Security\_Information:  
 Metadata\_Security\_Classification\_System: N/A  
 Metadata\_Security\_Classification: Unclassified  
 Metadata\_Security\_Handling\_Description: N/A  
 Metadata\_Extensions:  
 Online\_Linkage: <<http://www.esri.com/metadata/esriprof80.html>>  
 Profile\_Name: ESRI Metadata Profile

Generated by **ME** version 2.8.6 on Wed Mar 30 14:29:24 2005

## Part 2: Tile-Specific Metadata

### Tile: 01074556

#### Environment:

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N38W030  | -80.000138889 | 37.999361111 | -78.999361111 | 39.000138889 | 253  | 1484 | 192.593676758 | 235.019210815 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:16:19 Thursday |
| N39W079  | -79.000138889 | 38.999361111 | -77.999361111 | 40.000138889 | 101  | 1017 | 371.049438477 | 163.559765991 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:38:12 Thursday |
| N38W078  | -78.000138889 | 37.999361111 | -76.999361111 | 39.000138889 | -21  | 570  | 36.738952637  | 52.366630554  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |
| N39W080  | -80.000138889 | 38.999361111 | -78.999361111 | 40.000138889 | 216  | 1273 | 638.807982398 | 194.185089111 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:40:58 Thursday |
| N38W079  | -79.000138889 | 37.999361111 | -77.999361111 | 39.000138889 | 43   | 1227 | 353.119232178 | 196.984664917 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |
| N39W078  | -78.000138889 | 38.999361111 | -76.999361111 | 40.000138889 | -8   | 748  | 190.851715088 | 96.483070374  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |

#### Spatial\_Domain:

##### Bounding Coordinates:

West\_Bounding\_Coordinate:-79.19915144

East\_Bounding\_Coordinate:-77.63897197

North\_Bounding\_Coordinate:39.72993205

South\_Bounding\_Coordinate:38.5535064

### Tile: 07949871

#### Environment:

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N40W079  | -79.000138889 | 39.999361111 | -77.999361111 | 41.000138889 | 167  | 959  | 502.530302955 | 128.651092529 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:06:01 Thursday |
| N40W078  | -78.000138889 | 39.999361111 | -76.999361111 | 41.000138889 | 83   | 755  | 312.265228272 | 130.6118927   | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:03:30 Thursday |
| N39W079  | -79.000138889 | 38.999361111 | -77.999361111 | 40.000138889 | 101  | 1017 | 371.049438477 | 163.559765991 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:38:12 Thursday |
| N39W078  | -78.000138889 | 38.999361111 | -76.999361111 | 40.000138889 | -8   | 748  | 190.851715088 | 96.483070374  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |

#### Spatial\_Domain:

##### Bounding Coordinates:

West\_Bounding\_Coordinate:-78.98351648

East\_Bounding\_Coordinate:-77.0614962

North\_Bounding\_Coordinate:40.77130882

South\_Bounding\_Coordinate:39.78934207

**Title: 08865688****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N41W079  | -79.000138889 | 39.999861111 | -77.999861111 | 42.000138889 | 219  | 770  | 555.802121023 | 85.165904184  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:36:49 Thursday |
| N41W078  | -78.000138889 | 39.999861111 | -76.999861111 | 42.000138889 | 144  | 803  | 507.040357861 | 133.582511353 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:33:36 Thursday |
| N40W079  | -79.000138889 | 39.999861111 | -77.999861111 | 41.000138889 | 167  | 959  | 502.530309555 | 128.651092529 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:08:01 Thursday |
| N40W078  | -78.000138889 | 39.999861111 | -76.999861111 | 41.000138889 | 83   | 755  | 312.265228272 | 136.6118927   | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:03:30 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:****West\_Bounding\_Coordinate:-78.98351648****East\_Bounding\_Coordinate:-77.0614962****North\_Bounding\_Coordinate:41.75327557****South\_Bounding\_Coordinate:40.77130882****Title: 15731280****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N38W080  | -80.000138889 | 37.999861111 | -78.999861111 | 39.000138889 | 253  | 1484 | 792.393676758 | 235.019210815 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:16:19 Thursday |
| N37W078  | -78.000138889 | 36.999861111 | -76.999861111 | 38.000138889 | -76  | 168  | 62.799665544  | 29.547678284  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:54:10 Thursday |
| N38W078  | -78.000138889 | 37.999861111 | -76.999861111 | 39.000138889 | -21  | 570  | 86.738952637  | 52.366630551  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:11:54 Thursday |
| N37W079  | -79.000138889 | 36.999861111 | -77.999861111 | 38.000138889 | 41   | 1207 | 167.454559326 | 89.441680908  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:56:13 Thursday |
| N37W080  | -80.000138889 | 36.999861111 | -78.999861111 | 38.000138889 | 115  | 1290 | 399.801086426 | 192.210281372 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:58:15 Thursday |
| N38W079  | -79.000138889 | 37.999861111 | -77.999861111 | 39.000138889 | 43   | 1237 | 332.119232178 | 156.954664917 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:****West\_Bounding\_Coordinate:-79.19915144****East\_Bounding\_Coordinate:-77.63897197****North\_Bounding\_Coordinate:38.5535064****South\_Bounding\_Coordinate:37.37708076****Title: 27472325****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N41W081  | -81.000138889 | 40.999861111 | -79.999861111 | 42.000138889 | 170  | 521  | 325.30392456  | 65.855337197  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:42:59 Thursday |
| N41W080  | -80.000138889 | 40.999861111 | -78.999861111 | 42.000138889 | 248  | 694  | 462.767119141 | 58.314289093  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:39:49 Thursday |
| N41W079  | -79.000138889 | 39.999861111 | -77.999861111 | 42.000138889 | 219  | 770  | 555.802121023 | 85.165904184  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:36:49 Thursday |
| N40W081  | -81.000138889 | 39.999861111 | -79.999861111 | 41.000138889 | 174  | 484  | 341.692932129 | 40.372882843  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:10:53 Thursday |
| N40W080  | -80.000138889 | 39.999861111 | -78.999861111 | 41.000138889 | 158  | 912  | 401.52938081  | 109.982542945 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:08:26 Thursday |
| N40W079  | -79.000138889 | 39.999861111 | -77.999861111 | 41.000138889 | 167  | 959  | 502.530309555 | 128.651092529 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:06:01 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:****West\_Bounding\_Coordinate:-80.90553677****East\_Bounding\_Coordinate:-78.98351648****North\_Bounding\_Coordinate:41.75327557****South\_Bounding\_Coordinate:40.77130882****Title: 28901439****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX          | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|---------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N38W079  | -79.000138889 | 37.999861111 | -77.999861111 | 39.000138889 | 43   | 1227 | 332.119232178 | 156.954664917 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |
| N38W078  | -78.000138889 | 37.999861111 | -76.999861111 | 39.000138889 | -21  | 570  | 86.738952637  | 52.366630554  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |
| N37W079  | -79.000138889 | 36.999861111 | -77.999861111 | 38.000138889 | 41   | 1207 | 167.454559326 | 89.441680908  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:56:13 Thursday |
| N37W078  | -78.000138889 | 36.999861111 | -76.999861111 | 38.000138889 | -76  | 168  | 62.799665544  | 29.547678284  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:54:10 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:****West\_Bounding\_Coordinate:-78.4112977****East\_Bounding\_Coordinate:-77.201711****North\_Bounding\_Coordinate:38.37501159****South\_Bounding\_Coordinate:37.26956149**

**Title: 43140235****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX         | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|--------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N35W080  | -80.000138889 | 37.999861111 | 78.999361111 | 39.000138889 | 253  | 1484 | 792.393676758 | 235.019210815 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:16:19 Thursday |
| N35W081  | -81.000138889 | 37.999861111 | 79.999361111 | 39.000138889 | 204  | 1479 | 679.328491211 | 267.112762451 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:18:34 Thursday |
| N33W081  | -81.000138889 | 36.999861111 | 79.999361111 | 38.000138889 | 286  | 1226 | 690.018371582 | 130.921182861 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:03:21 Thursday |
| N33W080  | -80.000138889 | 36.999861111 | 78.999361111 | 38.000138889 | 115  | 1290 | 399.801086426 | 192.210281372 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:58:15 Thursday |

**Spatial Domain:****Bounding Coordinates:***West\_Bounding\_Coordinate:*-80.75933091*East\_Bounding\_Coordinate:*-79.19915144*North\_Bounding\_Coordinate:*38.5535064*South\_Bounding\_Coordinate:*37.37708076**Title: 44841636****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX         | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|--------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N39W081  | -81.000138889 | 38.999861111 | 79.999361111 | 40.000138889 | 176  | 711  | 366.923156738 | 61.572605133  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:56 Thursday |
| N39W080  | -80.000138889 | 37.999861111 | 78.999361111 | 39.000138889 | 253  | 1484 | 792.393676758 | 235.019210815 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:16:19 Thursday |
| N35W081  | -81.000138889 | 37.999861111 | 79.999361111 | 39.000138889 | 204  | 1479 | 679.328491211 | 267.112762451 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:18:34 Thursday |
| N39W080  | -80.000138889 | 38.999861111 | 78.999361111 | 40.000138889 | 216  | 1333 | 638.807983398 | 194.185089111 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:40:58 Thursday |

**Spatial Domain:****Bounding Coordinates:***West\_Bounding\_Coordinate:*-80.75933091*East\_Bounding\_Coordinate:*-79.19915144*North\_Bounding\_Coordinate:*39.72993205*South\_Bounding\_Coordinate:*38.5535064**Title: 50333339****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX         | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|--------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N39W077  | -77.000138889 | 38.999861111 | 75.999361111 | 40.000138889 | -57  | 375  | 110.979217529 | 83.311721802  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:31:54 Thursday |
| N40W077  | -77.000138889 | 39.999861111 | 75.999361111 | 41.000138889 | 12   | 641  | 224.42086792  | 108.811568396 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:00:58 Thursday |
| N40W078  | -78.000138889 | 39.999861111 | 76.999361111 | 41.000138889 | 83   | 755  | 312.265228272 | 130.6118927   | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:03:20 Thursday |
| N39W078  | -78.000138889 | 38.999861111 | 76.999361111 | 40.000138889 | -8   | 748  | 190.651715088 | 96.487070374  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |

**Spatial Domain:****Bounding Coordinates:***West\_Bounding\_Coordinate:*-77.19859874*East\_Bounding\_Coordinate:*-76.5946583*North\_Bounding\_Coordinate:*40.15772319*South\_Bounding\_Coordinate:*39.04420801**Title: 69642906****Environment:**

| COVERAGE | XMIN          | YMIN         | XMAX         | YMAX         | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|---------------|--------------|--------------|--------------|------|------|---------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N39W079  | -79.000138889 | 38.999861111 | 77.999361111 | 40.000138889 | 101  | 1017 | 371.049438477 | 163.550765991 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:28:12 Thursday |
| N39W078  | -78.000138889 | 38.999861111 | 76.999361111 | 40.000138889 | -8   | 748  | 190.651715088 | 96.487070374  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |
| N38W079  | -79.000138889 | 37.999861111 | 77.999361111 | 39.000138889 | 43   | 1227 | 353.119232178 | 196.984664917 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |
| N39W078  | -78.000138889 | 37.999861111 | 76.999361111 | 39.000138889 | -21  | 570  | 86.738952637  | 52.366630554  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |

**Spatial Domain:****Bounding Coordinates:***West\_Bounding\_Coordinate:*-78.4112977*East\_Bounding\_Coordinate:*-77.201711*North\_Bounding\_Coordinate:*39.48046168*South\_Bounding\_Coordinate:*38.37501159

**Title: 72948997****Environment:**

| COVERAGE | XMIN         | YMIN        | XMAX         | YMAX        | ZMIN | ZMAX | ZMEAN         | ZSIGMA       | ZUNITS | RESOLUTION | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|--------------|-------------|--------------|-------------|------|------|---------------|--------------|--------|------------|--------|-------------|-----------------------------|
| N39W078  | -78.00013889 | 38.99986111 | -76.99986111 | 40.00013889 | -8   | 748  | 190.851715088 | 96.483070374 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |
| N39W077  | -77.00013889 | 38.99986111 | -75.99986111 | 40.00013889 | -37  | 525  | 110.979217529 | 83.311721802 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:31:54 Thursday |
| N39W076  | -76.00013889 | 38.99986111 | -74.99986111 | 40.00013889 | -48  | 274  | 33.887851715  | 44.382086634 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:29:07 Thursday |
| N38W078  | -78.00013889 | 37.99986111 | -76.99986111 | 39.00013889 | -21  | 570  | 36.738932637  | 32.366630554 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |
| N38W077  | -77.00013889 | 37.99986111 | -75.99986111 | 39.00013889 | -44  | 119  | 17.275043488  | 21.887937836 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:09:17 Thursday |
| N38W076  | -76.00013889 | 37.99986111 | -74.99986111 | 39.00013889 | -35  | 51   | 8.724813652   | 7.574468613  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:05:55 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:***West\_Bounding\_Coordinate:*-77.201711*East\_Bounding\_Coordinate:*-75.9921243*North\_Bounding\_Coordinate:*39.48046168*South\_Bounding\_Coordinate:*38.37501159**Title: 75513725****Environment:**

| COVERAGE | XMIN         | YMIN        | XMAX         | YMAX        | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|--------------|-------------|--------------|-------------|------|------|---------------|---------------|--------|------------|--------|-------------|-----------------------------|
| N40W081  | -81.00013889 | 39.99986111 | -79.99986111 | 41.00013889 | 174  | 484  | 341.692932129 | 40.372882843  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:10:53 Thursday |
| N40W080  | -80.00013889 | 39.99986111 | -78.99986111 | 41.00013889 | 138  | 913  | 401.33908681  | 100.982542945 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:08:26 Thursday |
| N40W079  | -79.00013889 | 39.99986111 | -77.99986111 | 41.00013889 | 167  | 949  | 502.530307955 | 128.651092529 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 10:06:01 Thursday |
| N39W081  | -81.00013889 | 38.99986111 | -79.99986111 | 40.00013889 | 176  | 714  | 360.923156738 | 61.572605133  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:44:06 Thursday |
| N39W080  | -80.00013889 | 38.99986111 | -78.99986111 | 40.00013889 | 216  | 1233 | 638.807983398 | 194.185089111 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:40:58 Thursday |
| N39W079  | -79.00013889 | 38.99986111 | -77.99986111 | 40.00013889 | 191  | 1017 | 371.049438477 | 163.550765991 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:38:12 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:***West\_Bounding\_Coordinate:*-80.90553677*East\_Bounding\_Coordinate:*-78.98351648*North\_Bounding\_Coordinate:*40.77130882*South\_Bounding\_Coordinate:*39.78934207**Title: 86264021****Environment:**

| COVERAGE | XMIN         | YMIN        | XMAX         | YMAX        | ZMIN | ZMAX | ZMEAN        | ZSIGMA       | ZUNITS | RESOLUTION | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|--------------|-------------|--------------|-------------|------|------|--------------|--------------|--------|------------|--------|-------------|-----------------------------|
| N38W078  | -78.00013889 | 37.99986111 | -76.99986111 | 39.00013889 | -21  | 570  | 36.738932637 | 32.366630554 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |
| N38W077  | -77.00013889 | 37.99986111 | -75.99986111 | 39.00013889 | -44  | 119  | 17.275043488 | 21.887937836 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:09:17 Thursday |
| N38W076  | -76.00013889 | 37.99986111 | -74.99986111 | 39.00013889 | -35  | 51   | 8.724813652  | 7.574468613  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:07:55 Thursday |
| N37W078  | -78.00013889 | 36.99986111 | -76.99986111 | 38.00013889 | -76  | 168  | 62.799663544 | 29.513678384 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:51:10 Thursday |
| N37W077  | -77.00013889 | 36.99986111 | -75.99986111 | 38.00013889 | -44  | 69   | 13.262137413 | 15.141789575 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:51:54 Thursday |
| N37W076  | -76.00013889 | 36.99986111 | -74.99986111 | 38.00013889 | -47  | 89   | 1.281360626  | 4.040606976  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 08:50:06 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:***West\_Bounding\_Coordinate:*-77.201711*East\_Bounding\_Coordinate:*-75.9921243*North\_Bounding\_Coordinate:*38.37501159*South\_Bounding\_Coordinate:*37.26956149**94076717****Environment:**

| COVERAGE | XMIN         | YMIN        | XMAX         | YMAX        | ZMIN | ZMAX | ZMEAN         | ZSIGMA        | ZUNITS | RESOLUTION | IDATUM | VDATUM      | TIMESTAMP                   |
|----------|--------------|-------------|--------------|-------------|------|------|---------------|---------------|--------|------------|--------|-------------|-----------------------------|
| N39W081  | -81.00013889 | 38.99986111 | -79.99986111 | 40.00013889 | 176  | 714  | 360.923156738 | 61.572605133  | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:44:06 Thursday |
| N39W080  | -80.00013889 | 38.99986111 | -78.99986111 | 40.00013889 | 216  | 1233 | 638.807983398 | 194.185089111 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:40:58 Thursday |
| N39W079  | -79.00013889 | 38.99986111 | -77.99986111 | 40.00013889 | 191  | 1017 | 371.049438477 | 163.550765991 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:38:12 Thursday |
| N38W081  | -81.00013889 | 37.99986111 | -79.99986111 | 39.00013889 | 204  | 1479 | 679.328491211 | 267.112762451 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:18:34 Thursday |
| N38W080  | -80.00013889 | 37.99986111 | -78.99986111 | 39.00013889 | 253  | 1484 | 792.393576758 | 235.019210815 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:16:19 Thursday |
| N38W079  | -79.00013889 | 37.99986111 | -77.99986111 | 39.00013889 | 43   | 1227 | 333.119232178 | 196.984664917 | METERS | 0.00027778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |

**Spatial\_Domain:****Bounding\_Coordinates:***West\_Bounding\_Coordinate:*-80.90553677*East\_Bounding\_Coordinate:*-78.98351648*North\_Bounding\_Coordinate:*39.78934207*South\_Bounding\_Coordinate:*38.80737532

**95780076****Environment:**

| COVERAGE | XMIN         | YMIN         | XMAX          | YMAX        | ZMIN | ZMAX | ZMEAN          | ZSIGMA        | ZUNITS | RESOLUTION  | HDATUM | VDATUM      | TIMESTAMP                   |
|----------|--------------|--------------|---------------|-------------|------|------|----------------|---------------|--------|-------------|--------|-------------|-----------------------------|
| N39W079  | -79.00013889 | 38.999861111 | -77.999861111 | 40.00013889 | 101  | 1017 | 371.049438477  | 163.550765991 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:38:12 Thursday |
| N39W078  | -78.00013889 | 38.999861111 | -76.999861111 | 40.00013889 | 3    | 748  | 190.851715088  | 96.483070274  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:35:13 Thursday |
| N38W079  | -79.00013889 | 37.999861111 | -77.999861111 | 39.00013889 | 43   | 1227 | 352.1119232178 | 196.984664917 | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:14:07 Thursday |
| N38W078  | -78.00013889 | 37.999861111 | -76.999861111 | 39.00013889 | 21   | 870  | 36.758952637   | 52.366630554  | METERS | 0.000277778 | WGS84  | WGS84_GEOID | 11 Mar 04 09:11:54 Thursday |

*Spatial\_Domain:**Bounding\_Coordinates:**West\_Bounding\_Coordinate:-78.98351648**East\_Bounding\_Coordinate:-77.0614962**North\_Bounding\_Coordinate:39.78934207**South\_Bounding\_Coordinate:38.80737532*

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[illegible]

To search on a specific station identifier, use your browser's search mode

| USGS station id | Station name                                 | fix1 | fix2 | lat | syn1 | syn2 | syn3 |
|-----------------|----------------------------------------------|------|------|-----|------|------|------|
| 01654900        | Accatunk Creek near Amantide, VA             |      |      |     |      |      |      |
| 01654994        | Alloway Creek near Lamey, MD                 |      |      |     |      |      |      |
| 01651010        | Anacostia River near Bladenbur, MD           |      |      |     |      |      |      |
| 01651900        | Anientam Creek near Sharpsbur, MD            |      |      |     |      |      |      |
| 01660350        | Anima Creek near Garrisonville, VA           |      |      |     |      |      |      |
| 01639462        | Beor Brook near Frazierburg, MD              |      |      |     |      |      |      |
| 01643820        | Bearcreek Creek near Union, VA               |      |      |     |      |      |      |
| 01643600        | Benedict Creek near Hyattstown, MD           |      |      |     |      |      |      |
| 01659460        | Bl Pipe Creek at Bachman Mills, MD           |      |      |     |      |      |      |
| 01652095        | Black Run at Rawley Sprin, S, VA             |      |      |     |      |      |      |
| 01621400        | Black's Run at Harrisburg, VA                |      |      |     |      |      |      |
| 01643615        | Broad Run at Elman, MD                       |      |      |     |      |      |      |
| 01637920        | Broad Run near Jefferson, MD                 |      |      |     |      |      |      |
| 01635945        | Bottle Marsh Run near Middleton, VA          |      |      |     |      |      |      |
| 01656725        | Bull Run near Catheys, VA                    |      |      |     |      |      |      |
| 01657100        | Bull Run near Manassas, VA                   |      |      |     |      |      |      |
| 01656460        | Bullskin Run above Kabletown, WV             |      |      |     |      |      |      |
| 01664630        | Cabin John Creek at Rockville, MD            |      |      |     |      |      |      |
| 01611560        | Cameron River near Grant Casapton, WV        |      |      |     |      |      |      |
| 01642200        | Carroll Creek at Frederick, MD               |      |      |     |      |      |      |
| 016538050       | Cascades Creek at Olive, MD                  |      |      |     |      |      |      |
| 01653840        | Cascades Creek at Taylorsboro, VA            |      |      |     |      |      |      |
| 01614110        | Connecticut ne Creek trib near Faysville, PA |      |      |     |      |      |      |
| 01616450        | Connecticut ne Creek at Fairview, MD         |      |      |     |      |      |      |

[illegible]



# Potomac N WQ : Stream site locations

Table is in alphabetical order by stream name. To search on a specific stream identifier, use your browser's search mode.

| USGS station ID | Station name                                  | Latitude (DNMS) | Longitude (DNMS) | State code (FIPS) | County code (FIPS) |
|-----------------|-----------------------------------------------|-----------------|------------------|-------------------|--------------------|
| 01654000        | Accomac Cr. kn at Anandall, VA                | 384846          | 0771343          | 51                | 059                |
| 01638984        | Albany Cr. kn at Elm s, MD                    | 394349          | 0770915          | 42                | 001                |
| 01651010        | Anacostia Riv r at Blad rburg, MD             | 383525          | 0765620          | 24                | 023                |
| 01619500        | Anti am Cr. kn at Sharpsburg, MD              | 392761          | 0774552          | 24                | 043                |
| 01660350        | Aquia Cr. kn at Groesbeville, VA              | 382065          | 0772910          | 51                | 179                |
| 01650462        | B. ar Branch n ar Fritz lburg, MD             | 393753          | 0770438          | 24                | 013                |
| 01643820        | B. ar rdam Cr. kn at Union, VA                | 390235          | 0774601          | 51                | 107                |
| 01643360        | B. na tt Cr. kn at Hyattsville, MD            | 391831          | 0771755          | 24                | 021                |
| 01659400        | Big Pp. Cr. kn at Buchanan Mills, MD          | 393939          | 0766654          | 24                | 013                |
| 01650985        | Black Run at Rawl y Springs, VA               | 383030          | 0790331          | 51                | 165                |
| 01651400        | Black Run at Harrisonburg, VA                 | 382552          | 0785302          | 51                | 060                |
| 01643615        | Broad Run at Elm s, MD                        | 390722          | 0772852          | 24                | 021                |
| 01657950        | Broad Run at J. ff rson, MD                   | 392260          | 0773512          | 24                | 021                |
| 01655045        | Buffalo Marsh Run n ar Middl town, VA         | 390734          | 0781817          | 51                | 069                |
| 01656725        | Bull Run n at Culhorna, VA                    | 385321          | 0773414          | 51                | 153                |
| 01657000        | Bull Run n at Manassas, VA                    | 394752          | 0772728          | 51                | 059                |
| 01653460        | Bulliken Run abv. Kobl town, WV               | 391310          | 0775159          | 54                | 027                |
| 01646350        | Cabin John Cr. k at Rockvill, MD              | 390321          | 0770906          | 24                | 021                |
| 01611500        | Cacapon Riv. n ar Cr. at Cacapon, WV          | 393443          | 0781834          | 54                | 065                |
| 01642000        | Carroll Cr. kn at Fr. d rock, MD              | 392564          | 0772534          | 24                | 021                |
| 01638030        | Carocin Cr. kn at Oliv., MD                   | 391956          | 0773445          | 24                | 021                |
| 01638180        | Carocin Cr. kn at Taylorsville, VA            | 391518          | 0773436          | 51                | 107                |
| 01614110        | Conocochee agv. Cr. k Trk at Pay tt vill., PA | 395441          | 0773418          | 42                | 025                |
| 01614500        | Conocochee agv. Cr. k at Farvi w, MD          | 394257          | 0774928          | 24                | 043                |
| 01613082        | Cov. Run at Warfordsburg, PA                  | 394545          | 0781107          | 42                | 027                |
| 01643705        | Cromw. II Run n at Anoka, VA                  | 385551          | 0774836          | 51                | 061                |

|          |                                                           |        |         |    |     |
|----------|-----------------------------------------------------------|--------|---------|----|-----|
| 01656870 | Cub Run at Old L. Rd. n ar Chantilly, VA                  | 385256 | 0772813 | 51 | 059 |
| 01613090 | Cummins Run n ar N. denor, PA                             | 395249 | 0780842 | 42 | 057 |
| 01643725 | Driftcult Run n ar Vi. na, VA                             | 385411 | 0771908 | 51 | 059 |
| 01619990 | Dillon Run at Capon Bridg., WV                            | 391730 | 0782640 | 54 | 027 |
| 01605800 | Dry Run n ar Ch. m. Gov., WV                              | 383720 | 0793215 | 54 | 071 |
| 01614130 | Falling Spring at Chando rburg, PA                        | 395021 | 0775901 | 42 | 055 |
| 01656772 | Flat Branch at Manassas Park, VA                          | 394054 | 0772913 | 51 | 153 |
| 01659380 | Flat Run at Emmisburg, MD                                 | 394259 | 0771919 | 24 | 021 |
| 01656920 | Flatlick Branch n ar Chantilly, VA                        | 385203 | 0772751 | 51 | 059 |
| 01634670 | Folly Mills Cr. kn at Staunton, VA                        | 380542 | 0790515 | 51 | 015 |
| 01652370 | Fourmi. Run at Arlington, VA                              | 385204 | 0770740 | 51 | 013 |
| 01641930 | Glad Cr. kn at Walk rsvill, MD                            | 392814 | 0772220 | 24 | 021 |
| 01644000 | Goos Cr. kn at L. sburg, VA                               | 390110 | 0773440 | 51 | 107 |
| 01656102 | Goslin Run n ar Ad. n, VA                                 | 383640 | 0773304 | 51 | 153 |
| 01644481 | Gr. at S. n. co Cr. k at Gosh n, MD                       | 391204 | 0771216 | 24 | 031 |
| 01619200 | Hampton Cr. k at Hing rson, MD                            | 393811 | 0774216 | 24 | 045 |
| 01616215 | Happy Cr. k at Crosby Stadium at Front Royal, VA          | 385443 | 0781126 | 51 | 187 |
| 01614010 | Harlan Run n ar Spring Mills, WV                          | 393333 | 0773725 | 54 | 003 |
| 01637750 | Holmans Run at Quicksburg, VA                             | 384207 | 0784054 | 51 | 171 |
| 01605950 | Jordan Run n ar Hop vill, WV                              | 385908 | 0791559 | 54 | 023 |
| 01656655 | K. tt. Run n ar Nlk vill., VA                             | 384238 | 0773632 | 51 | 153 |
| 01610185 | Kams y Run n ar Lost Riv. r, WV                           | 385806 | 0785403 | 54 | 031 |
| 01644590 | L. ws Cr. k at Staunton, VA                               | 380903 | 0790334 | 51 | 790 |
| 01613510 | Littl. Cov. Cr. kn at Sylva, PA                           | 394424 | 0780150 | 42 | 057 |
| 01640000 | Littl. Pp. Cr. k at Arvmdal, MD                           | 393340 | 0770238 | 24 | 013 |
| 01618920 | Littl. s Run n ar G. oyburg, PA                           | 394653 | 0771144 | 42 | 001 |
| 01611205 | Majpl. Run n ar Sta. vill., WV                            | 392056 | 0783107 | 54 | 027 |
| 01617800 | Marsh Run at Grem s, MD                                   | 392053 | 0774638 | 24 | 043 |
| 01619140 | Marsh Run at R. id, MD                                    | 394237 | 0774027 | 24 | 043 |
| 01625000 | Middl. Riv. rn ar Grento s, VA                            | 381542 | 0785144 | 51 | 015 |
| 01604400 | Middl. Cr. kn at Burlington, WV                           | 392030 | 0785519 | 54 | 057 |
| 01639550 | Middl. Cr. kn at Hamburg, VA                              | 383907 | 0783042 | 51 | 139 |
| 01608300 | Mill Run n ar Romm y, WV                                  | 391809 | 0784802 | 54 | 027 |
| 01639000 | Monocacy Riv. r at Bridg. port, MD                        | 394043 | 0771406 | 24 | 021 |
| 01643020 | Monocacy Riv. r at R. ich Ford Bridg. n at Fr. d rick, MD | 392116 | 0772240 | 24 | 021 |
| 01620850 | Mussy Cr. kn at Spring Cr. k, VA                          | 382312 | 0799042 | 51 | 165 |
| 01621050 | Muddy Cr. k at Mount Clinton, VA                          | 382911 | 0785740 | 51 | 165 |

|           |                                                             |        |         |    |     |
|-----------|-------------------------------------------------------------|--------|---------|----|-----|
| 01652589  | Potomac Riv r b low Oxen Cr k at Washington, DC             | 384866 | 0770136 | 24 | 083 |
| 016546380 | Potomac Riv r at Chan Bldg, at Washington, DC               | 385546 | 0770702 | 51 | 013 |
| 01618000  | Potomac Riv r at Sh ph rd town, WV                          | 352604 | 0774807 | 54 | 037 |
| 01652588  | Potomac Riv r n at Al sandra, VA                            | 384902 | 0770218 | 11 | 001 |
| 01618200  | Rail snak Run n ar Sh ph rd town, WV                        | 352401 | 0774629 | 54 | 037 |
| 01638450  | Richard Cr k n ar War rd, MD                                | 381303 | 0773750 | 51 | 107 |
| 01614525  | Rockall Run at Fines w, MD                                  | 384207 | 0775045 | 24 | 043 |
| 01640155  | Same Cr k n ar Union Bldg, MD                               | 383215 | 0771016 | 24 | 013 |
| 01506500  | Savag Riv r n ar Barton, MD                                 | 383405 | 0790610 | 24 | 023 |
| 01605900  | Sen Cr k n ar On go, WV                                     | 385133 | 0792817 | 54 | 071 |
| 01616500  | Sh nendish Riv r at Millkill, WV                            | 381655 | 0774722 | 54 | 037 |
| 01631700  | Sho nak r Riv r n ar Pikes Run, VA                          | 383825 | 0785318 | 51 | 165 |
| 01639440  | Shv r Run n at Silv r Run, MD                               | 384038 | 0770537 | 24 | 013 |
| 01650900  | Sligo Cr k at Takoma Park, MD                               | 385859 | 0770002 | 24 | 031 |
| 01606500  | South Branch Potomac Riv r n ar P r rching, WV              | 385928 | 0791034 | 54 | 023 |
| 01608500  | South Branch Potomac Riv r n ar Springf id, WV              | 382649 | 0783916 | 54 | 027 |
| 01642425  | South Fork Lingnor Cr k at Lingnor, MD                      | 382425 | 0771240 | 24 | 021 |
| 01606600  | South Fork Lunc Cr k n ar Maywall, WV                       | 380407 | 0790734 | 54 | 023 |
| 01658500  | South Fork Quantico Cr k n ar Ind p id nt Hill, VA          | 383514 | 0772544 | 51 | 153 |
| 01631000  | South Fork Sh nendish Riv r at Front Royal, VA              | 385450 | 0781240 | 51 | 187 |
| 01629500  | South Fork Sh nendish Riv r n ar Lumpy, VA                  | 383846 | 0783206 | 51 | 139 |
| 01631020  | South Fork Sh nendish Riv r Bl Cabin Run at Front Royal, VA | 385615 | 0781252 | 51 | 187 |
| 01608700  | South Fork South Branch Potomac Riv r n ar Moor h id, WV    | 386044 | 0785723 | 54 | 031 |
| 01627500  | South Riv r at Harrison, VA                                 | 381307 | 0785013 | 51 | 015 |
| 01611120  | Sp rry Run at Rio, WV                                       | 380802 | 0783932 | 54 | 027 |
| 01661050  | St Cl m nt Cr k n at Cl m mts, MD                           | 382000 | 0764031 | 24 | 037 |
| 01611130  | T ar Coal Cr k n ar Rio, WV                                 | 381303 | 0784050 | 54 | 027 |
| 01605400  | Thorn Cr k n ar Martinsburg, WV                             | 383227 | 0792154 | 54 | 071 |

|            |                                                  |        |         |    |     |
|------------|--------------------------------------------------|--------|---------|----|-----|
| 0165101710 | SW-44 Maddy Cr k Flowpath study, VA              | 383213 | 0785237 | 51 | 165 |
| 0165101730 | SW-45 Centu nc J Muddy Cr k Flowpath study, VA   | 383211 | 0785721 | 51 | 165 |
| 0165101750 | SW-03 Maddy Cr k Flowpath study, VA              | 383265 | 0785715 | 51 | 165 |
| 0165101776 | SW-42 Maddy Cr k Flowpath study, VA              | 383262 | 0785712 | 51 | 165 |
| 0165101790 | SW-01 Maddy Cr k Flowpath study, VA              | 383152 | 0785709 | 51 | 165 |
| 01608150   | Madlock Run n ar Moor h id, WV                   | 380824 | 0785635 | 54 | 031 |
| 01638740   | Mannaburg Run n ar G usburg, PA                  | 385149 | 0771223 | 42 | 001 |
| 01650960   | North Branch Choptank Cr k n ar Berlin, VA       | 383358 | 0772548 | 51 | 179 |
| 01600700   | North Branch Potomac Riv r at Pine, MD           | 383359 | 0785025 | 54 | 057 |
| 01595160   | North Branch Potomac Riv r at Sh y r, MD         | 381867 | 0791826 | 24 | 023 |
| 01603100   | North Branch Potomac Riv r n ar Comb rd, MD      | 383718 | 0784624 | 24 | 001 |
| 01647720   | North Branch Rock Cr k n ar North ck, MD         | 380659 | 0770609 | 24 | 021 |
| 01643800   | North Fork Gues Cr k n ar Lucob, VA              | 380534 | 0774300 | 51 | 107 |
| 01653000   | North Fork Sh nendish Riv r at Mount Jackson, VA | 384444 | 0783821 | 51 | 171 |
| 01644000   | North Fork Sh nendish Riv r n ar Strasburg, VA   | 385836 | 0782011 | 51 | 187 |
| 01606720   | North Mill Cr k n ar P r rching, WV              | 385518 | 0791048 | 54 | 023 |
| 01652000   | North Riv r n ar Burk town, VA                   | 382025 | 0785450 | 51 | 165 |
| 01616560   | North Riv r n at Stuck will, VA                  | 382029 | 0791422 | 51 | 015 |
| 01634100   | Op quos Cr k n ar Martinsburg, VA                | 382525 | 0775620 | 54 | 003 |
| 01626365   | Paddy Run n ar L benon Church, VA                | 380255 | 0782940 | 51 | 069 |
| 016549200  | Pag Brook a Boye, VA                             | 380550 | 0780304 | 51 | 043 |
| 01601470   | Pain Branch at Coll g Park, MD                   | 380116 | 0765645 | 24 | 013 |
| 01654950   | Pm y Mountn Cr k at Laval, MD                    | 383926 | 0784835 | 24 | 001 |
| 01654950   | Pri cau Drith n ar Pl dman, VA                   | 381368 | 0785331 | 51 | 015 |
| 01624950   | Prt rti M Run n ar Cimmn, VA                     | 380754 | 0786240 | 51 | 015 |

|          |                                    |        |         |    |     |
|----------|------------------------------------|--------|---------|----|-----|
| 01633720 | Tenn Brook at Tense Brook, VA      | 385642 | 0782632 | 51 | 171 |
| 01645520 | Texas Run at Winch st r, VA        | 381012 | 0780940 | 51 | 840 |
| 01640240 | Texas Run at Ward nsrill, WV       | 385920 | 0783923 | 51 | 021 |
| 01617010 | Texas Run at Ward nsrill, WV       | 382715 | 0775341 | 54 | 003 |
| 01641450 | Wish Run at Wish Run, PA           | 384610 | 0776030 | 42 | 055 |
| 01605520 | Wish Run at Wish Run, PA           | 382632 | 0791220 | 51 | 091 |
| 01610063 | White Sulphur Run at Flunson, MD   | 383930 | 0782753 | 24 | 001 |
| 01638895 | White Sulphur Run at Two Tawms, PA | 384867 | 0771044 | 42 | 001 |
| 01657425 | Wolf Run at Clifton, VA            | 384469 | 0772151 | 51 | 059 |

### C.3. LANDUSE METADATA (NLCD)

|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
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| <p>National Land Cover Database Zone 59 Land Cover Layer</p> <h2>National Land Cover Database Zone 59 Land Cover Layer</h2> <p>Metadata also available as</p> <h3>Metadata:</h3> <ul style="list-style-type: none"> <li>• <a href="#">Identification Information</a></li> <li>• <a href="#">Data Quality Information</a></li> <li>• <a href="#">Spatial Data Organization Information</a></li> <li>• <a href="#">Spatial Reference Information</a></li> <li>• <a href="#">Entity and Attribute Information</a></li> <li>• <a href="#">Distribution Information</a></li> <li>• <a href="#">Acquisition Information</a></li> </ul> <hr/> <p><b>Identification Information:</b></p> <p><b>Citation:</b></p> <p><b>Originator:</b> U.S. Geological Survey<br/> <b>Publication Date:</b> 2003/09/01<br/> <b>Title:</b> National Land Cover Database Zone 59 Land Cover Layer<br/> <b>Edition:</b> 1:1<br/> <b>Geospatial Data Presentation Form:</b> remote-sensing image<br/> <b>Series Information:</b><br/> <b>Series Name:</b> None<br/> <b>Series Identification:</b> None<br/> <b>Publication Information:</b><br/> <b>Publication Place:</b> Sioux Falls, SD<br/> <b>Publisher:</b> U.S. Geological Survey<br/> <b>Other Citation Details:</b><br/> <b>References:</b> Homer, C., C. Huang, L. Yang, B. Wylie and M. Coan, 2004. Development of a 2001 national land cover database for the United States. Photogrammetric Engineering and Remote Sensing Vol. 70, No. 7, pp. 829-840 or online at <a href="http://www.mrlc.gov/publications">www.mrlc.gov/publications</a>. The USGS acknowledges the support of NARSAL at the University of Georgia in development of data in this zone.<br/> <b>Online Linkage:</b> <a href="http://2003/09/01/MLC02">2003/09/01/MLC02</a></p> <p><b>Description:</b><br/> <b>Abstract:</b><br/> The National Land Cover Database 2001 land cover layer for mapping zone 59 was produced through a cooperative project conducted by the Multi-Resolution Land Characteristics (MRLC) Consortium. The MRLC Consortium is a partnership of federal agencies (<a href="http://www.mrlc.gov">www.mrlc.gov</a>), consisting of the U.S. Geological Survey (USGS), the National Oceanic and Atmospheric Administration (NOAA), the U.S. Environmental Protection Agency (EPA), the U.S. Department of Agriculture (USDA), the U.S. Forest Service (USFS), the National Park Service (NPS), the U.S. Fish and Wildlife Service (FWS), the Bureau of Land Management (BLM) and the USDA Natural Resources Conservation</p> | <p>National Land Cover Database Zone 59 Land Cover Layer</p> <p>Service (NRCFS). One of the primary goals of the project is to generate a current, consistent, seamless, and accurate National Land cover Database (NLCD) circa 2001 for the United States at medium spatial resolution. This landcover map and all documents produced are available for download at <a href="http://www.mrlc.gov">www.mrlc.gov</a>. For more information on the project, refer to Homer et al. (2004) and <a href="http://www.mrlc.gov/mrlc2k4.asp">http://www.mrlc.gov/mrlc2k4.asp</a>.</p> <p>The NLCD 2001 is created by partitioning the U.S. into mapping zones. A total of 66 mapping zones were delineated within the conterminous U.S. based on ecoregion and geographical characteristics, edge matching features and the size re-variant of Landsat images. Mapping zone 59 encompasses whole or portions of several states, including the states of South Carolina, North Carolina, and Virginia. Questions about the NLCD mapping zone 59 can be directed to the NLCD 2001 land cover mapping team at the National Center, ERDC, Sioux Falls, SD (605) 594-4151 or <a href="mailto:mrlc@usgs.gov">mrlc@usgs.gov</a>.</p> <p><b>Purpose:</b><br/> The goal of this project is to provide the Nation with complete, current and consistent public domain information on its land use and land cover.</p> <p><b>Supplemental Information:</b><br/> Corner Coordinates (center of pixel, projection meters) Upper Left Corner: 124575 meters(X), 1841230 meters(Y) Lower Right Corner: 1627410 meters(X), 1377660 meters(Y) Spatial-specific information not available</p> <p><b>Time Period Information:</b><br/> <b>Range of Dates/Times:</b><br/> <b>Beginning Date:</b> 1999/03/0<br/> <b>Ending Date:</b> 2002/01/4</p> <p><b>Currentness:</b> Reference ground condition</p> <p><b>Status:</b> Progress: In work</p> <p><b>Spatial Domain:</b> Maintenance and update Frequency: As needed</p> <p><b>Bounding Coordinates:</b><br/> West Bounding Coordinate: -80.75933091<br/> East Bounding Coordinate: -77.63897197<br/> North Bounding Coordinate: 39.72993205<br/> South Bounding Coordinate: 37.37708076</p> <p><b>Keywords:</b><br/> <b>Theme:</b><br/> Theme Keyword Thesaurus: None<br/> Theme Keyword Land Cover<br/> Theme Keyword USGS<br/> Theme Keyword U.S. Geological Survey<br/> Theme Keyword USGS<br/> Theme Keyword digital spatial data<br/> Theme Keyword Thesaurus: ISO 19115 Category<br/> Theme Keyword imagery<br/> Theme Keyword Base Maps<br/> Theme Keyword Earth Cover<br/> <b>Place:</b></p> |
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| <p>National Land Cover Database Zone 59 Land Cover Layer</p> <p><b>Place Keyword, Thesaurus:</b><br/>U.S. Department of Commerce, 1995. Countries, dependencies, areas of special sovereignty, and their principal administrative divisions. Federal Information Processing Standard (1-4). Washington, D.C.: National Institute of Standards and Technology.</p> <p><b>Place Keyword, U.S.</b><br/><b>Place Keyword, US</b></p> <p><b>Place:</b><br/><b>Place Keyword, Thesaurus:</b> None<br/><b>Place Keyword, Zone 59</b></p> <p><b>Place:</b><br/><b>Place Keyword, Thesaurus:</b><br/>U.S. Department of Commerce, 1987. Codes for the identification of the States, the District of Columbia and the outlying areas of the United States, and associated areas (Federal Information Processing Standard 3-2). Washington, D.C.: National Institute of Standards and Technology.</p> <p><b>Place Keyword, South Carolina</b><br/><b>Place Keyword, North Carolina</b><br/><b>Place Keyword, Virginia</b><br/><b>Place Keyword, SC</b><br/><b>Place Keyword, NC</b><br/><b>Place Keyword, VA</b><br/><b>Place Keyword, Southern Piedmont</b><br/><b>Place Keyword, Northern Piedmont</b></p> <p><b>Access Constraints:</b> None<br/><b>Point of Contact:</b><br/><b>Contact Information:</b><br/><b>Contact Organization, Primary:</b><br/><b>Contact Organization, US Geological Survey</b><br/><b>Contact Position, Customer Services Representative</b><br/><b>Contact Address:</b><br/><b>Address, Type: mailing and physical address</b><br/><b>Address:</b> National Center, EROS<br/><b>Address:</b> 47914 252nd Street<br/><b>City:</b> Sioux Falls<br/><b>State or Province:</b> SD<br/><b>Postal Code:</b> 57198-0001<br/><b>Country:</b> USA<br/><b>Contact, Phone:</b> Telephone: 605.594.6151<br/><b>Contact, TDD:</b> Telephone: 605.594.6923<br/><b>Contact, Fax:</b> Telephone: 605.594.6589<br/><b>Contact, Electronic:</b> Mail Address: <a href="mailto:customers@usgs.gov">customers@usgs.gov</a><br/><b>Hours of Service:</b> 0600 - 1600 CT, M - F (6th CST-5h CDT GMT)<br/><b>Contact, Journals:</b><br/>The USGS point of contact is for questions relating to the data display and download from this web site. For questions regarding data content and quality, refer to: <a href="http://www.mrls.gov/mrls2k.asp">http://www.mrls.gov/mrls2k.asp</a> or email: <a href="mailto:mrls@usgs.gov">mrls@usgs.gov</a></p> <p><b>Data Set, Credit:</b> U.S. Geological Survey, NARSAL<br/><b>Security Information:</b><br/><b>Security, Classification, System:</b> None</p> | <p>National Land Cover Database Zone 59 Land Cover Layer</p> <p><b>Security, Classification:</b> Unclassified<br/><b>Security, Classification, System:</b> N/A<br/><b>Native Data Set, File Name:</b><br/>Microsoft Windows 2000 Version 5.1 (Build 2600) Service Pack 1, ESRI ArcCatalog 9.0.0.535</p> <p><b>Data Quality Information:</b><br/><b>Attribute Accuracy:</b><br/>The information on data quality for mapping zone 59 was generated by the Decision Tree algorithm that conducts a cross-validation for assessing classification and prediction reliability. A formal independent accuracy assessment of mapping zone 59 land cover has not been made. The regression tree algorithm employed in the DTD 2001 mapping process can provide relatively reliable estimates for land cover predictions if the accuracy data used for cross-validation are collected based on a statistically valid sampling design. For mapping zone 59 land cover modeling, a 5-fold cross-validation was conducted by dividing the entire training data set into 5 subsets of equal size. For each model run, an accuracy estimate was derived using one subset to evaluate the model prediction (with the model developed using the remaining training samples). This process was repeated 5 times. After all 5 runs, an average value of all accuracy estimates from the 5 runs were computed. Users should be cautioned that these cross-validation results provide users with only first order estimates of data quality, and should not be considered a formal accuracy assessment. This background map and all documents pertaining to it are considered "provisional" until a formal accuracy assessment can be conducted.</p> <p><b>Quantitative Attribute Accuracy Assessment:</b><br/><b>Attribute Accuracy, Zone 59:</b><br/><b>Attribute Accuracy, Zone 59:</b><br/>The above listed value is the overall accuracy obtained for the land cover data using a cross-validation estimate from the decision tree model. This document and the described landcover map are considered "provisional" until a formal accuracy assessment is completed. The U.S. Geological Survey can make no guarantee as to the accuracy or completeness of this information, and it is provided with the understanding that it is not guaranteed to be correct or complete. Conclusions drawn from this information are the responsibility of the user.</p> <p><b>Logical Consistency Report:</b><br/>The NLCD 2001 database for mapping zone 59 consists of three main data products including: (1) per pixel classified land-cover data (2) sub-pixel percent imperviousness and (3) sub-pixel percent canopy density. The land-cover database also includes three additional metadata products: (a) a spatial mode map of the land cover classification, (b) a spatial confidence of the land cover classification, and (c) a text file of logical statements related to the land cover classification.</p> <p>Conceptually, the descriptive tree is a classification tree generated by using the final minimum-map-unit land cover product (1. zero) as training data, and Landsat and other ancillary data as predictors. The goal of the descriptive tree is to summarize the effects of boosted trees (10 as venial classification trees) into a single condensed decision tree that can be used as a diagnostic tool for the classification process. This descriptive tree can be used to assess the relative importance of each of the input data sets on each land cover class. Such information may also be useful to summarize the minimum-mapping-unit classification to meet a user's specific</p> |
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works through raster modeling. Descriptive trees usually capture 60 to 80% of the information from the original land cover data.

The leaf or terminal nodes of the descriptive trees are assigned to so-called numbers (called node numbers) and mapped across the entire mapping zone on a pixel-by-pixel basis. These node numbers can then be matched with the various conditional statements associated with each respective terminal node. This spatial layer appears similar to a class map, but is the result of a supervised classification - not an unsupervised clustering. This node map can automatically be used as input by users to customize NLCD land cover, by linking the spatial extent of an individual node with the rules of the conditional statement.

The Land Cover spatial classification evidence data layer is provided to users to help determine the relative confidence of the NLCD 2001 land cover data. The evidence data layer is a map of the confidence of the classification. The confidence is a value between 0% and 100%, but indicates the confidence of the classification at each node based on the training data. This spatial confidence map should be considered as only one indicator of relative reliability of the land cover classification, rather than a precise estimate. Users should be aware that this estimate is made based on only training data, and is derived from a generalized descriptive decision tree that reproduces the final land cover data. However, this layer provides valuable insight for a user to determine the risk or confidence they choose to place in each pixel of land cover.

A logic statement from a descriptive tree classification describes each classification rule for each classified pixel. An example of the logic statement follows:

If tasseled-cap wetness > 140 and imperviousness = 0 and canopy density < 4, then classify as Water

This logic file can be used in combination with the spatial risk map to identify classification logic and allow modifications of the classification based on user's knowledge and/or additional data sets.

Additional information may be found at [http://www.mrl.gov/nlcd2k\\_nlcdage](http://www.mrl.gov/nlcd2k_nlcdage).

**Completeness Report:**

This NLCD product of mapping zone 59 Land Cover layer is the version dated 2/05/0131.

**Positional Accuracy:**

*Horizontal\_Positional\_Accuracy:*

*Vertical\_Positional\_Accuracy:*

*Horizontal\_Positional\_Accuracy\_Report:* N/A

*Vertical\_Positional\_Accuracy\_Report:* N/A

**Lineage:**

*Process\_Step:*

*Process:*

The land cover classification was achieved by use of a classification and decision tree; method (DT) using a combination of Landsat imagery and ancillary data. The specific DT program employed is called C5, which implements a gain ratio criterion in tree development and pruning (Quinlan, 1993). C5 also implemented several advanced features that can aid and improve land cover classification, including boosting and cross-validation. Boosting is a technique for improving classification accuracy, while cross-validation can provide certain level of estimation regarding the land cover classification quality. In addition, C5 can generate a confidence estimate for each classified pixel and record the associated classification logic in a text file.

that can be readily interpreted and incorporated into a metadata system.

To conduct the land cover classification using DT, a large quantity of training data is required. For mapping zone 59, training data were collected from several combined sources including USGS DOQQs. Note that the training data were used to map all land cover classes except for four classes in urban and sub-urban areas (developed open space, low intensity developed, medium intensity developed, high intensity developed). All urban and suburban land cover classes were mapped and easily assessed separately through a sub-pixel quantification of impervious surfaces using a regression tree modeling method.

Following the development of the land cover classification through decision tree modeling, additional steps were required to complete the final land cover product. The four classes in urban and suburban areas were determined from the imperviousness mapping product (determined in the next section). The threshold for the four classes is: (1) developed open space (imperviousness < 20%), (2) low intensity developed (imperviousness from 20 - 49%), (3) medium intensity developed (imperviousness from 50 - 79%), and (4) high intensity developed (imperviousness > 79%). Other classes of forest and non-forest were combined with the urban classes to complete the land cover product. Finally, visual inspection of the classification was made with areas that were wrongly classified delineated first as an "area of interest" (AOI), subsequently then limited manual editing was done to eliminate the classification error within the AOI.

The completed single pixel product was then generalized to a 1-acre (approximately 5 ETM+ 30 m pixel patch) minimum mapping unit product using a "smart eliminate" algorithm. This aggregation program subsamples pixels from the single pixel level to a 5-pixel patch using a "scenic" algorithm at doubling intervals. The algorithm consults a weighting matrix in guide merging of cover types by similarity, resulting in a product that preserves land cover logic as much as possible. As a caution, dates of Landsat ETM+ (TM) scenes used for land cover classification in zone 59 are as follows:

**SPRING:**

Index 5 for Path 15/Row 34 on 03/24/00 = Scene\_ID 701503400008450  
Index 7 for Path 15/Row 34 on 04/09/00 = Scene\_ID 701503400010050  
Index 8 for Path 16/Row 34 on 04/26/00 = Scene\_ID 701603400008550  
Index 9 for Path 16/Row 34 on 05/10/00 = Scene\_ID 701603400009210  
Index 3 for Path 16/Row 35 on 03/05/00 = Scene\_ID 501603400006450  
Index 3 for Path 16/Row 35 on 03/09/00 = Scene\_ID 7016034000026450  
Index 2 for Path 17/Row 34 on 03/25/01 = Scene\_ID 7017034000108450  
Index 1 for Path 17/Row 35 on 02/24/02 = Scene\_ID 7017034000205550  
Index 1 for Path 17/Row 36 on 02/24/02 = Scene\_ID 7017034000205550  
Index 8 for Path 18/Row 35 on 01/22/02 = Scene\_ID 5018034000202210  
LEAF ON (Summer):

Index 5 for Path 15/Row 34 on 05/03/00 = Scene\_ID 5015034000012410  
Index 3 for Path 15/Row 35 on 07/04/02 = Scene\_ID 7015034000218550  
Index 3 for Path 16/Row 34 on 02/26/00 = Scene\_ID 5016034000014710  
Index 3 for Path 16/Row 34 on 03/09/00 = Scene\_ID 7016034000014710  
Index 2 for Path 16/Row 34 on 06/09/02 = Scene\_ID 7016034000214650  
Index 1 for Path 13/Row 34 on 06/10/00 = Scene\_ID 7013034000016250  
Index 1 for Path 17/Row 35 on 06/10/00 = Scene\_ID 7017034000016250

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| National Land Cover Database Zone 98 Land Cover Layer                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | National Land Cover Database Zone 98 Land Cover Layer                                                                                                                                                                                                                                                                                                                    |
| <p>Index 1 for Path 17-Row 35 on 101600 = Scene_ID 701703600016250</p> <p>Index 5 for Path 18-Row 35 on 1043100 = Scene_ID 701803500012150</p> <p>Index 6 for Path 18-Row 35 on 1043100 = Scene_ID 701803500012150</p> <p>Index 7 for Path 15-Row 34 on 110600 = Scene_ID 7015034000131050</p> <p>Index 8 for Path 15-Row 34 on 110600 = Scene_ID 7015034000131050</p> <p>Index 9 for Path 16-Row 35 on 110800 = Scene_ID 701603500013150</p> <p>Index 10 for Path 16-Row 35 on 110800 = Scene_ID 701603500013150</p> <p>Index 11 for Path 16-Row 36 on 111000 = Scene_ID 701603600013150</p> <p>Index 12 for Path 17-Row 34 on 103090 = Scene_ID 7017034000931550</p> <p>Index 13 for Path 17-Row 35 on 101900 = Scene_ID 7017035000129251</p> <p>Index 14 for Path 17-Row 36 on 101600 = Scene_ID 7017036000129050</p> <p>Index 15 for Path 18-Row 35 on 102600 = Scene_ID 7018035000129550</p> | <p>Row_Count: 18120</p> <p>Column_Count: 12722</p> <p>Vertical_Primary: 1</p>                                                                                                                                                                                                                                                                                            |
| <p><b>Spatial Reference Information:</b></p> <p><b>Planar:</b></p> <p>Map_Projection: NAD 83, North American Datum of 1983</p> <p>Other_Coordinate_System_Definition:</p> <p>Standard_Parallel: 29.530000</p> <p>Standard_Parallel_2: 29.530000</p> <p>Longitude_of_Center_Meridian: -94.000000</p> <p>Latitude_of_Primary_Meridian: 21.000000</p> <p>Fake_Easting: 0.000000</p> <p>Fake_Northing: 0.000000</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Planar Coordinate Information:</b></p> <p>Planar_Coordinate_Information:</p> <p>Planar_Coordinate_Information:</p> <p>Coordinate_Representation:</p> <p>Abcissa_Resolution: 30.000000</p> <p>Ordinate_Resolution: 30.000000</p> <p>Planar_Distance: n/a; meters</p>                                                                                                |
| <p><b>Geodetic_Mask:</b></p> <p>Horizontal_Datum_Name: North American Datum of 1983</p> <p>Ellipsoid_Name: Geodetic Reference System 80</p> <p>Semi-major_Axis: 6378137.000000</p> <p>Denominator_of_Flattening_Ratio: 298.257222</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | <p><b>Entity and Attribute Information:</b></p> <p><b>Entity Type:</b></p> <p>Entity_Type_Label: Layer_1</p> <p>Entity_Type_Definition: NLDC Land Cover Layer</p> <p>Entity_Type_Definition_Source: National Land Cover Database 2001</p>                                                                                                                                |
| <p><b>Attribute:</b></p> <p>Attribute_Label: ObjectID</p> <p>Attribute_Definition: Internal feature number</p> <p>Attribute_Definition_Source: ESRI</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain:</p> <p>Whole numbers that are automatically generated.</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | <p><b>Attribute:</b></p> <p>Attribute_Label: Count</p> <p>Attribute_Definition:</p> <p>A nominal integer value that designates the number of pixels that have each value in the file; histogram column in ERDAS Imagine raster attributes table</p> <p>Attribute_Definition_Source: NLCD 2001</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain: Integer</p> |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Entity and Attribute Information:</b></p> <p><b>Entity Type:</b></p> <p>Entity_Type_Label: Layer_1</p> <p>Entity_Type_Definition: NLDC Land Cover Layer</p> <p>Entity_Type_Definition_Source: National Land Cover Database 2001</p>                                                                                                                                |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Attribute:</b></p> <p>Attribute_Label: ObjectID</p> <p>Attribute_Definition: Internal feature number</p> <p>Attribute_Definition_Source: ESRI</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain:</p> <p>Whole numbers that are automatically generated.</p>                                                                                            |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Attribute:</b></p> <p>Attribute_Label: Count</p> <p>Attribute_Definition:</p> <p>A nominal integer value that designates the number of pixels that have each value in the file; histogram column in ERDAS Imagine raster attributes table</p> <p>Attribute_Definition_Source: NLCD 2001</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain: Integer</p> |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Entity and Attribute Information:</b></p> <p><b>Entity Type:</b></p> <p>Entity_Type_Label: Layer_1</p> <p>Entity_Type_Definition: NLDC Land Cover Layer</p> <p>Entity_Type_Definition_Source: National Land Cover Database 2001</p>                                                                                                                                |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Attribute:</b></p> <p>Attribute_Label: ObjectID</p> <p>Attribute_Definition: Internal feature number</p> <p>Attribute_Definition_Source: ESRI</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain:</p> <p>Whole numbers that are automatically generated.</p>                                                                                            |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Attribute:</b></p> <p>Attribute_Label: Count</p> <p>Attribute_Definition:</p> <p>A nominal integer value that designates the number of pixels that have each value in the file; histogram column in ERDAS Imagine raster attributes table</p> <p>Attribute_Definition_Source: NLCD 2001</p> <p>Attribute_Domain_Values:</p> <p>Unrepresentable_Domain: Integer</p> |
| <p><b>Source and Citation Information:</b></p> <p>Source: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p> <p>Process: Produced by: Center for Global Change Science, University of Georgia</p>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | <p><b>Entity and Attribute Information:</b></p> <p><b>Entity Type:</b></p> <p>Entity_Type_Label: Layer_1</p> <p>Entity_Type_Definition: NLDC Land Cover Layer</p> <p>Entity_Type_Definition_Source: National Land Cover Database 2001</p>                                                                                                                                |

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| National Land Cover Database Zone 59 Land Cover Layer                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  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| <p><i>Attribute Label Value</i></p> <p><i>Attribute Definition:</i></p> <p>Land Cover Class Code Value: Class definitions marked with an asterisk (*) are Class NLCD Classes only</p> <p><i>Attribute Definition Source:</i> NLCD 2001</p> <p><i>Attribute Domain Value:</i></p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 1</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Open Water: All areas of open water, generally with less than 25% cover of vegetation or soil</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 11</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Open Water: All areas of open water, generally with less than 25% cover of vegetation or soil</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 12</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Partial Ice/Snow: All areas characterized by a perennial cover of ice and/or snow, generally greater than 25% of total cover</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 21</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Developed Open Space: Includes areas with a mixture of some natural and man-made vegetation, the form of which grasses, herbaceous surface account for less than 20 percent of total cover. These areas most commonly include tree-kil sand-family housing units, parks, golf courses, and vegetation planted in developed settings for recreation, erosion control, or aesthetic purposes</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 22</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Developed, Low Intensity: Includes areas with a mixture of constructed materials and vegetation. Impervious surfaces account for 20-49 percent of total cover. These areas most commonly include single-family</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 23</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Developed, Medium Intensity: Includes areas with a mixture of constructed materials and vegetation. Impervious surfaces account for</p> | <p>50-79 percent of the total cover. These areas most commonly include single-family housing units.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain Value:</i> 24</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Developed, High Intensity: Includes highly developed areas where people reside or work in high numbers. Examples include apartment complexes, row houses and commercial/industrial. Impervious surfaces account for 80 to 100 percent of the total cover.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 31</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Barren Land (Rock/Sand/Clay): Barren areas of bedrock, desert pavement, scree, talus, silt, volcanic material, glacial till, sand dunes, and other areas of bare mineral or organic material. Generally, vegetation accounts for less than 1% of total cover.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 32</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Unconsolidated Shore: Unconsolidated material such as silt, sand, or gravel that is subject to inundation and redistribution due to the action of water. Characterized by substrates lacking vegetation except for pioneering plants that become established during tree periods when growing vegetation is not present. Includes areas of sand, silt, and gravel that produce a number of landforms representing this class.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 41</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Deciduous Forest: Areas dominated by trees generally greater than 5 meters tall, and greater than 20% of total vegetation cover. More than 75 percent of the tree species shed foliage simultaneously in response to seasonal change.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value:</i> 42</p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Evergreen Forest: Areas dominated by trees generally greater than 5 meters tall, and greater than 20% of total vegetation cover. More than 75 percent of the tree species maintain their leaves all year. Canopy is never without green foliage.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> |

| National Land Cover Database Zone 59 Land Cover Layer                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  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| <p>class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 43</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Mixed Forest - Areas dominated by trees generally greater than 5 meters tall and greater than 20% of total vegetation cover. Neither deciduous nor evergreen species are greater than 75 percent of total tree cover.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 51</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Low Forest - Areas dominated by shrubs less than 20 centimeters tall with herbaceous vegetation typically greater than 20% of total vegetation. This type is often associated with grasses, sedges, herbs, and non-vascular vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 52</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Shrub Scrub - Areas dominated by shrubs less than 5 meters tall with shrub canopy typically greater than 20% of total vegetation. This class includes tree shrubs, young trees in an early successional stage, or trees and shrubs in a non-vascular vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 71</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Grassland/Herbaceous - Areas dominated by graminoid or herbaceous vegetation, generally greater than 80% of total vegetation. These areas are not subject to intensive management such as tillage, but can be utilized for grazing.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 72</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Sedge/Herbaceous - Alaska only areas dominated by sedges and forbs, generally greater than 80% of total vegetation. This type can occur with significant other grasses or other grass-like plants, and includes sedge, tundra, and sedge tussock tundra.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 73</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Low Forest - Alaska only areas dominated by forbs, sedges, or forbs/liches generally greater than 80% of total vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> | <p>class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 74</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Moss - Alaska only areas dominated by mosses, generally greater than 80% of total vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 81</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Pasture/Hay - Areas of grasses, legumes, or grass-legume mixtures planted for stock grazing or production of feed or hay crops. This class includes areas where the vegetation accounts for greater than 20 percent of total vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 82</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Cultivated Crops - Areas used for the production of annual crops, such as corn, soybeans, vegetables, tubers, and cotton, and also perennial woody crops such as orchards and vineyards. Crop vegetation accounts for greater than 20 percent of total vegetation. This class also includes areas where the vegetation accounts for greater than 20 percent of total vegetation.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 90</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Woody Wetlands - Areas where forest or shrub land vegetation accounts for greater than 20 percent of vegetative cover and the soil or substrate is periodically saturated with or covered with water.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 91</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Palustrine Forested Wetland* - Includes all tidal and non-tidal wetlands dominated by woody vegetation greater than 2 to 5 meters in height and all such wetlands that occur in tidal areas in which salinity due to ocean-derived salts is below 0.5 percent. Total vegetation coverage is greater than 20 percent.</p> <p><i>Enumerated Domain Value Definition Source:</i> NLCD 2001 land cover class descriptions</p> <p><i>Enumerated Domain:</i></p> <p><i>Enumerated Domain Value: 92</i></p> <p><i>Enumerated Domain Value Definition:</i></p> <p>Palustrine Scattered Wetland* - Includes all tidal and non-tidal wetlands dominated by woody vegetation less than 5 meters in height, and all such wetlands that occur in tidal areas in which salinity due to</p> |

| National Land Cover Database Zone 59 Land Cover Layer                                                                                                                                                                                                                                                                                                                                                                        | National Land Cover Database Zone 59 Land Cover Layer                                                                                                                                                                                                                                              |
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| <p>ocean-derived salts is below 0.5 percent. Total vegetation coverage is greater than 20 percent. The species present could be tree shrubs, young trees, and herbaceous plants that are small in stature in environmental conditions.</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 92<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 93</p> | <p>Present for most of the growing season in most years. Perennial plants include dominant trees and shrubs.</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 94<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 95</p> |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 96<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 97</p>                                                                                                                                                                                                                  | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 98<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 99</p>                                                                                        |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 100<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 101</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 102<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 103</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 104<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 105</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 106<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 107</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 108<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 109</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 110<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 111</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 112<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 113</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 114<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 115</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 116<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 117</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 118<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 119</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 120<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 121</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 122<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 123</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 124<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 125</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 126<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 127</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 128<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 129</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 130<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 131</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 132<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 133</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 134<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 135</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 136<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 137</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 138<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 139</p>                                                                                      |
| <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 140<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 141</p>                                                                                                                                                                                                                | <p>class descriptions</p> <p><i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 142<br/> <i>Enumerated Domain Value Definition:</i><br/> <i>Enumerated Domain Value:</i> 143</p>                                                                                      |

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| <p>National Land Cover Database Zone 59 Land Cover Layer</p> <p><b>Attribute:</b><br/> <b>Attribute_Label:</b> Blue<br/> <b>Attribute_Definition:</b><br/> Blue color code for RGB slice by value for canopy range display purposes. The value is arbitrarily assigned by the display software package, unless defined by user.<br/> <b>Attribute_Definition_Source:</b> NLCD 2001<br/> <b>Attribute_Domain:</b> Values:<br/> Range Domain:<br/> Range_Domain_Minimum: 0<br/> Range_Domain_Maximum: 100<br/> <b>Attribute_Measurement:</b> Percent<br/> <b>Attribute_Measurement_Resolution:</b> 0.1</p> <p><b>Attribute:</b><br/> <b>Attribute_Label:</b> Opacity<br/> <b>Attribute_Definition:</b><br/> A measure of how opaque or solid a color is displayed in a layer.<br/> <b>Attribute_Definition_Source:</b> NLCD 2001<br/> <b>Attribute_Domain:</b> Values:<br/> Range Domain:<br/> Range_Domain_Minimum: 0<br/> Range_Domain_Maximum: 100<br/> <b>Attribute_Measurement:</b> Percent<br/> <b>Attribute_Measurement_Resolution:</b> 0.1</p> <p><b>Overview:</b> Description:<br/> Entry and Attribute Overview:<br/> Class Red Green Blue<br/> 1 0.00000000 0.00000000 0.00000000<br/> 11 0.325490196 0.62745008 0.62745008<br/> 12 0.85490196 0.91372549 0.91372549<br/> 21 0.31372549 0.62745008 0.62745008<br/> 22 0.62745008 0.91372549 0.91372549<br/> 23 0.91372549 0.62745008 0.62745008<br/> 24 0.62745008 0.91372549 0.91372549<br/> 31 0.74117647 0.725490196 0.670588235<br/> 32 1.00000000 1.00000000 1.00000000<br/> 41 0.43137255 0.701960784 0.41960784<br/> 42 0.13725490 0.42352941 0.231372549<br/> 43 0.725491176 0.682745098 0.607843137<br/> 51 0.69417647 0.588235294 0.235294118<br/> 52 0.835294118 0.74705882 0.531333333<br/> 71 0.925490196 0.925490196 0.786078431<br/> 72 0.835294118 0.925490196 0.835294118<br/> 73 0.535294118 0.925490196 0.535294118<br/> 74 0.53725490 0.725490196 0.61960784<br/> 81 0.901960784 0.835294118 0.26235294<br/> 82 0.70960784 0.486274510 0.200000000<br/> 90 0.760784314 0.878431373 0.649019608</p> | <p>National Land Cover Database Zone 59 Land Cover Layer</p> <p><b>Entity and Attribute Detail:</b> Citation:<br/> Entity and Attribute Detail: Citation:<br/> Attribute accuracy is described, where present, with each attribute defined in the Entity and Attribute Section. Note: To ensure all areas of mapping zone 59 are completely covered a 3,000 meter (100 Landset pixels) buffer was added to the boundary of mapping zone 59.</p> <p><b>Distribution Information:</b><br/> <b>Distribution:</b><br/> <b>Contact Information:</b><br/> <b>Contact Organization:</b> U.S. Geological Survey<br/> <b>Contact Position:</b> Customer Service Representative<br/> <b>Contact Address:</b><br/> <b>Address Type:</b> mailing and physical address<br/> <b>Address:</b> National Center, EROS<br/> <b>City:</b> Sioux Falls<br/> <b>State or Province:</b> SD<br/> <b>Postal Code:</b> 57198-0001<br/> <b>Country:</b> US<br/> <b>Contact Voice Telephone:</b> 605/594-6151<br/> <b>Contact TDD/TTY Telephone:</b> 605/594-6933<br/> <b>Contact Facsimile Telephone:</b> 605/594-6589<br/> <b>Contact Electronic Mail Address:</b> cuserserv@usgs.gov<br/> <b>Hours of Service:</b> 0800 - 1600 CT, M - F (-6h CST; 5h CDT GMT)<br/> <b>Contact Instructions:</b><br/> The USGS point of contact is for questions relating to the data display and download from this web site. Questions about the NLCD mapping zone 59 can be directed to the NLCD 2001 land cover mapping team at the National Center, EROS, Sioux Falls, SD (605) 594-6151 or nrlcd@usgs.gov.</p> <p><b>Resource Description:</b> Downloadable data<br/> <b>Download:</b><br/> Although these data have been processed successfully on a computer system at the USGS, no warranty expressed or implied is made by the USGS regarding the use of this data on any other system, nor does the act of distribution constitute any such warranty. Data may have been compiled from various outside sources. Spatial information may not meet National Map Accuracy Standards. This information may be updated without notification. The USGS shall not be liable for any activity involving these data, translation, fitness of the data for a particular purpose, its use, or analysis results.</p> <p><b>Standard Order Process:</b><br/> <b>Digital Form:</b><br/> <b>Digital Transfer Information:</b><br/> <b>Format Name:</b> ArcInfo Export Format and/or ArcView Shapefile<br/> <b>Format Name:</b> ArcView Shapefile<br/> <b>Format Specification:</b> ASII<br/> <b>Transfer Size:</b> 0.001<br/> <b>Digital Transfer Option:</b><br/> <b>Online Option:</b><br/> <b>Compute Contact Information:</b></p> |
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| National Land Cover Database Zone 59 Land Cover Layer | <p>Network Address: <i>Network_Resource_Name</i> = <a href="http://seamless.usgs.gov/">http://seamless.usgs.gov/</a></p> <p>Access Instructions:</p> <p>The URL <a href="http://seamless.usgs.gov/">http://seamless.usgs.gov/</a> provides a map interface that allows for data downloads within a customer defined area of interest. Zoom tools are available that can be used to investigate areas of interest on the map interface. The download tool allows the customer to capture layers from the map, utilizing the Seamless Data Distribution System process for downloading. A re-ast summary page is then generated with the download layers listed. By clicking the "download" button on the summary page, a zip file will be generated that can be saved on the customer's computer. The file can then be unzipped and imported into various user software applications.</p> <p><i>Online Computer and Operating System:</i> Not available for dissemination</p> <p>Fees: None</p> <p><i>Marketing Materials:</i> Contact Customer Services Representative</p> <p><i>Technical Notes:</i> Contact Customer Services Representative</p> <p><i>Custom Order Process:</i> Contact Customer Services Representative</p> <p><i>Technical Prerequisites:</i> ESRI ArcMap Suite and/or ArcInfo software, and supporting operating systems.</p>         |
| National Land Cover Database Zone 59 Land Cover Layer | <p><i>Metadata Reference Information:</i></p> <p><i>Metadata Date:</i> 20030617</p> <p><i>Metadata Contact:</i></p> <p><i>Contact Information:</i></p> <p><i>Contact Organization - Primary:</i> Contact Organization: U.S. Geological Survey</p> <p><i>Contact Person:</i> Customer Services Representative</p> <p><i>Contact Address:</i></p> <p><i>Address Type:</i> mailing and physical address</p> <p><i>Address:</i> National Center, ER05</p> <p><i>City:</i> Sioux Falls</p> <p><i>State or Province:</i> SD</p> <p><i>Postal Code:</i> 57198-0601</p> <p><i>Country:</i> USA</p> <p><i>Contact Voice Telephone:</i> 605594-6151</p> <p><i>Contact TDD/TTY Telephone:</i> 605594-6933</p> <p><i>Contact Facsimile Telephone:</i> 605594-6589</p> <p><i>Contact Electronic Mail Address:</i> <a href="mailto:customer@usgs.gov">customer@usgs.gov</a></p> <p><i>Hours of Service:</i> 0800 CT, M-F (4th CST-5h, CDT GMT)</p> <p><i>Metadata Standard Version:</i> ERDC-IGAC Catalog for Digital Geospatial Metadata</p> <p><i>Metadata Time Convention:</i> local time</p> <p><i>Metadata Access Constraints:</i> None</p> <p><i>Metadata Security Information:</i></p> <p><i>Metadata Security Classification System:</i> None</p> <p><i>Metadata Security Classification:</i> None</p> <p><i>Metadata Security Handling Description:</i> None</p> |

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Address: John Hanson business center
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Metadata: 0.9.1
Metadata Standard Version: FIDO-STB-001-1998

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**APPENDIX D : DATA OVERVIEW**

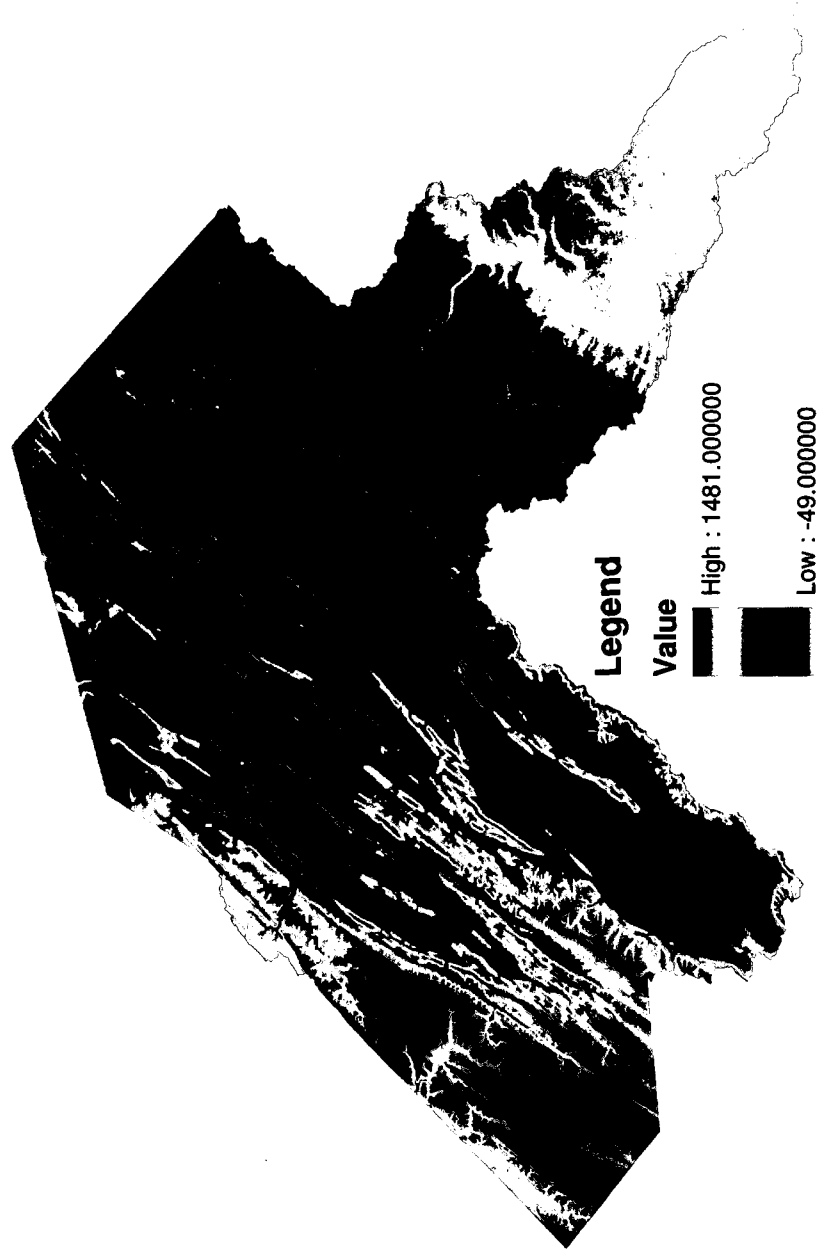


Figure D.1: Topographic characteristics of the Potomac Basin. Legend indicates Digital Elevation Model values relative to sea-level, in meters.



Figure D 2: Landsat-derived landclass information for the Potomac Basin. Legend indicates Landsat TM-2 class.

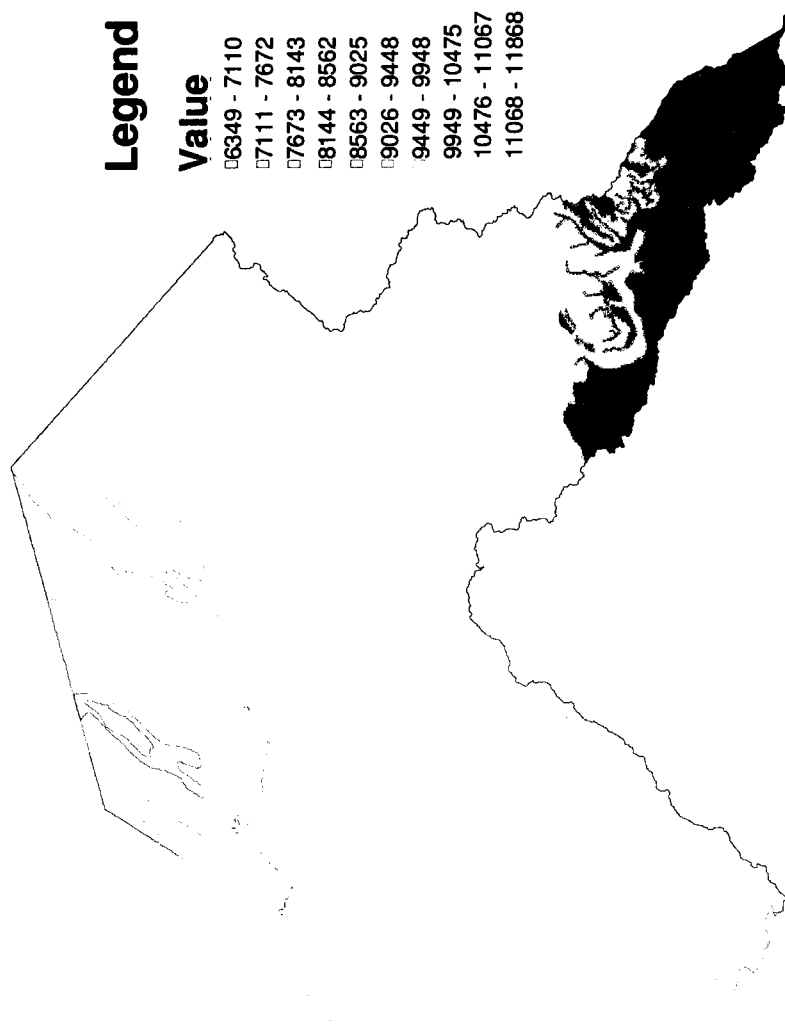


Figure D.3: Spatial variation in Soil Class in the Potomac Basin. Legend indicates soil class code.

**APPENDIX E: SAMPLE ANNAGNPS FILES**

# E.1. DISCRETUZATION RESULTS: ANNAGNPS\_CELL.DAT (8.3KM<sup>2</sup>)

| Cell ID | Area (km <sup>2</sup> ) | Population | Age | Sex | Marital Status | Religion   | Ethnicity | Language | Education   | Occupation   | Income   | Health | Disability | Other |
|---------|-------------------------|------------|-----|-----|----------------|------------|-----------|----------|-------------|--------------|----------|--------|------------|-------|
| 1       | 1.2                     | 120        | 25  | M   | Married        | Catholic   | White     | English  | High School | Teacher      | \$45,000 | Good   | None       | None  |
| 2       | 1.5                     | 150        | 30  | F   | Single         | Protestant | Black     | Spanish  | College     | Nurse        | \$55,000 | Good   | None       | None  |
| 3       | 1.8                     | 180        | 35  | M   | Married        | Jewish     | Asian     | Chinese  | University  | Engineer     | \$65,000 | Good   | None       | None  |
| 4       | 2.1                     | 210        | 40  | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Retail       | \$35,000 | Fair   | Minor      | None  |
| 5       | 2.4                     | 240        | 45  | M   | Single         | Buddhist   | White     | English  | College     | Software     | \$75,000 | Good   | None       | None  |
| 6       | 2.7                     | 270        | 50  | F   | Married        | Hindu      | Black     | English  | High School | Factory      | \$25,000 | Fair   | Minor      | None  |
| 7       | 3.0                     | 300        | 55  | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Doctor       | \$85,000 | Good   | None       | None  |
| 8       | 3.3                     | 330        | 60  | F   | Married        | Christian  | White     | English  | College     | Manager      | \$55,000 | Good   | None       | None  |
| 9       | 3.6                     | 360        | 65  | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Construction | \$40,000 | Fair   | Minor      | None  |
| 10      | 3.9                     | 390        | 70  | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Professor    | \$95,000 | Good   | None       | None  |
| 11      | 4.2                     | 420        | 75  | M   | Married        | Hindu      | Black     | English  | High School | Warehouse    | \$30,000 | Fair   | Minor      | None  |
| 12      | 4.5                     | 450        | 80  | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Lawyer       | \$70,000 | Good   | None       | None  |
| 13      | 4.8                     | 480        | 85  | M   | Single         | Christian  | White     | English  | College     | Analyst      | \$60,000 | Good   | None       | None  |
| 14      | 5.1                     | 510        | 90  | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Service      | \$20,000 | Fair   | Minor      | None  |
| 15      | 5.4                     | 540        | 95  | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Architect    | \$80,000 | Good   | None       | None  |
| 16      | 5.7                     | 570        | 100 | F   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 17      | 6.0                     | 600        | 105 | M   | Single         | Sikh       | Asian     | Punjabi  | University  | Scientist    | \$90,000 | Good   | None       | None  |
| 18      | 6.3                     | 630        | 110 | F   | Married        | Christian  | White     | English  | College     | Writer       | \$45,000 | Good   | None       | None  |
| 19      | 6.6                     | 660        | 115 | M   | Married        | Muslim     | Hispanic  | Spanish  | High School | Farmer       | \$10,000 | Fair   | Minor      | None  |
| 20      | 6.9                     | 690        | 120 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Artist       | \$35,000 | Good   | None       | None  |
| 21      | 7.2                     | 720        | 125 | M   | Single         | Hindu      | Black     | English  | High School | Chef         | \$25,000 | Fair   | Minor      | None  |
| 22      | 7.5                     | 750        | 130 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 23      | 7.8                     | 780        | 135 | M   | Married        | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 24      | 8.1                     | 810        | 140 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 25      | 8.4                     | 840        | 145 | M   | Single         | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 26      | 8.7                     | 870        | 150 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 27      | 9.0                     | 900        | 155 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 28      | 9.3                     | 930        | 160 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 29      | 9.6                     | 960        | 165 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 30      | 9.9                     | 990        | 170 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 31      | 10.2                    | 1020       | 175 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 32      | 10.5                    | 1050       | 180 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 33      | 10.8                    | 1080       | 185 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 34      | 11.1                    | 1110       | 190 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 35      | 11.4                    | 1140       | 195 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 36      | 11.7                    | 1170       | 200 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 37      | 12.0                    | 1200       | 205 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 38      | 12.3                    | 1230       | 210 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 39      | 12.6                    | 1260       | 215 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 40      | 12.9                    | 1290       | 220 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 41      | 13.2                    | 1320       | 225 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 42      | 13.5                    | 1350       | 230 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 43      | 13.8                    | 1380       | 235 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 44      | 14.1                    | 1410       | 240 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 45      | 14.4                    | 1440       | 245 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 46      | 14.7                    | 1470       | 250 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 47      | 15.0                    | 1500       | 255 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 48      | 15.3                    | 1530       | 260 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 49      | 15.6                    | 1560       | 265 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 50      | 15.9                    | 1590       | 270 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 51      | 16.2                    | 1620       | 275 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 52      | 16.5                    | 1650       | 280 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 53      | 16.8                    | 1680       | 285 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 54      | 17.1                    | 1710       | 290 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 55      | 17.4                    | 1740       | 295 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 56      | 17.7                    | 1770       | 300 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 57      | 18.0                    | 1800       | 305 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 58      | 18.3                    | 1830       | 310 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 59      | 18.6                    | 1860       | 315 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 60      | 18.9                    | 1890       | 320 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 61      | 19.2                    | 1920       | 325 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 62      | 19.5                    | 1950       | 330 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 63      | 19.8                    | 1980       | 335 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 64      | 20.1                    | 2010       | 340 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 65      | 20.4                    | 2040       | 345 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 66      | 20.7                    | 2070       | 350 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 67      | 21.0                    | 2100       | 355 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 68      | 21.3                    | 2130       | 360 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 69      | 21.6                    | 2160       | 365 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 70      | 21.9                    | 2190       | 370 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 71      | 22.2                    | 2220       | 375 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 72      | 22.5                    | 2250       | 380 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 73      | 22.8                    | 2280       | 385 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 74      | 23.1                    | 2310       | 390 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 75      | 23.4                    | 2340       | 395 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 76      | 23.7                    | 2370       | 400 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 77      | 24.0                    | 2400       | 405 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 78      | 24.3                    | 2430       | 410 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 79      | 24.6                    | 2460       | 415 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 80      | 24.9                    | 2490       | 420 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 81      | 25.2                    | 2520       | 425 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 82      | 25.5                    | 2550       | 430 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 83      | 25.8                    | 2580       | 435 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 84      | 26.1                    | 2610       | 440 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 85      | 26.4                    | 2640       | 445 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 86      | 26.7                    | 2670       | 450 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 87      | 27.0                    | 2700       | 455 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 88      | 27.3                    | 2730       | 460 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 89      | 27.6                    | 2760       | 465 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 90      | 27.9                    | 2790       | 470 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |
| 91      | 28.2                    | 2820       | 475 | M   | Married        | Hindu      | Black     | English  | High School | Driver       | \$15,000 | Fair   | Minor      | None  |
| 92      | 28.5                    | 2850       | 480 | F   | Married        | Sikh       | Asian     | Punjabi  | University  | Researcher   | \$75,000 | Good   | None       | None  |
| 93      | 28.8                    | 2880       | 485 | M   | Single         | Christian  | White     | English  | College     | Designer     | \$50,000 | Good   | None       | None  |
| 94      | 29.1                    | 2910       | 490 | F   | Married        | Muslim     | Hispanic  | Spanish  | High School | Operator     | \$18,000 | Fair   | Minor      | None  |
| 95      | 29.4                    | 2940       | 495 | M   | Married        | Buddhist   | Asian     | Chinese  | University  | Developer    | \$65,000 | Good   | None       | None  |
| 96      | 29.7                    | 2970       | 500 | F   | Married        | Hindu      | Black     | English  | High School | Worker       | \$12,000 | Fair   | Minor      | None  |
| 97      | 30.0                    | 3000       | 505 | M   | Married        | Sikh       | Asian     | Punjabi  | University  | Analyst      | \$70,000 | Good   | None       | None  |
| 98      | 30.3                    | 3030       | 510 | F   | Married        | Christian  | White     | English  | College     | Editor       | \$40,000 | Good   | None       | None  |
| 99      | 30.6                    | 3060       | 515 | M   | Single         | Muslim     | Hispanic  | Spanish  | High School | Technician   | \$22,000 | Fair   | Minor      | None  |
| 100     | 30.9                    | 3090       | 520 | F   | Married        | Buddhist   | Asian     | Chinese  | University  | Manager      | \$55,000 | Good   | None       | None  |



|   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |     |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |     |





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| 1312 | 1313 | 1314 | 1315 | 1316 | 1317 | 1318 | 1319 | 1320 | 1321 | 1322 | 1323 | 1324 | 1325 | 1326 | 1327 | 1328 | 1329 | 1330 | 1331 | 1332 | 1333 | 1334 | 1335 | 1336 | 1337 | 1338 | 1339 | 1340 | 1341 | 1342 | 1343 | 1344 | 1345 | 1346 | 1347 | 1348 | 1349 | 1350 | 1351 | 1352 | 1353 | 1354 | 1355 | 1356 | 1357 | 1358 | 1359 | 1360 | 1361 | 1362 | 1363 | 1364 | 1365 | 1366 | 1367 | 1368 | 1369 | 1370 | 1371 | 1372 | 1373 | 1374 | 1375 | 1376 | 1377 | 1378 | 1379 | 1380 | 1381 | 1382 | 1383 | 1384 | 1385 | 1386 | 1387 | 1388 | 1389 | 1390 | 1391 | 1392 | 1393 | 1394 | 1395 | 1396 | 1397 | 1398 | 1399 | 1400 | 1401 | 1402 | 1403 | 1404 | 1405 | 1406 | 1407 | 1408 | 1409 | 1410 | 1411 | 1412 | 1413 | 1414 | 1415 | 1416 | 1417 | 1418 | 1419 | 1420 | 1421 | 1422 | 1423 | 1424 | 1425 | 1426 | 1427 | 1428 | 1429 | 1430 | 1431 | 1432 | 1433 | 1434 | 1435 | 1436 | 1437 | 1438 | 1439 | 1440 | 1441 | 1442 | 1443 | 1444 | 1445 | 1446 | 1447 | 1448 | 1449 | 1450 | 1451 | 1452 | 1453 | 1454 | 1455 | 1456 | 1457 | 1458 | 1459 | 1460 | 1461 | 1462 | 1463 | 1464 | 1465 | 1466 | 1467 | 1468 | 1469 | 1470 | 1471 | 1472 | 1473 | 1474 | 1475 | 1476 | 1477 | 1478 | 1479 | 1480 | 1481 | 1482 | 1483 | 1484 | 1485 | 1486 | 1487 | 1488 | 1489 | 1490 | 1491 | 1492 | 1493 | 1494 | 1495 | 1496 | 1497 | 1498 | 1499 | 1500 | 1501 | 1502 | 1503 | 1504 | 1505 | 1506 | 1507 | 1508 | 1509 | 1510 | 1511 | 1512 | 1513 | 1514 | 1515 | 1516 | 1517 | 1518 | 1519 | 1520 | 1521 | 1522 | 1523 | 1524 | 1525 | 1526 | 1527 | 1528 | 1529 | 1530 | 1531 | 1532 | 1533 | 1534 | 1535 | 1536 | 1537 | 1538 | 1539 | 1540 | 1541 | 1542 | 1543 | 1544 | 1545 | 1546 | 1547 | 1548 | 1549 | 1550 | 1551 | 1552 | 1553 | 1554 | 1555 | 1556 | 1557 | 1558 | 1559 | 1560 | 1561 | 1562 | 1563 | 1564 | 1565 | 1566 | 1567 | 1568 | 1569 | 1570 | 1571 | 1572 | 1573 | 1574 | 1575 | 1576 | 1577 | 1578 | 1579 | 1580 | 1581 | 1582 | 1583 | 1584 | 1585 | 1586 | 1587 | 1588 | 1589 | 1590 | 1591 | 1592 | 1593 | 1594 | 1595 | 1596 | 1597 | 1598 | 1599 | 1600 | 1601 | 1602 | 1603 | 1604 | 1605 | 1606 | 1607 | 1608 | 1609 | 1610 | 1611 | 1612 | 1613 | 1614 | 1615 | 1616 | 1617 | 1618 | 1619 | 1620 | 1621 | 1622 | 1623 | 1624 | 1625 | 1626 | 1627 | 1628 | 1629 | 1630 | 1631 | 1632 | 1633 | 1634 | 1635 | 1636 | 1637 | 1638 | 1639 | 1640 | 1641 | 1642 | 1643 | 1644 | 1645 | 1646 | 1647 | 1648 | 1649 | 1650 | 1651 | 1652 | 1653 | 1654 | 1655 | 1656 | 1657 | 1658 | 1659 | 1660 | 1661 | 1662 | 1663 | 1664 | 1665 | 1666 | 1667 | 1668 | 1669 | 1670 | 1671 | 1672 | 1673 | 1674 | 1675 | 1676 | 1677 | 1678 | 1679 | 1680 | 1681 | 1682 | 1683 | 1684 | 1685 | 1686 | 1687 | 1688 | 1689 | 1690 | 1691 | 1692 | 1693 | 1694 | 1695 | 1696 | 1697 | 1698 | 1699 | 1700 | 1701 | 1702 | 1703 | 1704 | 1705 | 1706 | 1707 | 1708 | 1709 | 1710 | 1711 | 1712 | 1713 | 1714 | 1715 | 1716 | 1717 | 1718 | 1719 | 1720 | 1721 | 1722 | 1723 | 1724 | 1725 | 1726 | 1727 | 1728 | 1729 | 1730 | 1731 | 1732 | 1733 | 1734 | 1735 | 1736 | 1737 | 1738 | 1739 | 1740 | 1741 | 1742 | 1743 | 1744 | 1745 | 1746 | 1747 | 1748 | 1749 | 1750 | 1751 | 1752 | 1753 | 1754 | 1755 | 1756 | 1757 | 1758 | 1759 | 1760 | 1761 | 1762 | 1763 | 1764 | 1765 | 1766 | 1767 | 1768 | 1769 | 1770 | 1771 | 1772 | 1773 | 1774 | 1775 | 1776 | 1777 | 1778 | 1779 | 1780 | 1781 | 1782 | 1783 | 1784 | 1785 | 1786 | 1787 | 1788 | 1789 | 1790 | 1791 | 1792 | 1793 | 1794 | 1795 | 1796 | 1797 | 1798 | 1799 | 1800 | 1801 | 1802 | 1803 | 1804 | 1805 | 1806 | 1807 | 1808 | 1809 | 1810 | 1811 | 1812 | 1813 | 1814 | 1815 | 1816 | 1817 | 1818 | 1819 | 1820 | 1821 | 1822 | 1823 | 1824 | 1825 | 1826 | 1827 | 1828 | 1829 | 1830 | 1831 | 1832 | 1833 | 1834 | 1835 | 1836 | 1837 | 1838 | 1839 | 1840 | 1841 | 1842 | 1843 | 1844 | 1845 | 1846 | 1847 | 1848 | 1849 | 1850 | 1851 | 1852 | 1853 | 1854 | 1855 | 1856 | 1857 | 1858 | 1859 | 1860 | 1861 | 1862 | 1863 | 1864 | 1865 | 1866 | 1867 | 1868 | 1869 | 1870 | 1871 | 1872 | 1873 | 1874 | 1875 | 1876 | 1877 | 1878 | 1879 | 1880 | 1881 | 1882 | 1883 | 1884 | 1885 | 1886 | 1887 | 1888 | 1889 | 1890 | 1891 | 1892 | 1893 | 1894 | 1895 | 1896 | 1897 | 1898 | 1899 | 1900 | 1901 | 1902 | 1903 | 1904 | 1905 | 1906 | 1907 | 1908 | 1909 | 1910 | 1911 | 1912 | 1913 | 1914 | 1915 | 1916 | 1917 | 1918 | 1919 | 1920 | 1921 | 1922 | 1923 | 1924 | 1925 | 1926 | 1927 | 1928 | 1929 | 1930 | 1931 | 1932 | 1933 | 1934 | 1935 | 1936 | 1937 | 1938 | 1939 | 1940 | 1941 | 1942 | 1943 | 1944 | 1945 | 1946 | 1947 | 1948 | 1949 | 1950 | 1951 | 1952 | 1953 | 1954 | 1955 | 1956 | 1957 | 1958 | 1959 | 1960 | 1961 | 1962 | 1963 | 1964 | 1965 | 1966 | 1967 | 1968 | 1969 | 1970 | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 |
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| 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500 |     |      |
| 100 | 101 | 102 | 103 | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 | 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200  |
| 200 | 201 | 202 | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 | 214 | 215 | 216 | 217 | 218 | 219 | 220 | 221 | 222 | 223 | 224 | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 | 256 | 257 | 258 | 259 | 260 | 261 | 262 | 263 | 264 | 265 | 266 | 267 | 268 | 269 | 270 | 271 | 272 | 273 | 274 | 275 | 276 | 277 | 278 | 279 | 280 | 281 | 282 | 283 | 284 | 285 | 286 | 287 | 288 | 289 | 290 | 291 | 292 | 293 | 294 | 295 | 296 | 297 | 298 | 299 | 300  |
| 300 | 301 | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 | 324 | 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 | 390 | 391 | 392 | 393 | 394 | 395 | 396 | 397 | 398 | 399 | 400  |
| 400 | 401 | 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500  |
| 500 | 501 | 502 | 503 | 504 | 505 | 506 | 507 | 508 | 509 | 510 | 511 | 512 | 513 | 514 | 515 | 516 | 517 | 518 | 519 | 520 | 521 | 522 | 523 | 524 | 525 | 526 | 527 | 528 | 529 | 530 | 531 | 532 | 533 | 534 | 535 | 536 | 537 | 538 | 539 | 540 | 541 | 542 | 543 | 544 | 545 | 546 | 547 | 548 | 549 | 550 | 551 | 552 | 553 | 554 | 555 | 556 | 557 | 558 | 559 | 560 | 561 | 562 | 563 | 564 | 565 | 566 | 567 | 568 | 569 | 570 | 571 | 572 | 573 | 574 | 575 | 576 | 577 | 578 | 579 | 580 | 581 | 582 | 583 | 584 | 585 | 586 | 587 | 588 | 589 | 590 | 591 | 592 | 593 | 594 | 595 | 596 | 597 | 598 | 599 | 600  |
| 600 | 601 | 602 | 603 | 604 | 605 | 606 | 607 | 608 | 609 | 610 | 611 | 612 | 613 | 614 | 615 | 616 | 617 | 618 | 619 | 620 | 621 | 622 | 623 | 624 | 625 | 626 | 627 | 628 | 629 | 630 | 631 | 632 | 633 | 634 | 635 | 636 | 637 | 638 | 639 | 640 | 641 | 642 | 643 | 644 | 645 | 646 | 647 | 648 | 649 | 650 | 651 | 652 | 653 | 654 | 655 | 656 | 657 | 658 | 659 | 660 | 661 | 662 | 663 | 664 | 665 | 666 | 667 | 668 | 669 | 670 | 671 | 672 | 673 | 674 | 675 | 676 | 677 | 678 | 679 | 680 | 681 | 682 | 683 | 684 | 685 | 686 | 687 | 688 | 689 | 690 | 691 | 692 | 693 | 694 | 695 | 696 | 697 | 698 | 699 | 700  |
| 700 | 701 | 702 | 703 | 704 | 705 | 706 | 707 | 708 | 709 | 710 | 711 | 712 | 713 | 714 | 715 | 716 | 717 | 718 | 719 | 720 | 721 | 722 | 723 | 724 | 725 | 726 | 727 | 728 | 729 | 730 | 731 | 732 | 733 | 734 | 735 | 736 | 737 | 738 | 739 | 740 | 741 | 742 | 743 | 744 | 745 | 746 | 747 | 748 | 749 | 750 | 751 | 752 | 753 | 754 | 755 | 756 | 757 | 758 | 759 | 760 | 761 | 762 | 763 | 764 | 765 | 766 | 767 | 768 | 769 | 770 | 771 | 772 | 773 | 774 | 775 | 776 | 777 | 778 | 779 | 780 | 781 | 782 | 783 | 784 | 785 | 786 | 787 | 788 | 789 | 790 | 791 | 792 | 793 | 794 | 795 | 796 | 797 | 798 | 799 | 800  |
| 800 | 801 | 802 | 803 | 804 | 805 | 806 | 807 | 808 | 809 | 810 | 811 | 812 | 813 | 814 | 815 | 816 | 817 | 818 | 819 | 820 | 821 | 822 | 823 | 824 | 825 | 826 | 827 | 828 | 829 | 830 | 831 | 832 | 833 | 834 | 835 | 836 | 837 | 838 | 839 | 840 | 841 | 842 | 843 | 844 | 845 | 846 | 847 | 848 | 849 | 850 | 851 | 852 | 853 | 854 | 855 | 856 | 857 | 858 | 859 | 860 | 861 | 862 | 863 | 864 | 865 | 866 | 867 | 868 | 869 | 870 | 871 | 872 | 873 | 874 | 875 | 876 | 877 | 878 | 879 | 880 | 881 | 882 | 883 | 884 | 885 | 886 | 887 | 888 | 889 | 890 | 891 | 892 | 893 | 894 | 895 | 896 | 897 | 898 | 899 | 900  |
| 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 |





























[illegible]

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| 14501 | 14502 | 14503 | 14504 | 14505 | 14506 | 14507 | 14508 | 14509 | 14510 | 14511 | 14512 | 14513 | 14514 | 14515 | 14516 | 14517 | 14518 | 14519 | 14520 | 14521 | 14522 | 14523 | 14524 | 14525 | 14526 | 14527 | 14528 | 14529 | 14530 | 14531 | 14532 | 14533 | 14534 | 14535 | 14536 | 14537 | 14538 | 14539 | 14540 | 14541 | 14542 | 14543 | 14544 | 14545 | 14546 | 14547 | 14548 | 14549 | 14550 | 14551 | 14552 | 14553 | 14554 | 14555 | 14556 | 14557 | 14558 | 14559 | 14560 | 14561 | 14562 | 14563 | 14564 | 14565 | 14566 | 14567 | 14568 | 14569 | 14570 | 14571 | 14572 | 14573 | 14574 | 14575 | 14576 | 14577 | 14578 | 14579 | 14580 | 14581 | 14582 | 14583 | 14584 | 14585 | 14586 | 14587 | 14588 | 14589 | 14590 | 14591 | 14592 | 14593 | 14594 | 14595 | 14596 | 14597 | 14598 | 14599 | 14600 | 14601 | 14602 | 14603 | 14604 | 14605 | 14606 | 14607 | 14608 | 14609 | 14610 | 14611 | 14612 | 14613 | 14614 | 14615 | 14616 | 14617 | 14618 | 14619 | 14620 | 14621 | 14622 | 14623 | 14624 | 14625 | 14626 | 14627 | 14628 | 14629 | 14630 | 14631 | 14632 | 14633 | 14634 | 14635 | 14636 | 14637 | 14638 | 14639 | 14640 | 14641 | 14642 | 14643 | 14644 | 14645 | 14646 | 14647 | 14648 | 14649 | 14650 | 14651 | 14652 | 14653 | 14654 | 14655 | 14656 | 14657 | 14658 | 14659 | 14660 | 14661 | 14662 | 14663 | 14664 | 14665 | 14666 | 14667 | 14668 | 14669 | 14670 | 14671 | 14672 | 14673 | 14674 | 14675 | 14676 | 14677 | 14678 | 14679 | 14680 | 14681 | 14682 | 14683 | 14684 | 14685 | 14686 | 14687 | 14688 | 14689 | 14690 | 14691 | 14692 | 14693 | 14694 | 14695 | 14696 | 14697 | 14698 | 14699 | 14700 | 14701 | 14702 | 14703 | 14704 | 14705 | 14706 | 14707 | 14708 | 14709 | 14710 | 14711 | 14712 | 14713 | 14714 | 14715 | 14716 | 14717 | 14718 | 14719 | 14720 | 14721 | 14722 | 14723 | 14724 | 14725 | 14726 | 14727 | 14728 | 14729 | 14730 | 14731 | 14732 | 14733 | 14734 | 14735 | 14736 | 14737 | 14738 | 14739 | 14740 | 14741 | 14742 | 14743 | 14744 | 14745 | 14746 | 14747 | 14748 | 14749 | 14750 | 14751 | 14752 | 14753 | 14754 | 14755 | 14756 | 14757 | 14758 | 14759 | 14760 | 14761 | 14762 | 14763 | 14764 | 14765 | 14766 | 14767 | 14768 | 14769 | 14770 | 14771 | 14772 | 14773 | 14774 | 14775 | 14776 | 14777 | 14778 | 14779 | 14780 | 14781 | 14782 | 14783 | 14784 | 14785 | 14786 | 14787 | 14788 | 14789 | 14790 | 14791 | 14792 | 14793 | 14794 | 14795 | 14796 | 14797 | 14798 | 14799 | 14800 | 14801 | 14802 | 14803 | 14804 | 14805 | 14806 | 14807 | 14808 | 14809 | 14810 | 14811 | 14812 | 14813 | 14814 | 14815 | 14816 | 14817 | 14818 | 14819 | 14820 | 14821 | 14822 | 14823 | 14824 | 14825 | 14826 | 14827 | 14828 | 14829 | 14830 | 14831 | 14832 | 14833 | 14834 | 14835 | 14836 | 14837 | 14838 | 14839 | 14840 | 14841 | 14842 | 14843 | 14844 | 14845 | 14846 | 14847 | 14848 | 14849 | 14850 | 14851 | 14852 | 14853 | 14854 | 14855 | 14856 | 14857 | 14858 | 14859 | 14860 | 14861 | 14862 | 14863 | 14864 | 14865 | 14866 | 14867 | 14868 | 14869 | 14870 | 14871 | 14872 | 14873 | 14874 | 14875 | 14876 | 14877 | 14878 | 14879 | 14880 | 14881 | 14882 | 14883 | 14884 | 14885 | 14886 | 14887 | 14888 | 14889 | 14890 | 14891 | 14892 | 14893 | 14894 | 14895 | 14896 | 14897 | 14898 | 14899 | 14900 | 14901 | 14902 | 14903 | 14904 | 14905 | 14906 | 14907 | 14908 | 14909 | 14910 | 14911 | 14912 | 14913 | 14914 | 14915 | 14916 | 14917 | 14918 | 14919 | 14920 | 14921 | 14922 | 14923 | 14924 | 14925 | 14926 | 14927 | 14928 | 14929 | 14930 | 14931 | 14932 | 14933 | 14934 | 14935 | 14936 | 14937 | 14938 | 14939 | 14940 | 14941 | 14942 | 14943 | 14944 | 14945 | 14946 | 14947 | 14948 | 14949 | 14950 | 14951 | 14952 | 14953 | 14954 | 14955 | 14956 | 14957 | 14958 | 14959 | 14960 | 14961 | 14962 | 14963 | 14964 | 14965 | 14966 | 14967 | 14968 | 14969 | 14970 | 14971 | 14972 | 14973 | 14974 | 14975 | 14976 | 14977 | 14978 | 14979 | 14980 | 14981 | 14982 | 14983 | 14984 | 14985 | 14986 | 14987 | 14988 | 14989 | 14990 | 14991 | 14992 | 14993 | 14994 | 14995 | 14996 | 14997 | 14998 | 14999 | 15000 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|



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| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89   | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89   | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89   | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89   | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89   | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89</ |    |    |    |    |    |    |    |    |    |    |     |







| Global Project Performance Dashboard - Q3 2023 |                     |                   |              |                |                  |                 |              |                   |            |
|------------------------------------------------|---------------------|-------------------|--------------|----------------|------------------|-----------------|--------------|-------------------|------------|
| Project Overview                               |                     | Financial Metrics |              |                | Operational Data |                 |              | Compliance & Risk |            |
| Project ID                                     | Project Name        | Budget (M\$)      | Actual (M\$) | Variance (M\$) | Progress (%)     | Resources (FTE) | Issues Count | Audit Score       | Risk Level |
| P001                                           | Alpha Initiative    | 1.2               | 1.15         | 0.05           | 85%              | 15              | 12           | 92                | Low        |
| P002                                           | Beta Expansion      | 0.8               | 0.82         | -0.02          | 70%              | 10              | 8            | 88                | Medium     |
| P003                                           | Gamma Upgrade       | 2.5               | 2.6          | -0.1           | 90%              | 25              | 15           | 95                | Low        |
| P004                                           | Delta Integration   | 1.5               | 1.4          | 0.1            | 75%              | 18              | 10           | 90                | Medium     |
| P005                                           | Epsilon Launch      | 0.5               | 0.55         | -0.05          | 60%              | 8               | 5            | 85                | High       |
| P006                                           | Zeta Rollout        | 1.8               | 1.7          | 0.1            | 80%              | 20              | 12           | 91                | Medium     |
| P007                                           | Eta Deployment      | 0.9               | 0.92         | -0.02          | 72%              | 12              | 7            | 87                | Medium     |
| P008                                           | Theta Migration     | 2.1               | 2.2          | -0.1           | 88%              | 22              | 14           | 93                | Low        |
| P009                                           | Iota Integration    | 1.3               | 1.25         | 0.05           | 78%              | 16              | 9            | 89                | Medium     |
| P010                                           | Kappa Upgrade       | 0.7               | 0.73         | -0.03          | 65%              | 9               | 6            | 86                | High       |
| P011                                           | Lambda Launch       | 1.6               | 1.55         | 0.05           | 82%              | 19              | 11           | 90                | Medium     |
| P012                                           | Mu Deployment       | 0.6               | 0.62         | -0.02          | 68%              | 7               | 4            | 84                | High       |
| P013                                           | Nu Migration        | 2.3               | 2.4          | -0.1           | 89%              | 23              | 13           | 94                | Low        |
| P014                                           | Xi Integration      | 1.4               | 1.38         | 0.02           | 76%              | 17              | 10           | 88                | Medium     |
| P015                                           | Omicron Upgrade     | 0.8               | 0.85         | -0.05          | 62%              | 9               | 5            | 83                | High       |
| P016                                           | Pi Launch           | 1.9               | 1.85         | 0.05           | 81%              | 21              | 12           | 91                | Medium     |
| P017                                           | Rho Deployment      | 0.7               | 0.72         | -0.02          | 66%              | 8               | 5            | 85                | High       |
| P018                                           | Sigma Migration     | 2.0               | 2.1          | -0.1           | 87%              | 20              | 11           | 92                | Low        |
| P019                                           | Tau Integration     | 1.1               | 1.08         | 0.02           | 74%              | 14              | 8            | 87                | Medium     |
| P020                                           | Upsilon Upgrade     | 0.9               | 0.95         | -0.05          | 64%              | 10              | 6            | 84                | High       |
| P021                                           | Phi Launch          | 1.7               | 1.65         | 0.05           | 83%              | 18              | 11           | 90                | Medium     |
| P022                                           | Chi Deployment      | 0.6               | 0.63         | -0.03          | 67%              | 7               | 4            | 85                | High       |
| P023                                           | Psi Migration       | 2.2               | 2.3          | -0.1           | 86%              | 22              | 12           | 93                | Low        |
| P024                                           | Omega Integration   | 1.3               | 1.28         | 0.02           | 77%              | 16              | 9            | 88                | Medium     |
| P025                                           | Alpha Upgrade       | 0.8               | 0.84         | -0.04          | 63%              | 9               | 5            | 83                | High       |
| P026                                           | Beta Launch         | 1.5               | 1.48         | 0.02           | 80%              | 17              | 10           | 89                | Medium     |
| P027                                           | Gamma Deployment    | 0.7               | 0.75         | -0.05          | 61%              | 8               | 5            | 82                | High       |
| P028                                           | Delta Migration     | 2.4               | 2.5          | -0.1           | 89%              | 24              | 13           | 94                | Low        |
| P029                                           | Epsilon Integration | 1.2               | 1.18         | 0.02           | 75%              | 15              | 8            | 87                | Medium     |
| P030                                           | Zeta Upgrade        | 0.9               | 0.96         | -0.06          | 65%              | 10              | 6            | 84                | High       |
| P031                                           | Eta Launch          | 1.8               | 1.75         | 0.05           | 82%              | 20              | 11           | 91                | Medium     |
| P032                                           | Theta Deployment    | 0.6               | 0.64         | -0.04          | 68%              | 7               | 4            | 85                | High       |
| P033                                           | Iota Migration      | 2.1               | 2.2          | -0.1           | 88%              | 21              | 12           | 92                | Low        |
| P034                                           | Kappa Integration   | 1.4               | 1.35         | 0.05           | 76%              | 17              | 9            | 88                | Medium     |
| P035                                           | Lambda Upgrade      | 0.8               | 0.86         | -0.06          | 62%              | 9               | 5            | 83                | High       |
| P036                                           | Mu Launch           | 1.6               | 1.58         | 0.02           | 81%              | 18              | 10           | 90                | Medium     |
| P037                                           | Nu Deployment       | 0.7               | 0.73         | -0.03          | 66%              | 8               | 5            | 85                | High       |
| P038                                           | Xi Migration        | 2.3               | 2.4          | -0.1           | 89%              | 23              | 13           | 93                | Low        |
| P039                                           | Omicron Integration | 1.1               | 1.09         | 0.01           | 74%              | 14              | 8            | 87                | Medium     |
| P040                                           | Pi Upgrade          | 0.9               | 0.97         | -0.07          | 64%              | 10              | 6            | 84                | High       |
| P041                                           | Rho Launch          | 1.7               | 1.68         | 0.02           | 83%              | 18              | 11           | 90                | Medium     |
| P042                                           | Sigma Deployment    | 0.6               | 0.65         | -0.05          | 67%              | 7               | 4            | 85                | High       |
| P043                                           | Tau Migration       | 2.2               | 2.3          | -0.1           | 86%              | 22              | 12           | 92                | Low        |





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| 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 | 390 | 391 | 392 | 393 | 394 | 395 | 396 | 397 | 398 | 399 | 400 | 401 | 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500 | 501 | 502 | 503 | 504 | 505 | 506 | 507 | 508 | 509 | 510 | 511 | 512 | 513 | 514 | 515 | 516 | 517 | 518 | 519 | 520 | 521 | 522 | 523 | 524 | 525 | 526 | 527 | 528 | 529 | 530 | 531 | 532 | 533 | 534 | 535 | 536 | 537 | 538 | 539 | 540 | 541 | 542 | 543 | 544 | 545 | 546 | 547 | 548 | 549 | 550 | 551 | 552 | 553 | 554 | 555 | 556 | 557 | 558 | 559 | 560 | 561 | 562 | 563 | 564 | 565 | 566 | 567 | 568 | 569 | 570 | 571 | 572 | 573 | 574 | 575 | 576 | 577 | 578 | 579 | 580 | 581 | 582 | 583 | 584 | 585 | 586 | 587 | 588 | 589 | 590 | 591 | 592 | 593 | 594 | 595 | 596 | 597 | 598 | 599 | 600 | 601 | 602 | 603 | 604 | 605 | 606 | 607 | 608 | 609 | 610 | 611 | 612 | 613 | 614 | 615 | 616 | 617 | 618 | 619 | 620 | 621 | 622 | 623 | 624 | 625 | 626 | 627 | 628 | 629 | 630 | 631 | 632 | 633 | 634 | 635 | 636 | 637 | 638 | 639 | 640 | 641 | 642 | 643 | 644 | 645 | 646 | 647 | 648 | 649 | 650 | 651 | 652 | 653 | 654 | 655 | 656 | 657 | 658 | 659 | 660 | 661 | 662 | 663 | 664 | 665 | 666 | 667 | 668 | 669 | 670 | 671 | 672 | 673 | 674 | 675 | 676 | 677 | 678 | 679 | 680 | 681 | 682 | 683 | 684 | 685 | 686 | 687 | 688 | 689 | 690 | 691 | 692 | 693 | 694 | 695 | 696 | 697 | 698 | 699 | 700 | 701 | 702 | 703 | 704 | 705 | 706 | 707 | 708 | 709 | 710 | 711 | 712 | 713 | 714 | 715 | 716 | 717 | 718 | 719 | 720 | 721 | 722 | 723 | 724 | 725 | 726 | 727 | 728 | 729 | 730 | 731 | 732 | 733 | 734 | 735 | 736 | 737 | 738 | 739 | 740 | 741 | 742 | 743 | 744 | 745 | 746 | 747 | 748 | 749 | 750 | 751 | 752 | 753 | 754 | 755 | 756 | 757 | 758 | 759 | 760 | 761 | 762 | 763 | 764 | 765 | 766 | 767 | 768 | 769 | 770 | 771 | 772 | 773 | 774 | 775 | 776 | 777 | 778 | 779 | 780 | 781 | 782 | 783 | 784 | 785 | 786 | 787 | 788 | 789 | 790 | 791 | 792 | 793 | 794 | 795 | 796 | 797 | 798 | 799 | 800 | 801 | 802 | 803 | 804 | 805 | 806 | 807 | 808 | 809 | 810 | 811 | 812 | 813 | 814 | 815 | 816 | 817 | 818 | 819 | 820 | 821 | 822 | 823 | 824 | 825 | 826 | 827 | 828 | 829 | 830 | 831 | 832 | 833 | 834 | 835 | 836 | 837 | 838 | 839 | 840 | 841 | 842 | 843 | 844 | 845 | 846 | 847 | 848 | 849 | 850 | 851 | 852 | 853 | 854 | 855 | 856 | 857 | 858 | 859 | 860 | 861 | 862 | 863 | 864 | 865 | 866 | 867 | 868 | 869 | 870 | 871 | 872 | 873 | 874 | 875 | 876 | 877 | 878 | 879 | 880 | 881 | 882 | 883 | 884 | 885 | 886 | 887 | 888 | 889 | 890 | 891 | 892 | 893 | 894 | 895 | 896 | 897 | 898 | 899 | 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 |
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| 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 |
| 100 | 101 | 102 | 103 | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 | 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200  |
| 200 | 201 | 202 | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 | 214 | 215 | 216 | 217 | 218 | 219 | 220 | 221 | 222 | 223 | 224 | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 | 256 | 257 | 258 | 259 | 260 | 261 | 262 | 263 | 264 | 265 | 266 | 267 | 268 | 269 | 270 | 271 | 272 | 273 | 274 | 275 | 276 | 277 | 278 | 279 | 280 | 281 | 282 | 283 | 284 | 285 | 286 | 287 | 288 | 289 | 290 | 291 | 292 | 293 | 294 | 295 | 296 | 297 | 298 | 299 | 300  |
| 300 | 301 | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 | 324 | 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 | 390 | 391 | 392 | 393 | 394 | 395 | 396 | 397 | 398 | 399 | 400  |
| 400 | 401 | 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500  |
| 500 | 501 | 502 | 503 | 504 | 505 | 506 | 507 | 508 | 509 | 510 | 511 | 512 | 513 | 514 | 515 | 516 | 517 | 518 | 519 | 520 | 521 | 522 | 523 | 524 | 525 | 526 | 527 | 528 | 529 | 530 | 531 | 532 | 533 | 534 | 535 | 536 | 537 | 538 | 539 | 540 | 541 | 542 | 543 | 544 | 545 | 546 | 547 | 548 | 549 | 550 | 551 | 552 | 553 | 554 | 555 | 556 | 557 | 558 | 559 | 560 | 561 | 562 | 563 | 564 | 565 | 566 | 567 | 568 | 569 | 570 | 571 | 572 | 573 | 574 | 575 | 576 | 577 | 578 | 579 | 580 | 581 | 582 | 583 | 584 | 585 | 586 | 587 | 588 | 589 | 590 | 591 | 592 | 593 | 594 | 595 | 596 | 597 | 598 | 599 | 600  |
| 600 | 601 | 602 | 603 | 604 | 605 | 606 | 607 | 608 | 609 | 610 | 611 | 612 | 613 | 614 | 615 | 616 | 617 | 618 | 619 | 620 | 621 | 622 | 623 | 624 | 625 | 626 | 627 | 628 | 629 | 630 | 631 | 632 | 633 | 634 | 635 | 636 | 637 | 638 | 639 | 640 | 641 | 642 | 643 | 644 | 645 | 646 | 647 | 648 | 649 | 650 | 651 | 652 | 653 | 654 | 655 | 656 | 657 | 658 | 659 | 660 | 661 | 662 | 663 | 664 | 665 | 666 | 667 | 668 | 669 | 670 | 671 | 672 | 673 | 674 | 675 | 676 | 677 | 678 | 679 | 680 | 681 | 682 | 683 | 684 | 685 | 686 | 687 | 688 | 689 | 690 | 691 | 692 | 693 | 694 | 695 | 696 | 697 | 698 | 699 | 700  |
| 700 | 701 | 702 | 703 | 704 | 705 | 706 | 707 | 708 | 709 | 710 | 711 | 712 | 713 | 714 | 715 | 716 | 717 | 718 | 719 | 720 | 721 | 722 | 723 | 724 | 725 | 726 | 727 | 728 | 729 | 730 | 731 | 732 | 733 | 734 | 735 | 736 | 737 | 738 | 739 | 740 | 741 | 742 | 743 | 744 | 745 | 746 | 747 | 748 | 749 | 750 | 751 | 752 | 753 | 754 | 755 | 756 | 757 | 758 | 759 | 760 | 761 | 762 | 763 | 764 | 765 | 766 | 767 | 768 | 769 | 770 | 771 | 772 | 773 | 774 | 775 | 776 | 777 | 778 | 779 | 780 | 781 | 782 | 783 | 784 | 785 | 786 | 787 | 788 | 789 | 790 | 791 | 792 | 793 | 794 | 795 | 796 | 797 | 798 | 799 | 800  |
| 800 | 801 | 802 | 803 | 804 | 805 | 806 | 807 | 808 | 809 | 810 | 811 | 812 | 813 | 814 | 815 | 816 | 817 | 818 | 819 | 820 | 821 | 822 | 823 | 824 | 825 | 826 | 827 | 828 | 829 | 830 | 831 | 832 | 833 | 834 | 835 | 836 | 837 | 838 | 839 | 840 | 841 | 842 | 843 | 844 | 845 | 846 | 847 | 848 | 849 | 850 | 851 | 852 | 853 | 854 | 855 | 856 | 857 | 858 | 859 | 860 | 861 | 862 | 863 | 864 | 865 | 866 | 867 | 868 | 869 | 870 | 871 | 872 | 873 | 874 | 875 | 876 | 877 | 878 | 879 | 880 | 881 | 882 | 883 | 884 | 885 | 886 | 887 | 888 | 889 | 890 | 891 | 892 | 893 | 894 | 895 | 896 | 897 | 898 | 899 | 900  |
| 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 |





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| 4243 | 4244 | 4245 | 4246 | 4247 | 4248 | 4249 | 4250 | 4251 | 4252 | 4253 | 4254 | 4255 | 4256 | 4257 | 4258 | 4259 | 4260 | 4261 | 4262 | 4263 | 4264 | 4265 | 4266 | 4267 | 4268 | 4269 | 4270 | 4271 | 4272 | 4273 | 4274 | 4275 | 4276 | 4277 | 4278 | 4279 | 4280 | 4281 | 4282 | 4283 | 4284 | 4285 | 4286 | 4287 | 4288 | 4289 | 4290 | 4291 | 4292 | 4293 | 4294 | 4295 | 4296 | 4297 | 4298 | 4299 | 4300 | 4301 | 4302 | 4303 | 4304 | 4305 | 4306 | 4307 | 4308 | 4309 | 4310 | 4311 | 4312 | 4313 | 4314 | 4315 | 4316 | 4317 | 4318 | 4319 | 4320 | 4321 | 4322 | 4323 | 4324 | 4325 | 4326 | 4327 | 4328 | 4329 | 4330 | 4331 | 4332 | 4333 | 4334 | 4335 | 4336 | 4337 | 4338 | 4339 | 4340 | 4341 | 4342 | 4343 | 4344 | 4345 | 4346 | 4347 | 4348 | 4349 | 4350 | 4351 | 4352 | 4353 | 4354 | 4355 | 4356 | 4357 | 4358 | 4359 | 4360 | 4361 | 4362 | 4363 | 4364 | 4365 | 4366 | 4367 | 4368 | 4369 | 4370 | 4371 | 4372 | 4373 | 4374 | 4375 | 4376 | 4377 | 4378 | 4379 | 4380 | 4381 | 4382 | 4383 | 4384 | 4385 | 4386 | 4387 | 4388 | 4389 | 4390 | 4391 | 4392 | 4393 | 4394 | 4395 | 4396 | 4397 | 4398 | 4399 | 4400 | 4401 | 4402 | 4403 | 4404 | 4405 | 4406 | 4407 | 4408 | 4409 | 4410 | 4411 | 4412 | 4413 | 4414 | 4415 | 4416 | 4417 | 4418 | 4419 | 4420 | 4421 | 4422 | 4423 | 4424 | 4425 | 4426 | 4427 | 4428 | 4429 | 4430 | 4431 | 4432 | 4433 | 4434 | 4435 | 4436 | 4437 | 4438 | 4439 | 4440 | 4441 | 4442 | 4443 | 4444 | 4445 | 4446 | 4447 | 4448 | 4449 | 4450 | 4451 | 4452 | 4453 | 4454 | 4455 | 4456 | 4457 | 4458 | 4459 | 4460 | 4461 | 4462 | 4463 | 4464 | 4465 | 4466 | 4467 | 4468 | 4469 | 4470 | 4471 | 4472 | 4473 | 4474 | 4475 | 4476 | 4477 | 4478 | 4479 | 4480 | 4481 | 4482 | 4483 | 4484 | 4485 | 4486 | 4487 | 4488 | 4489 | 4490 | 4491 | 4492 | 4493 | 4494 | 4495 | 4496 | 4497 | 4498 | 4499 | 4500 | 4501 | 4502 | 4503 | 4504 | 4505 | 4506 | 4507 | 4508 | 4509 | 4510 | 4511 | 4512 | 4513 | 4514 | 4515 | 4516 | 4517 | 4518 | 4519 | 4520 | 4521 | 4522 | 4523 | 4524 | 4525 | 4526 | 4527 | 4528 | 4529 | 4530 | 4531 | 4532 | 4533 | 4534 | 4535 | 4536 | 4537 | 4538 | 4539 | 4540 | 4541 | 4542 | 4543 | 4544 | 4545 | 4546 | 4547 | 4548 | 4549 | 4550 | 4551 | 4552 | 4553 | 4554 | 4555 | 4556 | 4557 | 4558 | 4559 | 4560 | 4561 | 4562 | 4563 | 4564 | 4565 | 4566 | 4567 | 4568 | 4569 | 4570 | 4571 | 4572 | 4573 | 4574 | 4575 | 4576 | 4577 | 4578 | 4579 | 4580 | 4581 | 4582 | 4583 | 4584 | 4585 | 4586 | 4587 | 4588 | 4589 | 4590 | 4591 | 4592 | 4593 | 4594 | 4595 | 4596 | 4597 | 4598 | 4599 | 4600 | 4601 | 4602 | 4603 | 4604 | 4605 | 4606 | 4607 | 4608 | 4609 | 4610 | 4611 | 4612 | 4613 | 4614 | 4615 | 4616 | 4617 | 4618 | 4619 | 4620 | 4621 | 4622 | 4623 | 4624 | 4625 | 4626 | 4627 | 4628 | 4629 | 4630 | 4631 | 4632 | 4633 | 4634 | 4635 | 4636 | 4637 | 4638 | 4639 | 4640 | 4641 | 4642 | 4643 | 4644 | 4645 | 4646 | 4647 | 4648 | 4649 | 4650 | 4651 | 4652 | 4653 | 4654 | 4655 | 4656 | 4657 | 4658 | 4659 | 4660 | 4661 | 4662 | 4663 | 4664 | 4665 | 4666 | 4667 | 4668 | 4669 | 4670 | 4671 | 4672 | 4673 | 4674 | 4675 | 4676 | 4677 | 4678 | 4679 | 4680 | 4681 | 4682 | 4683 | 4684 | 4685 | 4686 | 4687 | 4688 | 4689 | 4690 | 4691 | 4692 | 4693 | 4694 | 4695 | 4696 | 4697 | 4698 | 4699 | 4700 | 4701 | 4702 | 4703 | 4704 | 4705 | 4706 | 4707 | 4708 | 4709 | 4710 | 4711 | 4712 | 4713 | 4714 | 4715 | 4716 | 4717 | 4718 | 4719 | 4720 | 4721 | 4722 | 4723 | 4724 | 4725 | 4726 | 4727 | 4728 | 4729 | 4730 | 4731 | 4732 | 4733 | 4734 | 4735 | 4736 | 4737 | 4738 | 4739 | 4740 | 4741 | 4742 | 4743 | 4744 | 4745 | 4746 | 4747 | 4748 | 4749 | 4750 | 4751 | 4752 | 4753 | 4754 | 4755 | 4756 | 4757 | 4758 | 4759 | 4760 | 4761 | 4762 | 4763 | 4764 | 4765 | 4766 | 4767 | 4768 | 4769 | 4770 | 4771 | 4772 | 4773 | 4774 | 4775 | 4776 | 4777 | 4778 | 4779 | 4780 | 4781 | 4782 | 4783 | 4784 | 4785 | 4786 | 4787 | 4788 | 4789 | 4790 | 4791 | 4792 | 4793 | 4794 | 4795 | 4796 | 4797 | 4798 | 4799 | 4800 | 4801 | 4802 | 4803 | 4804 | 4805 | 4806 | 4807 | 4808 | 4809 | 4810 | 4811 | 4812 | 4813 | 4814 | 4815 | 4816 | 4817 | 4818 | 4819 | 4820 | 4821 | 4822 | 4823 | 4824 | 4825 | 4826 | 4827 | 4828 | 4829 | 4830 | 4831 | 4832 | 4833 | 4834 | 4835 | 4836 | 4837 | 4838 | 4839 | 4840 | 4841 | 4842 | 4843 | 4844 | 4845 | 4846 | 4847 | 4848 | 4849 | 4850 | 4851 | 4852 | 4853 | 4854 | 4855 | 4856 | 4857 | 4858 | 4859 | 4860 | 4861 | 4862 | 4863 | 4864 | 4865 | 4866 | 4867 | 4868 | 4869 | 4870 | 4871 | 4872 | 4873 | 4874 | 4875 | 4876 | 4877 | 4878 | 4879 | 4880 | 4881 | 4882 | 4883 | 4884 | 4885 | 4886 | 4887 | 4888 | 4889 | 4890 | 4891 | 4892 | 4893 | 4894 | 4895 | 4896 | 4897 | 4898 | 4899 | 4900 | 4901 | 4902 | 4903 | 4904 | 4905 | 4906 | 4907 | 4908 | 4909 | 4910 | 4911 | 4912 | 4913 | 4914 | 4915 | 4916 | 4917 | 4918 | 4919 | 4920 | 4921 | 4922 | 4923 | 4924 | 4925 | 4926 | 4927 | 4928 | 4929 | 4930 | 4931 | 4932 | 4933 | 4934 | 4935 | 4936 | 4937 | 4938 | 4939 | 4940 | 4941 | 4942 | 4943 | 4944 | 4945 | 4946 | 4947 | 4948 | 4949 | 4950 | 4951 | 4952 | 4953 | 4954 | 4955 | 4956 | 4957 | 4958 | 4959 | 4960 | 4961 | 4962 | 4963 | 4964 | 4965 | 4966 | 4967 | 4968 | 4969 | 4970 | 4971 | 4972 | 4973 | 4974 | 4975 | 4976 | 4977 | 4978 | 4979 | 4980 | 4981 | 4982 | 4983 | 4984 | 4985 | 4986 | 4987 | 4988 | 4989 | 4990 | 4991 | 4992 | 4993 | 4994 | 4995 | 4996 | 4997 | 4998 | 4999 | 5000 |
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**APPENDIX F: QUAL-IT SOURCES**

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Figure 1

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1. **Introduction**  
 2. **Methodology**  
 3. **Results**  
 4. **Discussion**  
 5. **Conclusion**

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1. The first part of the paper is devoted to the study of the properties of the function  $f(x)$  defined by the equation  $f(x) = \sum_{n=0}^{\infty} a_n x^n$ , where  $a_n$  are the coefficients of the power series. The function  $f(x)$  is shown to be analytic in the disk  $|x| < 1$  and to have a removable singularity at  $x = 1$ . The function  $f(x)$  is also shown to be bounded in the disk  $|x| < 1$  and to have a limit as  $x \rightarrow 1^-$ . The function  $f(x)$  is also shown to be continuous at  $x = 1$ .

2. The second part of the paper is devoted to the study of the properties of the function  $g(x)$  defined by the equation  $g(x) = \sum_{n=0}^{\infty} b_n x^n$ , where  $b_n$  are the coefficients of the power series. The function  $g(x)$  is shown to be analytic in the disk  $|x| < 1$  and to have a removable singularity at  $x = 1$ . The function  $g(x)$  is also shown to be bounded in the disk  $|x| < 1$  and to have a limit as  $x \rightarrow 1^-$ . The function  $g(x)$  is also shown to be continuous at  $x = 1$ .

## **APPENDIX G: CONCEPTUAL PROCESSES IN RIVERINE WATER QUALITY KINETICS MODEL**

This Appendix contains Chapter 5 of the following reference

Chapra, S.C., Pelletier, G.J. and Tao, H. 2007. QUAL2K: A Modeling Framework for Simulating River and Stream Water Quality, Version 2.07: Documentation and Users Manual. Civil and Environmental Engineering Dept., Tufts University, Medford, MA., Steven.Chapra@tufts.edu

and is presented as an illustrative example of conceptual elements in a modern water quality model.

## 5 CONSTITUENT MODEL

### 5.1 Constituents and General Mass Balance

The model constituents are listed in Table 5.

Table 5 Model state variables

| Variable                   | Symbol     | Units*                 |
|----------------------------|------------|------------------------|
| Conductivity               | $\sigma$   | umhos                  |
| Inorganic suspended solids | $m_i$      | mg/L                   |
| Bottom algae biomass       | $\sigma_b$ | mg/L                   |
| Steady reacting CBOD       | $c_1$      | mgO <sub>2</sub> /L    |
| Fast reacting CBOD         | $c_2$      | mgO <sub>2</sub> /L    |
| Organic nitrogen           | $n_o$      | µg/L                   |
| Ammonia nitrogen           | $n_a$      | µg/L                   |
| Nitrate nitrogen           | $n_n$      | µg/L                   |
| Organic phosphorus         | $p_o$      | µg/L                   |
| Inorganic phosphorus       | $p_i$      | µg/L                   |
| Phosphate                  | $p_p$      | µg/L                   |
| Cellulose                  | $x_c$      | mg/L                   |
| Phytogen                   | $x_p$      | mg/L                   |
| Alkalinity                 | $Al$       | mgCaCO <sub>3</sub> /L |
| Total inorganic carbon     | $c_t$      | mg/L                   |
| Bottom algae biomass       | $\sigma_b$ | mg/L                   |
| Bottom algae phosphorus    | $p_b$      | mg/L                   |
| Bottom algae nitrogen      | $n_b$      | mg/L                   |

\* For all but the bottom algae variables, a general mass balance for a constituent in an element is written as (Figure 17)

$$\frac{dC_i}{dt} = \frac{Q_{in}}{V_i} C_{i-1} - \frac{Q_{out}}{V_i} C_i + \frac{E_i}{V_i} (C_{i-1} - C_i) + \frac{W_i}{V_i} + S_i \quad (63)$$

where  $W_i$  is the external loading of the constituent to element  $i$  (g/d or mg/d), and  $S_i$  is source and sinks of the constituent due to reactions and mass transfer mechanisms (g/d or mg/d).

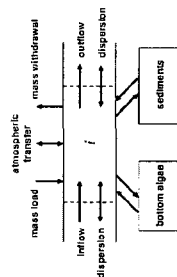


Figure 17 Mass balance.

The external load is computed as (recall Eq. 2),

$$W_i = \sum_{j=1}^N Q_{j \rightarrow i} C_{j-1} - \sum_{j=1}^N Q_{i \rightarrow j} C_i \quad (64)$$

where  $C_{j-1}$  is the  $j$ th point source concentration for element  $i$  (mg/L or µg/L), and  $C_{i \rightarrow j}$  is the  $j$ th non-point source concentration for element  $i$  (mg/L or µg/L).

For bottom algae, the transport and loading terms are omitted.

$$\frac{d\sigma_b}{dt} = S_{\sigma_b} \quad (65)$$

$$\frac{dN_b}{dt} = S_{N_b} \quad (66)$$

$$\frac{dP_b}{dt} = S_{P_b} \quad (67)$$

where  $S_{\sigma_b}$  is sources and sinks of bottom algae biomass due to reactions (mg/d or µg/d),  $S_{N_b}$  is sources and sinks of bottom algae nitrogen due to reactions (mg/d or µg/d), and  $S_{P_b}$  is sources and sinks of bottom algae phosphorus due to reactions (mg/d or µg/d).

The sources and sinks for the state variables are depicted in Figure 18 (note that the internal loads of nitrogen and phosphorus in the bottom algae are not depicted). The mathematical representations of these processes are presented in the following sections.

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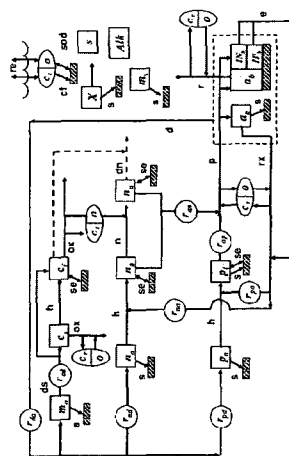


Figure 18. Model kinetics and mass transfer processes. The state variables are defined in the text. The processes are defined as: (a) plant photosynthesis, (b) plant respiration, (c) plant death, (d) sediment oxygen demand (SOD), (e) sediment inorganic carbon flux (ICF), (f) sediment oxygen demand (SOD), (g) sediment oxygen demand (SOD), and (h) sediment oxygen demand (SOD).

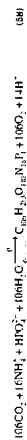
## 5.2 Reaction Fundamentals

### 5.2.1 Biochemical Reactions

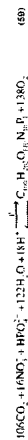
The following chemical equations are used to represent the major biochemical reactions that take place in the model (Shinn and Morgan 1996):

Plant Photosynthesis and Respiration:

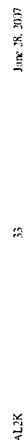
Ammonium as substrate:



Shake as substrate:



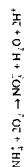
Nitrification:



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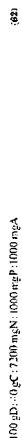
Denitrification:



Note that a number of additional reactions are used in the model such as those involved with simulating pH and unutilized ammonia. These will be outlined when those topics are discussed later in this document.

### 5.2.2 Stoichiometry of Organic Matter

The model requires that the stoichiometry of organic matter (i.e., phytoplankton and detritus) be specified by the user. The following representation is suggested as a first approximation (Bedfield et al. 1993, Chapra 1997):



where  $\text{gC}$  = mass of element C (g) and  $\text{mgA}$  = mass of element A (mg). The terms C, N, P, and A refer to dry weight, carbon, nitrogen, phosphorus, and chlorophyll *a*, respectively. It should be noted that chlorophyll *a* is the most variable of these parameters with a range of approximately 500–2000 mgA/kgA (Kass and Chapra 1993, Chapra 1997).

These values are then combined to determine stoichiometric ratios, as in

$$r_{\text{C}} = \frac{\text{gC}}{\text{gD}} \quad (63)$$

For example, the amount of detritus (in grams dry weight or gD) that is released due to the death of a unit amount of phytoplankton (in milligrams of chlorophyll *a*, or mgA) can be computed as

$$r_{\text{C}} = \frac{100 \text{ gD}}{100 \text{ mgA}} = 1.0 \frac{\text{gD}}{\text{mgA}}$$

### 5.2.2.1 Oxygen Generation and Consumption

The model requires that the rates of oxygen generation and consumption be prescribed. If ammonia is the substrate, the following ratio (based on Eq. 55) can be used to determine the grams of oxygen generated for each gram of plant matter that is produced through photosynthesis:

$$r_{\text{O}_2} = \frac{10 \text{ mol O}_2 (32 \text{ g/mol O}_2)}{10 \text{ mol C (12 g/mol C)}} = 2.67 \frac{\text{gO}_2}{\text{gC}} \quad (64)$$

If nitrate is the substrate, the following ratio (based on Eq. 56) applies:

$$r_{\text{O}_2} = \frac{138 \text{ mol O}_2 (32 \text{ g/mol O}_2)}{10 \text{ mol C (12 g/mol C)}} = 3.67 \frac{\text{gO}_2}{\text{gC}} \quad (65)$$

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Note that Eq. (58) is also used for the stoichiometry of the amount of oxygen consumed for plant respiration.

For nitrification, the following ratio is based on Eq. (61):

$$r_{O_2} = \frac{2 \text{ mole } O_2 (32 \text{ g}) / \text{mole } C_2H_5N}{1 \text{ mole } NH_4^+ (14 \text{ g}) / \text{mole } N} = 4.57 \frac{\text{g } O_2}{\text{g } N} \quad (60)$$

### 5.2.2.2 CBOO Utilization Due to Denitrification

As represented by Eq. (61), CBOO is utilized during denitrification,

$$r_{CBOO} = 3.67 \frac{\text{g } O_2}{\text{g } C} \cdot 5 \text{ mole } C \times 12 \text{ g } C / \text{mole } C_2H_5N \cdot 1 \text{ g } N = 0.00256 \frac{\text{g } O_2}{\text{mg } N} \quad (67)$$

### 5.2.3 Temperature Effects on Reactions

The temperature effect for all first-order reactions used in the model is represented by

$$k(T) = k(20^\circ) e^{(T-20)/\theta} \quad (68)$$

where  $k(T)$  is the reaction rate [d] at temperature  $T$  [°C] and  $\theta$  is the temperature coefficient for the reaction.

### 5.3 Composite Variables

In addition to the model's state variables, QIK also displays several composite variables that are computed as follows.

Total Organic Carbon (mgC/L):

$$TOC = \frac{C_s + C_f}{f_{OC}} + r_{CBOO} + r_{CBO} + r_{CBOO} \quad (69)$$

Total Nitrogen (µgN/L):

$$TN = n_s + n_{NH_4} + r_{NH_4} + r_{NH_4} \quad (70)$$

Total Phosphorus (µgP/L):

$$TP = p_s + p_f + r_{PO_4} + r_{PO_4} \quad (71)$$

Total Kjeldahl Nitrogen (µgN/L):

$$TKN = r_s + n_s + r_{NH_4} + r_{NH_4} \quad (72)$$

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Total Suspended Solids (mgD/L):

$$TSS = r_{SOD} + n_s + n_f \quad (73)$$

Ultimate Carbonaceous BOD (mgO<sub>2</sub>/L):

$$CBOD_u = r_s + r_f + r_{CBOO} + r_{CBOO} \quad (74)$$

### 5.4 Relationship of Model Variables and Data

For all but slow and fast CBOD ( $r_s$  and  $r_f$ ), there exists a relatively straightforward relationship between the model state variables and standard water quality measurements. These are outlined next. Then we discuss issues related to the more difficult problem of measuring CBOO.

#### 5.4.1 Non-CBOO Variables and Data

The following are measurements that are needed for comparison of non-CBOO variables with model output:

TEMP = temperature (°C)  
 TKN = total Kjeldahl nitrogen (µgN/L) or TN = total nitrogen (µgN/L)  
 NH<sub>4</sub> = ammonium nitrogen (µgN/L)  
 NO<sub>3</sub> = nitrate nitrogen (µgN/L)  
 NO<sub>2</sub> = nitrite nitrogen (µgN/L)  
 CHLA = chlorophyll *a* (µg/L)  
 TP = total phosphorus (µgP/L)  
 SRP = soluble reactive phosphorus (µgP/L)  
 TSS = total suspended solids (mgD/L)  
 VSS = volatile suspended solids (mgD/L)  
 YSS = total organic carbon (mgC/L)  
 DOC = dissolved organic carbon (mgC/L)  
 DO = dissolved oxygen (mgO<sub>2</sub>/L)  
 pH = pH  
 ALK = alkalinity (mgCaCO<sub>3</sub>/L)  
 COND = specific conductance (umhos)

The model state variables can then be related to these measurements as follows:

$$\Delta = \text{COND}$$

$$n_s = TSS - VSS \text{ or } TSS - r_s \text{ (TOC - DOC)}$$

$$n_f = \text{DO}$$

$$n_s = TKN - NH_4 - r_s \text{ CHLA} \quad \text{or} \quad n_s = TN - NO_2 - NO_3 - NH_4 - r_s \text{ CHLA}$$

$$n_{NH_4} = NH_4$$

$$n_s = NO_2 + NO_3$$

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-----------------------------------------------------|--------------------------------|
| $r^* = 1/r - SRP - r_{CHL}$ $\beta = SRP$ $q_2 = CHL$ $r = YSS - r_{CHL} \times r_{CHL} \times r_{CHL} \times r_{CHL} \times r_{CHL}$ $pH = PH$ $AR = ALK$ | <p><b>5.4.2 Carbonaceous BOD</b></p> <p>The interpretation of BOD measurements in natural waters is complicated by three primary factors:</p> <ul style="list-style-type: none"> <li>Filtered versus unfiltered. If the sample is unfiltered, the BOD will reflect oxidation of both dissolved and particulate organic carbon. Since QTK distinguishes between dissolved (<math>r_{CHL}</math>) and particulate (<math>r_{CHL}</math>) organic carbon, an unfiltered measurement will include both dissolved and particulate organic carbon. This is not the case for additional measurements of particulate BOD, which only reflect particulate organic carbon. This complicates the test through photosynthetic oxygen generation.</li> <li>Nitrogenous BOD. Along with the oxidation of organic carbon (CBOD), nitrification also contributes to oxygen depletion (NBOD). Thus, if the sample (a) contains reduced nitrogen and (b) nitrification is not inhibited, the measurement includes both types of BOD.</li> <li>Incubation time. Short-term, usually 5-day, BODs are typically performed. Because QTK uses ultimate CBOD, 5-day BODs must be converted to ultimate BODs in a sensible fashion.</li> </ul> <p>We suggest the following as practical ways to measure CBOD in a manner that accounts for the above factors and results in measurements that are compatible with QTK.</p> <p><b>Filtration.</b> The sample should be filtered prior to incubation in order to separate dissolved from particulate organic carbon.</p> <p><b>Nitrification inhibition.</b> Nitrification can be suppressed by adding a chemical inhibiting agent such as TCMP (2-chloro-6-trichloromethyl pyridine). The measurement then truly reflects CBOD. In the event that inhibition is not possible, the measured value can be corrected for nitrogen by subtracting the oxygen equivalents of the reduced nitrogen (<math>r_{CHL} \times TCN</math>) in the sample. However, as with all such difference-based adjustments, this correction may exhibit substantial error.</p> <p><b>Incubation time.</b> The model is based on ultimate CBOD, so two approaches are possible: (1) use a sufficiently long period so that the ultimate value is measured, or (2) use a 5-day measurement and extrapolate the result to the ultimate. The latter method is often compared with the formula</p> | $CBOD_{FNU} = \frac{CBOD_{FNU}}{1 - e^{-k_1}}$ <p>where <math>CBOD_{FNU}</math> = the ultimate dissolved carbonaceous BOD (<math>\text{mgO}_2/\text{L}</math>), <math>CBOD_{FNU}</math> = the 5-day dissolved carbonaceous BOD (<math>\text{mgO}_2/\text{L}</math>), and <math>k_1</math> = the CBOD decomposition rate in the bottle (<math>\text{d}^{-1}</math>).</p> <p>It should be noted that, besides practical considerations of time and expense, there may be other benefits from using the 5-day measurement with extrapolation, rather than performing the longer-term CBOD. Although extrapolation does introduce some error, the 5-day value has the advantage of being more readily obtained. This measurement can be taken even when nitrification can begin to be excited on longer time frames.</p> <p>If all the above provisions are implemented, the result should correspond to the model variables by</p> $r^* + r_{CHL} = CBOD_{FNU}$ <p><b>Slow versus Fast CBOD.</b> The final question relates to discrimination between fast and slow CBOD. Although we believe that there is currently no single, simple, economically-feasible answer to this problem, we think that the following 2 strategies represent the best current alternatives.</p> <p><b>Option 1:</b> Represent all the dissolved, oxidizable organic carbon with a single pool (fast CBOD). The model includes parameters to bypass slow CBOD. If no slow CBOD inputs are entered, this effectively drops it from the model. For this case,</p> $r_{CHL} = CBOD_{FNU}$ $r_{CHL} = 0$ <p><b>Option 2:</b> Use an ultimate CBOD measurement for the fast fraction and compute slow CBOD by difference with a DOC measurement. For this case,</p> $r_{CHL} = CBOD_{FNU}$ $r_{CHL} = r_{CHL} \times DOC = CBOD_{FNU}$ <p><b>Option 3:</b> works very nicely for systems where two distinct types of CBOD are present. For example, systems where there are more slowly oxidizable organic carbon than might be represented as fast CBOD. In this case, a traditional assumption of equal and opposite or allochthonous DOC from the watershed might be considered more realistic and hence could be lumped into the slow CBOD fraction. In such case, the hydrologic system covering the slow into the fast fraction could be set to zero to make the two terms independent.</p> <p>For both options, the <math>CBOD_{FNU}</math> can either be (a) measured directly using a long incubation time or (b) computed by extrapolation with Eq. 75. In both situations, a time frame of several</p> | <p><sup>1</sup>The inverse here FNU stands for Filtration, Nitrification inhibition and Ultimate.</p> | <p>QUAL2K 38 June 28, 2007</p> |
| $r^* = 1/r - SRP - r_{CHL}$ $\beta = SRP$ $q_2 = CHL$ $r = YSS - r_{CHL} \times r_{CHL} \times r_{CHL} \times r_{CHL} \times r_{CHL}$ $pH = PH$ $AR = ALK$ | <p><b>5.4.2 Carbonaceous BOD</b></p> <p>The interpretation of BOD measurements in natural waters is complicated by three primary factors:</p> <ul style="list-style-type: none"> <li>Filtered versus unfiltered. If the sample is unfiltered, the BOD will reflect oxidation of both dissolved and particulate organic carbon. Since QTK distinguishes between dissolved (<math>r_{CHL}</math>) and particulate (<math>r_{CHL}</math>) organic carbon, an unfiltered measurement will include both dissolved and particulate organic carbon. This is not the case for additional measurements of particulate BOD, which only reflect particulate organic carbon. This complicates the test through photosynthetic oxygen generation.</li> <li>Nitrogenous BOD. 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In the event that inhibition is not possible, the measured value can be corrected for nitrogen by subtracting the oxygen equivalents of the reduced nitrogen (<math>r_{CHL} \times TCN</math>) in the sample. However, as with all such difference-based adjustments, this correction may exhibit substantial error.</p> <p><b>Incubation time.</b> The model is based on ultimate CBOD, so two approaches are possible: (1) use a sufficiently long period so that the ultimate value is measured, or (2) use a 5-day measurement and extrapolate the result to the ultimate. The latter method is often compared with the formula</p> | $CBOD_{FNU} = \frac{CBOD_{FNU}}{1 - e^{-k_1}}$ <p>where <math>CBOD_{FNU}</math> = the ultimate dissolved carbonaceous BOD (<math>\text{mgO}_2/\text{L}</math>), <math>CBOD_{FNU}</math> = the 5-day dissolved carbonaceous BOD (<math>\text{mgO}_2/\text{L}</math>), and <math>k_1</math> = the CBOD decomposition rate in the bottle (<math>\text{d}^{-1}</math>).</p> <p>It should be noted that, besides practical considerations of time and expense, there may be other benefits from using the 5-day measurement with extrapolation, rather than performing the longer-term CBOD. Although extrapolation does introduce some error, the 5-day value has the advantage of being more readily obtained. This measurement can be taken even when nitrification can begin to be excited on longer time frames.</p> <p>If all the above provisions are implemented, the result should correspond to the model variables by</p> $r^* + r_{CHL} = CBOD_{FNU}$ <p><b>Slow versus Fast CBOD.</b> The final question relates to discrimination between fast and slow CBOD. Although we believe that there is currently no single, simple, economically-feasible answer to this problem, we think that the following 2 strategies represent the best current alternatives.</p> <p><b>Option 1:</b> Represent all the dissolved, oxidizable organic carbon with a single pool (fast CBOD). The model includes parameters to bypass slow CBOD. If no slow CBOD inputs are entered, this effectively drops it from the model. For this case,</p> $r_{CHL} = CBOD_{FNU}$ $r_{CHL} = 0$ <p><b>Option 2:</b> Use an ultimate CBOD measurement for the fast fraction and compute slow CBOD by difference with a DOC measurement. For this case,</p> $r_{CHL} = CBOD_{FNU}$ $r_{CHL} = r_{CHL} \times DOC = CBOD_{FNU}$ <p><b>Option 3:</b> works very nicely for systems where two distinct types of CBOD are present. For example, systems where there are more slowly oxidizable organic carbon than might be represented as fast CBOD. In this case, a traditional assumption of equal and opposite or allochthonous DOC from the watershed might be considered more realistic and hence could be lumped into the slow CBOD fraction. In such case, the hydrologic system covering the slow into the fast fraction could be set to zero to make the two terms independent.</p> <p>For both options, the <math>CBOD_{FNU}</math> can either be (a) measured directly using a long incubation time or (b) computed by extrapolation with Eq. 75. In both situations, a time frame of several</p> | <p><sup>1</sup>The inverse here FNU stands for Filtration, Nitrification inhibition and Ultimate.</p> | <p>QUAL2K 37 June 28, 2007</p> |

weeks to a month (i.e., a 20- to 30-day CBOD) is probably a valid period in order to oxidize most of the readily degradable organic carbon. We base this assumption on the fact that bottle rates for sewage-derived organic carbon are on the order of 0.05 to 0.3/d (Chapter 10). As in Figure 19, such rates suggest that much of the readily oxidizable CBOD will be exerted in about 20 to 30 days.

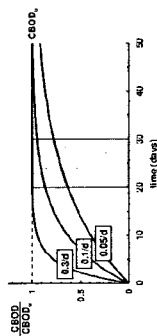


Figure 19 Progression of CBOD test for various levels of the bottle decomposition rate.

In addition, we believe that practitioners should consider conducting long-term CBOD tests at 30°C rather than at the commonly employed temperature of 20°C. The choice of 20°C originated from the fact that the average daily temperature of most receiving water and wastewater treatment plants in the temperate zone is assumed to be approximately 20°C.

If the CBOD measurement is intended to be used for regulation or to assess treatment plant performance, it makes sense to standardize the test at a particular temperature. And for such purposes, 20°C is as reasonable a choice as any. However, if the intent is to measure an ultimate CBOD, anything that speeds up the process while not jeopardizing the measurement's integrity would seem beneficial.

The saprophytic bacteria that break down nonliving organic carbon in natural waters and sewage thrive best at temperatures from 30°C to 40°C. Thus, a temperature of 30°C is not high enough that the bacterial assemblage would shift to thermophilic organisms that are atypical of natural waters and sewage. The bacteria should be higher oxidation rates, which would result in more rapid degradation of the organic carbon. The CBOD test is a good choice for determining the bacterial decomposition, a 20-day BOD at 30°C should be equivalent to a 30-day BOD at 20°C.

## 5.5 Consilient Reactions

The mathematical relationships that describe the individual reactions and concentrations of the model state variables (Table 5) are presented in the following paragraphs.

### 5.5.1 Conservative Substance (s)

By definition, conservative substances are not subject to reactions:

$$\dot{S}_i = 0 \quad (76)$$

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## 5.5.2 Phytoplankton ( $\phi_p$ )

Phytoplankton increase due to photosynthesis. They are lost via respiration, death, and settling

$$\dot{S}_{\phi_p} = \text{PhysiPhoto} - \text{PhysiResp} - \text{PhysiDeath} - \text{PhysiSed} \quad (77)$$

### 5.5.2.1 Photosynthesis

Phytoplankton photosynthesis is computed as

$$\text{PhysiPhoto} = I_p \phi_p \delta_{\phi_p} \quad (78)$$

where  $I_p$  = phytoplankton photosynthesis rate (/d) is a function of temperature, nutrients, and light.

$$I_p = k_{\phi_p} (I / I_{0.95} \delta_{\phi_p}) \quad (79)$$

where  $k_{\phi_p}(T)$  = the maximum photosynthesis rate at temperature  $T$  (/d),  $\phi_p$  = phytoplankton concentration (mg/L),  $I$  = incident light intensity (μmol photons/m<sup>2</sup>/s), and  $\delta_{\phi_p}$  = the phytoplankton light saturation coefficient (dimensionless number between 0 and 1).

**Nutrient Limitation.** Michaelis-Menten equations are used to represent growth limitation for inorganic nitrogen, phosphorus and inorganic carbon. The minimum value is then used to compute the nutrient limitation factor.

$$\phi_p = \min \left\{ \frac{I_p}{k_{\phi_p} + I_p}, \frac{I_p}{k_{\phi_p} + I_p}, \frac{I_p}{k_{\phi_p} + I_p} \right\} \quad (80)$$

where  $k_{\phi_p}$  = nitrogen half saturation constant (μM/L),  $k_{\phi_p}$  = phosphorus half saturation constant (μM/L),  $k_{\phi_p}$  = inorganic carbon half saturation constant (mole/L),  $\text{HCO}_3^-$  = dissolved carbon dioxide concentration (mole/L), and  $\text{HCO}_3^-$  = bicarbonate concentration (mole/L).

**Light Limitation.** It is assumed that light attenuation through the water follows the Beer-Lambert law.

$$PAR(z) = PAR_0 e^{-k_d z} \quad (81)$$

where  $PAR(z)$  = photosynthetically available radiation (PAR) is depth  $z$  below the water surface (μmol/L), and  $k_d$  = the light extinction coefficient (m<sup>-1</sup>). The PAR at the water surface is assumed to be a fixed fraction of the solar radiation (Steetz 1984, Baker and Fennel 1987):

$$PAR(0) = 0.47 I_0$$

The extinction coefficient is related to model variables by

<sup>1</sup>  $I_0$  = energy per day. A lumen is equal to a calorie per square centimeter. Note that a lumen is related to the μm<sup>2</sup> by the following: approximately 1 μm<sup>2</sup> is equal to 0.45 lumen/day. LUCOR, Lincoln, NE.

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$$k_{\text{bg}} = k_{\text{bg}} + \alpha_{\text{bg}} + \alpha_{\text{bg}} \cdot I_{\text{bg}} + \alpha_{\text{bg}} \cdot I_{\text{bg}}^2 \quad (82)$$

where  $k_{\text{bg}}$  is the background coefficient accounting for extinction due to water and color [mL  $\mu\text{m}^{-1}$ ],  $\alpha_{\text{bg}}$ ,  $\alpha_{\text{bg}}$ , and  $\alpha_{\text{bg}}$  are constants accounting for the impact of inorganic suspended solids (LingDong), particulate organic matter (LingDong), and chlorophyll (LingDong and LingDong), respectively. Suggested values for these coefficients are listed in Table 6.

Table 6 Suggested values for light extinction coefficients

| Symbol               | Value  | Reference        |
|----------------------|--------|------------------|
| $\alpha_{\text{bg}}$ | 0.0008 | Li and Wu (1978) |
| $\alpha_{\text{bg}}$ | 0.1734 | Li and Wu (1978) |
| $\alpha_{\text{bg}}$ | 0.0008 | Li and Wu (1978) |
| $\alpha_{\text{bg}}$ | 0.654  | Li and Wu (1978) |

Three models are used to characterize the impact of light on phytoplankton photosynthesis (Figure 20):

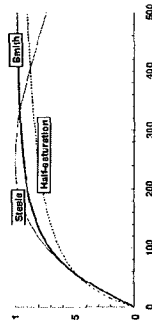


Figure 20. The three models used for phytoplankton and bottom algae photosynthesis light dependence. The plot shows growth attenuation versus PAR intensity (I<sub>0</sub>).

Half-Saturation (Baird, Menden-Deuer, Light Model, 1933):

$$F_{\text{H}} = \frac{I(I_0)}{K_{\text{H}} + I(I_0)} \quad (83)$$

where  $F_{\text{H}}$  is phytoplankton growth rate due to light and  $K_{\text{H}}$  is the phytoplankton light parameter. In the case of the half-saturation model, the light parameter is half-saturation coefficient [I<sub>0</sub>]. This function can be combined with the Beer-Lambert law and integrated over water depth,  $H$  [m], to yield the phytoplankton light attenuation coefficient:

$$F_{\text{H}} = \frac{1}{K_{\text{H}}} \ln \left( \frac{K_{\text{H}} + I(0)}{K_{\text{H}} + I(H)} \right) \quad (84)$$

Smith's function (Smith 1959):

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$$F_{\text{L}} = \frac{I(I_0)}{K_{\text{L}} + I(I_0)} \quad (85)$$

where  $K_{\text{L}}$  is the Smith parameter for phytoplankton [I<sub>0</sub>], that is, the PAR at which growth is 70.7% of the maximum. This function can be combined with the Beer-Lambert law and integrated over water depth to yield

$$F_{\text{L}} = \frac{1}{K_{\text{L}}} \ln \left( \frac{I(0)/K_{\text{L}} + (1 + I(0)/K_{\text{L}})^2}{I(H)/K_{\text{L}} + (1 + I(H)/K_{\text{L}})^2} \right) \quad (86)$$

Sheil's function (Sheil 1962):

$$F_{\text{L}} = \frac{I(I_0)}{K_{\text{L}}} \quad (87)$$

where  $K_{\text{L}}$  is the PAR at which phytoplankton growth is optimal [I<sub>0</sub>]. This function can be combined with the Beer-Lambert law and integrated over water depth to yield

$$F_{\text{L}} = \frac{2.71828}{K_{\text{L}}} \left( \frac{I(0)}{K_{\text{L}}} - e^{-\frac{I(0)}{K_{\text{L}}}} \right) - e^{-\frac{I(H)}{K_{\text{L}}}} \quad (88)$$

### 5.5.2.2 Losses

Respiration. Phytoplankton respiration is represented as a first-order rate that is attenuated at low oxygen concentration.

$$\text{PhytoResp} = F_{\text{resp}}(T) \cdot \eta_{\text{r}} \quad (89)$$

where  $F_{\text{resp}}(T)$  is temperature-dependent phytoplankton respiration rate [g/d] and  $\eta_{\text{r}}$  is attenuation due to low oxygen [dimensionless]. Oxygen attenuation is modeled by Eq. 119 to (121) with the oxygen dependency represented by the parameter  $K_{\text{O}_2}$ .

Death. Phytoplankton death is represented as a first-order rate:

$$\text{PhytoDeath} = k_{\text{d}}(T) \cdot \eta_{\text{d}} \quad (90)$$

where  $k_{\text{d}}(T)$  is temperature-dependent phytoplankton death rate [d].

Settling. Phytoplankton settling is represented as

$$\text{PhytoSett} = \frac{S_{\text{d}}}{H} \cdot \eta_{\text{d}} \quad (91)$$

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where  $\alpha_s$  = phytoplankton settling velocity [m/d].

### 5.5.3 Bottom algae ( $\phi_b$ )

Bottom algae increase due to photosynthesis. They are lost via respiration and death.

$$S_b = \text{BotAlgPhoto} - \text{BotAlgResp} - \text{BotAlgDeath} \quad (69)$$

#### 5.5.3.1 Photosynthesis

Two representations can be used in model bottom algae photosynthesis. The first is based on a temperature-corrected zero-order rate attenuated by nutrient and light limitation (McIntyre 1973, Rutherford et al. 1993).

$$\text{BotAlgPhoto} = C_p (T)^{0.5} \phi_{ps} \phi_n \quad (70)$$

where  $C_p(T)$  is the zero-order temperature-dependent maximum photosynthesis rate [ $\text{mgC}/(\text{mgC} \cdot \text{d})$ ],  $\phi_{ps}$  is bottom algae nutrient attenuation factor (dimensionless number between 0 and 1), and  $\phi_n$  is the bottom algae light attenuation coefficient (dimensionless number between 0 and 1).

The second uses a first-order model:

$$\text{BotAlgPhoto} = C_p (T)^{0.5} \phi_{ps} \phi_n \phi_{ps} \quad (71)$$

where, for this case,  $C_p(T)$  is the first-order temperature-dependent maximum photosynthesis rate [ $\text{d}^{-1}$ ], and  $\phi_n$  is bottom algae space limitation attenuation factor.

**Temperature Effect.** As for the first-order rates, an Arrhenius model is employed to quantify the effect of temperature on bottom algae photosynthesis.

$$C_p(T) = C_{pA} (20)^{T-20} \quad (72)$$

**Nutrient Limitation.** The effect of nutrient limitation on bottom plant photosynthesis is modeled in a different way than for the phytoplankton. Rather than being dependent on external nutrient concentrations, photosynthesis rate is dependent on intracellular nutrient using a limitation originally developed by Droop (1974).

$$\phi_n = m_n \left[ 1 - \frac{q_N}{q_N + \frac{[H_2CO_3] + [HCO_3^-]}{K_N}} \right] \quad (73)$$

where  $q_N$  and  $q_P$  are the cell quotas of nitrogen [ $\text{mgN}/(\text{mgC})$ ] and phosphorus [ $\text{mgP}/(\text{mgC})$ ], respectively;  $q_N$  and  $q_P$  are the minimum cell quotas of nitrogen [ $\text{mgN}/(\text{mgC})$ ] and phosphorus [ $\text{mgP}/(\text{mgC})$ ], respectively; and  $K_N$  is inorganic carbon half-saturation constant for the bottom algae [ $\text{mole/L}$ ]. The minimum cell quotas are the levels of intracellular nutrient at which growth ceases.

The cell quotas represent the ratio of the intracellular nutrient to the bottom plant's biomass.

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$$\phi_n = \frac{N}{N_s} \quad (74)$$

$$\phi_p = \frac{P}{P_s} \quad (75)$$

where  $N$  = intracellular nitrogen concentration [ $\text{mgN}/(\text{mgC})$ ] and  $P$  = intracellular phosphorus concentration [ $\text{mgP}/(\text{mgC})$ ].

**Light Limitation.** In contrast to the phytoplankton, light limitation at any time is determined by the amount of PAR reaching the bottom of the water column. This quantity is computed with the Beer Lambert law (Eq. 83) evaluated at the bottom of the river.

$$I(H) = I(0)e^{-K_d H} \quad (76)$$

As with the phytoplankton, three models (Eq. 83, 84, and 87) are used to characterize the impact of light on bottom algae photosynthesis. Substituting Eq. (99) into these models yields the following formulas for the bottom algae light attenuation coefficient.

For S-Saturation Light Model (Paerl 1975):

$$\phi_n = \frac{I(0)e^{-K_d H}}{K_n + I(0)e^{-K_d H}} \quad (77)$$

Smith's Function (Smith 1959):

$$\phi_n = \frac{I(0)e^{-K_d H}}{I(0)e^{-K_d H} + (I(0)e^{-K_d H})^2} \quad (78)$$

Model's Equation (Stock 1987):

$$\phi_n = \frac{I(0)e^{-K_d H}}{K_n + I(0)e^{-K_d H}} \quad (79)$$

where  $K_n$  is the appropriate bottom algae light parameter for each light model.

**Space Limitation.** If a first-order growth model is used, a term must be included to impose a space limitation on the bottom algae. A logistic model is used for this purpose as in

$$\phi_n = 1 - \frac{a_n}{a_n + c} \quad (80)$$

where  $a_n$  = the carrying capacity [ $\text{mgC}/(\text{m}^2)$ ].

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### 5.5.3.2 Losses

Respiration. Bottom algae respiration is represented as a first-order rate that is attenuated at low oxygen concentrations,

$$\text{BotAlgRes} = F_{\text{res}} k_{\text{res}}(T) u_{\text{O}_2} \quad (108)$$

where  $k_{\text{res}}(T)$  = temperature-dependent bottom algae respiration rate [d] and  $F_{\text{res}}$  = attenuation due to low oxygen (dimensionless). Oxygen attenuation is modeled by Eq. (119) in (121) with the oxygen dependency represented by the parameter  $k_{\text{res}}$ .

Deaths. Bottom algae death is represented as a first-order rate,

$$\text{BotAlgDeath} = k_{\text{d}}(T) u_{\text{O}_2} \quad (109)$$

where  $k_{\text{d}}(T)$  = the temperature-dependent bottom algae death rate [d].

### 5.5.4 Bottom Algae Internal Nitrogen ( $N_i$ )

The change in intracellular nitrogen in bottom algal cells is calculated from

$$S_{\text{N}} = \text{BotAlgUpN} - F_{\text{N}} \text{BotAlgDeath} - \text{BotAlgExN} \quad (110)$$

where  $\text{BotAlgUpN}$  = the uptake rate of nitrogen by bottom algae (mgN/m<sup>2</sup>/d),  $\text{BotAlgDeath}$  = bottom algae death (mgAl/m<sup>2</sup>/d), and  $\text{BotAlgExN}$  = the bottom algae excretion of nitrogen (mgN/m<sup>2</sup>/d), which is computed as

$$\text{BotAlgExN} = F_{\text{N}} k_{\text{res}}(T) u_{\text{O}_2} \quad (111)$$

where  $k_{\text{res}}(T)$  = the temperature-dependent bottom algae excretion rate [d].

The  $N$  uptake rate depends on both external and intracellular nutrients as in (Rhee 1973),

$$\text{BotAlgUpN} = \rho_{\text{N}} \frac{N_{\text{ext}} + N_{\text{int}}}{k_{\text{N,ext}} + N_{\text{ext}} + k_{\text{N,int}} + N_{\text{int}}} \quad (112)$$

where  $\rho_{\text{N}}$  = the maximum uptake rate for nitrogen (mgN/mgAl/d),  $k_{\text{N,ext}}$  = half-saturation constant for external nitrogen [mgN/L] and  $k_{\text{N,int}}$  = half-saturation constant for intracellular nitrogen (mgN/mgAl<sup>-1</sup>).

### 5.5.5 Bottom Algae Internal Phosphorus ( $P_i$ )

The change in intracellular phosphorus in bottom algal cells is calculated from

$$S_{\text{P}} = \text{BotAlgUpP} - F_{\text{P}} \text{BotAlgDeath} - \text{BotAlgExP} \quad (113)$$

where  $\text{BotAlgUpP}$  = the uptake rate of phosphorus by bottom algae (mgP/m<sup>2</sup>/d),  $\text{BotAlgDeath}$  = bottom algae death (mgAl/m<sup>2</sup>/d), and  $\text{BotAlgExP}$  = the bottom algae excretion of phosphorus (mgP/m<sup>2</sup>/d), which is computed as

$$\text{BotAlgExP} = F_{\text{P}} k_{\text{res}}(T) u_{\text{O}_2} \quad (114)$$

where  $k_{\text{res}}(T)$  = the temperature-dependent bottom algae excretion rate [d].

The  $P$  uptake rate depends on both external and intracellular nutrients as in (Rhee 1973),

$$\text{BotAlgUpP} = \rho_{\text{P}} \frac{P_{\text{ext}} + P_{\text{int}}}{k_{\text{P,ext}} + P_{\text{ext}} + k_{\text{P,int}} + P_{\text{int}}} \quad (115)$$

where  $\rho_{\text{P}}$  = the maximum uptake rate for phosphorus (mgP/mgAl/d),  $k_{\text{P,ext}}$  = half-saturation constant for external phosphorus [mgP/L] and  $k_{\text{P,int}}$  = half-saturation constant for intracellular phosphorus (mgP/mgAl<sup>-1</sup>).

### 5.5.6 Detritus ( $m_d$ )

Detritus or particulate organic matter (POM) increases due to plant death. It is lost via dissolution and settling

$$S_{\text{m}} = c_{\text{m}} \text{PhyDetDeath} + F_{\text{d}} \text{BotAlgDeath} - \text{DetDis} - \text{DetSettl} \quad (116)$$

where

$$\text{DetDis} = k_{\text{d}}(T) m_{\text{d}} \quad (117)$$

where  $k_{\text{d}}(T)$  = the temperature-dependent detritus dissolution rate [d] and

$$\text{DetSettl} = \frac{v_{\text{d}}}{H} m_{\text{d}} \quad (118)$$

where  $v_{\text{d}}$  = detritus settling velocity [m/d].

### 5.5.7 Slowly Reacting CBOD ( $C_2$ )

Slowly reacting CBOD increases due to detritus dissolution. It is lost via hydrolytic and oxidation,

$$S_{\text{O}_2} = (1 - F_{\text{d}}) v_{\text{d}} \text{DetDis} - \text{SlowChyd} - \text{SlowCOx} \quad (119)$$

where  $F_{\text{d}}$  = the fraction of detrital dissolution that goes to fast reacting CBOD (dimensionless), and

$$\text{SlowChyd} = k_{\text{h}}(T) C_2 \quad (120)$$

where  $k_{\text{h}}(T)$  = the temperature-dependent slow CBOD hydrolysis rate [d], and

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$$S_{\text{SlowCO}_2} = F_{\text{slow}} k_{\text{slow}} / T k_e \quad (116)$$

where  $k_{\text{slow}}(T)$  is the temperature-dependent slow CBOD oxidation rate  $[d]$  and  $F_{\text{slow}}$  = attenuation due to low oxygen (dimensionless).

### 5.5.8 Fast Reacting CBOD ( $c$ )

Fast reacting CBOD is gained via the dissolution of detritus and the hydrolysis of slowly-reacting CBOD. It is lost via oxidation and denitrification.

$$S_{\text{F}} = F_{\text{F}} / r_{\text{F}} \text{ DetDiss} + S_{\text{SlowCH}_2\text{OH}} - F_{\text{FastCO}_2} - r_{\text{FastDenitr}} \quad (117)$$

where

$$F_{\text{FastCO}_2} = F_{\text{slow}} k_{\text{F}} / T k_e \quad (118)$$

where  $k_{\text{F}}(T)$  is the temperature-dependent fast CBOD oxidation rate  $[d]$  and  $F_{\text{slow}}$  = attenuation due to low oxygen (dimensionless). The parameter  $r_{\text{FastDenitr}}$  is the ratio of oxygen equivalents lost per atomic nitrogen that is denitrified (Eq. 67). The term  $\text{DetDiss}$  is the rate of denitrification  $\text{mgN/L/d}$ . It will be defined in Sec. 5.5.12 below.

Three formulations are used to represent the oxygen attenuation:

Half-Saturation:

$$F_{\text{Fast}} = \frac{S}{K_{\text{half}} + S} \quad (119)$$

where  $K_{\text{half}}$  = half saturation constant for the effect of oxygen on fast CBOD oxidation  $[\text{mgO}_2/\text{L}]$ .

Exponential:

$$F_{\text{Fast}} = (1 - e^{-K_{\text{exp}} S}) \quad (120)$$

where  $K_{\text{exp}}$  = exponential coefficient for the effect of oxygen on fast CBOD oxidation  $[\text{L/mgO}_2]$ .

Second-Order Half Saturation:

$$F_{\text{Fast}} = \frac{S^2}{K_{\text{half}} + S^2} \quad (121)$$

where  $K_{\text{half}}$  = half-saturation constant for second-order effect of oxygen on fast CBOD oxidation  $[\text{mgO}_2/\text{L}]^2$ .

### 5.5.9 Organic Nitrogen ( $n$ )

Organic nitrogen increases due to plant death. It is lost via hydrolysis and settling.

$$S_{\text{N}} = r_{\text{N}} \text{ PhytoDeath} + r_{\text{N}} \text{ BotNigDeath} - \text{ONHydr} - \text{ONSettl} \quad (122)$$

The rate of organic nitrogen hydrolysis is computed as

$$\text{ONHydr} = k_{\text{N}}(T)^{n_{\text{N}}} \quad (123)$$

where  $k_{\text{N}}(T)$  is the temperature-dependent organic nitrogen hydrolysis rate  $[d]$ .

$$\text{ONSettl} = \frac{r_{\text{N}}}{H} \quad (124)$$

where  $r_{\text{N}}$  = organic nitrogen settling velocity  $[\text{m/d}]$ .

### 5.5.10 Ammonia Nitrogen ( $n$ )

Ammonia nitrogen increases due to organic nitrogen hydrolysis, phytoplankton respiration excretion and bottom plant excretion. It is lost via nitrification and plant photosynthesis.

$$S_{\text{N}} = \text{DONHydr} - r_{\text{N}} \text{ PhytoRes} - \text{Nitrif} + \text{BotAlgaeN} - r_{\text{N}} \text{ PhytoPhyto} - P_{\text{BotAlgaeN}} \quad (125)$$

The ammonia nitrification rate is computed as

$$\text{Nitrif} = F_{\text{Nitrif}} k_{\text{N}}(T) P_{\text{N}} \quad (126)$$

where  $k_{\text{N}}(T)$  is the temperature-dependent nitrification rate for ammonia nitrogen  $[d]$  and  $F_{\text{Nitrif}}$  = attenuation due to low oxygen (dimensionless). Oxygen attenuation is modeled by Eq. (119) to (121) with the oxygen dependency represented by the parameter  $K_{\text{Nitrif}}$ .

The coefficients  $P_{\text{N}}$  and  $P_{\text{N}}$  are the preferences for ammonium as a nitrogen source for phytoplankton and bottom algae, respectively.

$$P_{\text{N}} = \frac{r_{\text{N}} k_{\text{N}}}{(k_{\text{Nitrif}} + r_{\text{N}})(k_{\text{Nitrif}} + r_{\text{N}})} + \frac{r_{\text{N}} k_{\text{Nitrif}}}{(r_{\text{N}} + r_{\text{N}})(k_{\text{Nitrif}} + r_{\text{N}})} \quad (127)$$

$$P_{\text{N}} = \frac{r_{\text{N}} k_{\text{N}}}{(k_{\text{Nitrif}} + r_{\text{N}})(k_{\text{Nitrif}} + r_{\text{N}})} + \frac{r_{\text{N}} k_{\text{Nitrif}}}{(r_{\text{N}} + r_{\text{N}})(k_{\text{Nitrif}} + r_{\text{N}})} \quad (128)$$

where  $k_{\text{Nitrif}}$  = preference coefficient of phytoplankton for ammonium  $[\text{mgN/m}^3]$  and  $k_{\text{Nitrif}}$  = preference coefficient of bottom algae for ammonium  $[\text{mgN/m}^3]$ .

### 5.5.11 Unionized Ammonia

The model simulates total ammonia. In water, the total ammonia consists of two forms: ammonium ion,  $\text{NH}_4^+$ , and unionized ammonia,  $\text{NH}_3$ . At normal pH (6 to 8), most of the total

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ammonia will be in the ionic form. However at high pH, unionized ammonia predominates. The amount of unionized ammonia can be computed as:

$$n_{\text{am}} = F_{\text{am}} n_{\text{a}} \quad (129)$$

where  $n_{\text{am}}$  = the concentration of unionized ammonia [mg/L], and  $F_{\text{am}}$  = the fraction of the total ammonia that is in unionized form.

$$F_{\text{am}} = \frac{K_{\text{a}}}{10^{-\text{pH}} + K_{\text{a}}} \quad (130)$$

where  $K_{\text{a}}$  = the equilibrium coefficient for the ammonia dissociation reaction, which is related to temperature by

$$\ln K_{\text{a}} = 0.096(18.4 - \frac{2729.92}{T_{\text{a}}}) \quad (131)$$

where  $T_{\text{a}}$  is absolute temperature [K] and  $\ln K_{\text{a}} = \ln(K_{\text{a}}/K_{\text{a}}^{\text{ref}})$ . Note that the fraction of the total ammonia that is in ionized form,  $F_{\text{am}}$ , can be computed as  $1 - F_{\text{am}}$ , or

$$F_{\text{a}} = \frac{10^{-\text{pH}}}{10^{-\text{pH}} + K_{\text{a}}} \quad (132)$$

#### 5.5.12 Nitrate Nitrogen ( $n_{\text{N}}$ )

Nitrate nitrogen increases due to nitrification of ammonia. It is lost via denitrification and plant photosynthesis:

$$S_{\text{N}} = \text{Nitrif} - \text{Denitr} - n_{\text{N}}(1 - P_{\text{N}})/\text{PhysioPhos} - (1 - P_{\text{N}})/\text{BioAlgaePhosN} \quad (133)$$

The denitrification rate is computed as

$$\text{Denitr} = (1 - F_{\text{O}_2})K_{\text{dN}}(T) n_{\text{N}} \quad (134)$$

where  $K_{\text{dN}}(T)$  = the temperature-dependent denitrification rate of nitrate nitrogen [d] and  $F_{\text{O}_2}$  = effect of low oxygen on denitrification (dimensionless) as modeled by Eqs. (119) to (121); with the oxygen dependency represented by the parameter  $K_{\text{dO}_2}$ .

#### 5.5.13 Organic Phosphorus ( $p_{\text{a}}$ )

Organic phosphorus increases due to plant death. It is lost via hydrolysis and settling

$$S_{\text{p}} = r_{\text{p}}/\text{PhysDeath} + r_{\text{p}}/\text{BvAlgaeDeath} - \text{OPHyd} - \text{OPSettl} \quad (135)$$

where the rate of organic phosphorus hydrolysis is computed as

$$\text{OPHyd} = k_{\text{p}}(T) p_{\text{a}} \quad (136)$$

where  $k_{\text{p}}(T)$  = the temperature-dependent organic phosphorus hydrolysis rate [d]. Organic phosphorus settling is determined as

$$\text{OPSettl} = \frac{v_{\text{op}}}{H} p_{\text{a}} \quad (137)$$

where  $v_{\text{op}}$  = organic phosphorus settling velocity [m/d].

#### 5.5.14 Inorganic Phosphorus ( $p_{\text{i}}$ )

Inorganic phosphorus increases due to organic phosphorus hydrolysis, phytoplankton necromass, and bacterial production and decreases due to plant uptake and bioassimilation. In addition, a settling loss is included for cases in which inorganic phosphorus is lost due to sorption onto suitable particulate matter such as iron oxyhydroxides:

$$S_{\text{p}} = \text{COPHyd} + r_{\text{p}}/\text{PhysDeath} + \text{BioAlgaeP} - \text{IPSettl} - r_{\text{p}}/\text{PhysioPhos} - \text{IPSettl} \quad (138)$$

where

$$\text{IPSettl} = \frac{v_{\text{ip}}}{H} p_{\text{i}} \quad (139)$$

where  $v_{\text{ip}}$  = inorganic phosphorus settling velocity [m/d].

#### 5.5.15 Inorganic Suspended Solids ( $m_{\text{i}}$ )

Inorganic suspended solids are lost via settling.

$$S_{\text{m}} = -\text{InorgSettl}$$

where:

$$\text{InorgSettl} = \frac{v_{\text{is}}}{H} m_{\text{i}} \quad (140)$$

where  $v_{\text{is}}$  = inorganic suspended solids settling velocity [m/d].

#### 5.5.16 Dissolved Oxygen ( $o$ )

Dissolved oxygen increases due to plant photosynthesis. It is lost via fast CBOD oxidation, nitrification and plant respiration. Depending on whether the water is undersaturated or oversaturated it is gained or lost via reaeration.

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$$S_{\text{O}_2} = \mu_{\text{O}_2} \text{Photo} - r_{\text{O}_2} \text{BOD} + r_{\text{O}_2} \text{FAC} \text{Oxid} - r_{\text{O}_2} \text{NH}_4 \text{Nitr} \quad (144)$$

where

$$\text{OxRate} = k_{\text{O}_2} (P_{\text{O}_2} - P_{\text{O}_2}^{\text{sat}}) \quad (145)$$

where  $k_{\text{O}_2}$  = the temperature dependent oxygen reactivation coefficient [d<sup>-1</sup>],  $r_{\text{O}_2}$  (d/cv) = the saturation concentration of oxygen [mgO<sub>2</sub>/L] at temperature  $T$ , and elevation above sea level, elev.

### 5.3.16.1 Oxygen Saturation

The following equation is used to represent the dependence of oxygen saturation on temperature (APHA 1995)

$$\ln(r_{\text{O}_2}(T, 0)) = -1.39.34(1) + \frac{1.575(1) \times 10^5}{T_e} - \frac{6.642(308) \times 10^7}{T_e^2} \quad (146)$$

where  $r_{\text{O}_2}(T, 0)$  = the saturation concentration of dissolved oxygen in freshwater at 1 atm [mgO<sub>2</sub>/L] and  $T_e$  = absolute temperature [K] where  $T_e = T + 273.15$ .

The effect of elevation is accounted for by

$$r_{\text{O}_2}(T, elev) = r_{\text{O}_2}(T, 0) (1 - 0.000146(elev)) \quad (147)$$

### 5.3.16.2 Reaeration Formulas

The reaeration coefficient (at 20 °C) can be prescribed on the **Reach Worksheet**. If reaeration is not prescribed (that is, it is blank or zero for a particular reach), it is computed as a function of the river's hydraulics and (optionally) wind velocity.

$$K_d(20) = k_{\text{re}}(20) + \frac{K_{\text{re}}(20)}{H} \quad (148)$$

where  $K_d(20)$  = the reaeration rate at 20 °C, computed based on the river's hydraulic characteristics ( $K_d(1)$ ,  $K_d(20)$ ) = the reaeration mass transfer coefficient based on wind velocity [we/L], and  $H$  = mean depth [m].

### Hydraulic-based Formulas

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$$L_{\text{u}}(20) = 3.9 \frac{U^{1.25}}{H^{0.75}} \quad (149)$$

where  $U$  = mean water velocity [m/s] and  $H$  = mean water depth [m].

Churchill (Churchill et al., 1962):

$$L_{\text{u}}(20) = 5.026 \frac{U}{H^{0.75}} \quad (150)$$

Owens-Gibbs (Owens et al., 1964)

$$L_{\text{u}}(20) = 5.32 \frac{U^{1.25}}{H^{0.75}} \quad (151)$$

Tauxemine-Rodriguez and Naei, 1976:

$$\text{Low flow: } Q = 3.028 \text{ to } 0.4247 \text{ cfs (1 to 15 cfs)} \quad (152)$$

$$L_{\text{u}}(20) = 31.83 U^{0.5}$$

High flow:  $Q = 0.4247$  to  $8.938$  cfs (15 to 3000 cfs):

$$L_{\text{u}}(20) = 15.308 U^{0.5} \quad (153)$$

where  $S$  = channel slope [m/m].

Thinc's and Dawson (Thinc's and Dawson, 2001):

$$L_{\text{u}}(20) = 2.16(1 - 0.75^{0.5}) \frac{U}{H} \quad (154)$$

where  $U$  = shear velocity [m/s], and  $F$  = the Froude number [dimensionless]. The shear velocity and the Froude number are defined as

$$U_* = \sqrt{g R_s S} \quad (155)$$

and

$$F = \frac{U}{\sqrt{g R_s}} \quad (156)$$

where  $g$  = gravitational acceleration ( $\approx 9.81 \text{ m/s}^2$ ),  $R_s$  = hydraulic radius [m],  $S$  = channel slope [m/m], and  $H$  = the hydraulic depth [m]. The hydraulic depth is defined as

$$H = \frac{A}{B} \quad (157)$$

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- $S_{\infty} = 1_{\infty} \text{PhysO}2\text{H}2\text{O} \rightarrow 1_{\infty} \text{BovAl}2\text{H}2\text{O} \rightarrow 1_{\infty} \text{EacCO}2\text{H}2\text{O} \rightarrow 1_{\infty} \text{NH}4\text{H}2\text{O}$   
 $\rho_{\infty} \text{PhysRCp} \quad \rho_{\infty} \text{BovAlRCp} \quad \rho_{\infty} \text{EacAlRCp} \quad \rho_{\infty} \text{NH}4\text{RCp}$  (144)
- where
- $\text{OxRate} = k_{\text{Ox}}(T)k_{\text{Ox}}(T) \exp(-r)$  (145)
- where  $k_{\text{Ox}}(T)$  = the temperature dependent oxygen reactivation coefficient [d/dT, sec<sup>-1</sup>] = the saturation concentration of oxygen [mgO<sub>2</sub>/L] at temperature, T, and elevation above sea level, elev;
- ### 5.3.16.1 Oxygen Saturation
- The following equation is used to represent the dependence of oxygen saturation on temperature (APHA 1995)
- $$\ln(s_1(T, 0)) = -1.5934(1) + \frac{1.5755(1) \times 10^5}{T_e} - \frac{6.62308 \times 10^7}{T_e^2} + \frac{1.2418(10) \times 10^{10}}{T_e^3} - \frac{6.621949 \times 10^{11}}{T_e^4}$$
- where  $s_1(T, 0)$  = the saturation concentration of dissolved oxygen in freshwater at 1 atm [mgO<sub>2</sub>/L] and  $T_e$  = absolute temperature [K] where  $T_e = T + 273.15$ ;
- The effect of elevation is accounted for by
- $$s_1(T, elev) = s_1^{*}(T) \exp(-0.000145 \cdot elev)$$
- 5.3.16.2 Resaturation Formulas
- The resaturation coefficient (at 20 °C) can be described on the **Roach Worksheet**. If resaturation is not prescribed (that is, it is blank or zero for a particular reach), it is computed as a function of the river's hydraulics and (optionally) wind velocity.
- $$k_{\text{R}}(20) = k_{\text{R}}(20) + \frac{K_{\text{R}}(20)}{H}$$
- where  $k_{\text{R}}(20)$  = the resaturation rate at 20 °C computed based on the river's hydraulic characteristics ( $T^*$ ,  $K_{\text{R}}(20)$  = the resaturation mass-transfer coefficient based on wind velocity, m/s), and  $H$  = mean depth [m].
- Hydraulic-based Formulas:**
- U.S. Corps of Engineers (U.S. Corps of Engineers and Johnson 1958):
- $$k_{\text{R}}(20) = 3.9 \frac{U^{1.35}}{H^{0.5}}$$
- where  $U$  = shear velocity [m/s], and  $F_{\text{R}}$  = the Froude number (dimensionless). The shear velocity and the Froude number are defined as
- $$U = \sqrt{g R S}$$
- and
- $$F_{\text{R}} = \frac{U}{\sqrt{g D}}$$
- where  $g$  = gravitational acceleration (= 9.81 m/s<sup>2</sup>),  $R$  = hydraulic radius [m],  $S$  = channel slope [m/m], and  $D$  = the hydraulic depth [m]. The hydraulic depth is defined as
- $$H = \frac{A}{B}$$
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- 146)  $k_{\text{R}}(20) = 3.9 \frac{U^{1.35}}{H^{0.5}}$
- where  $U$  = mean water velocity [m/s] and  $H$  = mean water depth [m].
- Churchill (Churchill et al. 1962):
- $$k_{\text{R}}(20) = 5.026 \frac{U}{H^{0.5}}$$
- Owens-Gibbs (Owens et al. 1964)
- $$k_{\text{R}}(20) = 5.32 \frac{U^{0.45}}{H^{0.5}}$$
- Tauxemine-Rodriguez and Naiman (1976):
- Low flow:  $Q = 0.028$  to  $0.4247$  cfs (1 to 15 cfs)
- $$k_{\text{R}}(20) = 31.83 U^{0.5}$$
- High flow:  $Q = 0.4247$  to  $84.533$  cfs (15 to 3000 cfs):
- $$k_{\text{R}}(20) = 15.308 U^{0.5}$$
- where  $S$  = channel slope [m/m].
- Tauxemine-Rodriguez (Tauxemine and Dawson 2001):
- $$k_{\text{R}}(20) = 2.16(1 - 0.000145 \cdot elev) \frac{U}{H}$$
- where  $U$  = shear velocity [m/s], and  $F_{\text{R}}$  = the Froude number (dimensionless). The shear velocity and the Froude number are defined as
- $$U = \sqrt{g R S}$$
- and
- $$F_{\text{R}} = \frac{U}{\sqrt{g D}}$$
- where  $g$  = gravitational acceleration (= 9.81 m/s<sup>2</sup>),  $R$  = hydraulic radius [m],  $S$  = channel slope [m/m], and  $D$  = the hydraulic depth [m]. The hydraulic depth is defined as
- $$H = \frac{A}{B}$$
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= hydroxyl ion,  $\text{OH}^-$  = hydroxyl ion, and  $\gamma = \text{total inorganic carbon concentration (mole L}^{-1}\text{)}$ .  
The brackets [ ] designate molar concentrations.

Note that the alkalinity is expressed in units of  $\text{eq/L}$  for the internal calculations. For input and output, it is expressed as  $\text{mg/L CaCO}_3$ . The two units are related by

$$\text{Alk (mg CaCO}_3\text{/L)} = 50,000 \times \text{Alk (eq/L)} \quad (172)$$

The equilibrium constants are corrected for temperature by

$$\text{Harner and Hamer (1953):}$$

$$\text{p}K_w = -4282.3 + 1713.2 \log_{10}(T_w) - 0.01357 T_w \quad (173)$$

Plummer and Busenberg (1982):

$$\log K_1 = -155.504 - 0.0609164 T_w + 1834.37/T_w + 126.8339 \log T_w - 1.684915/T_w^2 \quad (174)$$

Plummer and Busenberg (1982):

$$\log K_2 = -107.8871 - 0.03252849 T_w + 5151.70/T_w + 38.92261 \log T_w - 563.7139/T_w^2 \quad (175)$$

The nonlinear system of five simultaneous equations (166 through 170) can be solved numerically for the five unknowns:  $[\text{H}_2\text{CO}_3^*]$ ,  $[\text{HCO}_3^-]$ ,  $[\text{CO}_3^{2-}]$ ,  $[\text{OH}^-]$ , and  $[\text{H}^+]$ . An efficient solution method can be derived by combining Eqs. (167), (168) and (170) to define the quantities (Stumm and Morgan 1980)

$$\alpha_0 = \frac{[\text{H}^+]^2}{[\text{H}^+]^2 + K_1[\text{H}^+] + K_1K_2} \quad (176)$$

$$\alpha_1 = \frac{K_1[\text{H}^+]}{[\text{H}^+]^2 + K_1[\text{H}^+] + K_1K_2} \quad (177)$$

$$\alpha_2 = \frac{K_1K_2}{[\text{H}^+]^2 + K_1[\text{H}^+] + K_1K_2} \quad (178)$$

where  $\alpha_0$ ,  $\alpha_1$ , and  $\alpha_2$  are the fractions of total inorganic carbon in carbon dioxide, bicarbonate, and carbonate, respectively. Equations (166), (171), (177) and (178) can then be combined to yield

$$\text{Alk} = (\alpha_1 + 2\alpha_2) \gamma + \frac{K_w}{[\text{H}^+]} - [\text{H}^+] \quad (179)$$

Thus, solving for pH reduces to determining the new  $[\text{H}^+]$  of

$$f([\text{H}^+]) = (\alpha_1 + 2\alpha_2) \gamma + \frac{K_w}{[\text{H}^+]} - [\text{H}^+] - \text{Alk} \quad (180)$$

where pH is then calculated with

$$\text{pH} = -\log_{10}([\text{H}^+]) \quad (181)$$

The use of Eq. (180) is determined with a numerical method. The user can choose either the Newton-Raphson or the bisection method. Chien and Caudle (1990) has specified on the QUAL2K sheet. The Newton-Raphson is faster and is the default method. However, it can sometimes diverge. In such case, because it is more stable, the bisection method would be preferable.

#### 5.5.19 Total Inorganic Carbon (C<sub>T</sub>)

Total inorganic carbon concentration increases due to fast carbon oxidation and plant respiration. It is lost via plant photosynthesis. Depending on whether the water is undersaturated or oversaturated with  $\text{CO}_2$ , it is gained or lost via aeration.

$$C_{T,i} = r_{\text{FastCO}_2} + r_{\text{PlantPhoto}} + r_{\text{PlantResp}} + r_{\text{BioAlgResp}} - r_{\text{CO}_2} \text{Photo} - r_{\text{CO}_2} \text{Reaer} \quad (182)$$

where

$$\text{CO}_2\text{Reaer} = k_a (C^* - C_{\text{CO}_2}) \quad (183)$$

where  $k_a(T)$  = the temperature-dependent carbon dioxide reaeration coefficient ( $\text{d}^{-1}$ ), and  $[\text{CO}_2] =$  the saturation concentration of carbon dioxide ( $\text{moles/L}$ ).

The stoichiometric coefficients are computed as\*

$$r_{\text{CO}_2} = r_{\text{CO}_2} \left( \frac{\text{gC}}{\text{mgA}} \right) \times \left( \frac{\text{molC}}{12 \text{ gC}} \right) \times \left( \frac{\text{m}^3}{1000 \text{ L}} \right) \quad (184)$$

$$r_{\text{CO}_2} = \frac{1}{r_{\text{CO}_2}} \left( \frac{\text{gC}}{\text{mgA}} \right) \times \left( \frac{\text{molC}}{12 \text{ gC}} \right) \times \left( \frac{\text{m}^3}{1000 \text{ L}} \right) \quad (185)$$

#### 5.5.19.1 Carbon Dioxide Saturation

The  $\text{CO}_2$  saturation is computed with Henry's law,

$$[\text{CO}_2] = K_H P_{\text{CO}_2} \quad (186)$$

\* The conversion  $\text{m}^3 = 1000 \text{ L}$  is included because all mass balances express volume in  $\text{m}^3$ , whereas total inorganic carbon is expressed in  $\text{mole/L}$ .

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<sup>2</sup> Dr. Pieter Tans, NOAA/ES&L ([www.esl.noaa.gov/gmc/cpptrends](http://www.esl.noaa.gov/gmc/cpptrends))

According to Eq. (60), nitrification utilizes ammonium and creates nitrate. Hence, because a positive  $\text{I}_\text{r}$  is taken up and a negative ion is created, the alkalinity is decreased by two equivalents. The change in alkalinity can be related to the nitrification rate by

$$S_{NH_4} = -2 \text{ eq} \frac{\text{moleN}}{\text{moleN} 14.007 \text{ gN } 10^3 \text{ gN}} \frac{50.000 \text{ mgC}_2\text{CO}_3}{1 \text{ eq}} \text{NH}_4^+ \left( \frac{\text{gN}}{\text{Ld}} \right) \quad (181)$$

### 5.5.20.2 Denitrification

According to Eq. (61), denitrification utilizes nitrate and creates nitrogen gas. Hence, because a negative ion is taken up and a neutral compound is created, the alkalinity is increased by one equivalent. The change in alkalinity can be related to the denitrification rate by

$$S_{den} = \text{1 eq} \frac{\text{moleN}}{\text{moleN} 14.007 \text{ gN } 10^3 \text{ gN}} \frac{50.000 \text{ mgC}_2\text{CO}_3}{1 \text{ eq}} \text{DN} \left( \frac{\text{gN}}{\text{Ld}} \right) \quad (182)$$

where the  $1 \text{ eq}$  coefficient is that from the processes into the corresponding amount of alkalinity. The stoichiometric coefficients are derived from Eqs. (58) through (61) as in

### 5.5.20.3 Organic P Hydrolysis

Hydrolysis of organic P results in the creation of inorganic phosphate. Depending on the pH, the phosphate can be in the form of  $\text{H}_2\text{PO}_4^-$  or  $\text{HPO}_4^{2-}$ . The alkalinity is increased by one or two equivalents, respectively. The change in alkalinity can be related to the P hydrolysis rate by<sup>a</sup>

$$S_{phos} = -(\alpha_{H_2PO_4} + 2\alpha_{HPO_4}) \frac{\text{eq}}{\text{moleP}} \frac{\text{moleP}}{\text{moleP} 30.974 \text{ gP } 10^3 \text{ gP}} \frac{50.000 \text{ mgC}_2\text{CO}_3}{1 \text{ eq}} \text{PHYD} \left( \frac{\text{gP}}{\text{Ld}} \right) \quad (183)$$

where

$$\alpha_{H_2PO_4} = \frac{K_{a1} [\text{H}^+]}{[\text{H}^+] + K_{a1} [\text{H}^+] + K_{a1} K_{a2} [\text{H}^+] + K_{a1} K_{a2} K_{a3}} \quad (184)$$

$$\alpha_{HPO_4} = \frac{K_{a1} K_{a2} [\text{H}^+]}{[\text{H}^+] + K_{a1} [\text{H}^+] + K_{a1} K_{a2} [\text{H}^+] + K_{a1} K_{a2} K_{a3} [\text{H}^+] + K_{a1} K_{a2} K_{a3} K_{a4}} \quad (185)$$

$$\alpha_{PO_4} = \frac{K_{a1} K_{a2} K_{a3} [\text{H}^+]}{[\text{H}^+] + K_{a1} [\text{H}^+] + K_{a1} K_{a2} [\text{H}^+] + K_{a1} K_{a2} K_{a3} [\text{H}^+] + K_{a1} K_{a2} K_{a3} K_{a4} [\text{H}^+] + K_{a1} K_{a2} K_{a3} K_{a4} K_{a5}} \quad (186)$$

where  $K_{a1} = 10^{-7.5}$ ,  $K_{a2} = 10^{-7.2}$ , and  $K_{a3} = 10^{-12.9}$ .

### 5.5.20.4 Organic N Hydrolysis

Hydrolysis of organic N results in the creation of ammonia. Depending on the pH, the ammonia will either be in the form of ammonium ion with a single positive charge ( $\text{pH} < 9$ ) or neutral

<sup>a</sup> Note that although it is almost always negligible, Eq. (183)  $\text{PHYD}$  is for completeness.

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ammonia ( $\text{gN} (\text{pH} > 9)$ ). Hence, when the positive ions are created, the alkalinity is increased by one equivalent. The change in alkalinity can be related to the N hydrolysis rate by

$$S_{NH_4} = \text{1 eq} \frac{\text{moleN}}{\text{moleN} 14.007 \text{ gN } 10^3 \text{ gN}} \frac{50.000 \text{ mgC}_2\text{CO}_3}{1 \text{ eq}} \text{NH}_4^+ \left( \frac{\text{gN}}{\text{Ld}} \right) \quad (187)$$

### 5.5.20.5 Phytoplankton Photosynthesis

Phytoplankton photosynthesis takes up nitrogen as either ammonia or nitrate and phosphorus as inorganic phosphate. If ammonia is the primary nitrogen source, this leads to a decrease in alkalinity because the uptake of the positively charged ammonium ions is more greater than the release of the positively charged phosphate ions. If nitrate is the primary nitrogen source, this leads to an increase in alkalinity because both nitrate and phosphate are negatively charged.

The following representation relates the change in alkalinity to phytoplankton photosynthesis depending on the nutrient sources as well as their speciation as governed by the pH.

$$S_{photo} = \frac{50.000 \text{ mgC}_2\text{CO}_3}{1 \text{ eq}} \left\{ -\alpha_{NH_4} \frac{\text{eq}}{\text{moleN} 14.007 \text{ gN } 10^3 \text{ gN}} \frac{\text{gN}}{\text{Ld}} - \alpha_{NO_3} \frac{\text{eq}}{\text{moleN} 14.007 \text{ gN } 10^3 \text{ gN}} \frac{\text{gN}}{\text{Ld}} + \alpha_{H_2PO_4} + 2\alpha_{HPO_4} + 3\alpha_{PO_4} \right\} \frac{\text{eq}}{\text{moleP} 30.974 \text{ gP } 10^3 \text{ gP}} \frac{\text{gP}}{\text{Ld}} \times \text{PhytoPhoto} \left( \frac{\text{gP}}{\text{Ld}} \right) \quad (188)$$

### 5.5.20.6 Phytoplankton Respiration

Phytoplankton respiration releases ammonia and inorganic phosphate. Because the release of the phosphate ions is more than the release of the ammonium ions, this leads to an increase in alkalinity. The following representation relates the change in alkalinity to phytoplankton respiration including the effect of pH on the nutrient's speciation.

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A schematic of the model is depicted in Figure 24. As can be seen, the approach allows oxygenated surface sediment-water fluxes to be computed based on the downward flux of organic matter from the water column. The model is divided into two layers: a thin (1 mm) surface aerobic layer mediated by a thicker (10 cm) lower anoxic layer. Organic carbon, nitrogen and phosphorus are delivered to the anaerobic sediments via the settling of particulate organic matter (i.e., phytoplankton and detritus). There they are transformed by mineralization reactions into dissolved methane, ammonium and inorganic phosphorus. These constituents are then transported to the aerobic layer where some of the methane and ammonium are converted back into oxygen. The model is also used to estimate the fluxes of SOD along with the sediment-water fluxes of carbon, nitrogen and phosphorus that are also generated in the process.

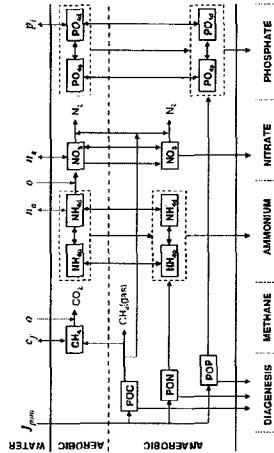


Figure 24 Schematic of SOD-nutrient flux model of the sediments.

### 5.6.1 Diagenesis

As summarized in Figure 25, the first step in the computation is to determine how much of the downward flux of particulate organic matter (POM) is converted into soluble reactive forms in the anaerobic sediments. This process is referred to as diagenesis. First the real downward flux is computed as the sum of the fluxes of phytoplankton and detritus settling from the water column

$$J_{POM} = c_p \cdot v_p + c_d \cdot v_d \quad (200)$$

where  $J_{POM}$  is the downward flux of POM ( $\text{gD m}^{-2} \text{d}^{-1}$ ),  $c_p$  is the ratio of dry weight to chlorophyll ( $\text{gD/mgChl}$ ),  $v_p$  is phytoplankton settling velocity ( $\text{m/d}$ ),  $c_d$  is phytoplankton concentration ( $\text{mgD/m}^3$ ),  $v_d$  is detritus settling velocity ( $\text{m/d}$ ), and  $m_d$  is detritus concentration ( $\text{gD/m}^3$ ).

$$S_{POM} = \frac{50,000 \text{ mgC/CO}_2}{1 \text{ eq}} \left\{ \frac{1 \text{ eq}}{\text{molN}} \frac{\text{molN}}{\text{molN}} \frac{\text{gN}}{14,007 \text{ gN}} \frac{\text{gN}}{10^3 \text{ gN}} \right. \\ \left. - (c_p \cdot v_p + c_d \cdot v_d) \cdot \frac{1 \text{ eq}}{\text{molP}} \frac{\text{molP}}{\text{molP}} \frac{\text{gP}}{30,974 \text{ gP}} \frac{\text{gP}}{10^3 \text{ gP}} \right. \\ \left. \times \text{PhytoRes} \left( \frac{\text{gC}}{\text{gD}} \right) \right\} \quad (199)$$

### 5.5.20.7 Bottom Algae Nutrient Uptake

Bottom algae take up nitrogen as either ammonia or nitrate and phosphorus as inorganic phosphate. The following representation relates the change in alkalinity to bottom algae uptake rates depending on the nutrient sources as well as their speciation as governed by the pH.

$$S_{ALG} = \frac{50,000 \text{ mgC/CO}_2}{1 \text{ eq}} \left\{ \left( \frac{1 \text{ eq}}{\text{molN}} \frac{\text{molN}}{\text{molN}} \frac{\text{gN}}{14,007 \text{ gN}} \frac{\text{gN}}{10^3 \text{ gN}} \right) \times \frac{\text{BtAlg} \cdot \text{pH} \cdot \text{pH} \cdot \text{pH}}{H(\text{pH})} \right. \\ \left. + (c_p \cdot v_p + c_d \cdot v_d) \cdot \frac{1 \text{ eq}}{\text{molP}} \frac{\text{molP}}{\text{molP}} \frac{\text{gP}}{30,974 \text{ gP}} \frac{\text{gP}}{10^3 \text{ gP}} \times \frac{\text{BtAlg} \cdot \text{pH} \cdot \text{pH} \cdot \text{pH}}{H(\text{pH})} \right\} \quad (200)$$

### 5.5.20.8 Bottom Algae Nutrient Excretion

Bottom algae excrete ammonia and inorganic phosphorus. The following representation relates the change in alkalinity to bottom algae excretion rates including the effect of pH on the nutrient's speciation.

$$S_{ALG} = \frac{50,000 \text{ mgC/CO}_2}{1 \text{ eq}} \left\{ \frac{1 \text{ eq}}{\text{molN}} \frac{\text{molN}}{\text{molN}} \frac{\text{gN}}{14,007 \text{ gN}} \frac{\text{gN}}{10^3 \text{ gN}} \times \frac{\text{BtAlg} \cdot \text{pH} \cdot \text{pH} \cdot \text{pH}}{H(\text{pH})} \right. \\ \left. - (c_p \cdot v_p + c_d \cdot v_d) \cdot \frac{1 \text{ eq}}{\text{molP}} \frac{\text{molP}}{\text{molP}} \frac{\text{gP}}{30,974 \text{ gP}} \frac{\text{gP}}{10^3 \text{ gP}} \times \frac{\text{BtAlg} \cdot \text{pH} \cdot \text{pH} \cdot \text{pH}}{H(\text{pH})} \right\} \quad (201)$$

### 5.6 SOD/Nutrient Flux Model

Sediment nutrient fluxes and sediment oxygen demand (SOD) are based on a model developed by Dr. Taro (Dr. Taro et al. 1991, Dr. Taro and Fitzpatrick, 1993, Dr. Taro 2001). The present version also benefited from James Martin's (Mississippi State University, personal communication) efforts to incorporate the Dr. Taro approach into EPA's WASP modeling framework.

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$$J_{POC} = k_{POC} \cdot \partial_z^2 \frac{H_2}{H_2 + H_2^0} \cdot H_2 \cdot POC_{OC} \quad (203)$$

In a similar fashion, a mass balance can be written and solved for the slowly reacting dissolved organic carbon. This result is then added to Eq. 198 to arrive at the total flux of dissolved carbon generated in the anoxic sediments.

$$J_P = J_{POC} + J_{DOC} \quad (204)$$

Similar equations are developed to compute the diffusive fluxes of nitrogen,  $J_N$  [ $\text{gN/m}^2/\text{d}$ ], and phosphorus,  $J_P$  [ $\text{gP/m}^2/\text{d}$ ].

## 5.5.2 Ammonium

Based on the mechanisms depicted in Figure 24, mass balances can be written for (a) ammonium in the aerobic layer and the anoxic layer.

$$H_1 \frac{dNH_4}{dt} = \omega_1 \left( J_{NH_4} - J_{NH_4}^{(1)} \right) + K_{NH_4} \left( J_{NH_4} - J_{NH_4}^{(1)} \right) - \omega_2 NH_4 \quad (207)$$

$$H_2 \frac{dNH_4}{dt} = J_N + \omega_2 \left( J_{NH_4} - J_{NH_4}^{(1)} \right) + K_{NH_4} \left( J_{NH_4} - J_{NH_4}^{(1)} \right) - \omega_3 NH_4 \quad (208)$$

where  $H_1$  is the thickness of the aerobic layer [m],  $NH_4$  and  $NH_4^{(1)}$  are the concentration of total ammonium in the aerobic layer and the anoxic layer, respectively [ $\text{gN/m}^3$ ],  $\omega_1$  is the ammonium concentration in the overlying water [mg/L],  $K_{NH_4}$  is the reaction velocity for ammonium in the aerobic layer [d<sup>-1</sup>],  $\omega_2$  is the concentration of ammonium in the anoxic layer [mg/L],  $\omega_3$  is the concentration in the overlying water [mg/L], and  $K_{NH_4}$  is the oxygen half-saturation constant [ $\text{mgO}_2/\text{L}$ ], and  $J_N$  is the diffusive flux of ammonium [ $\text{gN/m}^2/\text{d}$ ].

The fraction of ammonium in dissolved ( $J_{NH_4}$ ) and particulate ( $J_{NH_4}^{(1)}$ ) form are computed as

$$J_{NH_4} = \frac{J_{NH_4}^{(1)}}{1 + \frac{J_{NH_4}^{(1)}}{J_{NH_4}}} \quad (209)$$

$$J_{NH_4}^{(1)} = \frac{J_{NH_4}}{1 + \frac{J_{NH_4}^{(1)}}{J_{NH_4}}} \quad (210)$$

where  $m_1$  is the solids concentration in layer 1 [ $\text{gD/m}^3$ ], and  $m_2$  is the partition coefficient for ammonium in layer 1 [ $\text{m}^3/\text{gD}$ ].

The mass transfer coefficient for particle mixing due to bioturbation between the layers,  $\omega_2$  [ $\text{m/d}$ ], is computed as

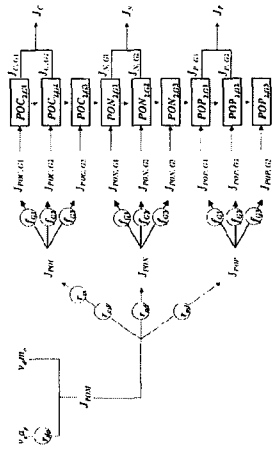


Figure 25 Representation of how settling particulate organic particles (phytoplankton and detritus) are transformed into fluxes of dissolved carbon ( $J_C$ ), nitrogen ( $J_N$ ) and phosphorus ( $J_P$ ) in the anoxic sediments.

Stoichiometric ratios are then used to divide the POM flux into carbon, nitrogen and phosphorus. Note that for convenience, we will express the particulate organic carbon (POC) as oxygen equivalents using the stoichiometric coefficient  $\omega_C$ . Each of the nutrient fluxes is further broken down into their reactive fractions: labile (OL), slowly reacting (OS), and non-reacting (ON).

These fluxes are then entered into mass balances to compute the concentration of each fraction in the anoxic layer. For example, for labile POC, a mass balance is written as

$$H_2 \frac{dPOC_{OL}}{dt} = J_{POC_{OL}} - k_{POC_{OL}} \partial_z^2 \frac{H_2}{H_2 + H_2^0} \cdot H_2 \cdot POC_{OL} \quad (203)$$

where  $H_2$  is the thickness of the anoxic layer [m],  $POC_{OL}$  is the concentration of the labile fraction of POC in the anoxic layer [ $\text{gC/m}^3$ ],  $J_{POC_{OL}}$  is the flux of labile POC delivered to the anoxic layer [ $\text{gC/m}^2/\text{d}$ ],  $k_{POC_{OL}}$  is the mineralization rate of labile POC [ $\text{d}^{-1}$ ],  $\partial_z^2 \frac{H_2}{H_2 + H_2^0}$  is the temperature correction factor for labile POC mineralization (dimensionless), and  $\omega_C$  is the burial velocity [m/d]. At steady state, Eq. 193 can be solved for

$$POC_{OL} = \frac{J_{POC_{OL}}}{k_{POC_{OL}} \partial_z^2 \frac{H_2}{H_2 + H_2^0} \cdot H_2 + \omega_C} \quad (204)$$

The flux of labile dissolved carbon,  $J_{C_{OL}}$  [ $\text{gC/m}^2/\text{d}$ ], can then be computed as

$$\theta_s = \frac{D_s g_{12}^{1/2}}{H_1} \frac{HK_{12} I_{12} / I_{10}}{H_2 K_{12} + n} \quad (211)$$

where  $D_s$  = diffusion coefficient for bioirrigation [m<sup>2</sup>/d],  $\theta_s$  = temperature coefficient (dimensionless),  $HK_{12}$  = reference GI concentration for bioirrigation [ $\mu\text{C}/\text{m}^3$ ] and  $K_{12} n$  = oxygen half-saturation constant for bioirrigation [ $\mu\text{C}/\text{m}^3$ ].

The mass transfer coefficient for pore water diffusion between the layers,  $K_{12}$  [m/d], is computed as

$$K_{12} = \frac{D_s g_{12}^{1/2}}{H_1 I_{12}} \quad (212)$$

where  $D_s$  = pore water diffusivity coefficient [m<sup>2</sup>/d], and  $\theta_s$  = temperature coefficient (dimensionless).

The mass transfer coefficient between the water and the aerobic sediments,  $s$  [m/d], is computed as

$$s = \frac{SOD}{n} \quad (213)$$

where  $SOD$  = the sediment oxygen demand [ $\mu\text{C}/\text{m}^2/\text{d}$ ].

At steady state, Eqs. 201 and 202 are two simultaneous nonlinear algebraic equations. The equations can be linearized by assuming that the  $NK_{12}$  term in the Michaelis-Menten term for denitrification is constant. The final linear equations can then be solved for  $NH_4$  and  $NH_3$ . The flux of ammonium to the overlying water can then be computed as

$$J_{NH_4} = \left( f_{NH_4} NH_{4,1} - \frac{n_{NH_4}}{1000} \right) \quad (214)$$

### 5.5.3 Nitrate

Mass balances for nitrate can be written for the aerobic and anaerobic layers as

$$H_1 \frac{dNO_{1,2}}{dt} = K_{12} (NO_{1,2} - NO_{1,1}) - v_{12} NO_{1,1} + \left( \frac{\theta_s - 1}{1000} \right) \left( \frac{K_{12} SOD}{\theta_s} - \frac{K_{12} SOD}{\theta_s} \right) \frac{f_{NH_4} NH_{4,1}}{K_{NH_4} + NH_{4,1}} - \frac{K_{12} SOD}{\theta_s} \frac{f_{NH_4} NH_{4,1}}{K_{NH_4} + NH_{4,1}} - \frac{K_{12} SOD}{\theta_s} \frac{f_{NH_4} NH_{4,1}}{K_{NH_4} + NH_{4,1}} \quad (215)$$

$$H_2 \frac{dNO_{2,2}}{dt} = J_N + K_{12} (NO_{1,2} - NO_{2,2}) + v_{12} (NO_{1,1} - NO_{2,2}) - K_{12} SOD \frac{f_{NH_4} NH_{4,1}}{K_{NH_4} + NH_{4,1}} \quad (216)$$

where  $NO_{1,1}$  and  $NO_{2,2}$  = the concentration of nitrate in the aerobic layer and the anaerobic layer, respectively [ $\mu\text{C}/\text{m}^3$ ],  $n_{NH_4}$  = the nitrate concentration in the overlying water [ $\mu\text{C}/\text{m}^3$ ],  $K_{NH_4}$  and

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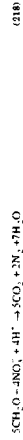
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$K_{NH_4}$  = the reaction velocities for denitrification in the aerobic and anaerobic sediments, respectively [m/d], and  $\theta_s$  = temperature correction factor for denitrification (dimensionless). In the same fashion as for Eqs. 201 and 202, Eqs. 209 and 210 can be linearized and solved for  $NH_4$  and  $NO_3$ . The flux of nitrate to the overlying water can then be computed as

$$J_{NO_3} = \left( \frac{NO_{3,1}}{1000} - \frac{n_{NO_3}}{1000} \right) \quad (217)$$

Denitrification requires a carbon source as represented by the following chemical equation



The carbon requirement (expressed in oxygen equivalents per milligram) can therefore be computed as

$$r_{carbon} = 2.87 \frac{5 \text{ mole } CO_2}{\text{gC}} \times 1.2 \frac{\text{gC/moleC}}{\text{gC}} \times \frac{1 \text{ gN}}{14 \text{ gN/moleN}} = 0.024 \frac{\text{gO}_2}{\text{mgN}} \quad (219)$$

Therefore, the oxygen equivalents consumed during denitrification,  $J_{NO_3}$  [ $\mu\text{C}/\text{m}^2/\text{d}$ ], can be computed as

$$J_{NO_3} = 1000 \frac{\text{mgN}}{\text{gN}} \times r_{carbon} \left( \frac{K_{NO_3}}{s} \frac{g_{NO_3}}{1000} - K_{NO_3} \frac{g_{NO_3}}{1000} \right) \quad (220)$$

### 5.6.4 Methane

The dissolved carbon generated by diagenesis is converted to methane in the anaerobic sediments. Because methane is readily oxidized to carbon dioxide and carbon monoxide, methane gas is produced. A mass balance equation for methane can be written for the anaerobic layer, an analytical model developed by D. Trem et al. (1993) is used to determine the steady-state flux of dissolved methane corrected for gas loss delivered to the aerobic sediments.

First, the carbon diagenesis flux is corrected for the oxygen equivalents consumed during denitrification

$$J_{CH_4} = J_C - J_{NO_3} \quad (221)$$

where  $J_{CH_4}$  = the carbon diagenesis flux corrected for denitrification [ $\mu\text{C}/\text{m}^2/\text{d}$ ]. In other words, this is the total anaerobic methane production flux expressed in oxygen equivalents.

If  $J_{CH_4}$  is sufficiently large ( $> 2 \text{ M}_{CH_4}$ ), methane gas will form. In such cases, the flux can be corrected for its gas loss

$$J_{CH_4} = \sqrt{2K_{CH_4} J_{CH_4}} \quad (222)$$

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where  $f_{\text{meth}}$  = the flux of dissolved methane (expressed in oxygen equivalents) that is generated by methanogenic bacteria and diffuses into the aerobic layer (mol  $\text{O}_2/\text{m}^2/\text{d}$ ).  $C_s$  = the saturation concentration of methane expressed in oxygen equivalents [mol  $\text{O}_2/\text{m}^3$ ]. If  $T_{\text{ref}} = 20^\circ\text{C}$ , then no gas forms and

$$J_{\text{CH}_4} = J_{\text{CH}_4} \quad (221)$$

The methane saturation concentration is computed as

$$C_s = 10 \left( 1 + \frac{H}{10} \right)^{1.024^{T-T_{\text{ref}}}} \quad (224)$$

where  $H$  = water depth (m) and  $T$  = water temperature ( $^\circ\text{C}$ ).

A methane mass balance can then be written for the aerobic layer as

$$H_1 \frac{dCH_4}{dt} = J_{\text{CH}_4} + \left( \frac{1}{s} - CH_4 \right) \left( \frac{K_{\text{CH}_4}}{s} \right) \theta_{\text{CH}_4}^{T-T_{\text{ref}}} CH_4 \quad (225)$$

where  $CH_4$  = methane concentration in the aerobic layer [g  $\text{O}_2/\text{m}^3$ ],  $\theta$  = first CBOD in the overlying water [g  $\text{O}_2/\text{m}^3$ ],  $K_{\text{CH}_4}$  = the reaction velocity for methane oxidation in the aerobic overlying water [d $^{-1}$ ],  $\theta_{\text{CH}_4}$  = temperature correction factor (dimensionless). At steady state, this balance can be solved for

$$CH_4 = \frac{J_{\text{CH}_4} + \frac{K_{\text{CH}_4}}{s} \theta_{\text{CH}_4}^{T-T_{\text{ref}}}}{s + \frac{K_{\text{CH}_4}}{s} \theta_{\text{CH}_4}^{T-T_{\text{ref}}}} \quad (226)$$

The flux of methane to the overlying water,  $J_{\text{CH}_4}$  [g  $\text{O}_2/\text{m}^2/\text{d}$ ], can then be computed as

$$J_{\text{CH}_4} = s(CH_4 - C_s) \quad (227)$$

## 5.5.5 SOD

The SOD [g  $\text{O}_2/\text{m}^2/\text{d}$ ] is equal to the sum of the oxygen consumed in methane oxidation and nitrification.

$$\text{SOD} = \text{CSOD} + \text{NSOD} \quad (228)$$

where CSOD = the amount of oxygen demand generated by methane oxidation [g  $\text{O}_2/\text{m}^2/\text{d}$ ] and NSOD = the amount of oxygen demand generated by nitrification [g  $\text{O}_2/\text{m}^2/\text{d}$ ]. These are computed as

$$\text{CSOD} = \frac{K_{\text{CH}_4}}{s} \theta_{\text{CH}_4}^{T-T_{\text{ref}}} CH_4 \quad (229)$$

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$$\text{NSOD} = f_{\text{ox}} \frac{K_{\text{NH}_4} \theta_{\text{NH}_4}^{T-T_{\text{ref}}}}{s} \frac{K_{\text{NH}_4}}{K_{\text{NH}_4} + \text{NH}_4} \frac{2K_{\text{NH}_4}}{K_{\text{NH}_4} + \text{NH}_4} f_{\text{ox}} \text{NH}_4 \quad (230)$$

where  $f_{\text{ox}}$  = the ratio of oxygen to nitrogen consumed during nitrification (= 4.57 g  $\text{O}_2/\text{g N}$ ).

## 5.5.6 Inorganic Phosphorus

Mass balances can be written for inorganic phosphorus in the aerobic layer and the anaerobic layer as

$$H_1 \frac{dPO_4}{dt} = \omega_2 [f_{\text{ox}} PO_4 - f_{\text{ox}} PO_4] + K_{\text{P}} [f_{\text{ox}} PO_4 - f_{\text{ox}} PO_4] - \left( \frac{\omega_2}{1000} - f_{\text{ox}} PO_4 \right) \quad (231)$$

$$H_2 \frac{dPO_4}{dt} = f_{\text{ox}} \omega_2 [f_{\text{ox}} PO_4 - f_{\text{ox}} PO_4] + K_{\text{P}} [f_{\text{ox}} PO_4 - f_{\text{ox}} PO_4] - \left( \frac{\omega_2}{1000} - f_{\text{ox}} PO_4 \right) + \left( \frac{\omega_2}{1000} - f_{\text{ox}} PO_4 \right) \quad (232)$$

where  $PO_4$  and  $PO_4$  = the concentration of total inorganic phosphorus in the aerobic layer and the anaerobic layer, respectively [g  $\text{P}/\text{m}^3$ ],  $\omega$  = the inorganic phosphorus in the overlying water [mg  $\text{P}/\text{m}^3$ ], and  $f_{\text{ox}}$  = the degradation flux of phosphorus [g  $\text{P}/\text{m}^2/\text{d}$ ].

The fraction of phosphorus in dissolved ( $f_{\text{ox}}$ ) and particulate ( $f_{\text{ox}}$ ) form are computed as

$$f_{\text{ox}} = \frac{1}{1 + \frac{\omega_2}{\omega_2} \frac{f_{\text{ox}}}{f_{\text{ox}}}} \quad (233)$$

$$f_{\text{ox}} = 1 - f_{\text{ox}} \quad (234)$$

where  $\omega_2$  = the partition coefficient for inorganic phosphorus in layer 1 [m $^3/\text{g P}$ ].

The partition coefficient in the anaerobic layer is set to an input value. For the aerobic layer, if the oxygen concentration in the overlying water remains exceeds a critical concentration,  $\omega_{\text{crit}}$  [g  $\text{O}_2/\text{m}^3$ ], then the partition coefficient is increased to represent the sorption of phosphorus onto iron oxyhydroxides as in

$$\omega_2 = \omega_2 \left( \frac{\omega_{\text{crit}}}{\omega_{\text{crit}}} \right) \quad (235)$$

where  $\Delta \omega_{\text{crit}}$  is a factor that increases the aerobic layer partition coefficient relative to the anaerobic coefficient.

If the oxygen concentration falls below  $\omega_{\text{crit}}$ , then the partition coefficient is decreased smoothly until it reaches the anaerobic value at zero oxygen.

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$$\pi_{j,t} = \pi_{j,t} \left( \Delta \pi_{j,t} \right)^{1/(1+\alpha)} \quad (236)$$

Equations 235 and 236 can be solved for  $P_{O_2}$  and  $P_{O_2}$ . The flux of phosphate to the overlying water can then be computed as

$$J_{P,t} = J_{P,t} \left( \frac{P_{O_2} - P_{O_2}}{1000} \right) \quad (237)$$

### 5.6.7 Solution Scheme

Although the foregoing sequence of equations can be solved, a single computation will not yield a correct result because of the interdependence of the equations. For example, the surface mass transfer coefficient depends on  $SOD$ . The  $SOD$  in turn depends on the ammonium and methane fluxes, which depend on  $SOD$ . The procedure used in QUAL2K is an iterative technique that must be used. The procedure used in QUAL2K is:

1. Determine the digester fluxes,  $J_A$ ,  $J_N$ , and  $J_P$ .
2. Start with an initial estimate of  $SOD$ .

$$SOD_{est} = J_A + J_N + J_P \quad (238)$$

where  $r_{N,N}$  is the ratio of oxygen to nitrogen consumed for total conversion of ammonium to nitrogen gas via nitrification (1.714 gO/gN). This ratio accounts for the carbon utilized for denitrification.

3. Compute using

$$r = \frac{SOD_{est}}{r} \quad (239)$$

4. Solve for ammonium, nitrate and methane, and compute the  $SOD$  and  $NSOD$ .

5. Make a revised estimate of  $SOD$  using the following weighted average

$$SOD = \frac{SOD_{est} + r(SOD + NSOD)}{2} \quad (240)$$

6. Check convergence by calculating an approximate relative error

$$\epsilon_r = \left| \frac{SOD - SOD_{est}}{SOD} \right| \times 100\% \quad (241)$$

7. If  $\epsilon_r$  is greater than a pre-specified stopping criterion  $\epsilon$ , then set  $SOD_{est} = SOD$  and return to step 2.

8. If convergence is adequate ( $\epsilon \leq \epsilon_c$ ), then compute the inorganic phosphorus concentrations.

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9. Compute the ammonium, nitrate, methane and phosphate fluxes.

### 5.6.8 Supplementary Fluxes

Because of the presence of organic matter deposited prior to the summer steady-state period (e.g., during spring storms), the potential for the downward flux of particulate organic matter is sufficient to generate the observed  $SOD$ . In such cases, a supplementary  $SOD$  can be prescribed.

$$SOD = SOD + SOD_{sup} \quad (242)$$

where  $SOD_{sup}$  is the total sediment oxygen demand [gO/(m<sup>2</sup>·d)], and  $SOD$  is the supplementary  $SOD$  [gO/(m<sup>2</sup>·d)]. In addition, prescribed ammonia and methane fluxes can be used to supplement the computed fluxes.

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